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Title: All-in-one: a versatile gas sensor based on fiber enhanced Raman spectroscopy for monitoring postharvest fruit conservation and ripening

Fiber enhanced Raman gas spectroscopy has great potential for the simultaneous analysis of several gases with excellent selectivity and sensitivity for environmental monitoring, breath analysis for disease diagnostics, and various industrial applications.

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See Torsten Frosch *et al.*,  
*Analyst*, 2016, **141**, 2023.



[www.rsc.org/analyst](http://www.rsc.org/analyst)

Registered charity number: 207890

Cite this: *Analyst*, 2016, **141**, 2023

# All-in-one: a versatile gas sensor based on fiber enhanced Raman spectroscopy for monitoring postharvest fruit conservation and ripening†

Tobias Jochum,<sup>a</sup> Leila Rahal,<sup>a</sup> Renè J. Suckert,<sup>a</sup> Jürgen Popp<sup>a,b</sup> and  
Torsten Frosch<sup>\*a,b</sup>

In today's fruit conservation rooms the ripening of harvested fruit is delayed by precise management of the interior oxygen (O<sub>2</sub>) and carbon dioxide (CO<sub>2</sub>) levels. Ethylene (C<sub>2</sub>H<sub>4</sub>), a natural plant hormone, is commonly used to trigger fruit ripening shortly before entering the market. Monitoring of these critical process gases, also of the increasingly favored cooling agent ammonia (NH<sub>3</sub>), is a crucial task in modern postharvest fruit management. The goal of this work was to develop and characterize a gas sensor setup based on fiber enhanced Raman spectroscopy for fast (time resolution of a few minutes) and non-destructive process gas monitoring throughout the complete postharvest production chain encompassing storage and transport in fruit conservation chambers as well as commercial fruit ripening in industrial ripening rooms. Exploiting a micro-structured hollow-core photonic crystal fiber for analyte gas confinement and sensitivity enhancement, the sensor features simultaneous quantification of O<sub>2</sub>, CO<sub>2</sub>, NH<sub>3</sub> and C<sub>2</sub>H<sub>4</sub> without cross-sensitivity in just one single measurement. Laboratory measurements of typical fruit conservation gas mixtures showed that the sensor is capable of quantifying O<sub>2</sub> and CO<sub>2</sub> concentration levels with accuracy of 3% or less with respect to reference concentrations. The sensor detected ammonia concentrations, relevant for chemical alarm purposes. Due to the high spectral resolution of the gas sensor, ethylene could be quantified simultaneously with O<sub>2</sub> and CO<sub>2</sub> in a multi-component mixture. These results indicate that fiber enhanced Raman sensors have a potential to become universally usable on-site gas sensors for controlled atmosphere applications in postharvest fruit management.

Received 14th October 2015,

Accepted 9th February 2016

DOI: 10.1039/c5an02120k

www.rsc.org/analyst

## Introduction

Postharvest produce management encompassing storage and transport has become an important branch of modern logistics. Nowadays, more than half of the maritime transport of refrigerated products is represented by fruit transports.<sup>1</sup> Most of the imported fruit spends several days in transit between the country of production and the final market, where their ripening is typically performed by the wholesaler or retailer. Since consumers judge the quality of fruits by their appearance and sales increase if fresh, ready-to-eat produce are available,<sup>2</sup> postharvest technology and handling is a major challenge to successful fruit marketing. For all these reasons, thorough monitoring of fruit ripeness during the complete production chain is essential. To avoid fruit decay during transport and to optimize its quality on the market, most

fruits are shipped in conservation chambers, which delay the ripening process.<sup>3</sup> In low-oxygen (LO) or ultra-low oxygen chambers (ULO), fruits are exposed to low temperatures around 0 °C, high humidity (90–95%), low oxygen (approx. 2–3% O<sub>2</sub> for LO, 1–1.5% O<sub>2</sub> for ULO) and high carbon dioxide levels (approx. 2–5% CO<sub>2</sub> for LO, 1–1.5% CO<sub>2</sub> for ULO).<sup>4</sup> The role of ethylene (C<sub>2</sub>H<sub>4</sub>) in fruit ripening is twofold: since low C<sub>2</sub>H<sub>4</sub> concentrations are produced by the fruit itself during ripening, ethylene can act as a ripeness indicator; but it is also a natural plant hormone that triggers fruit ripening, as ethylene coordinates the expression of genes responsible for a variety of processes such as rise in respiration, autocatalytic ethylene production and changes in color, texture, flavor and aroma.<sup>5,6</sup> Depending on the fruit type, ethylene concentrations should thus be kept in low parts per million (ppm) or parts per billion (ppb) levels in conservation chambers to avoid early ripening and fruit losses;<sup>7</sup> whereas inside ripening rooms C<sub>2</sub>H<sub>4</sub> concentrations of up to 1000 ppm are possible.<sup>8</sup> In food cooling systems such as LO's and ULO's, monitoring of ammonia (NH<sub>3</sub>) is of particular interest because it becomes more and more the coolant of choice since substances with high ozone layer endangering potential are strictly regulated.

