

Cite this: *Nanoscale*, 2015, 7, 11199

# Broadband laser polarization control with aligned carbon nanotubes†

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We introduce a simple approach to fabricate an aligned carbon nanotube (ACNT) device for broadband polarization control in fiber laser systems. The ACNT device was fabricated by pulling from as-fabricated vertically-aligned carbon nanotube arrays. Their anisotropic properties are confirmed with various microscopy techniques. The device was then integrated into fiber laser systems (at two technologically important wavelengths of 1 and 1.5  $\mu\text{m}$ ) for polarization control. We obtained a linearly-polarized light output with the maximum extinction ratio of  $\sim 12$  dB. The output polarization direction could be fully controlled by the ACNT alignment direction in both lasers. To the best of our knowledge, this is the first time that the ACNT device is applied to polarization control in laser systems. Our results exhibit that the ACNT device is a simple, low-cost, and broadband polarizer to control laser polarization dynamics, for various photonic applications (such as material processing, polarization diversity detection in communications etc.), where linear polarization control is necessary.

Received 25th March 2015,  
Accepted 26th May 2015

DOI: 10.1039/c5nr01904d

www.rsc.org/nanoscale

## 1. Introduction

Carbon nanotubes (CNTs)<sup>1</sup> have been extensively investigated due to their inherent physical properties (e.g., electrical,<sup>2</sup> optical,<sup>3</sup> and thermal<sup>4,5</sup> properties), which enable various applications such as electron field emitters,<sup>6</sup> quantum resistors,<sup>7</sup> transistors,<sup>8</sup> atomic force microscopes,<sup>9</sup> mechanical memory elements,<sup>10</sup> etc.<sup>11–15</sup> Noteworthy, CNTs have recently attracted huge attention for various photonic and optoelectronic applications<sup>2</sup> because of their unique optical properties, such as broadband optical absorption,<sup>16–18</sup> large optical nonlinearity,<sup>19</sup> ultrafast carrier relaxation time,<sup>20</sup> and high damage threshold.<sup>21</sup> One of the most successful examples

is a CNT-based saturable absorber,<sup>22,23</sup> which has been employed for ultrafast pulse generation in solid-state,<sup>24</sup> semiconductors,<sup>25</sup> waveguides,<sup>26</sup> and fiber lasers.<sup>27</sup>

Due to the unique structure confinement in one-dimension, aligned CNTs (ACNTs) have been demonstrated to facilitate a large range of applications (such as touch screens,<sup>28</sup> solar cells,<sup>29</sup> sensors,<sup>30</sup> supercapacitors,<sup>31</sup> thermal interface materials,<sup>32</sup> batteries,<sup>33</sup> infrared and THz sources/detectors,<sup>34–36</sup> and anisotropic saturable absorbers<sup>37,38</sup>), underscoring superior performance compared to their randomly oriented counterpart. In particular, ACNTs have strong optical anisotropic characteristics<sup>39,40</sup> that enable polarizer applications, with superior performance when compared to the conventional bulk polarizers (e.g., prisms and fiber Bragg grating (FBG)<sup>41,42</sup>), such as easy fabrication, broad operation bandwidth (from ultraviolet,<sup>18</sup> visible,<sup>43</sup> infrared<sup>44</sup> to THz range<sup>45,46</sup>), and a high extinction ratio (up to 30 dB<sup>44</sup>).

Laser polarization control is very crucial for a large range of photonic applications ranging from fluorescence imaging, liquid crystal device characterization and manufacturing, to laser material processing, polarization diversity detection in communications and range finding. In this paper, we introduce a simple technique to fabricate an ACNT device, by which broadband (at 1 and 1.5  $\mu\text{m}$ ) laser polarization dynamics is fully controlled after integration into fiber laser systems. The maximum extinction ratio of  $\sim 12$  dB is achieved. To the best of our knowledge, it is the first time that such an ACNT device is

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†Electronic supplementary information (ESI) available. See DOI: 10.1039/c5nr01904d

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applied to fiber laser systems for polarization control. Our study demonstrates the unique broadband performance of ACNTs for various photonic and optoelectronic applications.

