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# Aggregation suppressed thin film nanocomposite (TFN) membranes prepared with an *in situ* generation of TiO<sub>2</sub> nanoadditives†

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We report a promising strategy for the preparation of nano-aggregation suppressed thin film nanocomposite (TFN) membranes *via* an *in situ* method. Tetra-butyl ortho-titanate (TBOT) was added to the organic phase to prepare the new TFN membranes (*in situ* TFN). The *in situ* addition of TBOT produced TiO<sub>2</sub> nanoparticles in the polyamide layer during interfacial polymerization. In comparison with TFN membranes fabricated by the conventional method (*ex situ* TFN preparation), the nanoparticles in the *in situ* synthesized TFN membranes exhibited better dispersion, and more TiO<sub>2</sub> nanoparticles were observed on the membrane surface. Surprisingly, at a rather low concentration of TBOT (250 mg L<sup>-1</sup>), the water flux of the *in situ* TFN membranes was increased by more than 50% in comparison with that of a pure polyamide membrane with negligible rejection loss, which was close to the performance of the state-of-the-art TFN membranes. The surface properties of the membranes were investigated by scanning electron microscopy (SEM), X-ray diffraction (XRD) analysis, X-ray photoelectron spectroscopy (XPS), and contact angle analysis. Our results demonstrate that *in situ* generation of nano-additives can effectively suppress nano-agglomeration and improve the performance and surface features of TFN membranes.

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## 1. Introduction

Nanofiltration is a highly efficient technology that is widely used in water softening, desalination, biomedicine, dyestuff production, and wastewater treatment.<sup>1–5</sup> In comparison with reverse osmosis (a pressure-driven membrane process operating at approximately 1–7 MPa), nanofiltration has lower operating pressure, higher flux, and greater energy efficiency.<sup>6,7</sup> Thin film composite (TFC) membranes, the membranes most commonly used for nanofiltration and reverse osmosis, are usually fabricated *via* interfacial polymerization (IP) of monomer reactants on a porous support membrane.<sup>8,9</sup> The performance of TFC membranes is primarily determined by the physicochemical properties of the top polyamide layer.<sup>10–13</sup> Many studies focusing on developing new monomers, optimizing the processes of membrane preparation, and additive doping have shown that water flux and/or separation ability may be enhanced by changing the free volume and cross-linking degree of the polyamide layer.<sup>14–17</sup>

Although efforts toward improving conventional TFC membranes are ongoing, significant advances in membrane performance are rare;<sup>18–21</sup> however, recent studies indicate that

the synthesis and incorporation of superhydrophilic nanoparticles into the PA layer to fabricate thin film nanocomposite (TFN) membranes may represent a significant breakthrough in membrane performance.<sup>22–26</sup> Recently, hydrophilic nanoparticles such as TiO<sub>2</sub>, zeolite, SiO<sub>2</sub>, graphene oxide (GO), and carbon nanotubes have been widely applied to endow TFN membranes with enhanced separation performance by altering membrane surface morphology.<sup>27–31</sup> TiO<sub>2</sub> nanoparticles (NPs) have attracted considerable interest because of their photocatalytic properties and hydrophilicity, which induce decomposition of organic chemicals and endow TFN membranes with anti-fouling properties.<sup>32,33</sup> For example, Lee and colleagues produced a high-TiO<sub>2</sub>-loaded TFN membrane by dispersing nanoparticles in an organic monomer solution during the interfacial polymerization process, and the resulting membrane exhibited a distinct surface structure and greater permeability;<sup>34</sup> however, nanoparticle agglomeration impaired the rejection performance of the membrane. Poor dispersion of hydrophilic nanoparticles in non-polar organic solvents seems to lead inevitably to agglomeration of nanoparticles in membranes.<sup>35–38</sup> Alternatively, dispersing nanoparticles into the aqueous phase is also not feasible, because it is difficult to phase-transfer large hydrophilic nanoparticles from water to the polyamide layer formed beside the organic phase.<sup>39–43</sup> To overcome the obstacle of nanoparticle aggregation, some researchers have improved nanoparticle dispersion in aqueous and organic solutions by modifying the particle surface. However, this method is complex and will sacrifice the surface property of nanoparticles.<sup>30,44</sup>

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In this contribution, we report a promising strategy for the fabrication of aggregation-suppressed TFN membranes with *in situ* generation of  $\text{TiO}_2$  additives in the active PA layer. Tetra-butyl *ortho*-titanate (TBOT), instead of  $\text{TiO}_2$  nanoparticles, was added to the organic phase containing 1,3,5-benzenetricarbonyl trichloride (TMC) monomers as the titanium source. TBOT hydrolysis can be utilized to produce  $\text{TiO}_2$  nanoparticles during or after interfacial polymerization, thus overcoming the limitation of  $\text{TiO}_2$  nanoparticle aggregation in non-polar organic solvents. In comparison with other methods of reducing nanoparticle aggregation, this new approach is much simpler and more effective. Moreover, TFN membranes prepared by directly adding different amounts of  $\text{TiO}_2$  NPs were compared with regard to performance and structure. A schematic illustration comparing our strategy of TFN membrane preparation utilizing TBOT loading (defined herein as the *in situ* method) with membrane preparation *via* direct addition of  $\text{TiO}_2$  nanoparticles (defined herein as the *ex situ* method) is presented in Fig. 1.