<sup>a</sup>Leibniz Institute of Photonic Technology, Jena, Germany<sup>b</sup>Institute of Physical Chemistry and Abbe Center of Photonics, Friedrich Schiller

University, Jena, Germany. E-mail: torsten.frosch@uni-jena.de, torsten.frosch@gmx.de

†Electronic supplementary information (ESI) available. See DOI: 10.1039/c5an02120k

In case of leakage, ammonia concentrations can rise easily to several hundred ppm or more, which demands safety actions for human protection.<sup>9</sup> Additionally, emergent ammonia could spoil stored fruit, *e.g.* by causing skin blackening.<sup>10</sup>

Commonly used fruit quality parameters such as firmness,<sup>11</sup> starch or sugar content<sup>12</sup> are not well suited for automated supervision, because they require unpacking or destructive sampling. Also, fruit color is often only weakly correlated to fruit ripeness.<sup>13</sup> Non-destructive methods to determine fruit ripeness by the level of soluble solids, ethylene concentration, chlorophyll or moisture content have been proposed, such as nuclear magnetic resonance<sup>14</sup> (NMR), proton magnetic resonance<sup>15</sup> (PMR), optical reflectance<sup>16</sup> or infrared absorption spectroscopy.<sup>17–19</sup> Recently, a variety of electronic nose (e-nose) approaches, widely utilizing chemoresistive gas sensors, attracted a lot of attention.<sup>20–22</sup> Here, mainly fruit-emitted aromatic volatiles or ethylene were measured to assess fruit ripening. Although most of these approaches are very sensitive, they rely upon expensive equipment<sup>23</sup> and/or are only suited to quantify a limited number of gases. Additionally, electrochemical sensors show gradual decrease in sensitivity which rapidly renders calibration data inapplicable.<sup>24</sup> Furthermore, chemoresistive metal oxide sensors for ethylene monitoring exhibit strong cross-interferences and are sensitive to humidity, which requires additional compensation methods.<sup>25</sup>

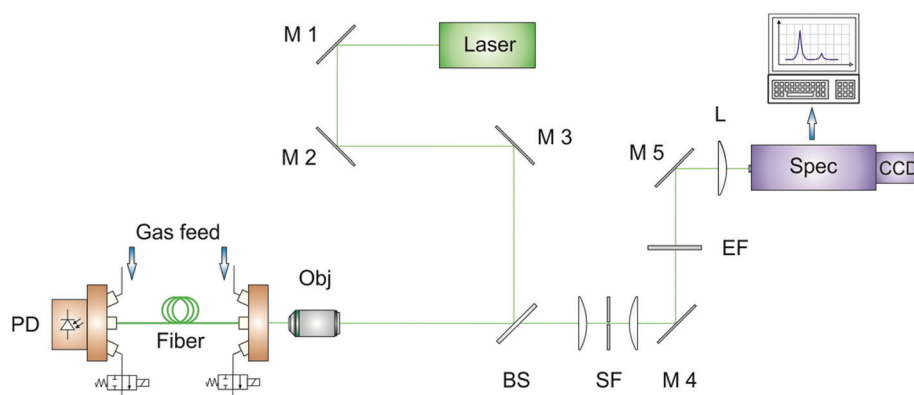
In this study, we present a gas sensor based on fiber enhanced Raman spectroscopy for on-site process gas monitoring throughout the complete postharvest production chain encompassing storage and transport in fruit conservation chambers as well as commercial fruit ripening in industrial ripening rooms. The gas sensor's capability was tested by obtaining and assessing a suitable sensor calibration for oxygen and carbon dioxide. Ammonia levels appropriate for chemical alarm purposes were established and successfully detected. Ethylene was measured down to a concentration of 100 ppm within a multi-gas mixture of O<sub>2</sub>, CO<sub>2</sub>, NH<sub>3</sub> and N<sub>2</sub> without any cross-sensitivity. The goal of the work presented here was to develop

and demonstrate the use of a single sensor covering simultaneously non-destructive oxygen, carbon dioxide, ethylene and ammonia monitoring over a wide concentration range of ppm up to percent levels while maintaining short measurement times.

