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# Advanced anti-corrosion coatings prepared from $\alpha$ -zirconium phosphate/polyurethane nanocomposites†

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This paper presents the first successful application of  $\alpha$ -zirconium phosphate/polyurethane (ZrP/PU) nanocomposites for corrosion protection. ZrP nanoplatelets were synthesized using a reflux method and modified with a polyetheramine surfactant (Jeffamine M1000) to form organic ZrP nanoplatelets. ZrP/PU nanocomposite films were based on PU and ZrP with different ZrP contents from 0.5–5 wt%. To probe the internal morphology of ZrP/PU nanocomposites, their cross-sections were examined by scanning and transmission electron microscopy. The results reveal that ZrP dispersed very well in PU films and that no substantial agglomeration occurred. Well-dispersed ZrP nanoplatelets in a PU matrix could effectively enhance the moisture barrier properties of ZrP/PU films. The water vapor transmission rate was significantly reduced to 84 g m<sup>-2</sup> per day for ZrP/PU films compared to 194 g m<sup>-2</sup> per day for pure PU films. Using a series of electrochemical measurements of corrosion potential ( $E_{\text{corr}}$ ), polarization resistance ( $R_p$ ), corrosion current ( $I_{\text{corr}}$ ), and electrochemical impedance spectroscopy, ZrP/PU coatings on cold-rolled steel electrodes were also found to exhibit enhanced corrosion protection properties compared to pure PU coatings.

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## 1. Introduction

The market size for corrosion protection in the United States was estimated to be \$2.2 trillion in 2016.<sup>1</sup> Many approaches for corrosion protection have been developed and proven. However, most are detrimental to our environment because they involve extensive materials. Zinc-based coatings are suitable for corrosion protection and environmentally friendly, but are typically brittle and expensive.<sup>2</sup> Recently, new organic coatings have attracted significant attention due to their potential for simple preparation and functionalization.<sup>3–7</sup> However, there is a great need for new anti-corrosion coatings that are able to take advantage of currently-used industrial processing approaches, such as those for coatings. Polymer/filler nanocomposites have received immense attention<sup>8–11</sup> due to their excellent properties, low cost, and lower concentrations needed

compared to conventional materials.<sup>12</sup> Their barrier and anti-corrosion properties can be further improved by the addition of a variety of fillers, such as clays,<sup>13–17</sup> boron nitride nanosheets,<sup>18,19</sup> carbon nanotubes,<sup>20,21</sup> graphene nanosheets,<sup>22,23</sup> and alumina nanosheets,<sup>24</sup> into polymer preparations. Recently, nanocomposites of  $\alpha$ -zirconium phosphate (ZrP) and polymers have been studied for use as anti-corrosion coatings due to their good gas barrier properties.<sup>25</sup> The aspect ratio of used ZrP nanoplatelets may be controlled by different concentrations of phosphoric acid.<sup>26</sup> For the polymer material, polyurethane (PU) has been considered one of the most versatile ones; its properties can be changed by varying the polyol and isocyanate precursors, and it is widely utilized for coatings, paints, adhesives, foams, footwear, car parts, and sound insulating plates.<sup>27–30</sup> To the best of our knowledge, ZrP/PU nanocomposites have rarely been studied. In this article, ZrP, produced from zirconium(IV) oxide chloride powder by a reflux method followed by exfoliation with monoamine, was selected as the nanofiller to add to PU. ZrP nanoplatelets dispersed in the PU matrix were characterized by electron microscopy and Fourier transform infrared (FTIR) spectroscopy. The moisture barrier and optical transparency properties of PU and ZrP/PU films were evaluated using a permeation test system and ultraviolet-visible (UV-VIS) spectrophotometry. In addition, the anti-corrosion performance of ZrP/PU nanocomposite coatings on the surface of a cold-rolled steel (CRS) substrate was studied in a 3.5 wt% NaCl aqueous solution by monitoring the open

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circuit potential (OCP) and tracing the quasi-stationary polarization (Tafel plot) of the coated CRS electrode. Electrochemical impedance spectroscopy (EIS) was also conducted to obtain insight into the processes occurring in the composite coating in a corrosive environment.

