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# Automated solid-phase extraction of organic pollutants using melamine–formaldehyde polymer-derived carbon foams

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The adsorptive potential of melamine–formaldehyde (MF) polymer derived elastic carbon foams (CF) has been explored for the first time for the extraction of low levels of environmental pollutants from water samples. The prepared CFs are obtained from the direct carbonization under nitrogen atmosphere of MF. CFs are used as flow-through supports and are implemented for automated solid-phase extraction using the sequential injection analysis technique. In comparison to other carbon-based materials, the use of monolithic networks based on CFs showed low-pressure and good mass transfer of the analytes, enabling the efficient extraction of bisphenol A, 4-*tert*-octylphenol and 4-*n*-nonylphenol from water samples prior to their quantification using liquid chromatography. Different experimental parameters such as selection of the eluent, sample and eluent volumes, and pre-concentration and elution flow rates, were evaluated. Under the selected conditions, the detection limits were between 0.02 and 0.08  $\mu\text{g L}^{-1}$  and the relative standard deviations (RSD, 10  $\mu\text{g L}^{-1}$ ) ranged from 4.1–4.8%. Batch-to-batch reproducibility for three different carbon sponges was 5.8–6.3%. The obtained preconcentration factors were between 24 and 38, using a volume of 4 mL of sample. The CFs are chemically robust and flexible, and reusable at least 50 times. Different water samples such as well water, wastewater and leachates from a solid waste treatment plant were analyzed to investigate the capability of CFs for real sample analysis.

of SPE procedures is achieved using the different generations of flow analysis techniques,<sup>3–5</sup> including both micro-column,<sup>6,7</sup> or disk based packing.<sup>8,9</sup> Among the different materials used for SPE, novel carbon forms have been constantly studied as sorbents for this application, including carbon nanotubes,<sup>10,11</sup> or graphene.<sup>12,13</sup> However, the inherent morphology of these materials is far from the desired for flow-through SPE applications, requiring more complex extraction devices for their automation,<sup>14,15</sup> or alternatively, incorporating the carbon particles into functional devices such as microextraction fibers,<sup>16,17</sup> silica,<sup>18</sup> or magnetic  $\text{Fe}_3\text{O}_4$  particles.<sup>19</sup>

A novel type of carbon-based supports recently reported in the scientific literature are the monolithic 3D networks composed by elastic carbon foams (CF),<sup>20–24</sup> obtained from the direct carbonization in an inert atmosphere of melamine–formaldehyde–sodium bisulfite polymer foams (MF).<sup>25,26</sup> MFs have been used for the last 20 years as pipe insulator and soundproofing material, and more recently as an abrasive cleaner. CFs are based on three-dimensional interconnected porous network architectures, have a high surface area ( $>200 \text{ m}^2 \text{ g}^{-1}$ ) and showed promising applications as oil adsorbents,<sup>20,21</sup> or as flexible electrodes for batteries.<sup>22–24</sup>

Many applications of foams as sorbents for SPE applications have been based on the use of polyurethane foam, which has been extensively studied for the preconcentration of trace metals.<sup>27</sup> In this case, a chelating ligand is previously immobilized into the foam prior to metal extraction,<sup>28</sup> or alternatively, the metal complex is formed prior to the preconcentration step.<sup>29</sup> However, to the authors knowledge, and despite of the promising features for adsorption of CFs derived from MF, no examples of their use as sorbents for SPE have been reported so far. CFs have a huge potential as sorbent for SPE applications since they are moldable, have a low density and a high flexibility causing very low backpressures, enabling the use of higher flow rates without compromising the performance of the extraction.

Herein, we propose for the first time the use of MF-derived CFs as sorbents for the automated SPE of environmental pollutants. The obtained CFs are molded with the desired size

## 1. Introduction

Solid-phase extraction (SPE) is a widely used sample preparation technique for analyte clean-up and preconcentration.<sup>1</sup> The incorporation of the sorbent in flow-through supports such as cartridges or membrane disks facilitates the implementation of the overall SPE procedure.<sup>2</sup> A high versatility on the automation

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and shape, in order to be incorporated in a miniaturized flow-through holder used as SPE device, and implemented into a sequential injection analysis (SIA) system.<sup>4</sup> The versatile use of the SIA technique in combination with the proposed sorbent has been evaluated for the simultaneous SPE of trace levels of three endocrine disrupting phenols (bisphenol A, 4-*tert*-octylphenol and 4-*n*-nonylphenol), prior to their quantification using liquid chromatography. The applicability of the CFs for real sample analysis has been studied by analyzing the selected endocrine disrupting phenols in different types of water samples.