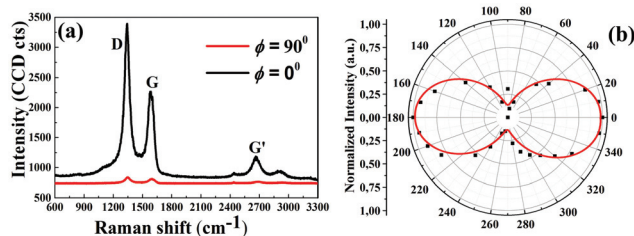
## 2. Fabrication and characterization of the ACNT device

The ACNT device was made by pulling out from a vertically-aligned CNT array,<sup>30</sup> and fabricated by the chemical vapour deposition method.<sup>47</sup> Then the ACNT film was directly transferred onto the surface of a quartz substrate (as shown in Fig. 1(a) after inserting into a mirror mount). Note that our direct-dry transfer fabrication method is also compatible to other photonic devices (*e.g.*, fibers and silicon devices).

In order to characterize the alignment performance, various microscopy techniques were utilized, such as optical microscopy (Fig. 1(b)), and scanning electron microscopy (SEM, Fig. 1(c)). As shown in the figure, CNT arrays were highly-aligned along the pulling direction. The diameter of the CNTs was measured to be  $\sim 5$  nm by transmission electron microscopy (TEM, Fig. 1(d)). It denotes that our sample consists typically of few-walled CNTs.

In order to achieve the best polarization performance, we optimize the output performance with different film thicknesses (from  $\sim 100$  nm to  $\sim 300$  nm), shown in Fig. S1 of the ESI.† We find that thicker samples give better performance, and the output performance (*e.g.*, extinction ratio (ER)) saturates when the thickness is  $\sim 300$  nm. Therefore, an  $\sim 300$  nm ACNT film is selected in our experiment.

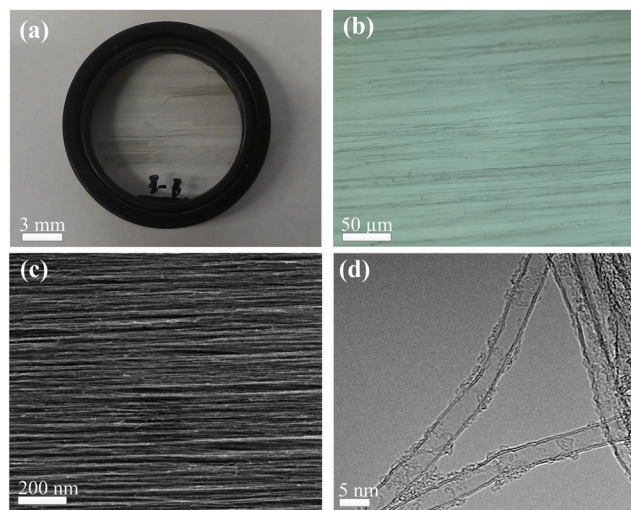
For ACNTs, their Raman scattering intensity varies with different excitation polarization directions. In our experiment, a polarized Raman spectroscopy (WITec Alpha 300 RA) was utilized to characterize the anisotropic properties of the ACNT samples. Polarized Raman spectra were obtained by changing



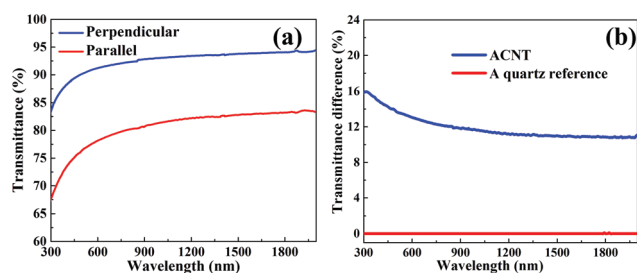
**Fig. 2** (a) Polarized Raman spectra of the ACNT device, (b) G-peak Raman intensity as a function of the angle, and the red line depicts the fitting result with the equation. The excitation laser wavelength is 532 nm.

the input polarization direction ( $\phi$ ) of the excitation laser from  $0^\circ$  to  $360^\circ$  with respect to the CNT alignment direction. When  $\phi = 0^\circ$  and  $\phi = 90^\circ$ , the incident excitation polarization direction is parallel and perpendicular to the ACNT alignment direction, respectively. Typical Raman spectra (Fig. 2(a)) shows three dominating features, namely D, G, and G' modes, as typically observed for few-walled carbon nanotubes.<sup>48,49</sup> It has been reported that the G-band of Raman modes at around  $1580\text{ cm}^{-1}$  is highly sensitive to CNT alignment.<sup>48</sup> When we change the angle  $\phi$ , the intensity of the G-peak and D-peak changes from the maximum (at  $\phi = 0^\circ$ ) to the minimum (at  $\phi = 90^\circ$ ), which is in accordance with the polarized absorbance of the aligned carbon nanotube.<sup>50,51</sup> The ratio between the maximum and the minimum intensity is  $\sim 22$ . In our study, the G-peak intensity at different angles  $\phi$  is presented in Fig. 2(b). It indicates that the Raman scattering intensity of ACNTs is sensitive to the polarization direction of the pump light, which is in good agreement with the equation:  $I(\phi) \propto \cos^2(\phi)$ <sup>48</sup> for ACNTs. Such anisotropic Raman properties clearly show that CNTs are well aligned.

