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## An optimised synthesis of high performance radiation-grafted anion-exchange membranes†

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High performance benzyltrimethylammonium-type alkaline anion-exchange membranes (AEM), for application in electrochemical devices such as anion-exchange membrane fuel cells (AEMFC), were prepared by the radiation grafting (RG) of vinylbenzyl chloride (VBC) onto 25  $\mu\text{m}$  thick poly(ethylene-co-tetrafluoroethylene) (ETFE) films followed by amination with trimethylamine. Reductions in the electron-beam absorbed dose and amount of expensive, potentially hazardous VBC were achieved by using water as a diluent (reduced to 30–40 kGy absorbed dose and 5 vol% VBC) instead of the prior state-of-the-art method that used organic propan-2-ol diluent (required 70 kGy dose and 20 vol% VBC monomer). Furthermore, the water from the aqueous grafting mixture was easily separated from the residual monomer (after cooling) and was reused for a further grafting reaction: the resulting AEM exhibited an ion-exchange capacity of 2.1  $\text{mmol g}^{-1}$  (cf. 2.1  $\text{mmol g}^{-1}$  for the AEM made using a fresh grafting mixture). The lower irradiation doses resulted in mechanically stronger RG-AEMs compared to the reference RG-AEM synthesised using the prior state-of-the-art method. A further positive off-shoot of the optimisation process was the discovery that using water as a diluent resulted in an enhanced (*i.e.* more uniform) distribution of VBC grafts as proven by Raman microscopy and corroborated using EDX analysis: this led to enhancement in the  $\text{Cl}^-$  anion-conductivities (up to 68  $\text{mS cm}^{-1}$  at 80  $^\circ\text{C}$  for the optimised fully hydrated RG-AEMs vs. 48  $\text{mS cm}^{-1}$  for the prior state-of-the-art RG-AEM reference). A down-selected RG-AEM with an ion-exchange capacity = 2.0  $\text{mmol g}^{-1}$ , that was synthesised using the new greener protocol with a 30 kGy electron-beam absorbed dose, led to an exceptional beginning-of-life  $\text{H}_2/\text{O}_2$  AEMFC peak power density of 1.16  $\text{W cm}^{-2}$  at 60  $^\circ\text{C}$  in a benchmark test using industrial standard Pt-based electrocatalysts and unpressurised gas supplies: this was higher than the 0.91  $\text{W cm}^{-2}$  obtained with the reference RG-AEM (IEC = 1.8  $\text{mmol g}^{-1}$ ) synthesised using the prior state-of-the-art protocol.

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## Introduction

### Background to the interest in anion-exchange membranes (AEM)

Due to the geopolitics related to fossil fuel supplies and the need to lower  $\text{CO}_2$  emissions, there has been an extensive investigation into fuel cells over a number of decades. Proton-exchange membrane fuel cells (PEMFC) represent one of the most researched, and well known, energy conversion technologies available today.<sup>1–3</sup> Even though commercial PEMFC vehicles are now on the market (*e.g.* the Toyota Mirai fuel cell car), a large-scale market introduction of PEMFCs continues to face challenges such as durability, the lack of  $\text{H}_2$  infrastructure, and the continued use of Pt-based electrocatalysts. The catalysts comprise nearly half of the high-volume cost of PEMFCs.<sup>5,6</sup>



The use of alkaline anion-exchange membranes (AEM)<sup>7</sup> in anion-exchange membrane fuel cells (AEMFC), which have a high pH *in situ* environment, holds the promise of the ability to use a wider range of non-Pt-group electrocatalysts compared to PEMFCs.<sup>8,9</sup> Furthermore, AEMFCs offer other potential advantages, such as lower membrane cost and cheaper cell components (*e.g.* thin, easily stamped, metal bipolar plates) due to a less corrosive *in situ* environment compared with the use of polymeric superacid materials in PEMFCs. As a consequence, the development of AEMs and AEMFCs has become a significant avenue of fuel cell research, particularly in the last 10 years.<sup>10</sup>

### Radiation-grafted (RG) membranes

A useful method for the production of membranes such as ion-exchange membranes, is radiation induced graft polymerisation.<sup>11,12</sup> Radiation grafting (RG) is the process by which a precursor material is treated with high energy radiation (such as that from the commercial electron-beam accelerators or <sup>60</sup>Co  $\gamma$ -ray facilities used to sterilise baby bottles or medical products in the UK) to produce an activated material that contains either radicals or peroxide groups (without and with the presence of O<sub>2</sub>, respectively, during the irradiation step): hence the precursor material is turned into a graft initiating material that can then react with vinyl monomers. RG membranes have several points of attractiveness including: the utilisation of pre-formed commercial polymer films (thus no film formation step through solvent casting is required), the ease of control of the degree of monomer grafting *via* adjustment of a number of reaction parameters, and having no requirements for the use of highly reactive chemical initiators or catalysts (that can leave chemical fragments in the final product). Thus, RG is an especially convenient method for the repeatable synthesis of large batches of functional membranes for fundamental studies, for the wider distribution of samples for evaluation by other teams, and ultimately for use in a variety of applications (ion-exchange, energy conversion *etc.*). This includes facilitating the comparison of the properties of a range of ion-exchange membranes where they feature comparable ion-exchange capacities (IEC) and the same precursor material but with different ionic moieties (*i.e.* the only effective variable between different ion-exchange membranes is the ionic head-group).<sup>13</sup>

However, radiation induced grafting usually requires large radiation absorbed doses to obtain high levels of monomer (*e.g.* styrene) grafting throughout the thicknesses of the polymer films.<sup>14</sup> The use of high irradiation doses typically results in a detrimental reduction in the mechanical properties of the synthesised membranes (*e.g.* undesirable breaking of C–C bonds in the precursor polymer backbone).<sup>15</sup> For example, a rule of thumb is that the mechanical properties of poly(ethylene-*co*-tetrafluoroethylene) (ETFE) films excessively degrade after absorbing radiation doses of more than 30–50 kGy in air.<sup>15</sup> Therefore, there is a need for the synthesis of RG ion-exchange membranes with high IECs using lower radiation doses.

### Prior state-of-the-art RG-AEMs

RG-based AEMs have been researched by many groups using a variety of strategies involving the RG of vinyl monomers onto fluorinated (FEP),<sup>16</sup> partially-fluorinated (*e.g.* ETFE<sup>17</sup> and PVDF<sup>18</sup>) and non-fluorinated (*e.g.* LDPE)<sup>19,20</sup> films with subsequent amination to yield anion-exchange (anion conducting) materials. Vinylbenzyl chloride (VBC) is an ideal monomer for the preparation of AEMs due to its dual reactive –CH=CH<sub>2</sub> and –CH<sub>2</sub>Cl functional groups. However, VBC is both expensive and hazardous when used in large quantities (*e.g.* potentially mutagenic and acutely toxic). It is therefore vital to significantly reduce the quantity of VBC monomers used in the grafting step. This has been carried out most widely by the dilution of VBC with organic solvents such as propanol<sup>4,21</sup> and toluene.<sup>22</sup> Specifically, our group has previously used propan-2-ol diluent to lower the VBC concentration to 20 vol% for grafting onto ETFE film that had been electron-beam irradiated to a high 70 kGy absorbed dose (the prior state-of-the-art “reference” method).<sup>4</sup>

### RG-membranes using water as an alternative solvent in the grafting step

From the perspective of green sustainable chemistry, an organic solvent-free method is desirable. Wada *et al.*<sup>23</sup> found that the water-based, emulsion graft polymerisation of vinyl acetate onto poly(3-hydroxybutyrate) film enhanced the degree of grafting by *ca.* 100 times higher than when an organic diluent, such as methanol, was used. The study of Mohamed *et al.*<sup>24</sup> suggests that this emulsion graft mechanism is governed by diffusion of monomer micelles to the base polymer material.

### Aim and objectives of this study

The aim of the study is to optimise the method for synthesising AEMs containing a benchmark cationic head-group chemistry (benzyltrimethylammonium chloride) by pre-irradiation grafting of VBC monomers onto electron-beamed (in air) 25  $\mu$ m ETFE film. The objectives include: a significant reduction in the concentration of VBCs, elimination of the organic diluent, and minimisation of the absorbed doses (for maximum mechanical stabilities). The successful fulfilment of these objectives and the production of high performance RG-AEMs, with enhanced properties compared to the reference AEM synthesised using the prior state-of-the-art protocol, are reported in this article. In parallel, the power of Raman microscopy through-plane mapping for studying the poly(VBC) graft distributions in RG-AEMs is demonstrated. It should be noted that this paper is not designed to be an exhaustive study of the physicochemical properties of the obtained RG-AEMs: only selected characterisations and tests were used to aid the elucidation of the most optimal synthesis of benchmark RG-AEMs.

## Experimental

### Chemicals and materials

Nowoflon ET ETFE film (25  $\mu$ m and 50  $\mu$ m thick,) was supplied by Nowofol Kunststoffprodukte GmbH (Germany). VBC



monomer (mixture of 3- and 4-isomers; 500–100 ppm *tert*-4-butylcatechol and 700–1100 ppm nitromethane inhibitors) was used without removal of the inhibitor and was supplied by Sigma-Aldrich. 1-Octyl-2-pyrrolidone and aqueous trimethylamine solution (TMA, 45 wt%) were also purchased from Sigma-Aldrich. Propan-2-ol and toluene were of reagent grade and supplied by Fisher Scientific (UK). All chemicals were used as received and the ultra-pure water (UPW) used was of resistivity = 18.2 M $\Omega$  cm.

