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## Turning antiferromagnetic $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$ into a 140 K ferromagnet using a nanocomposite strain tuning approach

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Ferromagnetic insulating thin films of  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$  (SSMO) on (001)  $\text{SrTiO}_3$  substrates with a  $T_C$  of 140 K were formed in self-assembled epitaxial nanocomposite thin films. High  $T_C$  ferromagnetism was enabled through vertical epitaxy of the SSMO matrix with embedded, stiff,  $\sim 40$  nm  $\text{Sm}_2\text{O}_3$  nanopillars giving a  $c/a$  ratio close to 1 in the SSMO. In contrast, bulk and single phase SSMO films of the same composition have much stronger tetragonal distortion, the bulk having  $c/a > 1$  and the films having  $c/a < 1$ , both of which give rise to antiferromagnetic coupling. The work demonstrates a unique and simple route to creating ferromagnetic insulators for spintronics applications where currently available ferromagnetic insulators are either hard to grow and/or have very low  $T_C$ .

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## Introduction

Ferromagnetic insulators (FMIs) are of great research interest due to the rare combination of ferromagnetism and insulating characteristics which are needed for oxide spintronics and multiferroics.<sup>1–3</sup> FMIs can be used in spin-filter barriers in magnetic tunnel junctions (MTJs). They are also important parent compounds for creating multiferroics, in which the coexistence of ferromagnetism and ferroelectricity leads to magneto-dielectric coupling.<sup>4–7</sup>

There are few spin-filter materials with very high efficiency. EuS and EuSe are rare examples, but the low  $T_{\text{CS}}$  (16.6 K for EuS and 4.6 K for EuSe) of these materials limits their application to liquid helium temperatures.<sup>5,8</sup> In order to realize higher temperature applications, EuO has been investigated ( $T_C$  of 69 K). Nevertheless, the challenging growth conditions hinder its use.<sup>9</sup> Other promising candidates with high  $T_C$  include ferrites, but these are not without their own problems. For instance, rare-earth nitrides suffer from stability problems

due to their rapid oxidation in air<sup>10</sup> while ferrites, although having above room temperature  $T_C$ ,<sup>11</sup> have complex spinel structures, making it difficult for their integration into tunnel hetero-structures made of half-metallic ferromagnetic perovskites such as  $\text{La}_{0.67}\text{Sr}_{0.33}\text{MnO}_3$  (LSMO).<sup>12</sup> Consequently, new practical FMIs are strongly needed. Perovskites are excellent candidates as they are chemically and structurally compatible with numerous oxide electrodes.<sup>13</sup>

Transition metal oxide perovskites are interesting because of their wide variety of structural, magnetic and transport properties.<sup>14,15</sup> For example,  $\text{RE}_{1-x}\text{AE}_x\text{MnO}_3$  (RE and AE represent a trivalent rare earth and a divalent alkaline earth element, respectively) systems exhibit a very rich electronic and magnetic phase diagram due to strong coupling between the charge, orbital and spin degrees of freedom.<sup>16,17</sup> However, only very few insulating perovskite manganites are ferromagnetic. Notable exceptions are  $\text{BiMnO}_3$  and  $\text{La}_{0.1}\text{Bi}_{0.9}\text{MnO}_3$  with  $T_{\text{CS}}$  of around 100 K. However, the growth of these materials is non-trivial.<sup>18,19</sup>  $\text{Sm}_{1-x}\text{Sr}_x\text{MnO}_3$  (SSMO), with  $x = 0.1$  to  $x = 0.3$ , is another potential perovskite FMI with a maximum  $T_C$  also of  $\sim 100$  K in bulk.<sup>20</sup> Recently, spin filter tunnel junctions based on SSMO were fabricated into devices,<sup>21</sup> giving 75% spin polarization. However, the junctions operated mainly at a low temperature of 5 K.<sup>22</sup> Thus despite the promising bulk properties, in strained films wide deviations in the ferromagnetic properties result.<sup>23–28</sup> Indeed, the physical properties of SSMO, of low band width, have great sensitivity to both strain and composition.<sup>29</sup> Even with minimization of substrate-induced strain using buffer layers and highly lattice matching

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substrates,<sup>23,26,27</sup> properties are very different from the bulk values because of incomplete strain relaxation and also possibly because of oxygen vacancy strain-accommodating defects.<sup>30</sup>

More recently, studies have focused on several perovskite systems where strain enhances  $T_C$ .<sup>31–34</sup> However, again strain relaxation with the film thickness leads to non-uniform properties through the film.<sup>35</sup>

The objective of this work is to use a nanocomposite thin film approach to create a stable ferromagnetic insulating phase which is not susceptible to substrate strain, which can be formed easily and which has uniform properties through the thickness. In nanocomposite films, strain is controlled in a matrix by using a stiff strain-controlling second phase pillar in the film which controls the *out-of-plane* strain.<sup>37</sup> In this case, the strain controlling pillars are  $\text{Sm}_2\text{O}_3$  ( $E_{\text{SmO}} = 240$  GPa<sup>38</sup> vs.  $E_{\text{SSMO}} = 130\text{--}160$  GPa,<sup>39</sup> where  $E$  is the average elastic modulus) and the matrix is SSMO.