## 2. Materials and methods

### 2.1. Chemicals and standard solutions

Methanol (HPLC grade,  $\geq 99.8\%$ ), ethanol ( $\geq 99.8\%$ ) and acetonitrile (99.9%), were obtained from Scharlau (Barcelona, Spain). 4-*n*-Nonylphenol ( $\geq 99.8\%$ ), 4-*tert*-octylphenol ( $\geq 97\%$ ) and bisphenol A ( $\geq 97\%$ ), were obtained from Sigma-Aldrich (St. Louis, USA). Melamine foam was purchased from a local store. A stock standard solution of each of the selected analytes ( $2000 \text{ mg L}^{-1}$ ) were prepared in methanol. An intermediate standard solution of a concentration of  $20 \text{ mg L}^{-1}$  was prepared by diluting the stock standard solutions in methanol. A stock working solution at the concentration of  $1 \text{ mg L}^{-1}$  was prepared from the intermediate stock standard solution daily in water. More diluted working solutions were prepared by diluting the intermediate working solution with water. In all instances, Milli-Q water from a Direct-8 purification system (resistivity  $> 18 \text{ M}\Omega \text{ cm}$ , Millipore Iberica, Spain) was used.

### 2.2. Preparation of elastic carbon foam for SPE

CF monolithic networks, were prepared from pieces of melamine-formaldehyde polymer foam (MF) ( $1 \text{ cm} \times 1 \text{ cm} \times 50 \text{ mm}$ ). MF was first washed with ethanol and dried in an oven at  $60 \text{ }^\circ\text{C}$ . The cleaned and dried MF was heated in an electric furnace to a final temperature of  $800 \text{ }^\circ\text{C}$  with a heating rate of  $5 \text{ }^\circ\text{C min}^{-1}$  under a nitrogen atmosphere. The foam was annealed at this temperature for 3 h, in order to complete the carbonization process. The as prepared CFs were cooled down to room temperature and washed thoroughly with pure water, prior to their use as sorbents for SPE.

### 2.3. Instrumentation

The SIA system is composed by a computer controlled bi-directional syringe pump (5000-step automatic burette (model Bu4) from Crison, Alella, Barcelona, Spain, <http://www.crison.es>). The syringe pump is equipped with a 5 mL glass syringe from Hamilton (Bonaduz, Switzerland, <http://www.hamiltoncompany.com>), and a three-way solenoid head valve (SV, N-Research, West Caldwell, NJ, <http://www.nresearch.com>). The normally open port (OFF) of the solenoid valve of the syringe is connected to the carrier reservoir (water). The normally closed position (ON) is connected through a holding coil to the central port of an eight port multiposition valve (MPV, Sciware Systems SL, Spain,

<http://www.sciware-sl.com>) used for the sequential selection of the sample the eluent, and to connect to the extraction device. All tubing is polytetrafluoroethylene 0.8 mm i.d., except the holding coil (1.6 mm i.d., 5 mL). The extraction device is a two-piece polymethyl methacrylate cylinder with a 1 mm i.d. channel and an internal cavity to hold the carbon foam, as used previously.<sup>8,9</sup> The extraction device is connected to an additional solenoid valve (V5, MTV-3-N1/4UKG, 2 bar maximum pressure, Takasago, Japan) enabling the collection of the eluate into a vial. The additional solenoid valve is controlled by the syringe pump module through an additional port. The syringe pump and the selection valve modules are controlled using the software package AutoAnalysis 5.0 (Sciware Systems SL).

A Jasco HPLC instrument equipped with a high-pressure pump (PU-4180), a manual injector ( $20 \mu\text{L}$ ), and a UV-vis diode array detector (MD-4017) was used for the separation and quantification of the selected analytes. Separation was performed at room temperature on a Phenomenex® Kinetex EVO C18 100A core-shell column ( $150 \text{ mm} \times 4.6 \text{ mm i.d. } 5 \mu\text{m}$ ) with a guard column ( $5 \text{ mm} \times 4.6 \text{ mm i.d.}$ ). The mobile phase was a mixture of methanol (solvent A) and pure water (solvent B) (75 : 25, v/v). The mobile phase was used at a flow rate of  $1.0 \text{ mL min}^{-1}$ . The detection was performed at 229 nm for all analytes.