### RG-AEM(Cl<sup>-</sup>) preparation using 25 $\mu$ m ETFE

A schematic summary of the preparation of ETFE-based RG-AEMs is shown in Scheme 1. The AEMs were prepared from pre-formed ETFE films using the pre-irradiation (in air) method previously reported<sup>10</sup> with modifications to the grafting step as detailed below and summarised in Table 1.

**Irradiation stage.** The ETFE films were subjected to electron-beam irradiation in air to different absorbed doses (using a 4.5 MeV Dynamatron Continuous DC Electron Beam Unit Synergy Health, South Marston, UK). As the irradiation step is performed in air, immediate reaction of the radicals that are formed with O<sub>2</sub> molecules leads to the creation of peroxide and hydroperoxide groups on the polymers: thus this pre-irradiation method is called “peroxidation”.<sup>11</sup> The peroxidated ETFE film then acts as a solid-state free-radical initiator for the subsequent graft polymerisation step. After irradiation, the films were transported back to the laboratory (at the University of Surrey) in dry ice (-78.5 °C) before they were stored in a freezer at -40 °C (to be used within 3 months of irradiation). The effect of extended cold storage on the survival of peroxide

groups in electron-beamed ETFE has been shown to produce no statistically significant reduction in the ion-exchange capacities (IEC) of the resulting RG-AEMs for up to 12 months.<sup>25</sup> This allows flexibility in producing large batches of RG-AEMs from a single electron-beam treatment.

**Grafting stage.** For the grafting step, the electron-beamed ETFE films (*ca.* 15 × 15 cm<sup>2</sup>) were immersed in different grafting solutions (*ca.* 200 cm<sup>3</sup>), containing VBC at concentrations of 5 or 20 vol% in various diluent combinations of water and propan-2-ol, in sealed vessels with the addition of a prior optimised 1 vol% of 1-octyl-2-pyrrolidone surfactant (details in ESI Table S1†). Full details of the grafting mixtures used for the preparation of each intermediate (pre-aminated) membrane are summarised in Table 1. The solutions were then purged with N<sub>2</sub> for 2 h before the vessels were sealed and heated at 70 °C for 24 h. Again, 70 °C has already been determined to be the optimal grafting temperature (see ESI Table S1†).

After the grafting step, the ETFE-*g*-poly(VBC) grafted films were thoroughly washed in toluene, and then heated in toluene at 70 °C for 5 h: this process is employed to remove excess unreacted VBC and any poly(VBC) homopolymer (polymerised VBC that is not chemically bound to the ETFE) that may be present in the grafted films. The resulting intermediate ETFE-*g*-poly(VBC) films were subsequently dried at 70 °C for 5 h in a vacuum oven to remove all traces of solvent. The degree of grafting (DoG, %) of the ETFE-*g*-poly(VBC) intermediate membranes was calculated as follows:

$$\text{DoG} = \frac{m_g - m_i}{m_i} \times 100\% \quad (1)$$

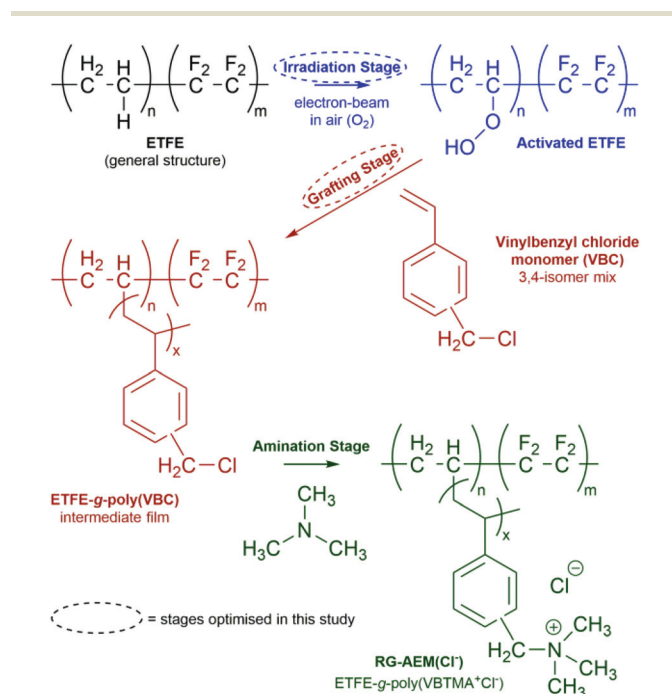
where  $m_g$  is the mass of the grafted sample and  $m_i$  is the initial mass of the irradiated ETFE films.

**Amination stage.** The intermediate ETFE-*g*-poly(VBC) films were then submerged in the aqueous TMA solutions at ambient temperature for 24 h (prior optimised for full amination).<sup>4</sup> These aminated membranes were then thoroughly washed in UPW, and subsequently heated in fresh UPW at 70 °C for 15 h: this procedure removes any unreacted TMA from the membranes.

**Final ion-exchange.** Final conversion to the pure Cl<sup>-</sup>-anion form ETFE-*g*-poly(vinylbenzyltrimethylammonium chloride) (ETFE-*g*-poly(VBTMA<sup>+</sup>Cl<sup>-</sup>)) RG-AEMs was ensured as follows: the crude AEMs (above) were submerged in aqueous NaCl solution (1 mol dm<sup>-3</sup>) for 15 h with one refreshing of the NaCl solution during this period. The resulting AEMs were then removed and thoroughly soaked in water to remove any excess co-ions (Na<sup>+</sup>) and counter-ions (Cl<sup>-</sup>): hence, the only counter-ions present were the Cl<sup>-</sup> anions that charge balance each covalently-bound cationic benzyltrimethylammonium group. These “as-synthesised” RG-AEM(Cl<sup>-</sup>)s were stored in UPW until required and were not allowed to dry out at any point before measurements or experiments were conducted on them.

### Optimised RG-AEM(Cl<sup>-</sup>) preparation using thicker 50 $\mu$ m ETFE

This study is primarily targeted at the development of thin RG-AEMs that were prepared using 25  $\mu$ m ETFE films: thinner



**Scheme 1** Outline of the RG-AEM synthesis process used in this study.



**Table 1** Summary of the conditions used to synthesise the RG-AEM(Cl<sup>-</sup>)s and their key properties. All electron-beam irradiations were carried out in air. All grafting steps were carried out at 70 °C in N<sub>2</sub>-purged monomer mixtures containing 1 vol% 1-octyl-2-pyrrolidone (surfactant). All means ± sample standard deviations are from *n* = 3 repeats on different samples of each RG-AEM

RG-AEM(Cl <sup>-</sup> )	E-R <sup>a</sup>	E-1	E-2	E-3	E-4	E-5	E-6	E-7
Electron-beam dose/kGy	70	40	40	40	40	40	30	20
[VBC] (vol%)	20	20	5	20	5	5	5	5
Propan-2-ol : H <sub>2</sub> O <sup>b</sup>	1 : 0	1 : 0	1 : 0	1 : 1	1 : 1	0 : 1	0 : 1	0 : 1
DoG <sup>c</sup> (%)	50	23	2	31	48	89	76	20
IEC <sup>d</sup> /mmol g <sup>-1</sup>	1.81 ± 0.01	1.09 ± 0.05	<0.1	1.44 ± 0.07	1.69 ± 0.05	2.13 ± 0.05	2.01 ± 0.02	0.87 ± 0.06
WU <sup>e</sup> (%)	67 ± 4	14 ± 4	<1%	30 ± 4	35 ± 2	57 ± 5	53 ± 6	15 ± 5
<i>T</i> <sub>dry</sub> <sup>f</sup> /μm	43 ± 2	32 ± 2	25 ± 2	45 ± 2	39 ± 3	47 ± 2	47 ± 2	36 ± 2
<i>T</i> <sub>hyd</sub> <sup>g</sup> /μm	56 ± 2	39 ± 2	25 ± 2	50 ± 2	45 ± 2	62 ± 3	60 ± 2	40 ± 3
TPS <sup>h</sup> (%)	29 ± 4	22 ± 4	0	13 ± 6	15 ± 4	32 ± 4	28 ± 4	10 ± 6
σ (80 °C, hydrated) <sup>i</sup> /mS cm <sup>-1</sup>	48 ± 2	24 ± 3	<1	32 ± 2	46 ± 4	68 ± 3	60 ± 2	16 ± 3

<sup>a</sup> Reference RG-AEM synthesised using the prior state-of-the-art protocol. <sup>b</sup> Diluent system used (vol%) = 100 – 1 vol% (surfactant) – VBC (vol%).

<sup>c</sup> Degree of grafting (calculated using eqn (1)). <sup>d</sup> Ion-exchange capacity (calculated using eqn (4)). <sup>e</sup> Gravimetric water uptake (calculated using eqn (2)). <sup>f</sup> Thickness of fully hydrated RG-AEM(Cl<sup>-</sup>). <sup>g</sup> Thickness of fully hydrated RG-AEM(Cl<sup>-</sup>). <sup>h</sup> Through plane (thickness) swelling (calculated using eqn (3)). <sup>i</sup> Fully hydrated Cl<sup>-</sup> in-plane anion conductivity measured in water using a 4-point probe method (data taken from Fig. 7 and calculated using eqn (5)).

electrolytes generally perform better in electrochemical applications (especially AEMFCs). However, for scientific rigor and comparison purposes, the optimal electron-beam dose, diluent system, and VBC monomer concentration were also determined when using thicker 50 μm ETFE films: parameters such as the grade and supplier of the ETFE, the temperature and the surfactant content were identical to those used for the grafting of the thinner ETFE. The key details of the synthesis of thicker RG-AEM(Cl<sup>-</sup>) are presented in ESI Table S2† with selected data highlighted at the end of this article.