## Materials and methods

### Experimental setup – optical part

Raman gas spectroscopy offers simultaneous detection and quantification of multi-gas mixtures in a wide concentration range from ppm levels up to pure compounds.<sup>26–33</sup> Due to the gas molecule's small Raman cross-sections, typically in the order of 10<sup>–23</sup> cm<sup>2</sup> sr<sup>–1</sup>,<sup>34</sup> Raman signals are intrinsically low and need to be enhanced. A novel approach is to use hollow-core photonic crystal fibers<sup>35</sup> (HC-PCF), which act as optical light guide as well as analyte container for the investigated processes gases.<sup>36,37</sup> The optical design of the Raman sensor is schematically depicted in Fig. 1. The laser beam from a frequency-doubled Nd:YAG laser (Laser Quantum, laser excitation wavelength  $\lambda_{\text{exc.}} = 532$  nm) is reflected by a dichroic beam-splitter (Semrock) into an objective (Olympus LUCPLFLN 20X), where it is focused in a 30 cm HC-PCF (NKT) with a bandgap suitable for low-attenuation guiding of Raman signals up to 3500 cm<sup>–1</sup>. This length is a good compromise between low analyte–laser interaction times within shorter fibers resulting in a lower overall Raman intensity<sup>38</sup> and the increasing attenuation of guided light within longer fibers. The central transmission wavelength of the HC-PCF is 532 nm and the hollow core has a diameter of approx. 5  $\mu\text{m}$ . Gases enter the HC-PCF *via* custom-made fiber adapters.<sup>39</sup> Adapters are installed at each end of the HC-PCF and provide reproducible laser coupling and scattered Raman light collection through optical windows as well as filling of the fiber with the analyte gases. The adapters can bear pressures up to 20 bar and have an internal dead volume of approx. 0.1 microliter. During measurements, the adapter's gas outlets were closed by mag-



**Fig. 1** Schematic sketch of the experimental setup. The 532 nm laser is guided by several mirrors (M1 to M3), a beamsplitter (BS) and an objective (Obj) into the hollow core photonic crystal fiber. The scattered Raman signal is coupled out in a backscattering geometry, passes the beamsplitter, a pinhole for spatial filtering (SF), an edge filter (EF) and a lens (L) and is eventually focused onto the spectrometer unit (Spec). Process gases are filled into the fiber *via* custom-made fiber adapters. A photodiode (PD) records the transmitted power during the gas measurements.





netic valves. After laser-molecule scattering, the redshifted Raman Stokes signal is coupled out of the fiber in a backscattering geometry, passing again the objective and the beamsplitter. Pinholes of 10 or 15  $\mu\text{m}$  diameter (Thorlabs) were used for spatial filtering of the silica Raman signal originating from the fiber cladding and thus for reducing the spectral background.<sup>40</sup> After passing an edge filter to suppress the Rayleigh signal, the scattered light is focused on the slit of the spectrometer (Acton SP2500, Princeton Instruments). A grating with 1800 lines per mm was chosen for high resolution. The setup magnifies light from the hollow core at the fiber exit to an approximately 60  $\mu\text{m}$  diameter spot with numerical aperture (NA) of 0.05 on the spectrometer entrance slit to achieve optimal etendue.