The morphology of the sorbent was analyzed using a scanning electron microscope (SEM) Hitachi S-3400N.

### 2.4. Samples

In order to investigate the capability of the method for real sample analysis, different types of water samples including well water, leachates from rainwater and wastewater samples were collected from Palma de Mallorca, Spain. The samples were filtered using a nylon membrane filter ( $0.45 \mu\text{m}$ , Millipore, Bedford, MA, USA) before use. Wastewater was collected from an urban wastewater treatment plant. Well water was collected from a well water reservoir located nearby an urban solid waste treatment plant. Leachate sample was collected from a solid waste treatment plant.

### 2.5. Extraction procedure

The SIA procedure for the application of CFs as sorbents for SPE was developed using the flow system schematically depicted in Fig. 1. Briefly, an appropriate sample volume is loaded into the holding coil through position 2 of the selection valve (SV). The SV is then connected to position 1 and the sample is pumped through the homemade holder containing a circular piece of CF, followed by a volume of carrier to wash the non-retained analytes in the CF. The circular piece of CF is 3.65 mm diameter and a thickness of 2.50 mm. By using an external solenoid valve placed at the outlet of the CF, the sample matrix is directed to a waste reservoir. Thereafter, the selection valve is connected to position 3 in order to load an appropriate amount of eluent, and then connected again to position 1 to flow the eluent through the CF. In this step, the additional solenoid valve is turned on enabling the collection of the eluent fraction in a vial, for subsequent HPLC analysis of the extracted analytes.



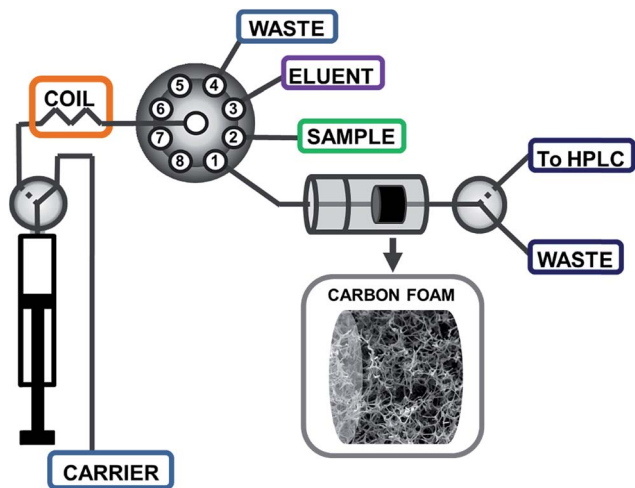


Fig. 1 Schematic depiction of the sequential injection analysis set-up for the determination of endocrine disrupting phenols using melamine-formaldehyde derived elastic carbon foams.

The collected solvent was evaporated under a gentle stream of nitrogen and reconstituted in 50  $\mu\text{L}$  of acetonitrile. A 20  $\mu\text{L}$  portion was used for HPLC analysis.

## 3. Results

### 3.1. Features of the CF sorbent

The CF used in this work as a novel sorbent for SPE in automated mode is based on a 3D interconnected monolithic carbon network (Fig. 2a and b), which is a replicate of the original MF (Fig. 2c). After carbonization, the MF structure shrinks and its color changes from white to a black color, maintaining the morphology of the 3D network and its flexibility (Fig. 2d–f). A larger piece of MF is carbonized to a CF, with the limitation of the diameter of the tubular oven used for the carbonization (26 mm). Several pieces of MF are carbonized simultaneously obtaining a substantial amount of CF in just one carbonization step. The larger CF pieces can be subsequently cut into smaller pieces and easily molded in different