## 2. Experimental

### 2.1 Materials

Zirconyl chloride ( $\text{ZrOCl}_2 \cdot 8\text{H}_2\text{O}$ , 98%, Aldrich), phosphoric acid ( $\text{H}_3\text{PO}_4$ , 85%, SHOWA), 4,4'-methylenebis(phenyl isocyanate) (4,4-MDI, 99%, Aldrich), poly(propylene glycol) (PPG1000, average  $M_n = 1000$ , Aldrich), 1,4-butylene glycol (1,4-BG, 99%, Aldrich), dibutyltin dilaurate (DBTDL, 95%, Aldrich), Jeffamine M1000 polyetheramine (Huntsman Chemical Corporation), Dimethylformamide (DMF, 99%, Aldrich) was dried under vacuum before use.

### 2.2 Synthesis of functional ZrP nanoplatelets

ZrP nanoplatelets were synthesized by using a refluxing method. Samples of zirconyl chloride (5.0 g) were refluxed with 12.0 M  $\text{H}_3\text{PO}_4$  (50.0 mL) in a Pyrex glass flask at 110 °C for 36 h. The ZrP product was washed several times with deionized (DI) water and ethanol. The as-prepared ZrP powder was then functionalized by a commercial monoamine intercalating agent (Jeffamine M1000) in DMF. A detailed synthesis process was described in previous studies.<sup>10,31</sup>

### 2.3 Preparation of ZrP/PU nanocomposites

Methylene diphenyl diisocyanate (MDI, 8.0 g) and polypropylene glycol (PPG,  $M_n = 1000$ , 10.0 g) were used to synthesize the PU pre-polymer. The components were reacted in DMF at 80 °C while mechanically stirring under nitrogen flow for 2 h. The desired amount of ZrP suspended in DMF was then added, followed by stirring for 2 h. Finally, the chain extender 1,4-butanediol (1,4-BD) was added to increase the pre-polymer size during a 2 h reaction. The as-prepared ZrP/PU solution was subsequently cast onto clean release paper by a scraping cutter and cured at elevated temperatures. All cast films were thermally imidized under the following conditions to complete imidization: films were heated at a rate of 0.6–1 °C  $\text{min}^{-1}$  to 50, 80, or 110 °C, kept isothermal at each temperature for 0.5 h, and finally heated to 110 °C for 6 h. The molar ratio of MDI to PPG in the pre-polymer was 3 : 1, and the total NCO/OH ratio in the PU was equal to 1. By changing the addition of ZrP from 0.5 to 1, 3, and 5 wt%, a series of transparent PU nanocomposite films was successfully synthesized, coded as ZrP-0.5/PU, ZrP-1/PU, ZrP-3/PU, and ZrP-5/PU, respectively. The synthesis process of ZrP/PU nanocomposites is shown in Fig. 1.

### 2.4 Characterization

The external morphology of ZrP and ZrP/PU nanocomposite films were observed by using field-emission scanning electron microscopy (FESEM, JSM-7100, JEOL, Japan), and field emission transmission electron microscope (FETEM, JEM-2100F, JEOL, Japan). The characterizations of ZrP/PU nanocomposites have

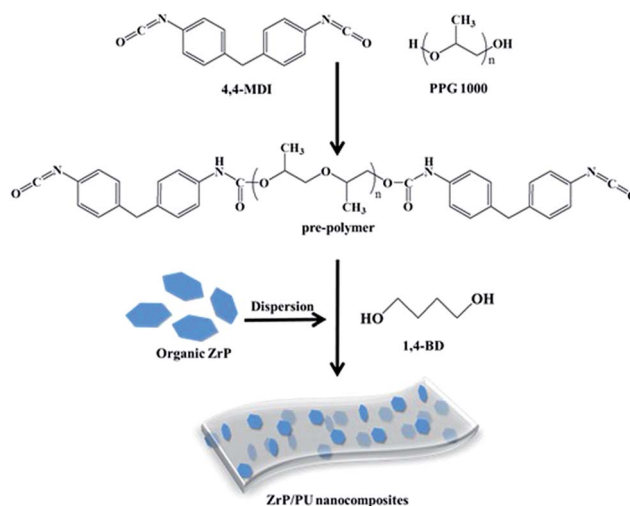


Fig. 1 Synthesis procedure of ZrP/PU nanocomposites.

been by analyzed instrument of attenuated total reflection Fourier transform infrared spectrometer (ATR-FTIR) application a Nicolet-380 spectrometer (Thermo, U.S.), and high resolution X-ray diffractometer (XRD, PANalytical X'Pert3 powder). The optical performance, including transmittance, haze of spin-coated thin films was inspected by a UV-Vis spectrometer (JASCO V-750). The water vapor transmission rate of each specimen with the size of 20  $\text{cm}^2$  was analyzed with a interpenetration test system (WVTR, Permatran-W 3/61, MOCON) at atmospheric pressure, 40 °C and 100% relative humidity (RH). Electrochemical tests of coated and uncoated mild steel strip were advanced in a conventional three electrode flat glass cell using an electrochemical workstation zive sp1 (Wonatech, Korea) in 3.5 wt% NaCl solutions.