### Gas feed and measurement

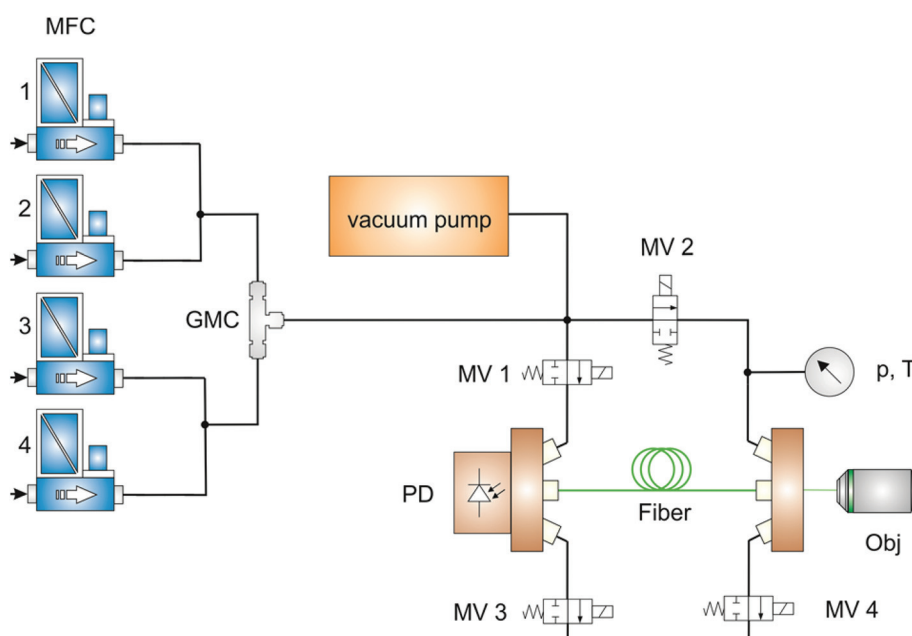
The gas feed line is schematically shown in Fig. 2. To simulate typical process gas compositions within the fruit ripening product chain, pure gases (purchased from Linde) were precisely mixed by mass flow controllers (Brooks Instrument) and subsequently injected. A gas mixing chamber provided homogeneous gas mixing and a stable gas flow, controlled by custom-made software based on LabView (National Instruments). Before each individual measurement, the fiber was automatically evacuated (inner pressure below 0.05 mbar) with a vacuum pump (Vacuubrand) to avoid cross-contamination. The gas mixture entered the HC-PCF from both ends with a pressure of approx. 2.0 bar by opening the magnetic valves 1 and 2 at the fiber adapters. During filling and measurement, magnetic valves 3 and 4 were shut. Given this pressure-driven filling procedure and the setup parameters, sub minute filling

times for all gases were expected according to the model of Wynne *et al.*<sup>41</sup> In separate test measurements beforehand, we observed stable Raman intensities for several applied gas concentrations after a filling time of one minute. Thus, all reported gas measurements were initiated one minute after opening the fiber adapter's magnetic valves 1 and 2. During measurements, all magnetic valves were shut. After each individual measurement, all gas-containing components were evacuated again to avoid cross-contamination with subsequent measurements. Alternatively, measured gases originating from fruit conservation or ripening chambers could also be redirected into the chamber *via* the magnetic valves 3 and 4 without any manipulation of the gas composition, which facilitates process monitoring *in situ*. Due to the compact and airtight design of the gas feed line, contamination of the analyte gases with ambient air was not observed in the Raman spectra.

Obtained spectra were normalized by absolute pressure and temperature (both measured with a pressure sensor, Keller), as well as by transmitted power (power sensor, Thorlabs). A beforehand acquired spectrum of pure Argon was used for background correction. For each gas, the respective Raman band in the background corrected spectrum was integrated, yielding a peak area  $A$ , and normalized with the average pressure  $p$  (in bar), temperature  $T$  (in Kelvin) and transmitted power  $P$  (in Watt) during the spectrum acquisition according to

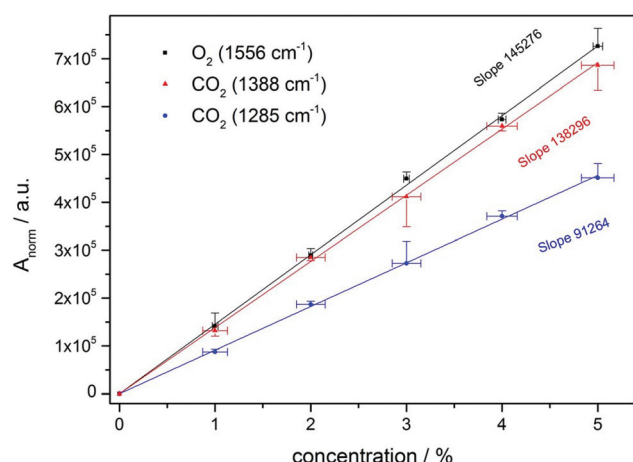
$$A_{\text{norm}} = \frac{A \times T}{p \times P} \quad (1)$$