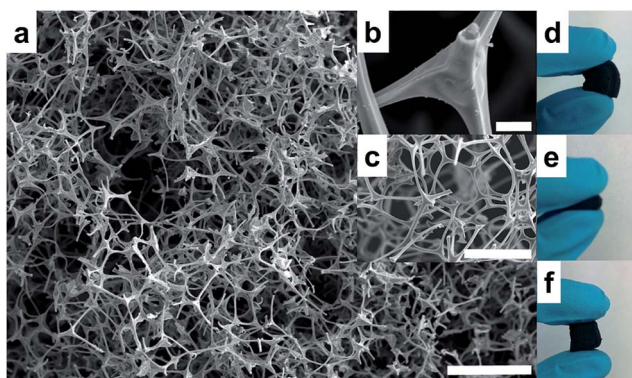


Fig. 2 (a) SEM images of the (a) CF (scale bar, 100  $\mu\text{m}$ ), (b) detail of the CF (scale bar, 5  $\mu\text{m}$ ), (c) precursor MF polymer foam (scale bar, 100  $\mu\text{m}$ ). (d–f) Images showing the flexibility of the melamine carbon foam.

shapes, just cutting them with a blade. In this case, CF is cut as a small disk that is fitted easily within a flow-through extraction holder due to its elastic behavior.

The obtained CFs are composed by carbon doped with nitrogen, and when obtained at temperatures ranging from 400 to 800  $^{\circ}\text{C}$  are moderately hydrophobic. These CFs are ideal sorbents for the SPE of moderately polar compounds such as bisphenols or alkylphenols. More hydrophobic CFs have been obtained using carbonization temperatures  $>1000$   $^{\circ}\text{C}$ .<sup>21</sup> Alternatively, the surface properties of CFs can be tuned by carbonizing the MF in the presence of copolymers,<sup>21</sup> or by post-combustion modification with chlorotrimethylsilane.<sup>30</sup>

### 3.2. Study of the extraction parameters for the SPE of phenolic endocrine disruptors using CF

The relevant parameters involved in the automated SPE process using CFs has been studied using bisphenol A (BPA), 4-*tert*-octylphenol (4-OP) and 4-*n*-nonylphenol (4-NP) as model analytes.

**3.2.1. Desorption solvent.** The selection of a suitable solvent for the efficient desorption of the analytes from the solid support is a critical parameter. Fig. 3 shows the results obtained for the elution of the analytes using methanol, ethanol, acetonitrile, acetone and 2-propanol. For this study, a volume of a standard solution of 2.5 mL containing the three analytes at a level of 50  $\mu\text{g L}^{-1}$  was pumped through the CF at a flow rate of 5  $\text{mL min}^{-1}$ . The analytes were eluted by 1 mL of the selected solvent at an elution rate of 1  $\text{mL min}^{-1}$ . The best elution performance was obtained using acetonitrile as the eluent, since the measured peak areas were 36–58% higher in the case of BPA. And for 4-OP and 4-NP, the measured peak areas were 23–56% higher and 16–39% higher for 4-NP, respectively. Therefore, acetonitrile was selected as the eluent with the best performance for further studies.

**3.2.2. Effect of sample volume.** In SPE, the use of a larger sample volume increases the preconcentration factor of the method, thus lowering the detection limit. However, if the

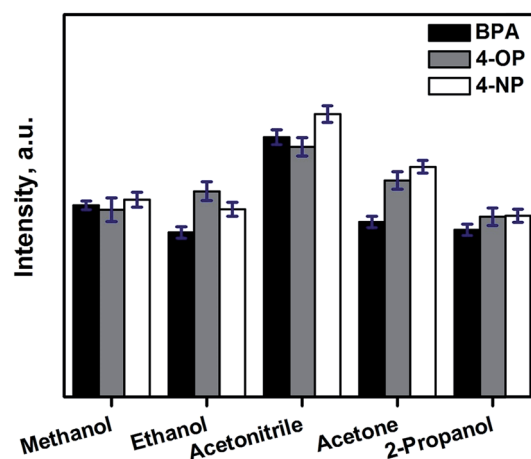


Fig. 3 Selection of the appropriate solvent for the elution of the selected endocrine disrupting phenols from the CF.