In such nanocomposite films, in the less-stiff matrix, the *out-of-plane* strain is controlled by vertical epitaxy, while the *in-plane* strain is determined by a combination of heteroepitaxy with the substrate as well by elastic interactions with the stiff nanopillars. Hence the relative mechanical properties (e.g. elastic moduli and thermal expansion coefficients) of the two materials in the composite film are important for controlling the *in-plane* strain.<sup>40</sup> Overall, a uniform and unconventional strain state can be induced in the matrix phase in thick ( $\sim\mu\text{m}$ ) nanocomposite films, something that is not possible in conventional thin films whose lattice parameters are dependent on planar epitaxy, with strain beginning to relax above just a few nm. In addition, for conventional films there is the problem of limited availability and high cost of single crystal substrates for precisely tuning lattice parameters in the films.

## Results and discussion

Since Sm readily substitutes into  $\text{SrMnO}_3$ , it was expected that Sm would displace Sr in the  $\text{SrMnO}_3$  matrix, leading to Sr expulsion from the film. Fig. 1(a) (top panel) shows a scanning transmission electron microscopy (STEM) image of a 120 nm thick nanocomposite showing the SmO nano-pillars embedded in the SSMO matrix. The bottom left panel of Fig. 1(a) shows a high angle annular dark field (HAADF) image. This image reveals a darker SrO phase on the surface of the nanocomposite film. The presence of the surface SrO in our films is consistent with the previous studies showing Sr migration to film surfaces to give poorly crystalline precipitates.<sup>41</sup> The selected area electron diffraction (SAED) pattern in the bottom right panel of Fig. 1(a) shows the high quality crystallinity of the STO substrate as well as the SmO and SSMO phases in the film.

A high resolution cross-sectional TEM image of a nanocomposite film shows a clean and sharp interface between the SmO nano-pillars and the SSMO matrix (see Fig. 1(b)). Two different orientations of the SmO nano-pillars were observed,

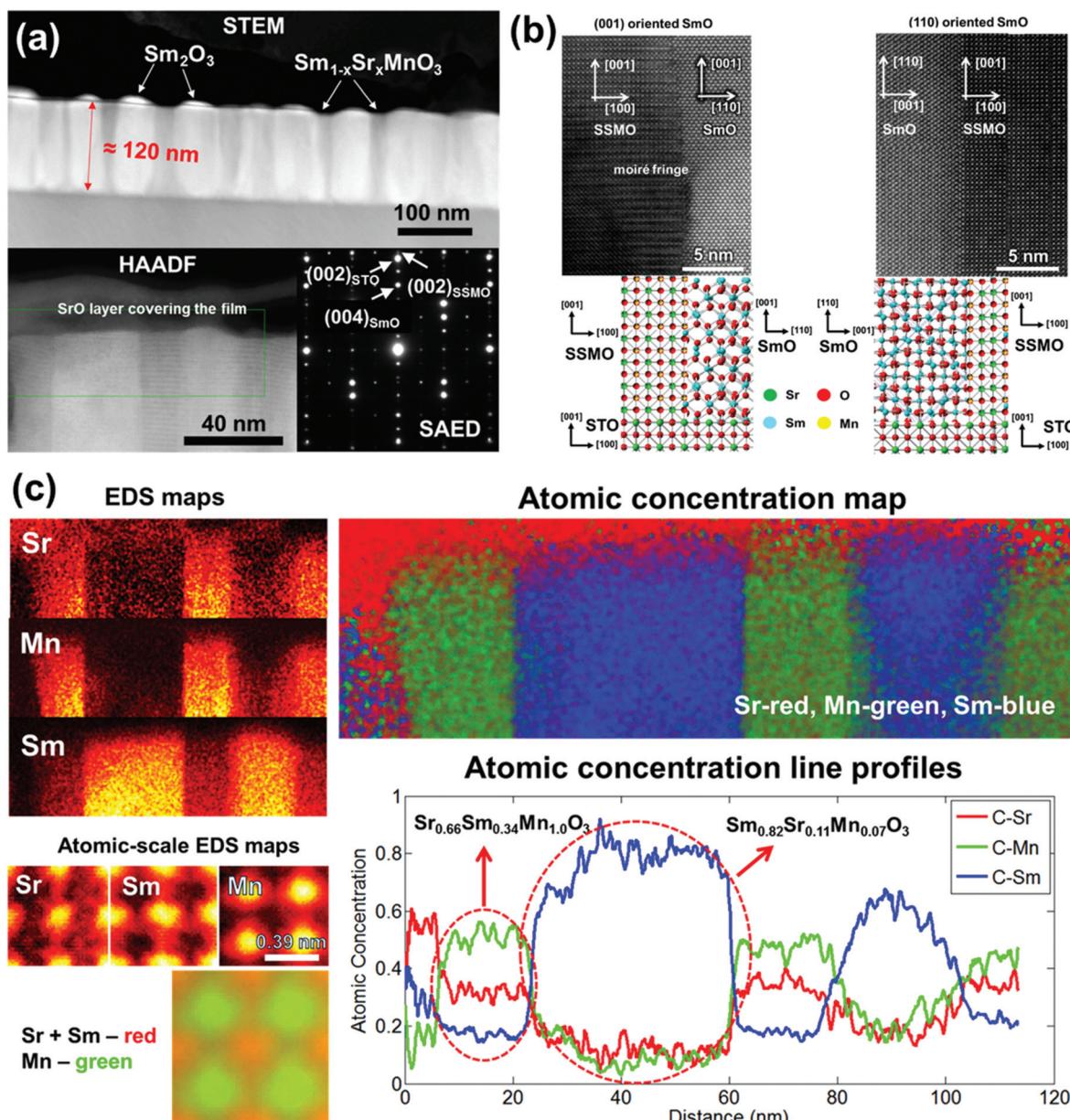
(110) and (001) while only one orientation of SSMO was observed, (001). As shown in the schematic crystal in the lower part of Fig. 1(b), the (110) SmO phase was oriented with the STO substrate *in-plane* with the [110]  $\text{SmO}||[100]$  STO. On the other hand, the (001) SmO was oriented *in-plane* with the [100]  $\text{SmO}||[100]$  STO. The SSMO phase was oriented *in-plane* with the [100]  $\text{SSMO}||[100]$  STO.