The three electrodes are Ag/AgCl as consultation, platinum as accessory, and test sample as the operating electrode. A total of 1.0  $\text{cm}^2$  area of operating electrode was uncovered to the solution. Before the electrochemical experiment, the operating electrode was approved to stabilize for 20 minutes, and then its open circuit potential (OCP) was calendared as a function of time for 600 seconds. After OCP stabilization, impedance measurements were made at exceptional corrosion potentials ( $E_{\text{corr}}$ ) over a frequency reach of 100 kHz to 0.1 Hz, with a signal vibration amplitude perturbation of 10 mV. Potentiodynamic polarization studies were conducted in the potential range of  $\pm 250$  mV at 0.002  $\text{mV s}^{-1}$  scan rate. The Tafel and impedance parameters were collected by curve fitting programs available in the software. Corrosion current density ( $I_{\text{corr}}$ ) was determined by superimposing a straight line along the linear portion of cathodic or anodic curve and extrapolating it through  $E_{\text{corr}}$ . Corrosion rate (CR, in mm per year) was calculated using the following equation:<sup>32,33</sup>

$$\text{CR (mm per year)} = \frac{I_{\text{corr}} (\text{A cm}^{-2}) \times M (\text{g})}{D (\text{g cm}^{-2}) \times V} \times 3270$$

where  $I_{\text{corr}}$  is the current density ( $\text{A cm}^{-2}$ ),  $M$  is the molecular mass,  $V$  is the valence (the number of electrons that are lost



during the oxidation reaction), 3270 is a constant, and  $D$  is the CRS density ( $\text{g cm}^{-3}$ ).

### 3. Results and discussion

#### 3.1 Synthesis and characterization of ZrP, PU and ZrP/PU

The SEM image in Fig. 2(a) shows that ZrP nanoplatelets were basically regular in shape.<sup>34,35</sup> These ZrP nanoplatelets had similar sizes, with a mean length of about 100–200 nm. The XRD spectrum of ZrP is shown in Fig. 2(b). The first strong refraction peak of ZrP at  $2\theta = 11.6^\circ$  corresponds to the ZrP interlayer of (002), the second refraction peaks of ZrP at  $2\theta = 19.7^\circ$  and  $20.1^\circ$  represent the ZrP interlayer of (110) and (-202). The third refraction peaks of ZrP at  $2\theta = 24.9^\circ$  and  $25.3^\circ$  indicate the ZrP interlayer of (112) and (-204).<sup>36–38</sup> The chemical structure of the ZrP nanoplatelets was characterized with an FTIR spectrometer over the spectral region of 400–4000  $\text{cm}^{-1}$ . As shown in Fig. 2(c), the -OH extending vibrations in water are clearly visible at 3509 and 3592  $\text{cm}^{-1}$ ; P-OH extending vibrations are visible at 3135  $\text{cm}^{-1}$ ; intermediate vibrations of water can be observed at 1616 and 1622  $\text{cm}^{-1}$ ; P-OH deformation vibrations are visible at 1248  $\text{cm}^{-1}$ ; peaks of orthophosphate groups can be identified at 1037 and 1071  $\text{cm}^{-1}$ ; the peak at 962  $\text{cm}^{-1}$  can be assigned to pyrophosphate groups; and finally, the peak at 560  $\text{cm}^{-1}$  can be associated to Zr-O extending vibrations.<sup>39,40</sup>