#### Gravimetric water uptake (WU) and through-plane swelling (TPS)

Excess surface water on fully hydrated RG-AEMs(Cl<sup>-</sup>) samples directly removed from UPW storage, was removed by dabbing with filter paper before immediate recording of the hydrated masses (*m*<sub>hyd</sub>) and thicknesses (*T*<sub>hyd</sub>). Thicknesses were recorded using an outside digital micrometer (error = ±2 μm). The RG-AEMs(Cl<sup>-</sup>) samples were subsequently dried in a vacuum oven at 50 °C for 15 h before the dry masses (*m*<sub>dry</sub>) and thicknesses (*T*<sub>dry</sub>) were recorded. All measurements were conducted with triplicate samples of each RG-AEM(Cl<sup>-</sup>). The gravimetric water uptakes (WU) and through-plane swellings (TPS) were calculated by:

$$\text{WU} = \frac{m_{\text{hyd}} - m_{\text{dry}}}{m_{\text{dry}}} \times 100\% \quad (2)$$

$$\text{TPS} = \frac{T_{\text{hyd}} - T_{\text{dry}}}{T_{\text{dry}}} \times 100\%. \quad (3)$$

#### Ion-exchange capacities (IEC)

The ion exchange capacities (IEC) were determined using the dried RG-AEM(Cl<sup>-</sup>) samples recovered from the WU measurements (above). The RG-AEM(Cl<sup>-</sup>) samples, of known dried mass, were immersed in aqueous NaNO<sub>3</sub> solution (20 cm<sup>3</sup>, 2.4 mol dm<sup>-3</sup>) for 5 h. The solutions were subsequently acidified with aqueous HNO<sub>3</sub> (2 cm<sup>3</sup>, 2 mol dm<sup>-3</sup>) and titrated with

standardised aqueous AgNO<sub>3</sub> solution (20.00 ± 0.06 mmol dm<sup>-3</sup>). A Metrohm 848 Titrino Plus autotitrator equipped with an Ag Titrode (Cl<sup>-</sup> anion selective electrode) was used for the titrations. The IEC (mmol g<sup>-1</sup>) was calculated from the end point (*E*<sub>p</sub>, cm<sup>3</sup>), taken as the maxima in the first differential plot of the Ag Titrode potential vs. volume data:

$$\text{IEC}_{\text{Cl}^-} = \frac{E_p \times 0.02}{m_{\text{dry}}} \quad (4)$$

#### Ionic conductivity (Cl<sup>-</sup> anions, in-plane, fully hydrated)

The membrane samples tested for ionic conductivity were taken directly from the RG-AEM(Cl<sup>-</sup>)s, which were stored in UPW after synthesis. The Cl<sup>-</sup> conductivities of fully hydrated RG-AEMs were measured using a Solartron 1260/1287 combination controlled by ZPlot/ZView software (Scribner Associates, USA). Impedance spectra were collected over a frequency range of 0.3 Hz–100 kHz (10 mV amplitude) with the samples mounted in a 4-probe BektTech BT-112 test cell (supplied by Alvatek, UK) that was submerged in UPW at controlled temperatures. Ionic resistance values were extracted from the low frequency *x*-axis intercept. The conductivity (σ/mS cm<sup>-1</sup>) was then calculated using:

$$\sigma = \frac{l}{Rwt} \quad (5)$$

where *t* is the distance between the Pt sense electrodes (0.425 cm), and *w* and *t* are the width and thickness of the RG-AEM(Cl<sup>-</sup>) sample, respectively.

#### Raman micro-spectroscopy

A DXR Raman microscope (Thermo Scientific) was used in this study. This instrument includes a near-IR (780 nm) excitation laser and a confocal microscope. Raman microscopy was used to visualize the through-plane distributions of components throughout the thickness of samples of each RG-AEM and their intermediate ETFE-*g*-poly(VBC) membranes. A 50× objec-



tive was used and the resulting laser spot diameter was 1–2  $\mu\text{m}$ . Raman measurements were recorded with 24 mW of laser power and a 50  $\mu\text{m}$  slit aperture. Spectra were collected using OMNIC<sup>TM</sup> software with an Array Automation function. Line maps were obtained using 1  $\mu\text{m}$  sized steps across the cross-sections of the pre-aminated ETFE-*g*-poly(VBC) samples. The area maps were recorded with 2  $\mu\text{m}$  sized steps in both *x* and *y* directions of the RG-AEM sample cross-sections. The vertical *z* displacement was fixed. A single spectrum was recorded at each point (shift range of 3350–200  $\text{cm}^{-1}$ , resolution <9  $\text{cm}^{-1}$ ). Each spectrum was averaged over 4 acquisitions for line maps and 2 acquisitions for the area maps (21 s per acquisition). Each pixel represents data extracted from each acquired spectrum.

### Energy-dispersive X-ray spectroscopy (EDX) analysis

EDX line map data were used to corroborate Raman through-plane distribution data for each intermediate (pre-aminated) ETFE-*g*-poly(VBC) membrane. The film samples were first placed vertically in a cured disk of Struers' epoxy resin and the surface was then polished using a diamond to obtain a flat (<0.04  $\mu\text{m}$  deviation) cross-sectional area of each membrane sample. To make the samples electronically conductive, all the EDX samples were coated with a 3 nm carbon layer. SEM images were obtained with a JSM-7100F Field Emission Scanning Electron Microscope (SEM). To study the distribution of the poly(VBC) grafts through the thickness of the ETFE-*g*-poly(VBC) samples, elemental EDX line maps, Cl (on the poly(VBC) grafts) and F (on ETFE base polymer), were recorded using a Noran system seven (v. 3.1) ultradry SSD X-ray detector.

### Relative tensile stress–strain testing

Mechanical tensile strength testing of the electron-beamed ETFE base polymer films and RG-AEM(Cl<sup>−</sup>) samples were characterised for modulus and ultimate tensile strength using stress–strain data recorded with a universal mechanical tester (Instron® 5500 Series Single Column Testing System). A rectangular membrane sample (6 cm × 1.5 cm) was stretched at a constant rate of 2 mm min<sup>−1</sup> until failure: the tests were repeated on *n* = 3 samples of each RG-AEM tested. These simple tests are for relative comparison between the samples only: we are not reporting absolute mechanical properties against ASTM standards.

### H<sub>2</sub>/O<sub>2</sub> anion-exchange membrane fuel cell (AEMFC) benchmark testing

**Electrode preparation.** The catalysed gas diffusion electrode (GDE) method was used. Prior to formulation of the electrocatalyst ink, a previously synthesised ETFE-*g*-poly(VBTMA<sup>+</sup>Cl<sup>−</sup>) anion-exchange ionomer (AEI) powder (based on radiation-grafted ETFE powder, Fluon Z8820X, supplied by AGC Chemicals Europe)<sup>26</sup> was ground with a pestle and mortar for 10 min. For the cathode GDE, Pt/C catalyst (Johnson Matthey UK, HiSpec 4000, 40% mass Pt) and AEI powder (20% mass of the total solids loading) were ground together and homogenised in 1 cm<sup>3</sup> UPW in a pestle and mortar for 10 min until a visually even ink was produced. Propan-2-ol (9 cm<sup>3</sup>) was then

added and the ink was then blended in the pestle and mortar for a further 5 min before being homogenised with ultrasound for 1 h. The catalyst ink was sprayed onto a Toray TGP-H-60 carbon paper gas diffusion substrate (Alfa Aesar) and dried in air. For the anode GDEs, PtRu/C (Johnson Matthey UK, HiSpec 12100, 50% mass Pt and 25% mass Ru) catalyst was used as a catalyst (instead of the Pt/C). The geometric surface areas of all GDEs were 5.0 cm<sup>2</sup> and the Pt loadings were 0.40 ± 0.02 mg<sub>Pt</sub> cm<sup>−2</sup> (geometric). Identical cathode and anode GDEs were fabricated for use with each RG-AEM that was tested.

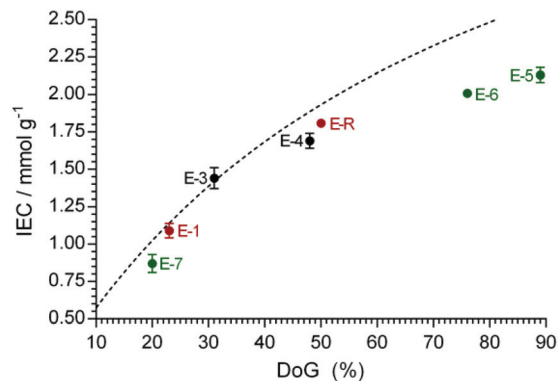
**AEMFC assembly and testing.** Two RG-AEMs were tested: E-R (the reference AEM made using the prior standard synthesis protocol) and E-6 (a down-selected RG-AEM with the best balance of mechanical properties and ionic conductivity that was synthesised using the new optimised synthesis protocol). All AEI-containing GDEs and the AEMs were immersed in aqueous KOH solution (1 mol dm<sup>−3</sup>) for 1 h followed by a thorough washing with water (to remove excess K<sup>+</sup> and OH<sup>−</sup> co- and counter-ions). The cathode and anode GDEs and AEM, for each membrane-electrode assembly (MEA), were assembled between two graphite plates to 5.5 N m torque with no prior hot-pressing of the MEA: after testing the GDEs were always adhered to the RG-AEM, which demonstrates the good contact achieved with this *in situ* “hot-press”. An 850C fuel cell test station (Scribner Associates, USA) was used for controlling the parameters during the testing. The fuel cell temperature was controlled at 60 °C, while H<sub>2</sub> and O<sub>2</sub> gas feeds were supplied to the anode and cathode, respectively, at a 1 dm<sup>3</sup> min<sup>−1</sup> flow rate with a dew point temperature of 60 °C (RH = 100%) and with no back-pressurisation. The MEAs were activated by controlling the cell voltage at 0.5 V during cell heating from room temperature to 60 °C (supplied with humidified gases) and then retaining this cell voltage until the current density had stabilised. Beginning-of-life AEMFC performance data, for relative comparison of the MEAs containing the test AEMs, were collected under simple potentiostatic discharge with 50 mV steps (a minimum of 1 min per data point, data taken when the current had stabilised). The internal ohmic resistances were estimated using the 850C internal current interrupt method.