The occurrence of the (110) orientation of SmO in the nanocomposite film is different from the case of single phase SmO films grown on the (001) STO which are typically (001) oriented.<sup>42</sup> The reason for this difference is that vertical epitaxial lattice matching between the [110] SmO and the [001] SSMO (0.9% misfit) in the (110) SmO films is much lower than the misfit between the [001] SmO and the [001] SSMO (6.6% misfit) in the (001) SmO films. Fig. 1(c) shows compositional characterization of the nanocomposite films by EDS, by atomic-scale EDS, by using atomic concentration maps, and by using atomic concentration line profiles. In the EDS maps, very sharp and clean interfaces can be observed from the bright regions for both Sr and Mn in the same area, with the bright region for Sm being in the adjacent area. The atomic-scale EDS maps show direct evidence of Sm substitution onto the Sr site. The atomic concentration maps and line profiles show the distinct nano-pillars of the composition  $\text{Sm}_{0.82}\text{Sr}_{0.11}\text{Mn}_{0.07}\text{O}_3$  and the matrix of the composition  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$ . Hence, there is a  $\sim 11\%$  substitution of Sr onto  $\text{Sm}_2\text{O}_3$  and  $\sim 34\%$  of Sm onto the Sr site in  $\text{SrMnO}_3$ .

$2\theta\text{-}\omega$  XRD scans of the nanocomposite films are shown in Fig. 2. Sharp peaks of the SSMO (002) and SmO (006) are observed in the Bragg–Brentano scan in Fig. 2(a) with some overlapping of the SSMO (002) and STO (001) peaks. No peaks associated with the (110) SmO were observed due to the overlapping of the SmO (440) with the STO (002) substrate peak. Owing to the poor crystallinity of the SrO phase on top of the nanocomposite film, even though it was observed in the high angle annular dark field (HAADF) image in Fig. 1(a), it was not observable by XRD in Fig. 2.

X-ray phi-scans of the STO substrate and the SSMO and SmO peaks in the nanocomposite (inset of Fig. 2(a)) show a cube-on-cube orientation of the SSMO on STO while the SmO shows a  $45^\circ$  *in-plane* rotation with respect to the STO substrate, consistent with the high resolution TEM images. Fig. 2(b) shows a reciprocal space map (RSM) of the nanocomposite film revealing the strain states of the phases in the nanocomposite film. As shown by the vertical dashed line,  $q_x$  of the SSMO (113) peak is shifted to the left compared to bulk SSMO, indicating a higher  $a$ -axis in the nanocomposite film compared to the bulk. For comparison, Fig. 2(c) shows a  $2\theta\text{-}\omega$  scan for a single phase SSMO film of the same thickness ( $\sim 100$  nm). In the  $2\theta\text{-}\omega$  scan the (002) SSMO peak is at a higher  $2\theta$  value of  $48.4^\circ$  compared to  $47.6^\circ$  for the nanocomposite, indicating that the nanocomposite film has a higher  $c$  parameter than the single phase film. Fig. 2(d) shows a reciprocal space map (RSM) of a single phase film. The SSMO (113) peak along  $q_x$  is displaced further from the bulk SSMO position and hence the  $a$ -axis is larger than the one in