## 2. Experimental section

### 2.1 Materials and chemicals

1,3,5-Benzenetricarbonyl trichloride (TMC, Sigma-Aldrich, St. Louis, MO, USA), tetra-butyl *ortho*-titanate (TBOT, Aladdin), titanium oxide (anatase 5–10 nm, Aladdin), piperazine (PIP, Sigma-Aldrich), *n*-hexane, and trisodium phosphate anhydrous ( $\text{Na}_3\text{PO}_4$ , Sigma-Aldrich) were purchased from commercial sources and used without further purification. A polysulfone (PSF) ultrafiltration membrane with a molecular weight cut-off of 50 000 dalton was used as the support.

### 2.2 Membrane fabrication

TFC and TFN (*in situ* and *ex situ*) membranes were fabricated following a typical interfacial polymerization procedure.<sup>34,45,46</sup> The aqueous solution was prepared by dissolving 0.2% PIP/ $\text{Na}_3\text{PO}_4$  (as a buffer solution) and 0.1% sodium dodecyl sulfonate (as a surfactant) in de-ionized water. The PSF support was coated with the aqueous phase for 5 min. After draining off the

excess solution, the membrane was dried for 5 min at room temperature and immersed in 0.1% TMC organic solution for 1 min to allow interfacial polymerization. Finally, the as-prepared TFC membranes were cured in a convection oven at 80 °C for 10 min.

TFN membranes were also fabricated with different amounts of TBOT (or  $\text{TiO}_2$  NPs) mixed into the TMC hexane solution before the interfacial polymerization process, but otherwise following the procedure described above. The experimental conditions were based on the assumption that hydrolysis of one molecule of TBOT produced one molecule of titanium dioxide. The preparation conditions for the *in situ* and *ex situ* TFN membranes are summarized in Table 1.

### 2.3 Characterization

**2.3.1 Scanning electron microscopy (SEM).** Each TFC and TFN membrane was rinsed with de-ionized water (DI) and dried at 30 °C for 12 h before characterization. The surface of each membrane was sputtered and inspected by SEM (HitachiS-4700 II, Japan) at 15.0 kV.

**2.3.2 X-ray diffraction (XRD) analysis.** The crystalline structure of the  $\text{TiO}_2$  nanoparticles was analysed by XRD analysis. *In situ*-generated  $\text{TiO}_2$  NPs (TBOT hydrolysis) were synthesized by dropping TBOT hexane solution into the aqueous phase (pH 10), followed by filtration and drying at 80 °C for 10 min. XRD spectra were obtained using a Thermo

Table 1 Preparation conditions for *in situ* and *ex situ* TFN membranes

Membranes	<i>In situ</i> synthesized	<i>Ex situ</i> synthesized
	TBOT ( $\text{mg L}^{-1}$ )	$\text{TiO}_2$ ( $\text{mg L}^{-1}$ )
TFN1	100	24
TFN2	250	60
TFN3	500	120
TFN4	1000	240
TFN5	2500	600

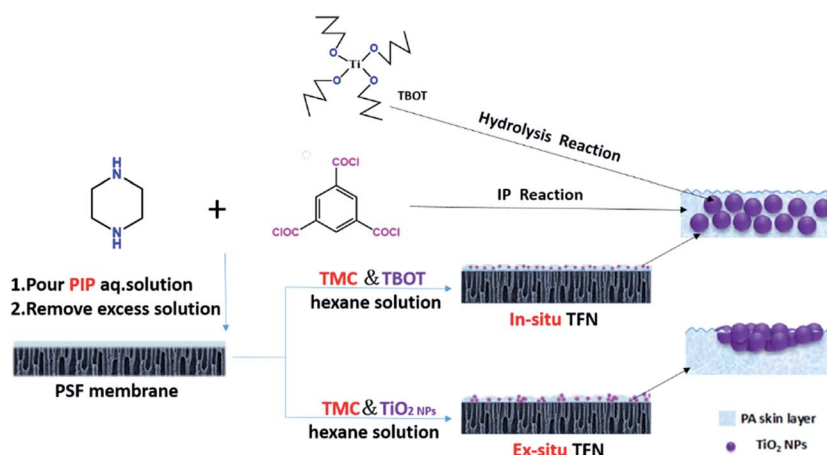


Fig. 1 Schematic illustration of TFN membrane fabrication *via* the *in situ* and *ex situ* processes.



Scientific ARL X'TRA Powder Diffractometer (Thermo Fisher Scientific, Waltham, MA, USA) at 40 kV (40 mA, in the interval  $20^\circ \leq 2\theta \leq 80^\circ$ ).

**2.3.3 Zeta-potential determination.** Zeta-potential measurements were performed with an electro kinetic meter (Anton Paar GmbH SurPASS 3, Austria). The background electrolyte solution was  $10^{-3}$  mol L<sup>-1</sup> KCl. The pH of the aqueous KCl solution was adjusted by adding high-purity aqueous solutions of 0.1 mol L<sup>-1</sup> NaOH or 0.1 mol L<sup>-1</sup> HCl.

**2.3.4 Contact angle measurement.** Membrane hydrophobicity was assessed by contact angle measurement (OCA15EC, Dataphysics, Germany). Each membrane was dried in an oven at 40 °C for 2 h, after which the sessile drop method was used to measure the contact angle of water. Water contact angles were measured at three different locations on the surface of each membrane (the average value was reported).