As not only macroscopic thermodynamic systems are temperature dependent, but also populations of molecular energy



**Fig. 2** Illustration of the gas feed line. After applying a vacuum, gases were injected by up to 4 mass flow controllers (MFC), additionally homogenized in a gas mixing chamber (GMC) and filled into the fiber *via* the magnetic valves 1 and 2. During measurements, the current pressure ( $p$ ) and temperature ( $T$ ) were monitored. In the end, measured gases were released by opening MV 3 and 4.





**Fig. 3** Calibration data showing the linearity of the normalized Raman peak area *versus* the concentration (linear fits onto the measured data with coefficients of determination ( $R^2$ ) larger than 0.999). The background corrected peak area was normalized by the current pressure (in bar), temperature (in Kelvin) and transmitted power (in Watt). Data points are mean normalized Raman peak areas, error bars represent standard errors.

levels and thus the Raman Stokes intensity, the used normalization formula applies only for moderate changes in temperature. The normalized peak area  $A_{\text{norm}}$  was referred to the applied gas concentrations in the sensor calibration (Fig. 3) and used in the subsequent measurements to quantify simulated process gas compositions.

## Results and discussion

### Monitoring of fruit conservation chamber gases

Sensor calibration to oxygen and carbon dioxide was performed with precisely mixed test gases of varying concentrations. A concentration range of 1 to 5 percent was chosen, since this reflects  $\text{O}_2$  and  $\text{CO}_2$  levels in fruit conservation chambers. After evacuation of the fiber, test gases containing equal levels of oxygen and carbon dioxide (remainder nitrogen) were filled in the fiber up to a pressure of approx. 2.0 bar. The temperature of gases entering the fiber was approx. 22 degree Celsius. Measurement time for one spectrum was 60 seconds (30 seconds exposure time and 2 accumulations). Thus, monitoring of  $\text{O}_2$  and  $\text{CO}_2$  concentration levels with suitable time resolution is feasible. Gas mixtures were measured in triplicate and averaged. After each single measurement, the

HC-PCF and other gas-containing parts were evacuated. The vibrational band  $\nu_0$  at  $1556\text{ cm}^{-1}$  of oxygen and the Fermi dyad of carbon dioxide (vibrational bands  $\nu_1$  at  $1285$  and  $2\nu_2$  at  $1388\text{ cm}^{-1}$ ) were selected for concentration analysis. As sensor calibration for  $\text{O}_2$  and  $\text{CO}_2$  was done simultaneously in multi-gas mixtures containing  $\text{O}_2$ ,  $\text{CO}_2$  and  $\text{N}_2$ , the time needed to set the sensor up had been minimized.

The results (Fig. 3) show the linearity of the normalized Raman peak area *versus* the compound concentration, which can be used to quantify unknown gas compositions. Mean normalized peak areas along with the respective standard deviation were calculated based on triplicate measurements for every concentration value. In general, small standard deviations of the mean normalized Raman peak area of about 5 percent or lower were achieved for all established gas concentrations during the sensor calibration, only the mean peak area of the 3 percent  $\text{CO}_2$  measurement shows standard deviations of approx. 13 percent. Most likely, this was caused by small deteriorations of the gas feed line and will be quantified and corrected by using inert gaseous tracers in future experiments. However, coefficients of determination ( $R^2$ ) of more than 0.999 for all linear calibration functions indicate a stable sensor calibration. The standard deviation of the concentration was calculated according to the product specifications of the used mass flow controllers. Because of its higher Raman cross section, the calibration function of the  $\text{CO}_2$  band at  $1388\text{ cm}^{-1}$  provides a larger slope than the one from the band at  $1285\text{ cm}^{-1}$ . Highest sensitivity was reached for oxygen.

Several gas mixtures common for fruit conservation chambers were established and quantified with the Raman sensor (Table 1). Since  $\text{CO}_2$  concentrations of the applied gases were overdetermined by using both Raman bands of the Fermi dyad, the accuracy of the total carbon dioxide level in the gas samples can be further enhanced by combining their concentration values originating from individual calibration data. For all test gas concentrations, calculated concentration values are in good agreement with established ones, the average deviation is smaller than 1 percent with respect to the individual reference concentration.