FTIR spectroscopy was also used to characterize ZrP/PU nanocomposites with varying ZrP content, with results shown in Fig. 3. Non-bonded N-H extending vibrations ( $\sim 3486 \text{ cm}^{-1}$ ), bonded N-H extending vibrations ( $3316 \text{ cm}^{-1}$ ), C-H extending vibrations ( $\sim 3000$  and  $\sim 2800 \text{ cm}^{-1}$ ), non-bonded C=O extending vibrations ( $1716 \text{ cm}^{-1}$ ), the urethane group ( $1689 \text{ cm}^{-1}$ ), N-H bending and C-N extending vibrations ( $1523 \text{ cm}^{-1}$ ), and C-O-C extending vibrations ( $1082 \text{ cm}^{-1}$ ) could be identified.<sup>41,42</sup> The NCO groups ( $2270 \text{ cm}^{-1}$ ) could not be observed in the spectra, indicating that the synthesis process had been completed.<sup>43</sup>

To probe the internal morphologies of PU and ZrP/PU nanocomposites, their cross-sections were examined by SEM

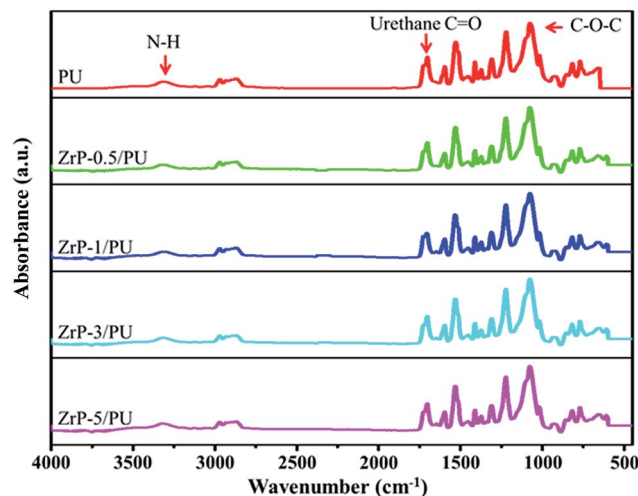


Fig. 3 FTIR spectra of PU and ZrP/PU films.

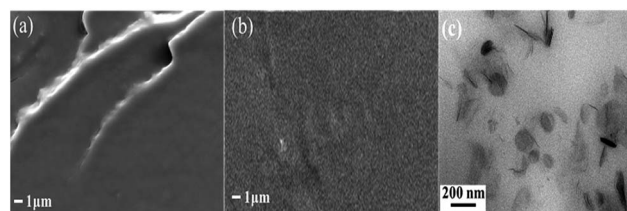


Fig. 4 SEM images of (a) PU and (b) ZrP-5/PU nanocomposite. (c) TEM image of ZrP-5/PU nanocomposite.

imaging. Fig. 4(a) and (b) show the cross-sectional SEM images of pure PU and ZrP-5/PU, respectively. The fracture surface of ZrP-5/PU was smooth and no aggregation of ZrP could be observed. TEM was used to investigate the three-dimensional morphology of as-prepared hybrid materials. Fig. 4(c) demonstrates that the hybrid material of PU with an incorporated ZrP concentration of 5 wt% exhibited good dispersion, which can influence the optical transparency, moisture barrier, and anti-corrosion properties of polymer nanocomposites.<sup>44</sup>

#### 3.2 Optical transparency of pure PU and ZrP/PU films

Fig. 5 shows the optical transmittance spectra of pure PU as well as ZrP/PU nanocomposite films. For pure PU, the transmittance was 99.63% at 550 nm. Although the transmittance of the nanocomposite films decreased as their ZrP content increased, the ZrP-5/PU films still retained their transparency (transmittance > 95%). For ZrP/PU films, the transmittance at 550 nm was 99.17, 98.45, 97.84, and 96.26% for ZrP contents of 0.5, 1, 3, and 5 wt%, respectively. The functional surface groups of ZrP likely facilitated the uniform dispersion of ZrP in DMF. The observed results suggest that the obtained ZrP/PU films were nearly colorless and had excellent optical transparencies.