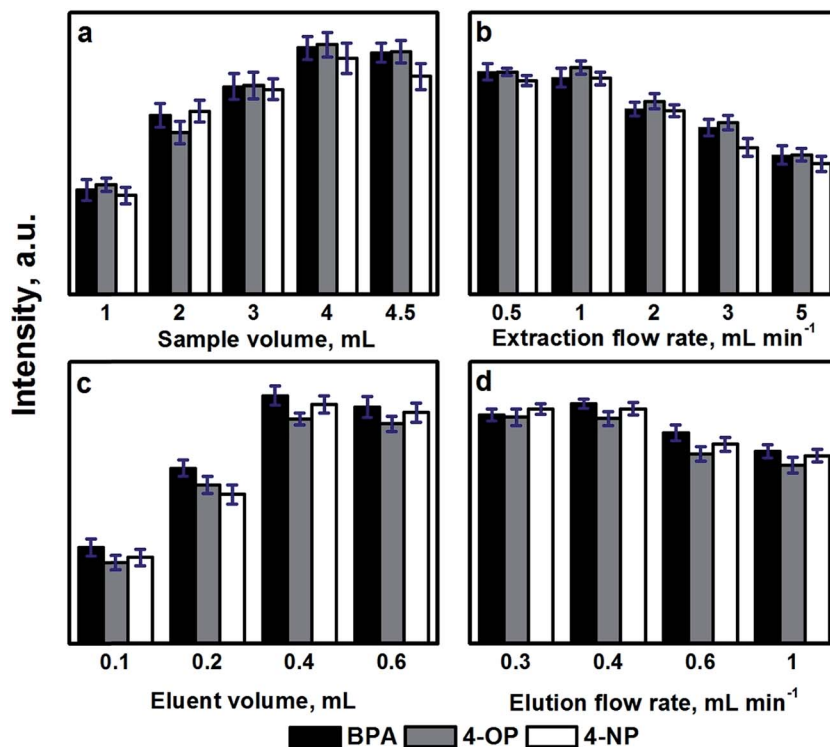


Fig. 4 Study of the effect of the sample volume (a), extraction flow rate (b), eluent volume (c) and elution flow rate (d) on the extraction of the selected endocrine disrupting phenols by using automated SPE with a CF as sorbent.

sorbent is close to saturation and the analyte breakthrough is high, a further increase on the sample volume will just increase the analysis time. To investigate the effect of the sample volume, this parameter was studied in the range from 1 to 4.5 mL, while keeping all the other experimental variables as described in Section 3.2.1. Fig. 4a shows that the extraction of the analytes increased while increasing the sample volume up to 4 mL. A further increase on the sample volume did not provide any significant improvement on the preconcentration factor. A volume of 4 mL was selected as the sample volume for further experiments.

**3.2.3. Preconcentration flow rate.** The flow rate in the preconcentration step is a critical factor in SPE. The analyte extraction efficiency usually increases by increasing the contact time between the sample and the SPE sorbent in the extraction process. However, the use of high extraction flow rates enhances the extraction throughput, but the contact time between phase decreases making a potential detrimental effect on the efficiency of the SPE process. The effect of the extraction flow rate on the SPE using CFs was studied from 0.5 to 5 mL min<sup>-1</sup>. Fig. 4b shows that there is no loss of extraction efficiency when the extraction flow rate is increased from 0.5 mL min<sup>-1</sup> to 1 mL min<sup>-1</sup>. However, using higher flow rates (2–5 mL min<sup>-1</sup>), a gradual decrease in the measured peak areas for the three analytes was observed. In order to obtain the maximum analyte peak areas without sacrifice the extraction throughput excessively, an extraction flow rate of 1 mL min<sup>-1</sup> was selected. However, extraction flow rates of up to 5 mL min<sup>-1</sup> were implemented without any apparent back pressure, in this case

obtaining extraction efficiencies 36–39% lower than using a flow rate of 1 mL min<sup>-1</sup>.

**3.2.4. Effect of elution volume.** The elution volume was studied in the range from 0.1 to 0.6 mL. Fig. 4c shows that best results were obtained when a volume of 0.4 mL of acetonitrile was used, and no further improvement was obtained using a larger eluent volume. Therefore, 0.4 mL of acetonitrile were selected as eluent volume for further experiments.

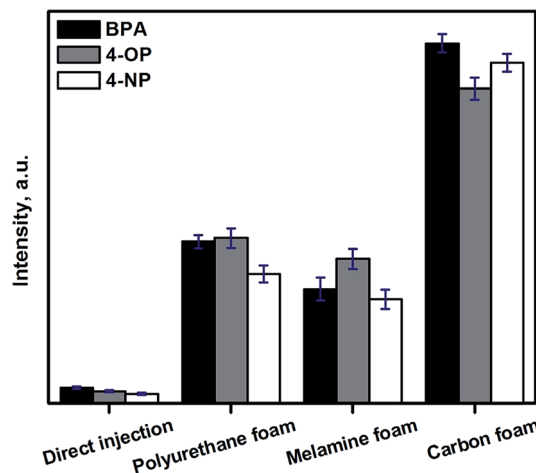


Fig. 5 Comparison of the CF foam for the solid-phase extraction of endocrine disruptive phenols by using polyurethane foam, melamine–formaldehyde polymer foam, and melamine–formaldehyde polymer derived carbon foam.