**2.3.5 Permeability and rejection determination.** The separation performance of all nanofiltration membranes was tested by determining the flux of pure water and measuring rejection of Na<sub>2</sub>SO<sub>4</sub> (0.2%) and NaCl (0.2%) solutions under a pressure of 1.0 MPa at 25 °C. The membranes were pre-compressed under a pressure of 1.0 MPa for 60 min before evaluation. Each experiment was conducted in triplicate. The effective membrane area was 7.1 cm<sup>2</sup>. Flux was calculated according to eqn (1):

$$\text{Water permeability} = \frac{V}{At} \quad (1)$$

where  $V$  (m<sup>3</sup>) is the volume of the permeation solution,  $t$  (h) is the time of exposure, and  $A$  (m<sup>2</sup>) is the effective permeable area of the membrane. Rejection performance was calculated according to eqn (2):

$$\text{Rejection} = \frac{C_f - C_p}{C_f} \times 100\% \quad (2)$$

where  $C_f$  and  $C_p$  are the solute concentrations of the permeation solution and feed solution, respectively. The conductivity of each solution was measured using a DDSJ-308A conductivity meter (Shanghai, China).

## 3. Results and discussion

### 3.1 Properties of TiO<sub>2</sub> nanoparticles

XPS and XRD were used to analyse the properties of TiO<sub>2</sub> nanoparticles (data shown in ESI†). XPS and XRD indicated that amorphous TiO<sub>2</sub> particles were produced from TBOT during membrane fabrication. The surface elemental composition and O/Ti ratio of commercially sourced TiO<sub>2</sub> and TiO<sub>2</sub> generated from TBOT are listed in Table 2. The O/Ti ratios of TiO<sub>2</sub> purchased from Aladdin and TiO<sub>2</sub> synthesized from TBOT were 2.5 and 3.1, respectively, which are both higher than the theoretical O/Ti ratio of TiO<sub>2</sub>. The relatively high oxygen content of TiO<sub>2</sub> from both sources can be attributed to Ti–OH bonds on the outer surface of TiO<sub>2</sub> and adsorbed chemicals such as H<sub>2</sub>O and O<sub>2</sub>. In comparison with calcinated TiO<sub>2</sub> purchased from Aladdin, amorphous TiO<sub>2</sub> synthesized from TBOT had a greater O/Ti ratio, which was expected to enhance surface hydrophilicity

Table 2 Surface elemental composition of TiO<sub>2</sub> nanoparticles

TiO <sub>2</sub> source	Atomic content (%)		O/Ti ratio	Crystal type
	O	Ti		
Commercial	71.26	28.74	2.5	Anatase
TBOT	75.56	24.44	3.1	Amorphous

and thus increase the water flux of TFN membranes. To the best of our knowledge, only a few studies have reported that the type of TiO<sub>2</sub> used in the membrane synthesis process influenced membrane performance. However, the effects of amorphous TiO<sub>2</sub> on membrane performance and other membrane properties have not been studied systematically.

### 3.2 Flux and rejection performance of TFN and TFC membranes

Fig. 2 shows the water flux and salt rejection performance of TFN and TFC membranes using pure water and salt solutions of Na<sub>2</sub>SO<sub>4</sub> and NaCl. Both types of TFN membrane displayed similar salt rejection performance. The water flux of TFN membranes prepared by directly adding TiO<sub>2</sub> NPs (*ex situ* method) exhibited a relatively small increase from 49.4 to 90.9 L m<sup>-2</sup> h<sup>-1</sup> as the amount of TiO<sub>2</sub> was increased, while that of the *in situ* TFN membranes increased significantly from 52.0 to 187.1 L m<sup>-2</sup> h<sup>-1</sup>. This difference in the effect of TiO<sub>2</sub> loading on the performance of *in situ* and *ex situ* membranes might be due to differences in nanoparticle dispersion. For *ex situ* prepared membranes, poor dispersion of nanoparticles in hexane reduces the amount of loaded TiO<sub>2</sub>.<sup>38</sup> As a result, the *in situ*-synthesized TFN membranes showed much better performance, including water flux and rejection of Na<sub>2</sub>SO<sub>4</sub> and NaCl, in comparison with that of the *ex situ* TFN membranes at any TiO<sub>2</sub> loading content. Interestingly, the Na<sub>2</sub>SO<sub>4</sub> rejection performance and water flux of the *in situ* TFN membranes were enhanced in comparison with those of the TFC membranes when the concentration of loaded TBOT was less than 500 mg L<sup>-1</sup>. The Na<sub>2</sub>SO<sub>4</sub> rejection performance of the *in situ* TFN membranes reached a maximum value of 95.3% when the amount of TBOT was 250 mg L<sup>-1</sup>. The water flux through the *in situ* TFN membranes prepared with 250 mg L<sup>-1</sup> TBOT was higher than that of most reported TFN membranes with adequate rejection performance.<sup>47–55</sup> However, rejection performance was impaired rapidly when the concentration of TBOT was increased beyond 500 mg L<sup>-1</sup>. These results indicate that the *in situ* process provides better dispersion of nanoparticles in both hexane and membranes in comparison with that provided by the *ex situ* process. Furthermore, TiO<sub>2</sub> synthesized from TBOT had a greater O/Ti ratio, which remarkably improved membrane hydrophilicity and thus increased water flux.