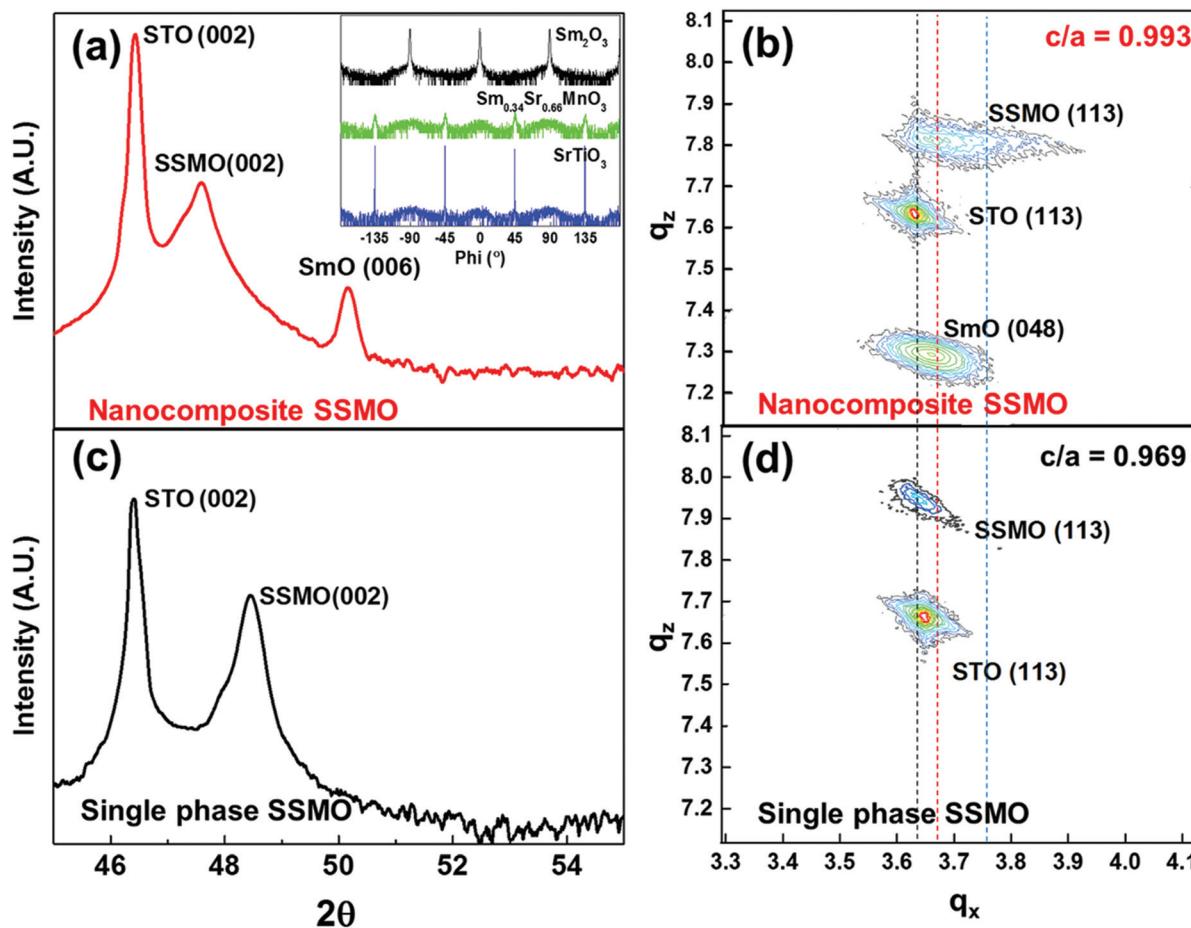


**Fig. 1** (a) High resolution cross sectional TEM image of the nanocomposite film (top). High-angle annular dark field (HAADF) image (bottom left) as well as selected area electron diffraction (SAED) (bottom right). (b) High resolution TEM image showing the interface between the nanopillar and matrix (top). Crystal orientation representation of the nanopillar and matrix as well as the substrate (bottom). (c) EDS map showing the compositions of the nanopillars and matrix (top left and top right). Atomic-scale EDS maps (bottom left) showing Sr and Sm occupying the same sites in the perovskite lattice and the atomic concentration line profile (bottom right) showing the lateral compositions of the nanopillars and matrix.

the nanocomposite film. The different strain states obtained in the nanocomposite and single phase SSMO films are analyzed and discussed below.