## Results and discussion

### Effect of irradiation and grafting conditions on the IEC, WU and TPS of the resulting RG-AEM(Cl<sup>−</sup>)s

ETFE-*g*-poly(vinylbenzyltrimethylammonium chloride)-type RG-AEMs (ETFE-*g*-poly(VBTMA<sup>+</sup>Cl<sup>−</sup>)) have been developed and studied at the University of Surrey over the last decade.<sup>4,13,17,27</sup> The prior state-of-the-art synthesis protocol involved radiation-induced grafting of ETFE films at 70 °C using grafting mixtures consisting of 79 vol% propan-2-ol, 1 vol% surfactant (1-octyl-2-pyrrolidone) and 20 vol% VBC monomers.<sup>4</sup> However, the use of these conditions mandated the use of a high absorbed dose of electron-beam radiation (70 kGy), which led to RG-AEMs with sub-optimal mechanical strengths. Therefore, a key priority of this study was the development of a





**Fig. 1** The relationship between ion-exchange capacity (IEC) and degree of grafting (DoG) for the RG-AEM(Cl<sup>-</sup>)s synthesised using propan-2-ol (red), 1:1 propan-2-ol: water (black) and water (green) as diluents in the grafting step. The data for E-2 is omitted for clarity as the IEC is effectively zero. Error bars give the sample standard deviations for measurements on  $n = 3$  samples of each RG-AEM. The dashed line gives the calculated IECs as a function of DoG (see eqn (6)).

new synthesis protocol that required lower absorbed doses of <50 kGy. As can be seen in Table 1 and Fig. 1, lowering the absorbed dose to 40 kGy without changing the other parameters, led to a 40% drop in IEC (E-1 vs. E-R).<sup>‡</sup> In addition, VBC is an expensive and toxic monomer, making the reduction in its use during reaction a priority. When both the radiation dose and the VBC concentration were simultaneously reduced (40 kGy, 5 vol% VBC), while still using propan-2-ol diluent, the IEC of the resulting RG-AEM (E-2) reduced to effectively zero.

Therefore, a change of diluent system was investigated to see what effect this had on the grafting process. It has been reported that enhanced grafting is achieved with the use of a non-solvent diluent.<sup>28</sup> Moreover, addition of water to the propan-2-ol was found to enhance the kinetics of styrene grafting onto FEP.<sup>29</sup> Thus, three different diluent mixtures were investigated with 5 vol% VBC and ETFE electron-beamed to 40 kGy absorbed dose: propan-2-ol only (E-2), 1:1 (v/v) propan-2-ol:water (E-4), and water only (E-5). The addition of water in the grafting step enhanced the IECs to values that were higher than when propan-2-ol and 20 vol% VBC were used (E-4 IEC =  $1.69 \pm 0.05$  mmol g<sup>-1</sup> and E-5 IEC =  $2.13 \pm 0.05$  mmol g<sup>-1</sup> vs. E-1 IEC =  $1.09 \pm 0.05$  mmol g<sup>-1</sup>, see Table 1). The VBC:water volume ratios for E-4 and E-5 were 1:9 and 1:19, respectively. The increase in the water content affects the amount, size, and life time of the colloidal micelles in the grafting mixture: the use of water increases the size of the micelles (ESI Table S3<sup>†</sup>), which had been previously reported to enhance the DoG.<sup>30</sup> For scientific rigor, a higher VBC content was investigated with the mixed propan-2-ol and water system (E-3, VBC:water volume ratio = 1:2). This led to a drop in IEC to  $1.44 \pm 0.07$  mmol g<sup>-1</sup>.

As the IEC of E-5 (made using 40 kGy and water diluent) was so high, an attempt was made to lower the dose further.

The IEC of E-6 (30 kGy and water diluent) remained high ( $2.01 \pm 0.02$  mmol g<sup>-1</sup>) but a further reduction to 20 kGy (E-7) led to a large drop in IEC ( $0.87 \pm 0.06$  mmol g<sup>-1</sup>). Therefore, electron-beam doses of <30 kGy can't be used for this specific RG process.

The relationship between the DoG and the IEC is shown in Fig. 1. The theoretical IEC<sub>calc</sub> values were calculated as a function of DoG, assuming full amination of the poly(VBC) grafted chains and no side reactions (e.g. cross-linking) upon the exposure of ETFE to radiation and on grafting:

$$\text{IEC}_{\text{calc}} = \frac{n_{\text{N}(\text{CH}_2)_3^+\text{Cl}^-}}{m_{\text{AEM}}} = \frac{1}{\frac{M_{\text{VBC}}}{\text{DoG}} + M_{\text{VBC}} + M_{\text{N}(\text{CH}_2)_3^+\text{Cl}^-}} \quad (6)$$

where  $M$  = molar masses/g mol<sup>-1</sup> of the species indicated by the subscripts,  $m$  = mass/g and  $n$  = amount/mol. The experimental IEC values correlate well with the theoretically calculated IEC values with larger deviations between experimental and theoretical values at higher levels of grafting. Spectroscopic data (see below) show that there is an undetectable level of -CH<sub>2</sub>Cl residual groups remaining, which generally indicates complete amination. The deviations between the experimental and theoretical values at higher levels of grafting are an indication that additional side reactions are occurring, which are likely with radical-based processes. A plausible hypothesis is that a number of the terminal -CH<sub>2</sub>Cl groups on the VBC react with active sites, during the grafting stage, to form cross-links (such that those particular benzene-ring-containing cross-linked moieties are not available for the amination reaction). Similar deviations between experimental and theoretical IECs at higher degrees of grafting have also been observed for PTFE-based RG proton exchange membranes containing sulfonated styrene groups.<sup>31</sup>

From Fig. 2, it can be seen that the gravimetric WU and TPS values generally increase with IEC, with the RG-AEM(Cl<sup>-</sup>)s synthesised using only propan-2-ol as diluent leading to larger deviations from the general trend. These data are early indications that RG using VBC in organic-diluent-free media (water only) produced RG-AEMs with more enhanced and predictable properties (especially at lower absorbed doses).

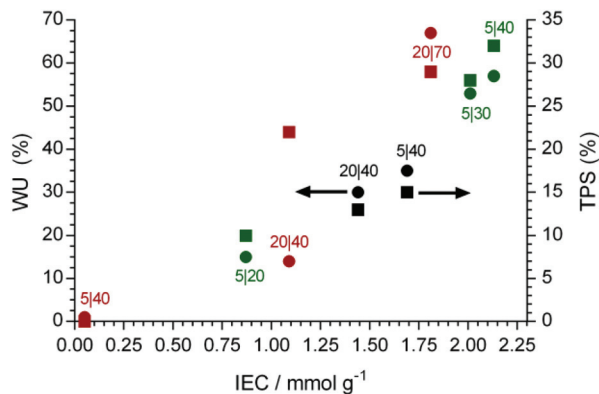
### Raman micro-spectroscopic and EDX data

Raman spectroscopy was used to compare the chemical composition of the virgin ETFE precursor film (before electron-beaming), an intermediate ETFE-g-poly(VBC) grafted membrane (that was ultimately used to produce E-5), and the final target RG-AEMs (Fig. 3). The spectrum of the ETFE showed CF<sub>2</sub> stretches at 833 cm<sup>-1</sup> and a CH<sub>2</sub> bend at 1442 cm<sup>-1</sup> as expected. The reaction of VBC with the irradiated ETFE film introduced new bands including an aromatic ring quadrant stretch at 1610 cm<sup>-1</sup>,<sup>32</sup> an aromatic meta stretch at 999 cm<sup>-1</sup>,<sup>32</sup> C-Cl stretches between 600–800 cm<sup>-1</sup>, and the highly characteristic CH<sub>2</sub> wag of the -CH<sub>2</sub>Cl at 1268 cm<sup>-1</sup>.<sup>32</sup>

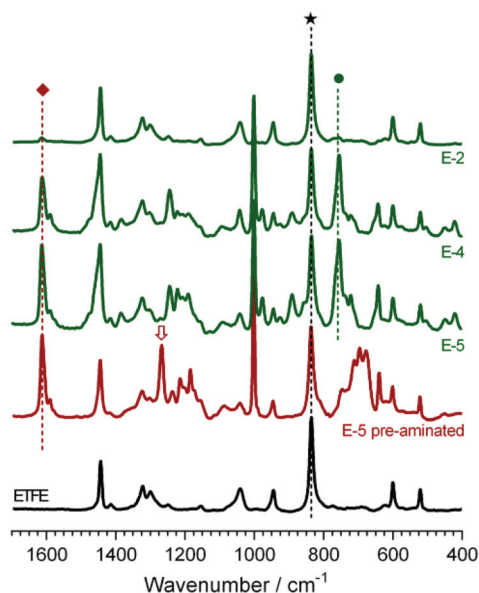
<sup>‡</sup>From the spectroscopic data in this study and prior studies, near complete amination is expected.