#### 3.3 Gas barrier properties of ZrP/PU films

Films of PU and ZrP/PU materials used for molecular barrier measurements were prepared to have a thickness of

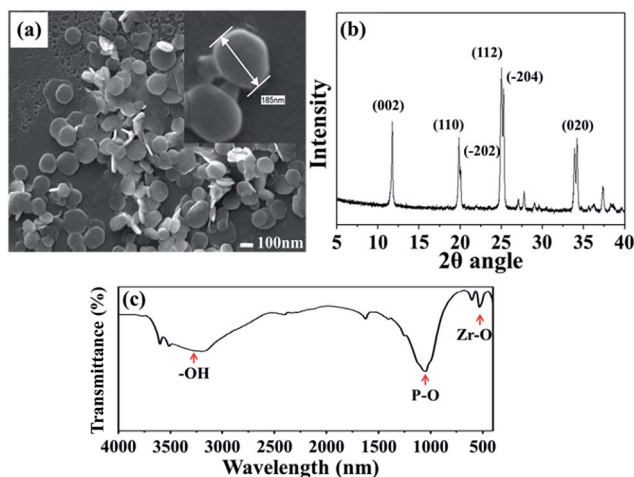


Fig. 2 (a) SEM image, (b) XRD spectrum and (c) FTIR spectrum of ZrP.



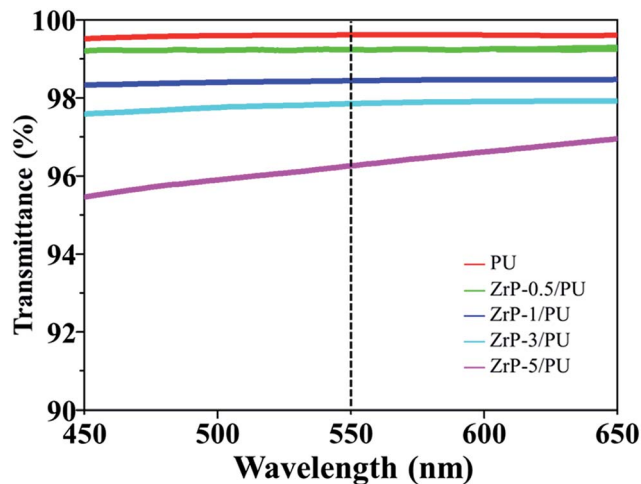


Fig. 5 UV-Vis spectra in the visible light range of PU and ZrP/PU films.

approximately 30  $\mu\text{m}$ . In comparison with PU, the ZrP/PU films exhibited lower  $\text{H}_2\text{O}$  permeability, as shown in Fig. 6. The  $\text{H}_2\text{O}$  permeability in terms of water vapor transmission rate (WVTR) of PU, ZrP-0.5/PU, ZrP-1/PU, ZrP-3/PU, and ZrP-5/PU was ca. 194, 164, 132, 107, and 84  $\text{g m}^{-2}$  per day, respectively. Thus, a significant decrease in WVTR was observed due to the addition of 5 wt% ZrP to the PU matrix. The good dispersion of ZrP in the PU matrix may have effectively extended the path of the water vapor passing through the hybrid film and thereby significantly improved the water vapor barrier property.<sup>45,46</sup>

### 3.4 Potentiodynamic measurements

For the corrosion protection experiments, a series of electrochemical measurements of PU and ZrP/PU coatings on CRS electrodes was used to investigate anti-corrosion effects in a 3.5 wt% NaCl aqueous solution. The measured corrosion potential ( $E_{\text{corr}}$ ), polarization resistance ( $R_p$ ), corrosion rate (CR), and corrosion current density ( $I_{\text{corr}}$ ) values are given in Table 1. Generally, a higher  $E_{\text{corr}}$  and lower  $I_{\text{corr}}$ ,  $R_p$ , and CR indicate

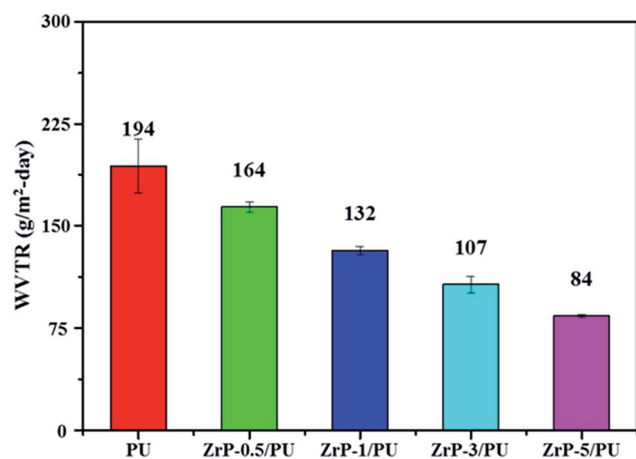


Fig. 6 WVTR of pure PU and ZrP/PU films. Note: WVTR was measured at a temperature of 40  $^{\circ}\text{C}$  and relative humidity (RH) of 100%.