### 3.3 Effects of preparation conditions on membranes performance

In contrast with the classical *ex situ* method of preparing TFN membranes, the *in situ* preparation method utilizes two



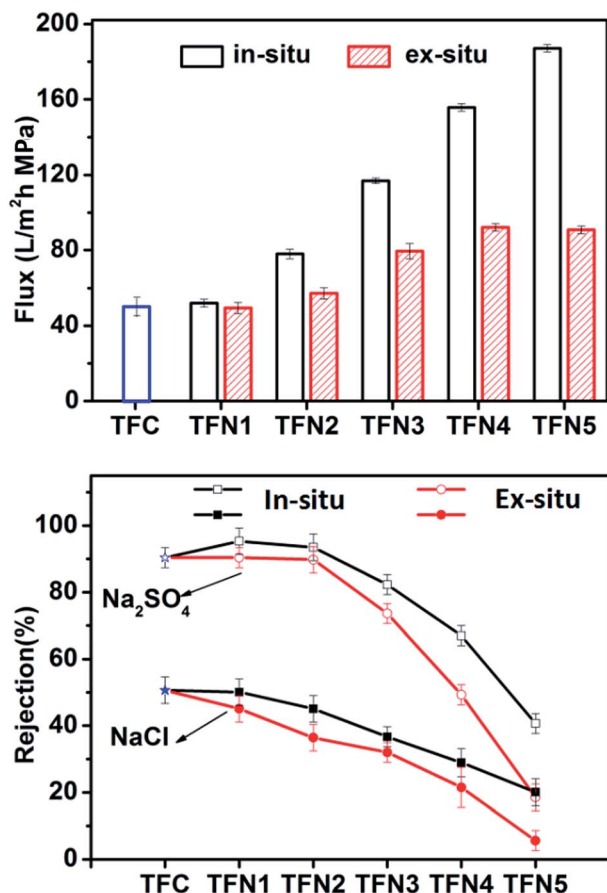


Fig. 2 Water flux and rejection performance of TFC and TFN membranes as functions of the amounts of TBOT and TiO<sub>2</sub> loaded into the membranes.

reactions: an initial interfacial polymerization reaction and a subsequent titanate hydrolysis reaction. The effects of preparation conditions (reaction time and monomer concentration) on membrane performance were investigated to identify the main factors affecting membrane performance and allow optimization of the preparation conditions for *in situ* TFN membranes (500 mg L<sup>-1</sup> TBOT was added to the organic phase during the preparation of each membrane).

Fig. 3 shows the relationship between reaction time and the performance of *in situ*-synthesized TFN membranes. As the reaction time was increased, the rejection performance of TFN membranes increased gradually and plateaued (53% to 87% for Na<sub>2</sub>SO<sub>4</sub> and 24.1% to 48.7% for NaCl), whereas water flux decreased gradually from 115.6 L m<sup>-2</sup> h<sup>-1</sup> to 101.6 L m<sup>-2</sup> h<sup>-1</sup>. These changes occurred because an interfacial reaction occurred between the aqueous phase of PIP and the organic phase of TMC, and the thickness of the polyamide functional layer was continuously increased. The small variation in flux also shows that the dispersion characteristics and other properties of TiO<sub>2</sub> synthesized by TBOT changed slightly as the reaction time was increased because hydrolysis of titanate completed in a very short time. This characteristic of titanate hydrolysis also ensures the stability and viability of TFN membranes produced using the *in situ* process. Rejection performance and water flux remained

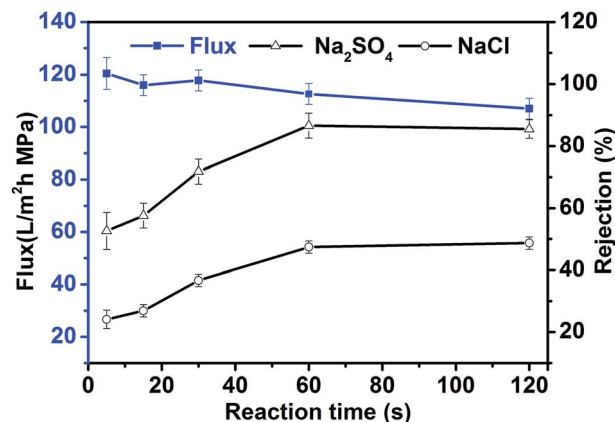


Fig. 3 Permeability of *in situ* synthesized TFN membranes as a function of the reaction time.

unchanged when the reaction time was longer than 60 s, which suggests that interfacial polymerization and hydrolysis might have both reached equilibrium after 60 s. Therefore, 60 s seems to be the appropriate reaction time for the preparation of *in situ* TFN membranes.

The monomer concentration may also affect membrane performance. Fig. 4a shows the performance of *in situ* TFN membranes produced using different piperazine (PIP) concentrations ranging from 0.5 g L<sup>-1</sup> to 5 g L<sup>-1</sup> under the following fabrication conditions: 500 mg L<sup>-1</sup> TBOT and 1 g L<sup>-1</sup> 1,3,5-benzenetricarbonyl trichloride (TMC) in hexane. The rejection performance of the membrane against Na<sub>2</sub>SO<sub>4</sub> and NaCl increased, while water flux decreased gradually, when the PIP concentration was increased from 0.5 to 2.0 g L<sup>-1</sup>. The membrane performance changed only slightly when the PIP concentration exceeded 2.0 g L<sup>-1</sup>. This pattern was mainly due to the rate of the interfacial polymerization reaction, which produced a denser and thicker polymer layer as the amount of PIP in the aqueous phase was increased. However, as the thickness of the polymer layer increases, it becomes more difficult for PIP to react with TMC.<sup>56</sup>

The water flux and rejection performance of *in situ* TFN membranes fabricated with different TMC concentrations and 2 g L<sup>-1</sup> PIP are shown in Fig. 4b. The rejection performance of *in situ* TFN membranes against Na<sub>2</sub>SO<sub>4</sub> and NaCl increased first, followed by a slight decline, as the TMC concentration was increased, while the water flux decreased as the TMC concentration was increased. The membranes showed optimal salt rejection performance when the TMC concentration was 1.0 to 1.5 g L<sup>-1</sup>. The concentration of TMC in the reaction mixture has a marked effect on the cross-linking degree of the PA layer. The density of the polymer layer increases as the concentration of TMC is increased, which enhances salt rejection performance and reduces water flux. However, excessive TMC content can lead to a rapid interfacial polymerization reaction that impairs rejection performance.<sup>57</sup>

Generally, in comparison with the concentration of TBOT, the monomer concentration had only a small influence on the rejection performance and water flux of the TFN membranes.