<sup>§</sup>This band is only present for the poly(3-VBC) graft segments and is not Raman active for the poly(4-VBC) containing graft segments.





**Fig. 2** A comparison between the gravimetric water uptake (WU, ●) and through plane swelling (TPS, ■) vs. IEC for the RG-AEM(Cl<sup>-</sup>)s synthesised using propan-2-ol only (red), 1:1 propan-2-ol and water only (green) diluents in the grafting step. The A|B numbers (e.g. 5|30) represent the VBC (vol%)/radiation dose (kGy), respectively. The means of  $n = 3$  repeats are shown and errors bars are omitted for clarity (the errors are presented in Table 1).



**Fig. 3** The Raman spectra (780 nm laser) of the precursor (pre-electron-beamed) ETFE film (black), the ETFE-*g*-poly(VBC) intermediate film used to produce E-5 (red) and the RG-AEMs E-2, E-4, and E-5 (green, with DoG = 2, 48, and 89%, respectively). The spectra were normalised to the intensity of the ETFE-derived peak at 835 cm<sup>-1</sup> (★) for ease of visual comparison. The band at 1610 cm<sup>-1</sup> (◆) relates to the benzene ring in the poly(VBC) grafts and the band at 753 cm<sup>-1</sup> (●) relates to the trimethylammonium group in the target RG-AAEMs. The band at 1268 cm<sup>-1</sup> (‡) relates to the -CH<sub>2</sub>Cl group in the ETFE-*g*-poly(VBC) intermediate (pre-aminated) membranes, which disappears on full amination. A complete set-of spectra for all RG-AEM(Cl<sup>-</sup>)s is presented in ESI Fig. S1.†

This latter band is highly diagnostic of the level of amination: in this study it disappears during the amination stage of the synthesis (quaternisation with trimethylamine), indicating

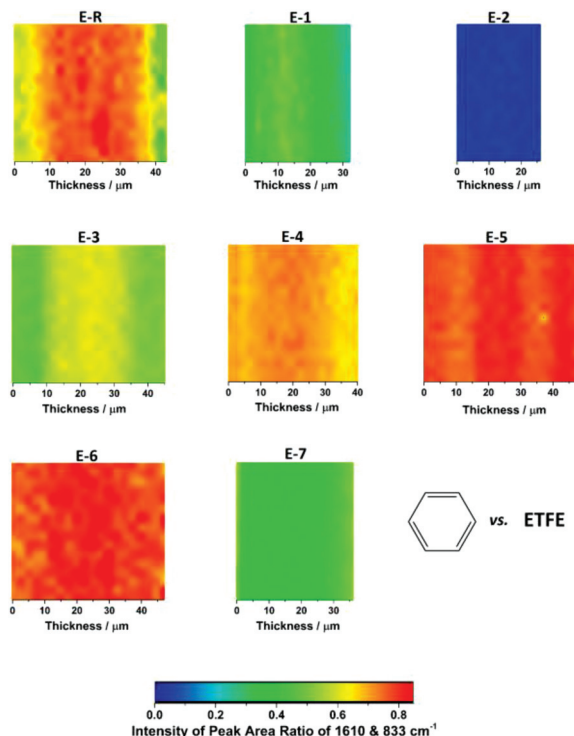
complete conversion of the -CH<sub>2</sub>Cl to the target benzyltrimethylammonium (BTMA) chloride groups. A new band at 753 cm<sup>-1</sup> was observed after quaternisation, which is indicative of the presence of -N<sup>+</sup>(CH<sub>3</sub>)<sub>3</sub> groups.<sup>4,32,33</sup> Three different RG-AEMs (E-2, E-4, and E-5) were chosen for further discussion for their low, medium and high DoGs and where the only difference between the synthesis of these RG-AEMs is the diluent used in the grafting stage. The differences in the DoG correlated with the relative intensity of the Raman bands at 1610 cm<sup>-1</sup> and 999 cm<sup>-1</sup> (that derive from the poly(VBC) grafts) vs. the intensity of the band at 833 cm<sup>-1</sup> (that derives from the ETFE precursor component).

The through-plane profile of poly(VBC) grafts was analysed using Raman spectroscopic mapping. The absolute values of the intensities of the spectroscopic bands can vary from spectra to spectra due non-uniformity of the evenness of the surface (relative to the incident angle and focal point of the laser beam) and changes in the fluorescence background (due to impurities or defects). Hence, the relative intensities of the bands vs. an internal benchmark (the ETFE-derived CF<sub>2</sub> band at 833 cm<sup>-1</sup>) were used to generate accurate maps. Fig. 4 shows the Raman maps for the synthesized RG-AEMs that mapped the relative area of the 1611 cm<sup>-1</sup> band (related to the grafted poly(VBC) component) vs. the area of the 833 cm<sup>-1</sup> band. The general intensities of the maps correlate well with the IECs and the thicknesses of the RG-AEMs: the higher the IEC, the higher the relative intensity of the 1610 cm<sup>-1</sup> band and the thicker the AEMs appear in the Raman maps. The reference RG-AEM E-R showed the least uniform grafting profile with lower levels of grafting at the surfaces of the membrane. This trend appears to be different from the grafting-front behaviour reported simultaneous grafting polymerisation, where the base polymers are submerged in the monomer solution and irradiated *in situ*.<sup>34</sup> The RG-AEMs synthesised using water as diluent and with absorbed doses of 30–40 kGy showed the highest levels of grafting.

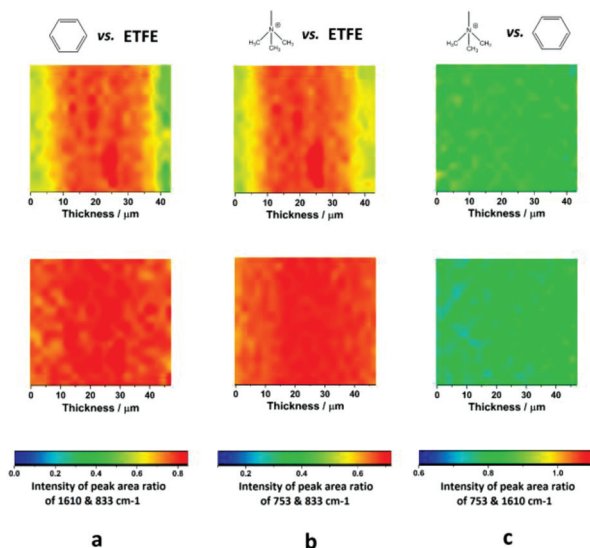
However, the distribution of benzyl groups may not represent the final distribution of trimethylammonium groups in the RG-AEMs. Hence, Fig. 5 shows Raman area ratio maps for E-6 and E-R: 1610 cm<sup>-1</sup>/833 cm<sup>-1</sup> (benzene vs. ETFE), 753 cm<sup>-1</sup>/833 cm<sup>-1</sup> (trimethylammonium vs. ETFE), and 753 cm<sup>-1</sup>/1610 cm<sup>-1</sup> (trimethylammonium vs. benzene). These data clearly show that the distributions of grafts (and hence the polymer-bound ammonium cations) are more uniform with the new optimised synthesis protocol, even with radiation absorbed doses as low as 30 kGy. These data also show that amination is uniform.

Raman line maps across a sample cross-section of each ETFE-*g*-poly(VBC) intermediate (pre-aminated) membrane (Fig. 6 (top)) correlated to the cross-sectional area maps recorded on the final RG-AEM(Cl<sup>-</sup>)s (as expected). These line maps were recorded so that the Raman data could be validated with an EDX line map (Fig. 6 (bottom)): as the F distribution represents the ETFE backbone and the Cl distribution represents the grafts (-CH<sub>2</sub>Cl groups),<sup>35</sup> the grafting level is represented by the Cl/F ratio. A comparison of Fig. 6 (top) and

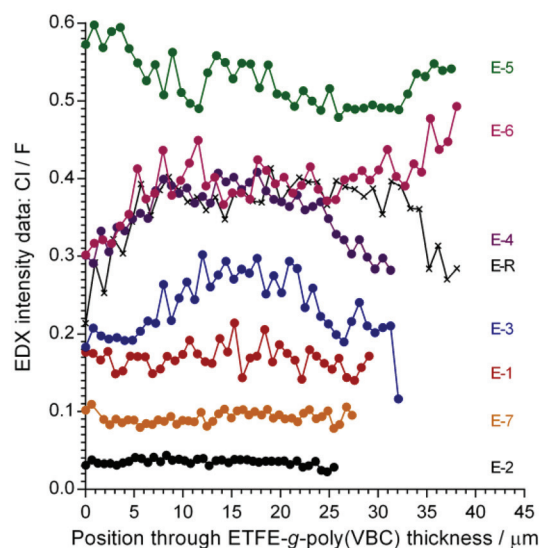
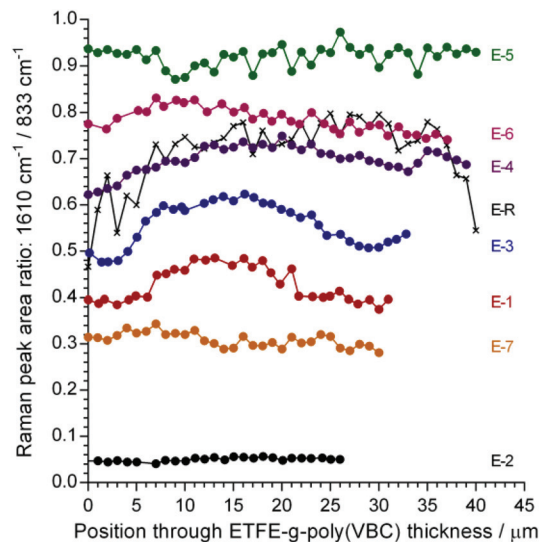




**Fig. 4** Raman micro-spectroscopic analysis of randomly selected cross-sections of each RG-AEM synthesised. The through-plane direction is from left to right in the maps. The maps show the relative area of the aromatic benzene band at  $1610\text{ cm}^{-1}$  (related to the poly(VBC) grafts) normalised to the area of the C–F band at  $833\text{ cm}^{-1}$  (related to the ETFE film). Each spectrum was recorded over 1–2  $\mu\text{m}$  laser spot sizes.