better corrosion protection. The potentiodynamic polarization curves for PU and ZrP/PU coatings are shown in Fig. 7. The  $I_{\text{corr}}$  and  $E_{\text{corr}}$  of pure uncoated CRS were  $4.2 \times 10^{-6}$   $\text{A cm}^{-2}$  and  $-873$  mV, respectively. However, after coating CRS with PU and ZrP/PU nanocomposite films, the  $I_{\text{corr}}$  decreased to  $4.28 \times 10^{-8}$   $\text{A cm}^{-2}$  for a pure PU coating and to as low as  $1.21 \times 10^{-9}$   $\text{A cm}^{-2}$  for a ZrP-5/PU coating. The corresponding  $E_{\text{corr}}$  increased from  $-606$  mV for pure PU-coated CRS to  $-307$  mV for ZrP-5/PU-coated CRS. The anti-corrosion properties of several other polymer nanocomposite coatings reported in the literature are provided in ESI, Table S1.†

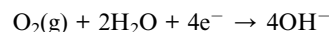
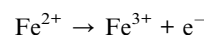
The CR was estimated to be 48.9 mm per year for bare CRS. Meanwhile, the CR of ZrP-5/PU-coated CRS was greatly lowered to  $1.42 \times 10^{-5}$  mm per year, 35 times less than that observed for PU-coated CRS ( $5.01 \times 10^{-4}$  mm per year).

The  $R_p$  was evaluated from Tafel plots, according to the Stern–Geary equation:<sup>46–48</sup>

$$R_p = \frac{b_a \times b_c}{2.303(b_a + b_c) \times I_{\text{corr}}}$$

where  $I_{\text{corr}}$  is determined by the intersection of the linear portions of the anodic and cathodic curves, and  $b_a$  and  $b_c$  are the anodic and cathodic slopes ( $\Delta E/\Delta \log I$ ), respectively.

The ZrP-5/PU coating exhibited the best anti-corrosion capability, as evidenced by its highest and lowest values for  $E_{\text{corr}}$  and  $I_{\text{corr}}$  (which correspond to a lower corrosion rate), respectively, compared to pure CRS and PU-coated CRS. The enhanced corrosion protection mechanism of the ZrP/PU coatings might be the increased tortuosity of diffusion pathways due to well-dispersed ZrP. The corrosion process in neutral solutions is presented in the following equations:<sup>27,45</sup>



It is known that, to cause corrosion, sufficient  $\text{H}_2\text{O}$  is required for the formation of rust and dissolution of steel. Effective prevention of corrosion of a metal substrate can therefore be achieved if  $\text{H}_2\text{O}$  is prevented from accessing its surface, which might be achieved by an increase in the tortuosity of diffusion pathways. For this reason, increased tortuosity may lead to good anti-corrosion properties.

### 3.5 Electrochemical impedance spectroscopy (EIS)

EIS is a powerful tool to study the corrosion protection mechanism of coatings. The magnitude of impedance was used to determine the resistance of coatings to the transportation of electrons and charges. Differences of several orders of magnitude in impedance were observed, as shown in the Nyquist plots (Fig. 8). The Nyquist plots of all samples were nearly semicircle arcs. We found that the charge transfer resistances of the



Table 1 Comparison of corrosion properties of PU and ZrP/PU films in terms of  $E_{\text{corr}}$ ,  $R_p$ ,  $I_{\text{corr}}$ , and CR, as measured by electrochemical methods

Sample name	Electrochemical measurements				
	$E_{\text{corr}}$ (mV)	$R_p$ (k $\Omega$ cm $^2$ )	$I_{\text{corr}}$ (A cm $^{-2}$ )	CR (mm per year)	Thickness ( $\mu\text{m}$ )
Neat CRS	-873	4.12	$4.20 \times 10^{-6}$	48.92	—
PU	-606	$1.40 \times 10^3$	$4.28 \times 10^{-8}$	$5.01 \times 10^{-4}$	30
ZrP-0.5/PU	-546	$1.35 \times 10^4$	$2.71 \times 10^{-9}$	$3.17 \times 10^{-5}$	36
ZrP-1/PU	-455	$1.66 \times 10^4$	$2.07 \times 10^{-9}$	$2.43 \times 10^{-5}$	34
ZrP-3/PU	-417	$2.03 \times 10^4$	$1.95 \times 10^{-9}$	$2.28 \times 10^{-5}$	32
ZrP-5/PU	-307	$3.17 \times 10^4$	$1.21 \times 10^{-9}$	$1.42 \times 10^{-5}$	35