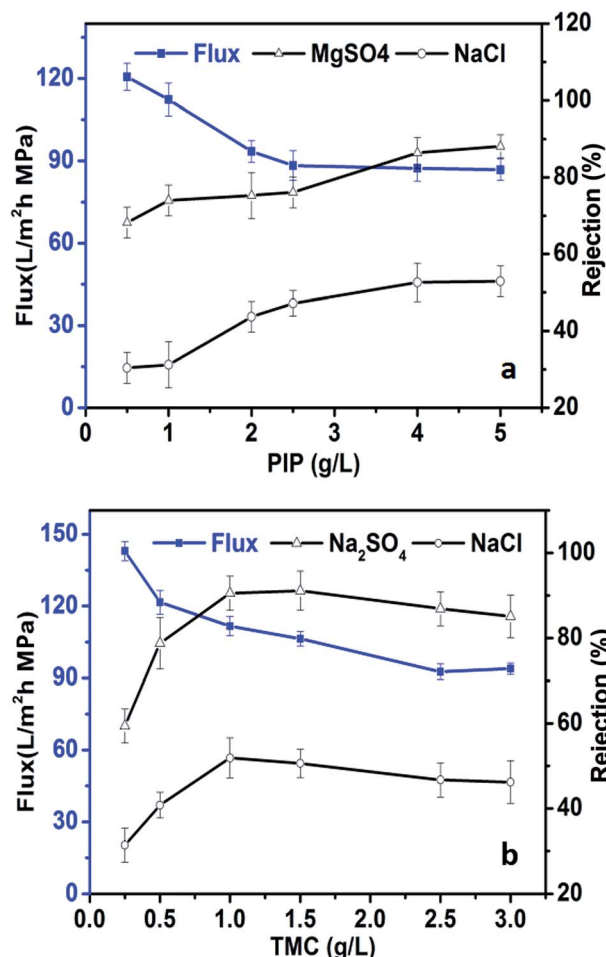


Fig. 4 Water flux and rejection performance of *in situ*-synthesized TFN membranes as functions of PIP and TMC concentrations.

Water flux was decreased from  $120.6 \text{ L m}^{-2} \text{ h}^{-1}$  to  $86.8 \text{ L m}^{-2} \text{ h}^{-1}$  when the PIP concentration was increased from  $0.5 \text{ g L}^{-1}$  to  $5 \text{ g L}^{-1}$ , whereas it was decreased from  $141.6 \text{ L m}^{-2} \text{ h}^{-1}$  to  $93.9 \text{ L m}^{-2} \text{ h}^{-1}$  when the TMC concentration was increased from  $0.25 \text{ g L}^{-1}$  to  $3 \text{ g L}^{-1}$ ; these effects on membrane performance were far smaller in magnitude than that of changing the TBOT concentration. The influence of preparation conditions (reaction time and concentration of TMC and PIP) on membrane permeability suggests that altering the TBOT concentration might influence membrane structure and change the size of membrane pores, which might have a greater impact on TFN performance in comparison with the effects of changing the monomer concentrations.

### 3.4 Surface morphologies of prepared membranes

SEM images were collected to characterize the surface morphology of membranes prepared in different manners (TFC, *in situ* synthesized, and *ex situ* synthesized). SEM images of a PSF support and TFC membrane are shown in Fig. 5. The PSF support had a porous surface. After the interfacial polymerization reaction, the surface of the TFC membrane had a "rubber particle-like" structure.

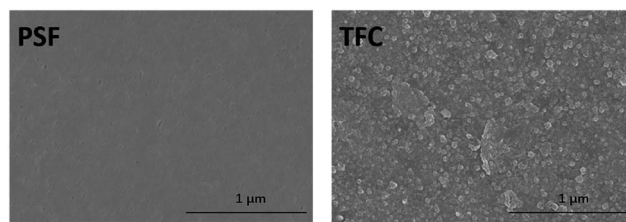


Fig. 5 SEM images of an ultrafiltration polysulfone support and a TFC membrane prepared without adding TBOT or  $\text{TiO}_2$  additives.