**Fig. 5** Raman micro-spectroscopic analysis of randomly selected cross-sections of E-R (top row) and E-6 (reference, bottom row). The through-plane direction is from left to right in the maps. (a) The relative area of the aromatic band at  $1610\text{ cm}^{-1}$  normalised to the ETFE band at  $833\text{ cm}^{-1}$ . (b) The relative area of the ammonium band at  $753\text{ cm}^{-1}$  normalised to the  $833\text{ cm}^{-1}$  band. (c) The relative area of the  $753\text{ cm}^{-1}$  band normalised to the  $1610\text{ cm}^{-1}$  band. Each spectrum was recorded over 1–2  $\mu\text{m}$  laser spot sizes.



**Fig. 6** A comparison of line maps of a select cross-section of each intermediate, pre-aminated, membrane (used to produce the final RG-AEM(Cl<sup>-</sup>) indicated), generated from: Raman (top) and EDX data (bottom).

(bottom) clearly shows that the graft distributions recorded by both techniques closely match.

### Cl<sup>-</sup> anion conductivities

One of the most important properties of any AEM is ion conductivity. It is important to note that the conductivities in this work were for the AAEMs in the as-synthesised Cl<sup>-</sup> form. This is the form of the RG-AEMs that is directly synthesised; this is before any exposure to extreme pH environments that may lead to changes in, or degradation of, the membranes (E-5 was found to lose 16% of its IEC when treated in an accelerated degradation study involving immersion in aqueous potassium hydroxide (1 mol dm<sup>-3</sup>) at 80 °C for 28 d, which is in line with observations from our recent head-group chemistry study).<sup>36</sup>



These  $\text{Cl}^-$  anion conductivities translate into  $\text{OH}^-$  conductivities of over  $130 \text{ mS cm}^{-1}$  at  $80^\circ\text{C}$  (ref. 36), a value that is competitive to other state-of-art high conductive AEMs, such as for the polymers based on poly(2,6-dimethyl-1,4-phenylene oxide) backbones that have reported  $\text{OH}^-$  conductivities in the range  $89\text{--}200 \text{ mS cm}^{-1}$  at  $80^\circ\text{C}$ .<sup>37–39</sup>

The in-plane ion conductivities of the fully hydrated RG-AEM( $\text{Cl}^-$ ) were measured at various temperatures by the four-probe impedance technique (Fig. 7). E-5, with the highest IEC (2.13  $\text{mmol g}^{-1}$ ), showed the highest  $\text{Cl}^-$  conductivity in water at  $80^\circ\text{C}$  ( $68 \pm 3 \text{ mS cm}^{-1}$ ), while reducing the radiation absorbed dose from 40 kGy to 30 kGy only led to a marginal drop in  $\text{Cl}^-$  conductivity under the same conditions (E-6,  $60 \pm 2 \text{ mS cm}^{-1}$ ). Both of the RG-AEM( $\text{Cl}^-$ )s, synthesised using water diluent, gave higher  $\text{Cl}^-$  conductivities than the reference (E-R,  $48 \pm 2 \text{ mS cm}^{-1}$ ) that was synthesised using propan-2-ol diluent and a high absorbed dose (70 kGy). From Fig. 7

**Table 2** The activation energies ( $E_a$ ) for the  $\text{Cl}^-$  conduction in the RG-AEM( $\text{Cl}^-$ )s

RG-AEM( $\text{Cl}^-$ )	$E_a^a/\text{kJ mol}^{-1}$
E-R (reference)	18
E-1	16
E-2	— <sup>b</sup>
E-3	17
E-4	18
E-5	17
E-6	17
E-7	20

<sup>a</sup> Calculated from the data in Fig. 7 (top) and eqn (7). <sup>b</sup> Non-Arrhenius.

(bottom), it is clear that the  $\text{Cl}^-$  conductivities generally increase with IEC.

The  $\text{Cl}^-$  conduction activation energies ( $E_a/\text{J mol}^{-1}$ ) were calculated using:

$$E_a = -b \times R \quad (7)$$

where  $R$  is the gas constant ( $8.314 \text{ J K}^{-1} \text{ mol}^{-1}$ ) and  $b$  is the slope of the  $\ln(\sigma/\text{S cm}^{-1})$  vs.  $(T/\text{K})^{-1}$  plots derived from the data presented in Fig. 7 (top). The  $E_a$  values are summarised in Table 2. The activation energies for the RG-AEM( $\text{Cl}^-$ )s with IECs  $>1.0 \text{ mmol g}^{-1}$  are similar, within the range  $16\text{--}18 \text{ kJ mol}^{-1}$ , which indicates that the  $\text{Cl}^-$  anions are conducting *via* the same mechanism.

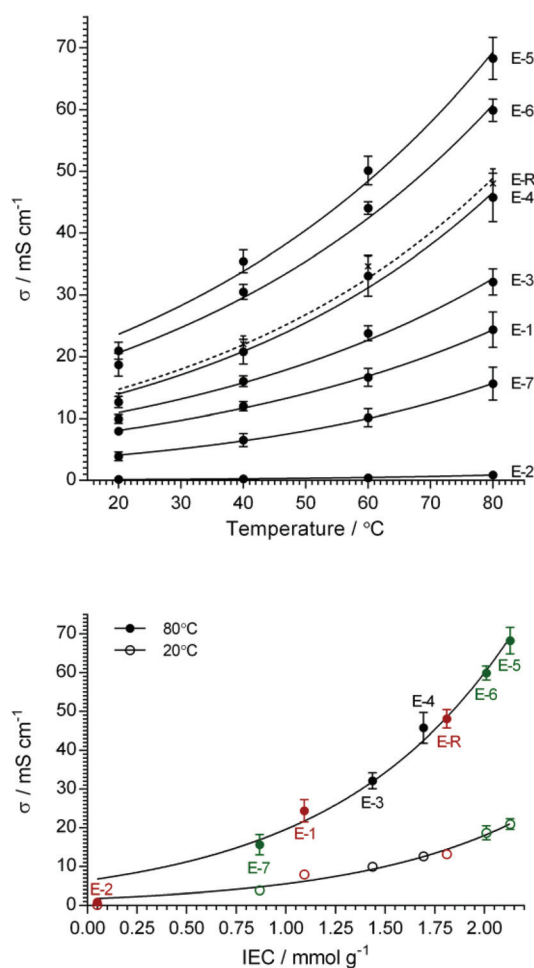
### Tensile strength testing

The tensile mechanical data for Nowoflon ETFE before and after exposure to electron-beam radiation are presented in Fig. 8 and Table 3. It is clear that exposure to increasing absorbed doses of radiation leads to both a decrease in the Young's modulus (from the initial slope of the curves below 3% strain) and the ultimate tensile strength of the ETFE. This is likely due to the increased levels of C–C bond breakage in the ETFE backbone.

After grafting and amination, the tensile properties of the RG-AEM( $\text{Cl}^-$ )s dramatically decreased (Fig. 9), especially for the reference E-R. However, it was evident that a reduction in the electron-beam absorbed dose produced stiffer and stronger RG-AEM( $\text{Cl}^-$ )s (Table 3): E-6 (30 kGy) yielded the best mechanical properties of the RG-AEM( $\text{Cl}^-$ )s tested. Furthermore, dynamic mechanical analysis (DMA) was used to compare the storage and loss modulus of E-R and E-6 over a larger temperature range up to  $175^\circ\text{C}$  (ESI Fig. S4†). The modulus of E-6 is higher than E-R for the entire temperature range.