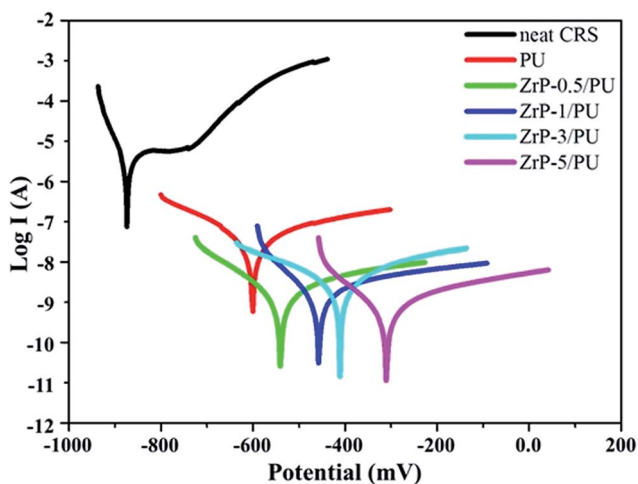


Fig. 7 Tafel plots for neat CRS, PU, and ZrP/PU films, measured in a 3.5 wt% aqueous NaCl solution.

samples, as determined by the intersection of the low frequency end of each semicircle arc with the real axis, were 14,  $2.93 \times 10^5$ ,  $4.46 \times 10^5$ ,  $6.42 \times 10^5$ ,  $8.28 \times 10^5$ , and  $10.09 \times 10^5 \Omega$ , respectively. The nanocomposite coatings thus served as effective physical barriers to prevent corrosive ions in the electrolyte

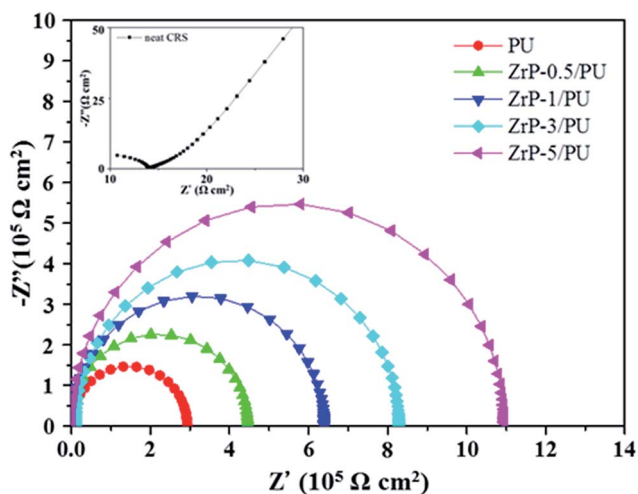


Fig. 8 Nyquist plots for PU and ZrP/PU films measured in 3.5 wt% aqueous NaCl solution. The inset shows the Nyquist plots for neat CRS.

from penetrating the coating to induce corrosion of the steel. These results clearly demonstrate that the samples with the highest ZrP content exhibited the best corrosion protection performance.<sup>49,50</sup>

## 4. Conclusions

This study is the first to report the preparation and corrosion protection performance of a series of hybrid nanocomposite materials of polyurethane (PU) and  $\alpha$ -zirconium phosphate (ZrP). Compared to pure PU films, ZrP/PU nanocomposite films with a low ZrP content (e.g., 5 wt%) show a reduction of about 40% in H<sub>2</sub>O permeability. The reduced H<sub>2</sub>O permeability was attributed to the good dispersion of the ZrP filler material, which increased the length of H<sub>2</sub>O gas diffusion pathways. A series of electrochemical studies was conducted on the corrosion protection properties of the ZrP/PU nanocomposite coatings. The corrosion potential and polarization resistance increased, whereas the corrosion current and the corrosion rate decreased with an increase in ZrP content, confirming that ZrP-PU coatings provide effective anti-corrosion protection. The ZrP/PU nanocomposites showed superior corrosion inhibition, suggesting that they have great potential for use in the anti-corrosion coating industry.

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