The influence of the TBOT and  $\text{TiO}_2$  concentrations on the selective layer was also examined (Fig. 6). In comparison with TFC membranes, the morphology of TBOT- and  $\text{TiO}_2$ -loaded membranes was modified clearly by the additives. Although the loading concentration of particles was rather low, obvious agglomeration was observed on the surface of the *ex situ* prepared TFN. However, agglomeration occurred only at the very high TBOT concentration of  $2500 \text{ mg L}^{-1}$  in the *in situ* synthesized TFN5 membrane. It is hypothesized that  $\text{TiO}_2$  nanoparticles produced by hydrolysis of TBOT were covered immediately by the polymer during the interfacial polymerization process, which enabled uniform dispersion of nanoparticles in the polyamide layer and minimized interaction between nanoparticles, thus suppressing agglomeration.<sup>58</sup> However, small  $\text{TiO}_2$  NPs were observed on the surface of the *ex situ* synthesized TFN membranes (especially apparent in Fig. 6d and e). Therefore, the beneficial properties of  $\text{TiO}_2$  NPs can be conferred only upon the membrane surface, rather than upon the polyamide layer, which limits the degree to which water flux can be enhanced. Interestingly, the surface of the *in situ* synthesized TFN membranes had a unique cross-linked structure. As the amount of loaded TBOT was increased, the circular cross-linked network structure of the polyamide layer became more obvious, which may have increased the surface area of the *in situ* synthesized membrane. This finding also explains why *in situ* TFN membranes fabricated with the addition of a relatively low concentration of TBOT showed amazing enhancement of water flux in comparison with TFC and *ex situ* TFN membranes. As shown in Fig. 6e, severe nanoparticle agglomeration, which occurred when the TBOT concentration was high, destroyed the structure of the top layer and thus markedly impaired rejection performance. These observations demonstrate that, in comparison with *ex situ* TFN membranes, *in situ*-synthesized TFN membranes fabricated with TBOT showed better dispersion of NPs and a more compact structure between the  $\text{TiO}_2$  NPs and active polyamide layer.

### 3.5 XPS analysis

Two types of reactions between aqueous PIP solutions and organic TMC solutions were expected. The first expected reaction was the network cross-linking reaction of the amine in PIP with the third remaining chloride group in TMC *via* amide linkage. The second expected reaction was the hydrolysis reaction of the third chloride group in TMC to carboxylic acid. Because each of these reactions can occur during TFN



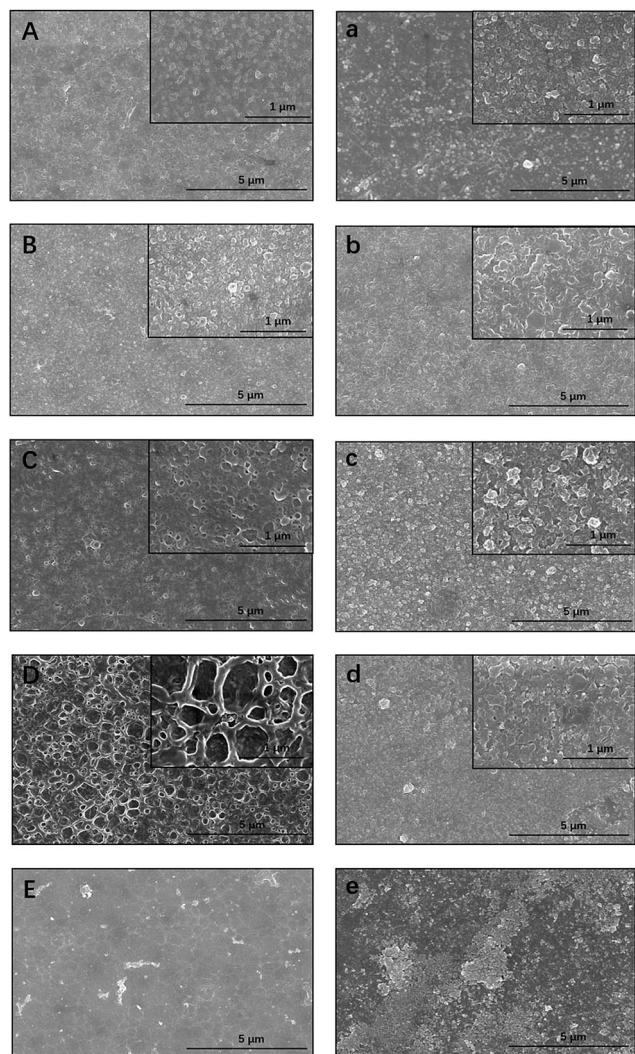


Fig. 6 SEM images of *in situ* synthesized membranes ((A) TFN1; (B) TFN2; (C) TFN3; (D) TFN4; (E) TFN5) and *ex situ* synthesized membranes ((a) TFN1; (b) TFN2; (c) TFN3; (d) TFN4; (e) TFN5).

membrane production, the polypiperazine amide may have two different chemical structures: linear or cross-linked. Although the permeability performance data and SEM images provide useful information about the TFN membranes, they cannot provide a thorough understanding of the surface composition of TFN membranes loaded with TBOT. XPS analysis is a suitable method for investigating the outer membrane layer and providing direct evidence of the elemental composition and chemical structure of the membrane surface.<sup>59,60</sup>

The results of the XPS analysis of the surface compositions of TFC and TFN membranes are listed in Table 3. Ti was more abundant on the surface of the *in situ*-synthesized TFN membranes in comparison with that of the *ex situ* membranes, which is entirely consistent with the hypothesis that the poor dispersion of TiO<sub>2</sub> NPs in hexane resulted in fewer nanoparticles entering the polyamide layer. Moreover, this finding also explains why *in situ* TFN membranes prepared with TBOT exhibited greater water flux.