**3.2.5. Effect of elution flow rate.** The flow rate of the eluent is another relevant parameter affecting the sensitivity and the reproducibility of the method. Fig. 4d shows the results of the elution flow rate, which was studied from 0.3 to 1 mL min<sup>-1</sup>. A flow rate of 0.3 mL min<sup>-1</sup> is the minimum flow rate allowed by the syringe pump used, when a 5 mL syringe is used. The extraction efficiency gradually decreased while increasing the elution flow rate, selecting a flow rate of 0.4 mL min<sup>-1</sup>. Working under the selected elution conditions, a complete analyte desorption was obtained observing no memory effects on the CF sorbent for subsequent measurements.

**3.2.6. Effect of carbonization on the extraction performance of polymer foams.** The extraction performance of BPA, 4-OP and 4-NP using the prepared CFs was compared with the direct use of commercially available MF and polyurethane foams (Fig. 5). The preconcentration factors for the three analytes were of 11–15 when commercially available polyurethane foam was used. The extraction performance decreased slightly when MF was used as sorbent, obtaining preconcentration factors of 7–12. However, after the conversion of the MF into a CF, a superior extraction performance was observed for the CF obtaining preconcentration factors of 24–38. These results show the superior performance of the CFs derived from MFs, rather than the direct use of the MF as sorbent. This is attributed to the

increase of the hydrophobicity of the MF after carbonization, and a subsequent enhancement on the preconcentration factor.

In this case, a carbonization temperature of 800 °C, is ideal to obtain CFs moderate polarity, which are ideal for the extraction of slightly polar analytes as the selected endocrine disrupting phenols. To obtain more polar CFs a lower carbonization temperature can be used, tuning the number of remaining polar groups (carbonyl, hydroxyl, ...) in the final CF. The hydrophobicity of CF can be increased by increasing the carbonization temperature, obtaining CF with an almost negligible presence of polar groups.<sup>21</sup>

### 3.3. Analytical features

The analytical features of the developed SIA method for the automated SPE of endocrine disrupting phenols using the CFs were established working under the selected experimental conditions studied in the previous sections. The obtained analytical features are summarized in Table 1. The linear dynamic range (LDR) of the method was established in the range of 0.5–200 µg L<sup>-1</sup>, and all analytes showed good linearity with determination coefficients (*r*<sup>2</sup>) greater than 0.9952. The limits of detection (LOD) were calculated based on peak-to-peak noise (*S/N* = 3), and ranged from 0.02 to 0.08 µg L<sup>-1</sup>. The limits of quantification (LOQ) based on *S/N* = 10, ranged from 0.34 to 0.85 µg L<sup>-1</sup>. The relative standard deviations (RSD) for

Table 1 Analytical features of the developed CF-SIA method

Analyte	LDR (µg L <sup>-1</sup> )	<i>r</i> <sup>2</sup>	LOQ (µg L <sup>-1</sup> )	LOD (µg L <sup>-1</sup> )	Precision <sup>a</sup> (RSD, %)				PF <sup>c</sup>
					Intra-day		Inter-day <sup>b</sup>	Batch-to-batch <sup>b</sup>	
					100 µg L <sup>-1</sup>	10 µg L <sup>-1</sup>			
BPA	0.5–200	0.9952	0.02	0.34	3.5	4.8	5.2	6.1	28
4-OP	1–200	0.9972	0.08	0.85	2.8	4.1	6.3	6.3	30
4-NP	1–200	0.9989	0.04	0.65	3.6	4.5	5.6	5.8	34

<sup>a</sup> Relative standard deviation (*n* = 6). <sup>b</sup> Spiking level, 50 µg L<sup>-1</sup>. Batch to batch = 3 sponges. <sup>c</sup> Preconcentration factor.