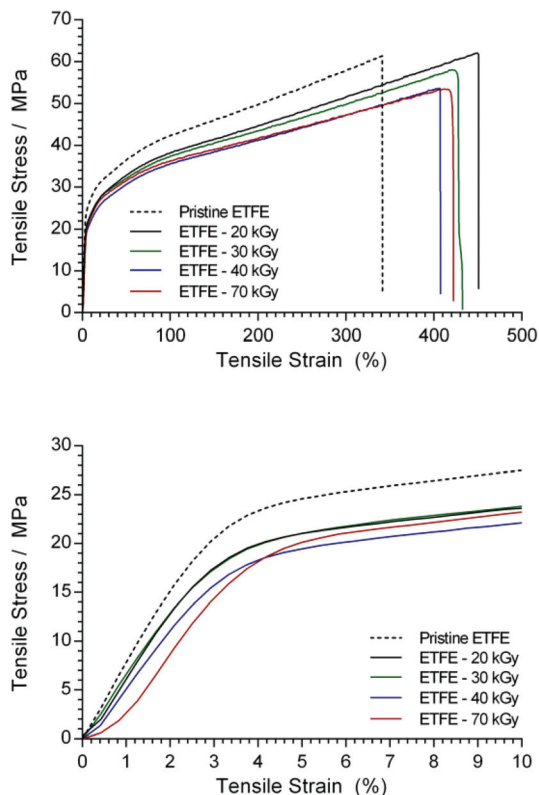
### $\text{H}_2/\text{O}_2$ Anion-Exchange Membrane Fuel Cell (AEMFC) benchmark testing of E-6 and E-R at $60^\circ\text{C}$

On a balance between the homogeneity of grafting, ionic conductivities, and mechanical properties of the RG-AEM( $\text{Cl}^-$ )s, E-6 was down-selected for a beginning-of-life AEMFC test with a relative comparison with the reference E-R (Fig. 10). The test conditions were highly optimised to produce the best performances (fast, fully humidified gas flows and the use of Pt-based

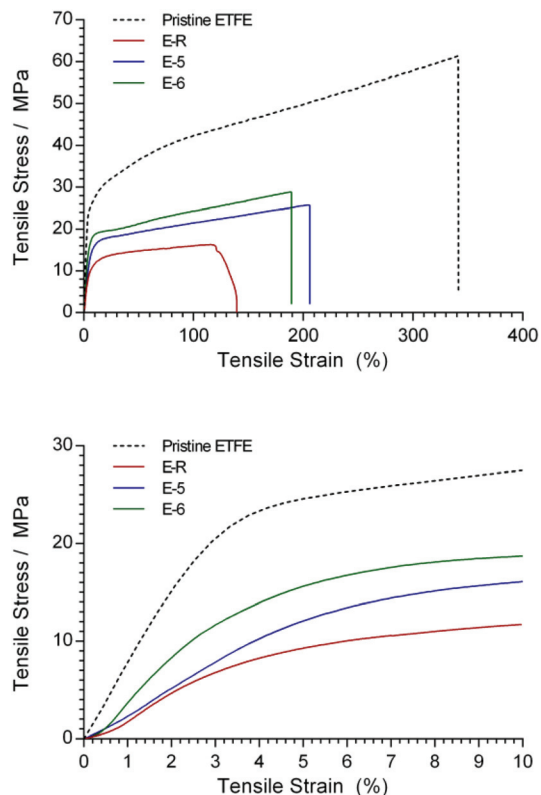


**Fig. 7** The  $\text{Cl}^-$  anion conductivities of the RG-AEM( $\text{Cl}^-$ ) as a function of temperature (top plot) and IEC (bottom plot). Error bars are sample standard deviations of measurements on  $n = 3$  samples of each RG-AEM ( $\text{Cl}^-$ ). The lines are arbitrary exponential growth fits as a visual guide only. The activation energies ( $E_a/\text{kJ mol}^{-1}$ ) calculated from Arrhenius  $\log \sigma/T^{-1}$  data, that is derived from the top plot, are presented in Table 2.





**Fig. 8** Tensile measurements of the 25  $\mu\text{m}$  ETFE before and after exposure to various absorbed radiation doses (4.5 MeV energy electron-beam).



**Fig. 9** Tensile measurements of the 25  $\mu\text{m}$  pristine ETFE and the RG-AEM(Cl<sup>-</sup>)s E-R, E-5, and E-6 (the latter two made using water diluent and 5 vol% VBC).

**Table 3** Estimated tensile mechanical properties of pristine ETFE, ETFE exposed to different doses of electron-beam radiation, and the RG-AEM(Cl<sup>-</sup>)s E-R, E-5, and E-6. Means and sample standard deviations from replicate measurements on  $n = 3$  samples of each membrane

	Young's modulus/MPa	Stress at break/MPa	Elongation at break (%)
ETFE – pristine	729 ± 26	62 ± 7	350 ± 29
ETFE – 20 kGy	620 ± 101	59 ± 3	461 ± 35
ETFE – 30 kGy	618 ± 92	57 ± 3	415 ± 72
ETFE – 40 kGy	530 ± 59	53 ± 3	407 ± 42
ETFE – 70 kGy	495 ± 72	52 ± 6	374 ± 49
E-R	110 ± 38	18 ± 4	148 ± 39
E-5	262 ± 9	27 ± 2	219 ± 46
E-6	416 ± 17	30 ± 8	189 ± 17

catalysts) but these allow meaningful relative performance evaluation of the RG-AEM(OH<sup>-</sup>)s under practically identical test conditions. PtRu/C and Pt/C were chosen as anode and cathode catalysts, respectively, as they were proven to have high performance in AEMFC:<sup>40</sup> this meant that electrocatalytic performance losses were minimised. The AEMFC test temperature was limited to 60 °C to minimise any *in situ* degradation of the RG-AEM and ionomer components.

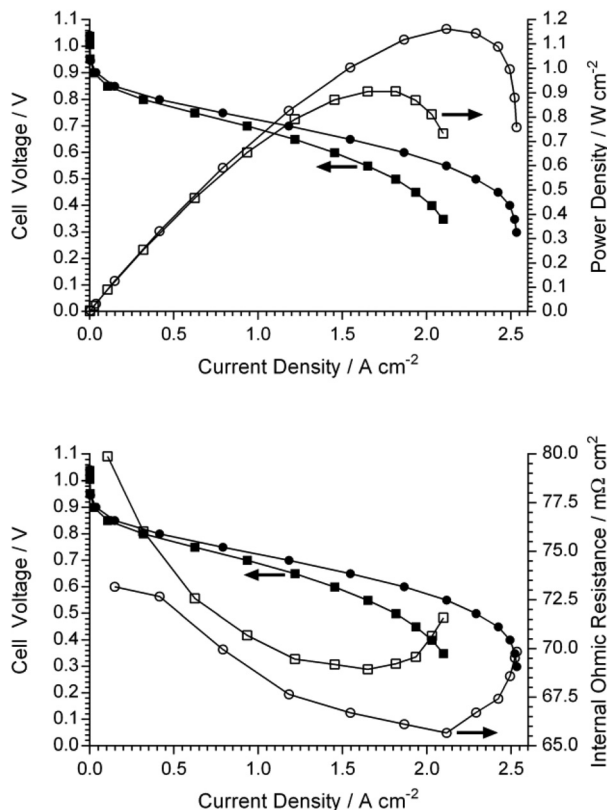
The peak power density of the AEMFC containing the reference E-R (geometric power density of 0.91 W cm<sup>-2</sup>) is compar-

able to the highest performing examples in the AEMFC literature (operated under similar conditions),<sup>40–43</sup> including the record performances reported by Zhuang *et al.*<sup>40</sup> It is clear that the AEMFC performance of E-6 (1.16 W cm<sup>-2</sup>) is higher relative to E-R with limiting current densities of 2.5 and 2.1 A cm<sup>-2</sup>, respectively. The improved performance of E-6 cannot be wholly explained by differences in the internal ohmic resistance: 67 mΩ cm<sup>2</sup> vs. 69 mΩ cm<sup>2</sup> for E-R at *ca.* 1.5 A cm<sup>-2</sup> would only lead to a 3 mV ohmic loss at this current density for E-R (and the difference in cell potential at this current density is larger than this). It is clear that mass transport losses initiate at lower current densities for E-R. This may arise from lower levels of back-diffusion of water from the anode (where it is generated) to cathode (where it is consumed), for this reference RG-AEM(OH<sup>-</sup>), leading to larger levels of flooding at the anode. Recall that the reference E-R had poorer grafting homogeneity. In summary, the higher performance of the AEMFC containing E-6 is attributed to the higher conductivity and more homogenous grafting of this RG-AAEM(OH<sup>-</sup>).

#### Comparison with the optimal conditions for the synthesis of RG-AEMs using thicker 50 $\mu\text{m}$ ETFE base films

As a small side study, the effect of water and propanol content in the grafting step was also investigated for thicker 50  $\mu\text{m}$  thick ETFE base films. ESI Table S2† summarises the synthesis

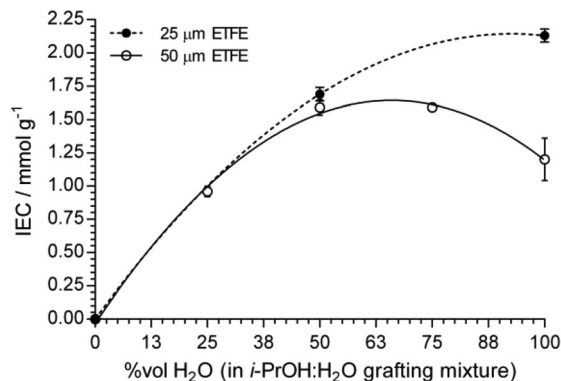




**Fig. 10** Initial, beginning-of-life  $\text{H}_2/\text{O}_2$  AEMFC test data at 60 °C for E-R (squares) and E-6 (circles) using PtRu/C anodes and Pt/C cathodes and with no gas back-pressurisation of the fully humidified gases.

variables and selected resulting properties of all six thicker RG-AEMs investigated. In contrast to the thinner RG-AEMs (made from 25  $\mu\text{m}$  thick ETFE), a mixed diluent (propan-2-ol :  $\text{H}_2\text{O}$  = 1 : 3 or 1 : 1) yielded the most optimal level of grafting: the RG-AEMs synthesised from the thicker ETFE clearly require the presence of propan-2-ol in the grafting mixture. This may relate to the speed of penetration of the VBC monomer into the full thickness of the 50  $\mu\text{m}$  thick ETFE during the grafting step and the facilitation of this by the presence of propan-2-ol. The above trend is clearly seen in Fig. 11, which compares the IECs of the thicker AEMs with the thinner AEMs as a function of water content in the grafting mixture.