Ammonia leakage in fruit conservation chambers can cause serious damage to humans and fruit. By evaluating the vibrational band of ammonia at  $3334\text{ cm}^{-1}$ ,<sup>42</sup> the Raman sensor could be used to monitor ammonia levels continuously and to detect potential leakages, such that immediate response is possible. Ammonia concentrations of 750 ppm (remainder  $\text{N}_2$ ) could be clearly detected (Fig. S2†). This concentration is suited for chemical alarm purposes,<sup>43</sup> since

**Table 1** Quantification of several gas mixtures common for conservation chambers (ULO – ultra low oxygen, LO – low oxygen). Concentration values are given in percent

Gas mixture	$\text{O}_2$ conc. reference	$\text{O}_2$ conc. measured	$\text{CO}_2$ conc. reference	$\text{CO}_2$ conc. measured	Conservation chamber type
1	1.50	1.53	1.50	1.52	ULO
2	2.00	2.00	3.00	2.91	LO
3	3.00	3.02	5.00	5.01	LO

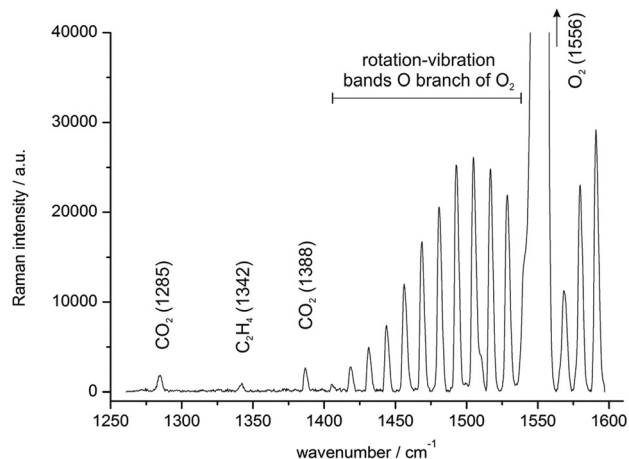


ammonia levels rise rapidly in case of leakage, and also higher concentrations up to percentage levels can be monitored without sensor re-calibration. Thus, all relevant process gases within standard ULO and LO fruit conservation chambers, namely  $O_2$ ,  $CO_2$  and  $NH_3$ , could be simultaneously monitored by the presented Raman sensor.

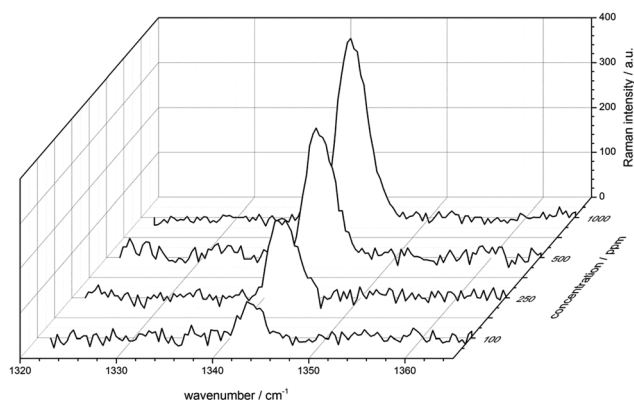
### Fruit ripening monitoring

Oxygen and carbon dioxide are important gaseous indicators also beyond conservation chambers. Since many fruits such as peaches, bananas, apples *etc.* are climacteric, their ripening is accompanied by a dramatic increase in respiration.<sup>44</sup> Thus, monitoring  $O_2$  and  $CO_2$  levels (fruit respiration) with the Raman gas sensor (see Fig. 3 and Table 1) could assess fruit ripening performance in ripening chambers.<sup>45</sup> Here, measuring the respiratory quotient (RQ) could yield auxiliary information about the ripening process, indicating pre-climacteric, climacteric or post-climacteric stages.<sup>46</sup> For instance,  $CO_2$  levels could rise approx. threefold during strawberry ripening under climacteric conditions.<sup>47</sup> Additionally, low carbon dioxide levels could indicate potential freeze damage, *e.g.* in oranges.<sup>48</sup>