The *in-plane* lattice parameters of the  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$  phase in both the nanocomposite film and single phase SSMO films were estimated by first determining the *out-of-plane* parameter from the  $2\theta\text{-}\omega$  scans, and then by using this value to extract the *in-plane* lattice parameter obtained from the RSM (113) peak. As shown in Table 1, the *in-plane* and *out-of-plane* lattice parameters in the nanocomposite film are  $3.846 \pm$

$0.016 \text{ \AA}$  and  $3.819 \pm 0.008 \text{ \AA}$ , respectively. These values are  $1.61 \pm 0.42\%$  in tension *in-plane* and  $-2.05 \pm 0.21\%$  in compression *out-of-plane* relative to bulk  $\text{Sm}_{0.37}\text{Sr}_{0.63}\text{MnO}_3$ , giving a  $c/a$  of  $0.993 \pm 0.024$ . In contrast, the *in-plane* and *out-of-plane* lattice parameters for the single phase SSMO film are  $3.876 \pm 0.009 \text{ \AA}$  and  $3.756 \pm 0.005 \text{ \AA}$ , respectively. These values are  $2.40 \pm 0.24\%$  in tension *in-plane* and  $-3.67 \pm 0.13\%$  in compression *out-of-plane* relative to bulk  $\text{Sm}_{0.37}\text{Sr}_{0.63}\text{MnO}_3$ , giving a  $c/a$  of  $0.969 \pm 0.014$ . The higher level of strain and overall low  $c/a$  in the single phase film arise because of the *in-plane* epitaxial



**Fig. 2** (a)  $2\theta-\omega$  XRD scan of a nanocomposite film showing the presence of SmO and SSMO phases and the STO substrate, all with the (00l) orientation. The inset shows a phi-scan, revealing the different *in-plane* orientations of SmO and SSMO with respect to the STO substrate. (b) RSM of the nanocomposite film with vertical dashed lines indicating the centers of the peaks along  $q_x$  (c)  $2\theta-\omega$  XRD scan of a single phase SSMO film showing the presence of the SSMO film and the STO substrate, both with the (00l) orientation. (d) RSM of the single phase SSMO film showing close alignment along  $q_x$  of the SSMO (113) peak with the STO (113) peak as a result of epitaxial growth which causes the SSMO *in-plane* lattice parameter to be equivalent to the STO *in-plane* lattice parameter.

**Table 1** Properties of nanocomposite films compared to single phase films and the bulk

Properties	$\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$ in the nanocomposite film	Single phase $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$ film	Bulk $\text{Sm}_{0.37}\text{Sr}_{0.63}\text{MnO}_3$ (ref. 36) (pseudo-cubic)
Thickness	120 nm	100 nm	N.A.
$a$ (Å)	$3.846 \pm 0.016$	$3.876 \pm 0.009$	3.785
$c$ (Å)	$3.819 \pm 0.008$	$3.756 \pm 0.005$	3.899
<i>In-plane</i> strain (%)	$1.61 \pm 0.42^a$	$2.40 \pm 0.24^a$	N.A.
<i>Out-of-plane</i> strain (%)	$-2.05 \pm 0.21^a$	$-3.67 \pm 0.13^a$	N.A.
Tetragonality ( $c/a$ )	$0.993 \pm 0.024$	$0.969 \pm 0.014$	<b>1.030</b>
Magnetic properties	Ferromagnetic	Antiferromagnetic	Antiferromagnetic
$T_C/T_N$ (K)	$T_C = 140$	$T_N = 100$	$T_N = 250$
Electrical properties	Insulating	Insulating	Insulating

<sup>a</sup> Strain calculated relative to bulk  $\text{Sm}_{0.37}\text{Sr}_{0.63}\text{MnO}_3$ .

straining from the STO substrate ( $a = 3.905$  Å). The partial relaxation of the *in-plane* lattice parameter to 3.876 Å is expected owing to the relatively thick film. The *out-of-plane* compression arises through elastic strain to conserve the cell volume.

On the other hand, in the nanocomposite film the *out-of-plane* compression arises from vertical epitaxy with the stiff  $\text{Sm}_2\text{O}_3$  nano-pillars. Here, for the (001)  $\text{Sm}_2\text{O}_3$  orientation 3 unit cells of SSMO match with 1 unit cell of SmO ( $3 \times 3.819$  Å ||  $1 \times 10.93$  Å), and for the (110) SmO orientation, 4 unit cells of



SSMO match with 1 unit cell of SmO ( $4 \times 3.819 \text{ \AA} \parallel 1 \times 10.93 \times \sqrt{2} \text{ \AA}$ ). The *in-plane* tension arises because upon cooling the film from the growth temperature, the stiff  $\text{Sm}_2\text{O}_3$  pillars with a lower coefficient of thermal expansion cause the vertically epitaxially coupled  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$  to expand.<sup>40</sup> The tension is *less* in the composite film compared to the single phase SSMO films because of the different mechanism of the strain control.