Table 2 Comparison of the present method with other published liquid- or solid-phase microextraction methods for the determination of endocrine disrupting phenols using HPLC

Extraction technique	Detection technique	Sample	LOD (µg L <sup>-1</sup> )	RSD (%)	Ref.
DLLME	HPLC-DAD	Water	0.07 (BPA)	6.0	31
Vortex-assisted LPME	HPLC-FLD	Water	0.02 (BPA) 0.01 (4-OP) 0.07 (4-NP)	5.9–8.0	32
Ionic liquid LPME	HPLC-FLD	Water	0.7 (4-OP) 0.3 (4-NP)	3.2–7.8	33
SPME	HPLC-FLD	Food packages	0.9 (BPA)	22	34
SPME	HPLC-FLD	Water	0.43 (BPA) 0.16 (4-OP) 0.29 (4-NP)	—	35
In-tube SPME	HPLC-FLD	Water	0.02 (BPA)	9.8	36
CF-SIA	HPLC-DAD	Water	0.02 (BPA) 0.08 (4-OP) 0.04 (4-NP)	2.8–6.3	This work



**Table 3** Summary of results obtained from the analysis of the studied compounds in different water samples and relative and spiking recoveries of spiked samples

Sample	Analyte	Measured ( $\mu\text{g L}^{-1}$ )	Added ( $\mu\text{g L}^{-1}$ )	Found ( $\mu\text{g L}^{-1}$ )	Spiking recovery (%)	Relative recovery (%)
Well water 1	BPA	ND <sup>b</sup>	10	9.32	93.2	91.7 (7.5) <sup>a</sup>
	4-OP	ND	10	9.22	92.2	90.1 (7.1)
	4-NP	ND	10	9.28	92.8	91.7 (6.8)
Well water 2	BPA	1.05	10	10.6	95.5	95.2 (5.2)
	4-OP	2.12	10	11.8	96.8	96.3 (6.2)
	4-NP	1.05	10	10.9	98.5	93.6 (6.1)
Leachates	BPA	1.45	10	11.2	97.5	93.6 (6.3)
	4-OP	1.02	10	10.7	96.8	94.6 (6.7)
	4-NP	ND	10	9.87	98.7	95.3 (7.2)
Wastewater	BPA	3.32	10	12.3	89.8	89.0 (7.5)
	4-OP	2.61	10	11.9	92.9	91.2 (6.8)
	4-NP	2.23	10	11.7	94.7	92.3 (6.9)

<sup>a</sup> RSD% value ( $n = 3$ ). <sup>b</sup> Not detected.

consecutive extractions using the same CF sorbent ranged between 2.8 and 3.6% ( $n = 6$ ,  $100 \mu\text{g L}^{-1}$ ), showing the high repeatability of the automated extraction procedure. Using more diluted analyte standard solutions, a good extraction repeatability was also achieved, obtaining RSDs ranging from 4.1–4.8% ( $n = 6$ ,  $10 \mu\text{g L}^{-1}$ ). Inter-day reproducibility was also evaluated using CFs prepared from the same carbonization batch (same piece of carbonized MF), showing a good reproducibility with obtained RSD values ranging from 5.2–6.3% ( $n = 6$ ,  $50 \mu\text{g L}^{-1}$ ). Batch-to-batch reproducibility was also evaluated comparing CFs prepared from different pieces of MF. The obtained RSD values (5.8–6.3%) from the comparison of three CF prepared from different MF batches showed the good batch-to-batch reproducibility.

The preconcentration factors obtained ranged from 24 to 38, showing the high performance of the developed automated SPE procedure using CFs. The extraction throughput working under the selected experimental conditions is  $7 \text{ h}^{-1}$ . However, in cases when the sensitivity of the method is not a crucial parameter and the purpose of SPE is just a sample clean-up, the use of higher flow rates ( $5 \text{ mL min}^{-1}$ ) increases the extraction throughput  $>40\%$ . As a difference with particle packed beds, CFs are flexible and no apparent backpressures are observed, even when high flow rates ( $5 \text{ mL min}^{-1}$ ) are applied using low-pressure instrumentation. This feature and their inherent chemical robustness makes them reusable for at least 50 times, when SPE in a reverse phase mode is used, as in the example of application reported in this work.