However, ethylene plays the main role in fruit ripening as ripeness indicator and plant hormone as well. Thus, it is beneficial to monitor  $O_2$ ,  $CO_2$  and  $C_2H_4$  concentrations simultaneously during forced fruit ripening. Fig. 4 displays a derived Raman spectrum of 20%  $O_2$ , 500 ppm  $CO_2$  and 250 ppm  $C_2H_4$ , simulating a possible fruit chamber atmosphere. The gas composition was precisely mixed by mass flow controllers and the complete measurement time was



**Fig. 4** Background corrected Raman spectrum of a simulated fruit chamber atmosphere containing 20%  $O_2$ , 500 ppm  $CO_2$  and 250 ppm  $C_2H_4$  (remainder  $N_2$ ). Due to the high spectral resolution of the Raman sensor, carbon dioxide (1285 and 1388  $cm^{-1}$ ) and ethylene bands (1342  $cm^{-1}$ ) could be separated from the rotation–vibration bands of the O branch of the fundamental  $\nu_0$  vibration of oxygen (at wavenumbers approx. from 1405 to 1540  $cm^{-1}$ ) without any cross-sensitivity. The Q branch of  $O_2$  (1556  $cm^{-1}$ ) was cut off for better visualization. Only Raman bands with assigned wavenumbers were needed for the analysis of the aforementioned gases.



**Fig. 5** Overview of the Raman signals of the vibrational band  $\nu_3$  of ethylene (1342  $cm^{-1}$ ) at 100, 250, 500 and 1000 ppm (front to rear). Ethylene was measured in a multi-gas mixture together with  $O_2$ ,  $CO_2$  and  $N_2$ .

10 minutes. Most prominent are the vibrational band  $\nu_0$  of oxygen (Q branch at 1556  $cm^{-1}$ ) and its rotation–vibration bands in the O branch (with rotational quantum number  $J = 25$  at approx. 1405  $cm^{-1}$  up to 1540  $cm^{-1}$  for  $J = 1$ );<sup>49</sup> but due to the high spectral resolution of the Raman sensor, the carbon dioxide (Fermi dyad at 1285 and 1388  $cm^{-1}$ ) and ethylene signals ( $CH_2$  scissoring vibration  $\nu_3$  at 1342  $cm^{-1}$ ) could be clearly distinguished from the stronger oxygen peaks within just a single measurement. For quantification of oxygen levels, only the mean normalized Raman peak area of the vibrational band (Q branch) is needed. The results additionally demonstrate the Raman sensor's high dynamic range of about 4 orders of magnitude.

To demonstrate the Raman sensor's sensitivity, several ethylene concentrations were established and measured. Fig. 5 displays the evolution of the vibrational band of ethylene at 1342  $cm^{-1}$  from 100 ppm up to 1000 ppm (mixed with 20%  $O_2$ , 500 ppm  $CO_2$  and remainder  $N_2$ ). Plotted are the background corrected mean Raman spectra, exposure time was 10 minutes for each measurement. The signal-to-noise ratio for 100 ppm ethylene yielded 7.2. Thus, fiber enhanced Raman spectroscopy is a capable technique for simultaneously quantifying ethylene in a mixture together with the major atmospheric gases  $N_2$ ,  $O_2$  and  $CO_2$ .

## Conclusion and outlook

A versatile gas sensor setup for on-site process gas monitoring throughout the complete postharvest fruit production chain was developed. Utilizing a hollow-core photonic crystal fiber for analyte gas confinement and sensitivity enhancement, simultaneous quantification of  $O_2$ ,  $CO_2$ ,  $NH_3$  and  $C_2H_4$  without cross-sensitivity was feasible in just one single measurement. Laboratory test measurements showed the reliability of the sensor calibration and were in good agreement with expected reference gas concentrations. Suitable ethylene concentrations



to assess fruit ripening were detected, preventing fruit to decline into senescence (typically over 100 ppm). Using one single sensor for all relevant process gases has many benefits; it reduces costs and facilitates user training, improves comparability of measured values and eliminates most systematic errors involved in the analysis or makes these errors constant. It is shown that fiber enhanced Raman spectroscopic sensors have a potential to become versatile applicable on-site gas sensors for controlled atmosphere applications in postharvest fruit management.

## Acknowledgements

Funding of the research project by the Free State of Thuringia (Germany) and the European Union (EFRE) is highly acknowledged (FKZ: 2012 FGR 0013). We thank Di Yan for valuable support and advice during sensor build-up.

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