Resistance *vs.* temperature plots comparing a nanocomposite film to a single phase SSMO film are shown in Fig. 3(a). An insulating profile was observed throughout the

measurement temperature range. Below 50 K, the resistance of both films is beyond the measurement limit. The electrical conduction mechanism at high temperatures follows the small polaron hopping (SPH) model.<sup>43,44</sup> The resistance as a function of temperature is given by  $R(T) = A T \exp(E_A/k_B T)$ , where  $E_A$  is the activation energy for conduction,  $T$  is the temperature and  $A$  is a constant. The activation energy  $E_A$  is determined by using linear fitting of the  $\ln(R/T)$  *vs.*  $1/T$  (dotted line in Fig. 3(a)), giving 94 meV for the nanocomposite film and 84 meV for the single phase SSMO film. Both these values are higher than the bulk SSMO value of 45–46 meV.<sup>45</sup> This is

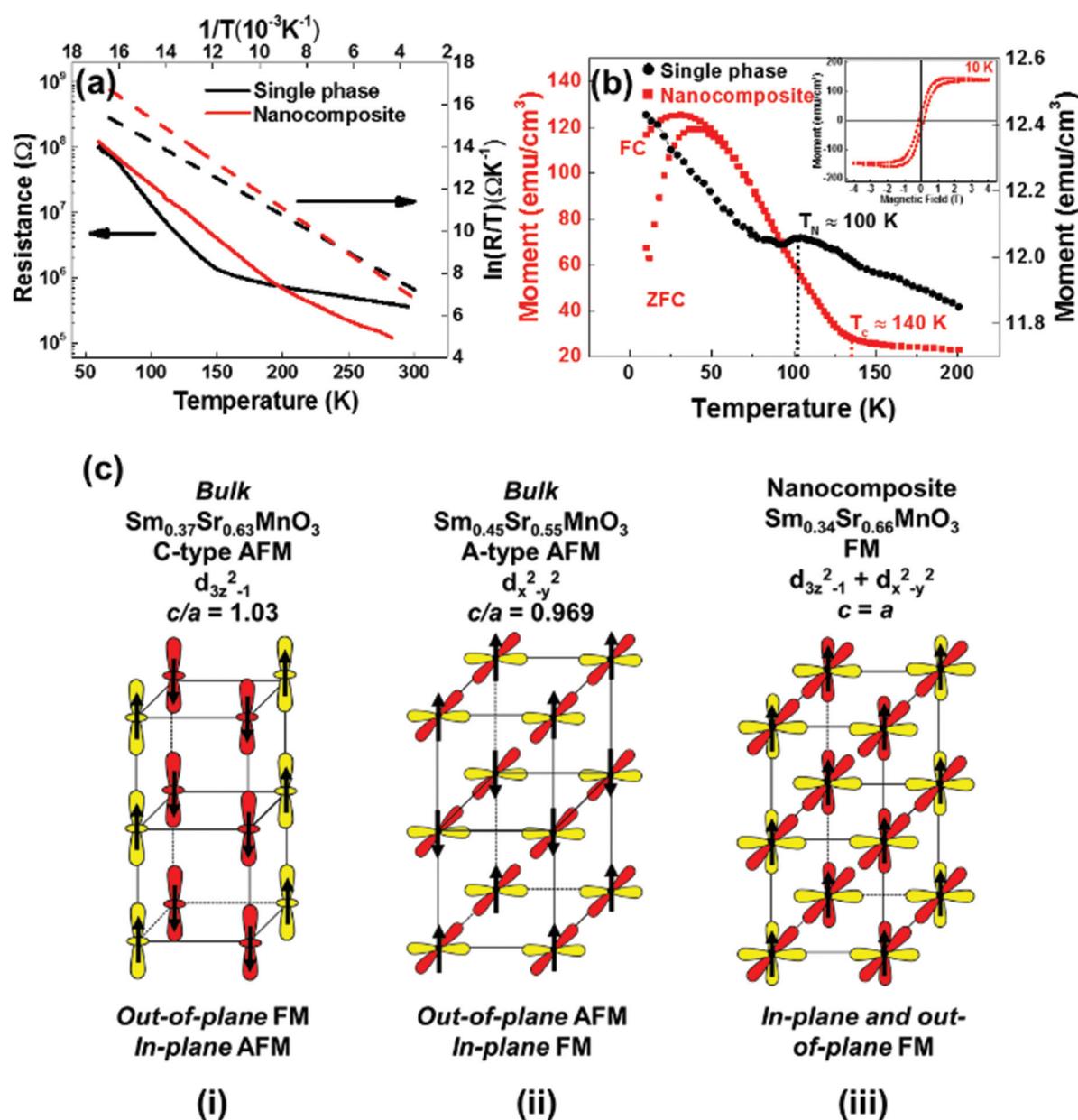


Fig. 3 (a) Resistance *vs.* temperature plot comparing the nanocomposite to a single phase film. The dotted lines in the plot shows linear fitting of  $1/T$  *vs.*  $\ln(R/T)$ . (b) Magnetization *vs.* temperature plot comparing the nanocomposite to a single phase film. The inset shows the magnetic hysteresis loop of the nanocomposite film. (c) Schematic diagram showing C-type and A-type AFM orbitals as well as FM orbitals with DE denoting double exchange coupling and SE denoting super-exchange coupling.



consistent with reduction of the electrical conduction because of strain in the films (and in the nanocomposite case, defects along the vertical interfaces between the two phases).

The comparative magnetic properties of the nanocomposite and single phase SSMO films are shown in Fig. 3(b).  $M$  vs.  $T$  plots show ferromagnetism with a  $T_C$  of 140 K for the nanocomposite film. We note that in the literature the highest  $T_C$  value in the ferromagnetic insulating (FMI) Sr-doped  $\text{SmMnO}_3$  system is 100 K<sup>22</sup> which is for the optimally doped (25% Sr doped) composition, and so the  $T_C$  of the SSMO phase formed in our nanocomposite films is 40 K higher than for any FMI Sr-doped  $\text{SmMnO}_3$  phase. In addition, the  $T_C$  of our nanocomposite films is 10 K higher than for the ferromagnetic metal (FMM), Sr-doped  $\text{SmMnO}_3$  (48% Sr).<sup>46</sup>