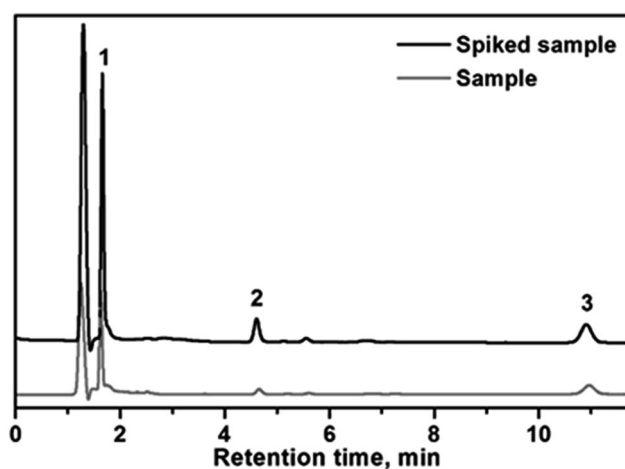
A comparison between the obtained LODs and the precision of the developed method and other previously developed sample pretreatment techniques for the extraction and determination of endocrine disrupting phenols are summarized in Table 2. As can be seen in the table, the obtained LODs are on par with those of other extraction techniques including dispersive liquid–liquid microextraction (DLLME),<sup>31</sup> liquid-phase microextraction (LPME),<sup>32,33</sup> or solid-phase microextraction (SPME).<sup>34–36</sup> Additionally, the developed SPE method is benefited from the advantageous features inherent to flow

analysis systems, obtaining an automated extraction method enabling high reproducibility and short analysis times when compared with other manual microextraction techniques.

The main advantages of the use of CFs as sorbents for SPE are: (1) extremely low cost and commercially available precursor material (MF). (2) A large amount of CF is obtained in just one carbonization step. (3) CFs are reusable. (4) CFs can be molded into any shape. (5) CFs are flexible, and can be used as flow-through supports at low pressures. (5) CFs have a monolithic shape, and they can be easily handled and packed.

### 3.4. Sample analysis

In order to study the accuracy and applicability of the method for the extraction and determination of the selected endocrine disrupting phenols in real samples, different water samples (well water, leachates and wastewater) were selected as a model for the real samples analysis. Quantification of the analytes was



**Fig. 6** HPLC chromatograms of a wastewater sample after SPE using the prepared CF before (a) and after spiking with  $20 \mu\text{g L}^{-1}$  of each analyte. Peaks: bisphenol A (1). 4-*tert*-Octylphenol (2). 4-*n*-Nonylphenol (3).



performed using the standard addition method. The real samples were spiked with the analytes at three different concentration levels (10, 20 and 50  $\mu\text{g L}^{-1}$ ). The results for sample analysis are shown in Table 2. The relative recovery was defined as the ratio of the measured concentration of the analyte in the samples and the measured concentration of analyte in pure water samples spiked with the same amount of analytes.

The results for sample analysis are shown in Table 3. As can be seen in the table, the relative recoveries were higher than 89.0%, for all analytes. In Fig. 6, is shown an example of chromatogram of the wastewater sample before and after spiking with 20  $\mu\text{g L}^{-1}$  of each analyte. These results confirm the suitability of the developed automated SPE method using CFs for real sample analysis.

## 4. Conclusion

In this study, a simple and reproducible strategy has been developed for the implementation of flexible carbon sorbents for SPE. It has been achieved by the direct carbonization of commercially available MF in an inert atmosphere. The prepared CFs showed excellent properties as flow through sorbents, such as high reproducibility, durability and pre-concentration factors using moderate extraction times. CFs are easily incorporated in flow analysis systems for the development of automated SPE procedures. In this case, the prepared CFs were successfully applied for the automated SPE of bisphenol A, 4-*tert*-octylphenol and 4-*n*-nonylphenol as model compound analytes.

The synthesized CFs present a significant hydrophobicity, and have a good affinity for the extraction of moderately polar phenols. However, the surface of the CFs can be tuned by the carbonization temperature or modified pre- or post-combustion, obtaining CFs with different surface properties. Future work can be directed towards the study of the presence of different functional groups on the CFs on depending of the carbonization temperature, as well as to develop novel clean-up applications for highly complex sample matrices, such as biological or food samples. Apart from MF, CFs can be obtained from other precursor materials, which can be potentially useful sorbents for novel SPE applications.<sup>37,38</sup>

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