Fig. S2† shows the Raman area maps (ratio of the areas of the 1610  $\text{cm}^{-1}$  to 833  $\text{cm}^{-1}$  bands) of the ETFE-*g*-poly(VBC) intermediate membranes used to synthesise the RG-AEM( $\text{Cl}^-$ )s from the thicker 50  $\mu\text{m}$  ETFE films. The intermediate (pre-aminated) membrane that was used to form the RG-AEM **E**<sub>50-R</sub> shows a higher level of grafting in the centre; this was also seen with the thinner E-R RG-AEM. EDX and Raman line maps confirm this effect (Fig. S3†). The most homogeneous grafting was seen for the intermediate to **E**<sub>50-3</sub>, which was synthesised using propan-2-ol :  $\text{H}_2\text{O}$  = 1 : 1. This led to the **E**<sub>50-3</sub> RG-AEM ( $\text{Cl}^-$ ) having the highest conductivity ( $48 \pm 2 \text{ mS cm}^{-1}$  at 80 °C in water) for the thicker RG-AEM( $\text{Cl}^-$ )s synthesised using a 40 kGy electron-beam absorbed dose.



**Fig. 11** The relationship between IEC and the water content (vol%) in the propan-2-ol :  $\text{H}_2\text{O}$  diluent mixture for the RG-AEM( $\text{Cl}^-$ )s made using 50  $\mu\text{m}$  ETFE (open) and 25  $\mu\text{m}$  ETFE (solid). The RG-AEMs were made using 40 kGy electron-beam absorbed dose and grafted at 70 °C with 5 vol% VBC and 1 vol% surfactant (see Table S2†). The lines are arbitrary 2<sup>nd</sup> order polynomial fits as a visual guide only. Error bars are sample standard deviation for data collected on  $n = 3$  samples of each RG-AEM( $\text{Cl}^-$ ).

### Recycling of water and solution

In order to assess the recyclability of the aqueous grafting mixture, it was used to graft two AEMs sequentially (**E-6A** then **E-6A\***) using the method used to synthesise **E-6** (Table 4). The second AEM, produced using the recycled grafting mixture, exhibited a much lower DoG and IEC. However, in a separate experiment, after grafting a further AEM (**E-6B**) using the **E-6** synthesis method, the residual grafting mixture was allowed to separate at 4 °C for 24 h to form distinct, clear aqueous and organic layers (see ESI Fig. S5†): the decanted aqueous layer was reconstituted by adding fresh VBC (5 vol%) and 1-octyl-2-pyrrolidinone (1 vol%). Use of this ‘recycled water’ reconstituted grafting mixture in a second graft reaction produced an AEM (**E-6B\***) whose measured properties were close to the original AEM produced using the fresh grafting mixture (**E-6B**). Gas chromatography mass spectrometry (GCMS) analysis of the aqueous layer prior to the second grafting showed the residual organic impurities to be predominantly vinyl benzyl alcohol (VBA) and 1-octyl-2-pyrrolidinone with only trace amounts of VBC (see ESI Fig. S6†). The presence of the impurity VBA did not appear to significantly affect the properties of the AEM synthesised using the ‘recycled’, reconstituted aqueous later (**E-6B** vs. **E-6B\***) from the data collected in this initial study: however, a full study of the presence and effect of VBA impurities on the grafting reaction will now be conducted to specifically investigate this. The organic layer, which was dissolved in acetonitrile to perform GCMS, contained VBC, VBA and 1-octyl-2-pyrrolidinone (see ESI Fig. S6†).

Since GCMS is unlikely to detect polymers, the residual organic layer (from the synthesis of **E-6A**, see ESI Fig. S5†) was also characterised using Raman spectroscopy (ESI Fig. S7†). To assist in the identification of the components in the organic residual layer, the Raman spectra of VBC, poly(VBC), and



**Table 4** Summary results of the recycling of grafting mixture components. All electron-beam irradiations were carried out on 25  $\mu\text{m}$  ETFE using 30 kGy absorbed doses in air. The synthesis of **E-6A** and **E-6B** was conducted with freshly prepared reagents using the same protocol as for the synthesis of **E-6** in Table 1. The synthesis of **E-6A\*** directly reused the grafting mixture recovered from the synthesis of **E-6A**. The synthesis of **E-6B\*** reused the recovered aqueous layer from the synthesis of **E-6B** with the fresh addition of the VBC monomer (5 vol%) and 1-octyl-2-pyrrolidone (1 vol%). All means  $\pm$  sample standard deviations are from  $n = 3$  repeats

RG-AEM(Cl <sup>-</sup> )	E-6A	E6-A*	E-6B	E-6B*
DoG (%)	69	57	76	79
IEC/mmol g <sup>-1</sup>	1.99 $\pm$ 0.01	1.25 $\pm$ 0.02	2.05 $\pm$ 0.01	2.05 $\pm$ 0.07
WU (%)	54 $\pm$ 4	26 $\pm$ 4	60 $\pm$ 5	55 $\pm$ 7
TPS (%)	40 $\pm$ 2	12 $\pm$ 1	42 $\pm$ 2	48 $\pm$ 3

1-octyl-2-pyrrolidone were also recorded. The Raman spectrum of the organic residual contained peaks that are related to VBC, with the additional presence of peaks related to smaller quantities of 1-octyl-2-pyrrolidone and possibly poly(vinylbenzyl chloride). An additional peak at 1032 cm<sup>-1</sup> is the C–O stretch of –CH<sub>2</sub>OH,<sup>32</sup> which indicates the presence of a quantity of vinylbenzyl alcohol (VBA): hence, the residual grafting mixture predominantly contains both VBC and VBA. The insufficient concentration of VBC and the impure nature of the residual grafting mixture are the reasons for the lower IEC of AEM synthesised from the complete residual mixture (**E-6A\***).

## Conclusions

This study reports the synthesis of a poly(ethylene-co-tetrafluoroethylene) (ETFE)-based radiation-grafted anion-exchange membrane (RG-AEM). This new RG-AEM was synthesised using an organic-solvent-free method and with reduced amounts of both monomer (vinylbenzyl chloride, VBC) concentration and electron-beam radiation absorbed dose compared to a reference RG-AEM synthesised using the prior state-of-the-art protocol. The new RG-AEM (synthesised using 25  $\mu\text{m}$  thick ETFE, 30 kGy dose and only 5 vol% VBC in water) exhibited superior *ex situ* properties such as ion-exchange capacity, grafting homogeneity, ionic conductivity, and mechanical strength compared with the previous reference RG-AEM (synthesised using 25  $\mu\text{m}$  thick ETFE, 70 kGy dose and 20 vol% VBC in propan-2-ol). The new RG-AEM also outperformed the reference RG-AEM in a simple, beginning-of-life H<sub>2</sub>/O<sub>2</sub> Anion-Exchange Membrane Fuel Cell (AEMFC) test at 60 °C. In addition, using potentially recyclable water as a diluent and using lower radiation doses moves the method closer to a commercially-relevant roll-to-roll process.

In contrast, a mixed water and propan-2-ol diluent was required for optimum RG of VBC onto thicker 50  $\mu\text{m}$  ETFE films: the use of only water as diluent led to lower levels of grafting. It should also be noted that the use of ETFE membranes from other suppliers may not have the same effect as

different suppliers incorporate different additives and copolymer components: *e.g.* most commercial ETFE polymers contain between 0.1–10 mol% perfluoro(alkylvinyl ether) monomer.<sup>30</sup> However, to reduce the number of experimental variables, other ETFE grades from different suppliers were not studied: we have always used the Nowofol ETFE as, prior studies (in our laboratories) have shown that this type of ETFE undergoes excellent radiation-grafting.

## Statement of author contribution

The paper is primarily the work of Lianqin Wang. Emanuele Magliocca conducted the optimisation of the surfactant concentration and grafting temperature. Emma Cunningham conducted the work on the optimisation of the grafting protocols for the thicker ETFE films. Julia Ponce-Gonzalez and Rachida Bance-Soualhi assisted with the membrane work and the optimised operation of the research instruments used in the study. Mohamed Nasef assisted with the interpretation of resulting data, especially regarding discussion on the emulsion polymerisation mechanism. Simon Poynton and Ricardo Escudero-Cid formulated and synthesised the powder ionomer, while William Mustain's efforts were instrumental in the development of the catalyst/ionomer-ink formulation and electrode-preparation protocols. John Varcoe, Robert Slade and Daniel Whelligan are the grant holders of the EPSRC projects that funded this work and assisted in all aspects of research direction and data analysis: John Varcoe was the principal investigator for the research and made a large contribution to the drafting of this paper.

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All of the raw data in this open access (CC-BY) article is freely available (in compliance with EPSRC rules): the meta-



data and details on how to access this raw data can be found at DOI: 10.15126/surreydata.00811704.

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