A cluster-glass like behaviour with a strong bifurcation between the field-cooled (FC) and zero field-cooled (ZFC) at 50 K was observed and the proposed origin of this is discussed later.<sup>47</sup> The inset of Fig. 3(b) shows the magnetic hysteresis loop of  $M$  vs.  $H$  at 10 K for the nanocomposite film. After subtracting the paramagnetic background from the substrate and  $\text{Sm}_2\text{O}_3$ , a clear ferromagnetic hysteresis loop is obtained. The coercivity ( $H_C$ ) and saturation magnetic moment ( $M_S$ ) are 100 Oe and 146 emu cm<sup>-3</sup> (1.93  $\mu_{\text{B}}/\text{Mn}$ ), respectively. This is comparable to the optimum 25% Sr doped  $\text{SmMnO}_3$  phase, as mentioned above.<sup>22</sup>

For the single phase SSMO films, AFM behavior was observed with a  $T_N$  of 100 K (Fig. 3(b)).<sup>20</sup> This is comparable to bulk  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$  which shows C-type antiferromagnet behaviour, although the  $T_N$  is higher for the bulk at  $\sim 250$  K, consistent with the very different levels of tetragonal distortion ( $c/a = 0.969$  for the single phase films vs. 1.030 for the bulk, as shown in Table 1).

We now turn to gain an understanding of the magnetic properties of the plain *versus* nanocomposite films obtained in this study. In doped manganites, magnetic interactions between the Mn atoms are determined by competition between FM double exchange interactions and AFM super-exchange.<sup>48</sup> The origin of the magnetic properties in the nanocomposite films can be understood by first realising that the level of structural distortion strongly influences these interactions. With Jahn-Teller effects at play, small distortions of  $\text{MnO}_6$  can stabilize either of the  $e_g$  orbitals,  $3z^2 - r^2$  or  $x^2 - y^2$ . For  $c/a > 1$  ( $c/a < 1$ ), the  $\text{MnO}_6$  octahedra are tensed (compressed) and consequently the  $3z^2 - r^2$  ( $x^2 - y^2$ ) orbitals are energetically favoured over the  $x^2 - y^2$  ( $3z^2 - r^2$ ) orbitals.

Hence, for  $c/a > 1$  the  $3z^2 - r^2$  orbitals have a higher occupancy. This results in 1-D FM double exchange interactions along the *out-of-plane* direction. The 1-D FM columns are AFM owing to super-exchange coupling. This results in a C-type AFM structure (as shown in Fig. 3(c i)). This is the case for bulk  $\text{Sm}_{0.37}\text{Sr}_{0.63}\text{MnO}_3$ ,  $c/a = 1.03$  (Table 1).