The atomic contents of the membrane surface can be also used to evaluate the degree of cross-linking of the polypiperazine amide layer. In order to avoid interference from carbon (carbon contamination of the sample surface is unavoidable), the O/N ratio was used to investigate the degree of cross-linking of the TFN membranes. The O/Ti ratio of the *in situ* TFN membranes was 3.1, whereas the O/Ti ratio of the *ex situ* membranes was 2.5 (Table 1). The O/N<sub>PA</sub> ratio can be obtained from the other information in Table 1. Theoretically, the O/N<sub>PA</sub> ratio varies from 1.0 for a fully cross-linked structure (C<sub>16</sub>H<sub>14</sub>N<sub>3</sub>O<sub>3</sub>) with good rejection performance to 2.0 for a fully linear structure (C<sub>13</sub>H<sub>12</sub>N<sub>2</sub>O<sub>4</sub>). As shown in Table 2, the O/N<sub>PA</sub> ratios of the *in situ* and *ex situ* TFN membranes increased with the addition of TBOT and TiO<sub>2</sub>, and the former had a relatively greater degree of cross-linking. Surprisingly, the O/N<sub>PA</sub> ratios of the *in situ* TFN1 and TFN2 membranes, in which a low concentration of TBOT was used, were equivalent to that of the TFC membrane (O/N ratio = 1.1). This finding confirms that a low concentration of TBOT does not impair the degree of cross-linking in the film, which is generally consistent with the results of the SEM imaging and permeability tests.

The deconvoluted, high-resolution O 1s peaks provide information about the chemical bonds of polypiperazine amide and TiO<sub>2</sub> in the *in situ*-synthesized TFN membranes generated with TBOT (Fig. 7). The O 1s spectra of TFC showed two peaks: a major peak from C=O at 531.6 eV and a smaller peak from the C-O of a carboxylic group at 533.0 eV.<sup>61</sup> According to the peak area ratio listed on the chart, the area of the C=O peak decreased with the addition of TBOT, while the area of the C-O peak increased. The C=O/C-O ratios for the TFC membrane and membranes TFN1–5 were 6.25, 6.28, 6.04, 4.65, 2.09, and 1.84, respectively. It can be concluded that the *in situ*-synthesized TFN membranes prepared with relatively low concentrations of TBOT had a relatively greater degree of cross-linking. This finding confirms that the low concentration of TBOT used in *in situ*-synthesized membranes TFN1 and TFN2 had no effect on cross-linking and therefore significantly increased water flux with a negligible loss of rejection performance.<sup>23</sup> Two other peaks obtained from the high resolution O (1s) spectra of the *in situ* TFN membranes produced with the addition of TBOT illustrate the presence of two types of titanium dioxide: lattice oxygen (L<sub>TiO<sub>2</sub></sub>) at 530.9 eV and adsorption oxygen (A<sub>TiO<sub>2</sub></sub>) at 529.9 eV. Interestingly, the L<sub>TiO<sub>2</sub></sub>/A<sub>TiO<sub>2</sub></sub> ratio of all *in situ* TFN membranes was approximately 2, which is in agreement with the results listed in Table 1. It is worth noting that adsorbed oxygen comes mainly from water in the air and is present on the titanium dioxide surface in the form of OH groups. Therefore, in comparison with the TiO<sub>2</sub> NPs of the *ex situ* TFN membranes, the *in situ*-synthesized TiO<sub>2</sub> of the *in situ* TFN membranes was more hydrophilic and thus significantly increased water flux.

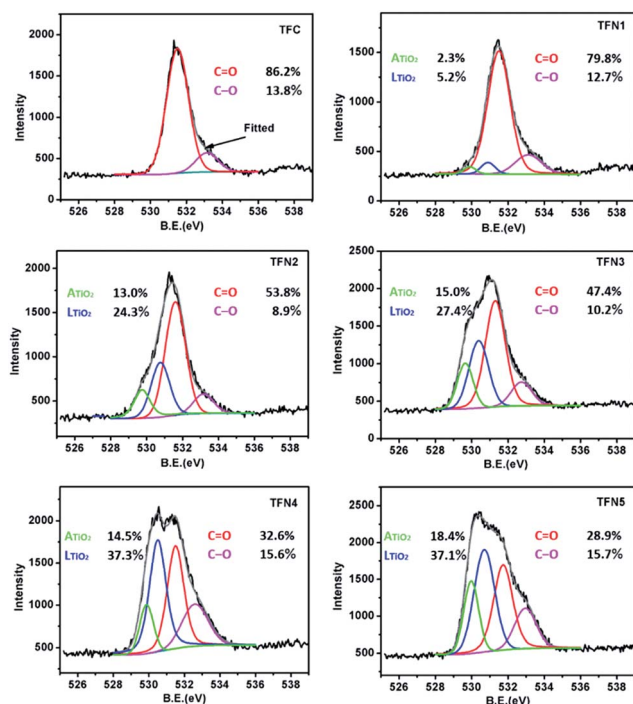
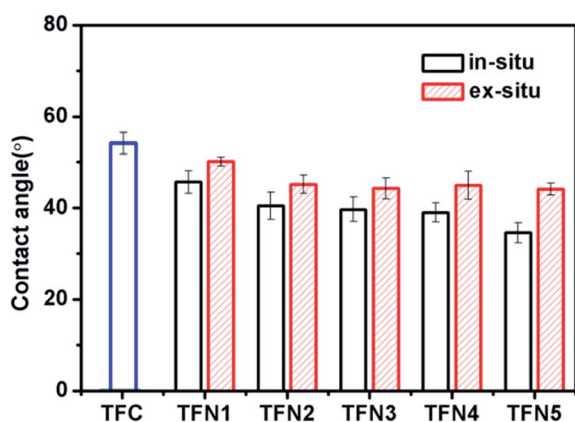
### 3.6 Hydrophilicity and charge properties

Fig. 8 shows the contact angles of the TFC membrane, *in situ*-synthesized TFN membranes, and *ex situ*-synthesized TFN membranes loaded with TBOT or TiO<sub>2</sub> NPs. Both types of TFN membrane had a contact angle lower than that of the TFC



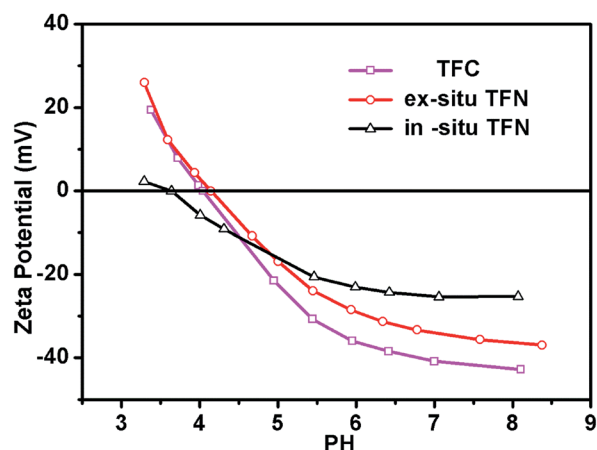
**Table 3** Surface elemental composition of TFC membranes, *in situ*-synthesized TFN membranes, and *ex situ*-synthesized TFN membranes

Membranes	<i>In situ</i> synthesized					<i>Ex situ</i> synthesized				
	Atomic contents (%)					Atomic contents (%)				
	C	N	O	Ti	O/N	C	N	O	Ti	O/N
TFN1	69.3	13.73	16.57	0.4	1.1	71.33	11.59	16.67	0.4	1.3
TFN2	65.91	11.84	20.33	1.92	1.2	70.66	11.85	16.9	0.59	1.3
TFN3	54.19	10.53	30.05	5.23	1.3	65.02	12.00	20.93	2.05	1.3
TFN4	53.18	7.05	32.48	7.29	1.4	57.68	9.80	27.38	5.14	1.5
TFN5	46.61	4.89	38.71	9.79	1.7	52.76	7.55	32.54	7.15	1.9

**Fig. 7** High resolution O 1s spectra for the TFC membrane and *in situ* TFN membranes.**Fig. 8** Contact angles of the *in situ*-synthesized and *ex situ*-synthesized TFN membranes.

membrane ( $54.8 \pm 1.3^\circ$ ), which was attributed to improvement of water flux by the presence of superhydrophilic titanium dioxide. The contact angle of the *in situ* TFN membranes was decreased markedly by the addition of TBOT (from  $45.7 \pm 2.5^\circ$  to  $34.6 \pm 2.2^\circ$ ), while enhancement of hydrophilicity was not obvious for the *ex situ* TFN membranes (the contact angle only decreased from  $50.1 \pm 1^\circ$  to  $44.1 \pm 1.3^\circ$ ) prepared by directly adding  $\text{TiO}_2$  NPs. These findings may explain why the *in situ* TFN membranes had greater  $\text{TiO}_2$  content and showed better dispersion of  $\text{TiO}_2$  in the polyamide layer in comparison with the *ex situ* TFN membranes.

The zeta potential of the TFC and TFN membranes was carefully investigated (Fig. 9). The zeta potential of the TFC membranes ranged from 19.5 mV to  $-42.8$  mV at pH values ranging from 3 to 8.5. However, the zeta potential of the *in situ* and *ex situ* membranes was increased after the addition of TBOT or  $\text{TiO}_2$  NPs. In comparison with the zeta potential of the *ex situ* membranes, that of the *in situ* TFN membrane surface was closer to neutral. Furthermore, the isoelectric point of the *in situ* TFN membranes was changed markedly from 4.0 to 3.6 after the addition of TBOT or  $\text{TiO}_2$  NPs, but that of the *ex situ* TFN membranes only increased by 0.1 (from 4.0 to 4.1), perhaps because of the different charge properties of *in situ*- and *ex situ*-synthesized  $\text{TiO}_2$ . Additionally, these results show that the zeta potential of the *in situ* TFN membranes is clearly higher than

**Fig. 9** pH dependence of the zeta-potential of the TFC membrane, *in situ*-synthesized TFN membranes, and *ex situ*-synthesized TFN membranes.



that of the other membranes at pH values ranging from 5 to 8. Generally, membrane surfaces with zeta potential close to zero exhibit good anti-fouling properties with regard to charged organic foulants because interaction between the charged surface and organic foulants is impaired.<sup>62</sup> Therefore, it can be concluded that the *in situ*-synthesized TFN membranes may have anti-fouling properties stronger than those of the TFC membrane and *ex situ*-synthesized TFN membranes.

## 4. Conclusions

We developed a promising strategy for the preparation of thin film nanocomposite membranes with *in situ* generation of TiO<sub>2</sub> NPs in the active layer. TBOT was added to the organic phase, where it served as a Ti source that was eventually hydrolysed, followed by aggregation of TiO<sub>2</sub> NPs in the selective layer, which improved NP dispersion and increased TiO<sub>2</sub> loading. In comparison with the TFN membranes prepared by directly adding TiO<sub>2</sub> NPs to the reaction mixture (*i.e. ex situ*), the *in situ*-generated TFN membranes showed enhanced permeability, even at a TBOT concentration as low as 250 mg L<sup>-1</sup>. The permeation tests implied that the concentration of TBOT was an important factor that determined the performance of the nanocomposite membrane, and larger water flux was observed at greater TBOT concentrations. The SEM images demonstrated that the surface morphology of the nanocomposite membranes was altered by TBOT loading, and a unique network structure was found on the particle surface. The surface composition of the TFN membranes was determined *via* XPS and XRD analysis to confirm that TBOT was transformed into TiO<sub>2</sub> nanoparticles that were present at the membrane surface.

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