For  $c/a < 1$ , the  $x^2 - y^2$  orbitals have a higher occupancy. This leads to strong double exchange coupling in the  $\text{MnO}_2$  planes which strengthens the ferromagnetic ordering *in-plane*. At the same time, super-exchange coupling stabilizes the antiferromagnetic ordering in the *out-of-plane* direction. This

results in an A-type AFM as shown in Fig. 3(c ii). This is the case for the single phase  $\text{Sm}_{0.37}\text{Sr}_{0.63}\text{MnO}_3$  films,  $c/a = 0.969$  (Table 1).

In our  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$  nanocomposite films,  $c/a = 0.993 \pm 0.024$  (Table 1). Hence, the tetragonal distortion is reversed compared to the bulk value. Because  $c$  is close to  $a$  there is more or less equal occupation of the  $x^2 - y^2$  and  $3z^2 - r^2$  orbitals which produces double exchange interactions in both the *in-plane* and *out-of-plane* directions, thus leading to ferromagnetic ordering in 3-dimensions (as shown in Fig. 3(c iii)).<sup>48</sup>

Besides the extent of tetragonal distortion in the films, we should consider the actual Mn–O–Mn bond lengths. This is because AFM super-exchange interactions depend on Mn–O distances more strongly than the FM double exchange interactions. Hence, longer Mn–O bond lengths make the AFM super-exchange coupling weaker, whereas they influence the FM double exchange much less.<sup>49</sup> Hence, in our films FM double exchange dominates over AFM super-exchange, leading to the observed FM behavior. Overall, however, the AFM interactions in the film compete with the FM interactions. This competition explains the cluster glass-like behaviour in the  $M$  vs.  $T$  plot below 50 K in Fig. 3(b).

On a final note, the creation of high  $T_C$  ferromagnetism in our nanocomposite films is achieved *via* strain coupling between two phases. The work parallels artificial super-lattice (SL) studies where magnetic phases are coupled to other phases in a parallel configuration. In the SL studies, strong enhancements of  $T_C$  have been found when the *in-plane* strain is controlled by lateral coupling of phases. A  $T_C$  of 650 K (increased by nearly 300 K compared to bulk and plain films) has been observed for LSMO–BTO (with *in-plane* straining of the LSMO by 1%).<sup>50</sup> A key difference between the SL films and the nanocomposite films is that the nanocomposite films self-assemble rather than being made by a complex layering process.

In summary, in nanocomposite  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$  (SSMO) films using self-assembled vertical, strain controlling  $\text{SmO}$  nanopillars embedded in the SSMO matrix, a low  $c/a$  ratio is induced in the SSMO. Essentially, using nanocomposite films has enabled us to create a ferromagnetic insulator in a relatively thick film out of an otherwise antiferromagnetic insulator. The strain states (in both magnitude and uniformity) induced using the nanocomposite approach cannot be realised in single phase films and hence a new dimension for property control is realized by using these structures.

## Experimental

Nanocomposite films of  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$ – $\text{Sm}_2\text{O}_3$  were grown on the (001)  $\text{SrTiO}_3$  substrates using pulsed laser deposition (PLD). The starting target materials for PLD were prepared using a stoichiometric mixture of  $\text{Sm}_2\text{O}_3$  +  $\text{SrCO}_3$  +  $\text{MnO}_2$  powders by solid state sintering at 1100 °C for 6 hours. A Lambda Physik KrF excimer laser ( $\lambda = 248$  nm) was used for target ablation. The laser energy density was set at 1 J cm<sup>-2</sup>



with a target-to-substrate distance of 4.5 cm and 1 Hz pulse repetition rate. The vertical nanocomposite films were grown at 750 °C and 20 Pa oxygen pressure, followed by a short post deposition annealing at the same temperature for 30 minutes under a 100 mbar oxygen atmosphere. The resulting thickness of the film is 120 nm.

A Panalytical high resolution X-ray diffractometer (with Cu  $\kappa$  radiation, a 2-bounce hybrid monochromator and 0.5 mm slit beam tunnel) was used to determine the phase and crystalline quality of the deposited films. Cross-sectional images of the film were obtained by high resolution transmission electron microscopy (HRTEM). Platinum contacts were deposited by standard magnetron DC sputtering to serve as the top contact for electrical measurement. Magnetic properties were characterized using a superconducting quantum interference device (SQUID).

## Conclusions

Nanocomposite films containing  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$  were grown on  $\text{SrTiO}_3$  (001) with 120 nm thickness. Stiff  $\text{Sm}_2\text{O}_3$  nanopillars formed in the matrix of  $\text{Sm}_{0.34}\text{Sr}_{0.66}\text{MnO}_3$ , gave a unique strain state of lower *in-plane* tensile and *out-of-plane* compression than can otherwise be realized in single phase films. This leads to a lower *c/a* value compared to both the single phase films and bulk. This *c/a* reduction leads to 140 K ferromagnetism and insulating behaviour. This work demonstrates a novel strain approach for tuning magnetic properties in thin films.

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