Fig. 3(a) shows the polarized transmittance of our ACNT device in the two orthogonal directions (*i.e.*, when the polarization direction of the input light is parallel or perpendicular to the CNT alignment direction), which is measured by polarized absorption spectroscopy. When the incident light polarization is perpendicular to the ACNT alignment direction, the trans-



**Fig. 1** (a) Our ACNT device on a 1-inch quartz substrate, (b) its optical microscopy image, (c) SEM image and (d) TEM image.



**Fig. 3** (a) Polarized transmittance of the ACNT device with the aligned direction parallel and perpendicular to the polarization direction of the incident light source, respectively. (b) The transmittance difference in the two orthogonal directions for the ACNT device and a pure quartz reference.



mittance is  $\sim 94\%$  at  $1.8\ \mu\text{m}$ , which is mainly attributed to the Fresnel loss ( $\sim 6\%$ ) of the quartz substrate. While for the parallel polarization light input, the transmittance is  $\sim 82\%$  at  $1.8\ \mu\text{m}$ . The result identifies the optical anisotropic absorption of our CNT device. The difference between two orthogonal directions is  $\sim 12\%$  at  $1.8\ \mu\text{m}$  ( $\sim 16\%$  at  $300\ \text{nm}$ , as shown in Fig. 3(b)), which is comparable to the typical performance reported for aligned carbon nanotubes (from  $15\%$  to  $20\%$  at different wavelengths<sup>43,44</sup>). Note that the transmittance difference remains almost constant from  $1$  to  $2\ \mu\text{m}$ , which shows the unique broad operation bandwidth of our device. For comparison, the transmittance difference at parallel and perpendicular directions of a pure quartz reference sample ( $3\ \text{mm}$  thick) was also tested. The result shows that the anisotropic absorption of our ACNT device is merely attributed to the ACNTs.

### 3. Laser setup

To utilize the broadband anisotropic characteristics of the ACNT device, fiber lasers operating at  $1$  and  $1.5\ \mu\text{m}$  were designed with identical layout (Fig. 4(a)). In the fiber laser at  $1.5\ \mu\text{m}$ : a  $1\ \text{m}$  erbium doped (Er-doped) fiber worked as the gain fiber, a wavelength division multiplexer (WDM) was used to couple the pump laser ( $980\ \text{nm}$  laser diode (LD)) into the gain fiber, the ACNT device was inserted inside a fiber-collimator based U-bench to modulate the intra-cavity polarization state, a high-reflectivity fiber based mirror (made by a  $3\ \text{dB}$  coupler as a nonlinear optical loop mirror) was provided for laser feedback, while a fiber coupler with  $20\%$  coupling ratio outputted the laser from the cavity for measurement. In the

$1\ \mu\text{m}$  fiber laser: the gain fiber was replaced by a  $0.5\ \text{m}$  ytterbium doped (Yb-doped) fiber, and other components (*e.g.*, WDM, LD, and coupler) with the same function were selected at  $1\ \mu\text{m}$ . In both laser systems, all fiber components were polarization independent, indicating no intra-cavity polarization preference without ACNTs.

An optical spectrum analyser (Hewlett Packard, 86140A) was utilized to measure the laser output spectrum. A polarization analyser (*i.e.*, a linear polarizer) mounted in a high-precision rotator was fixed after the output coupler, as illustrated in Fig. 4(b), to characterize the laser polarization output performance. By rotating the angle (marked as  $\varphi$  in Fig. 4(b)) between the axis (white line in Fig. 4(b)) of the polarization analyzer and the vertical direction (dotted line) from  $0^\circ$  to  $360^\circ$ , the power of the output laser beam after passing through the polarization analyzer was monitored by a power meter (OPHIR Nova II) to characterize the output polarization state.

### 4. Polarization control: results and discussions

#### 4.1 $1.5\ \mu\text{m}$ Er-doped fiber laser (EDFL)

In EDFL, continuous wave output performance was studied with a reference pure quartz substrate or with our ACNT device in the U-bench (Fig. 4(a)). Fig. 5(a) shows the typical output optical spectrum, identical for both cases (with the quartz reference and the ACNT device). The peak wavelength is  $\sim 1561\ \text{nm}$  with the full width at half maximum (FWHM) of  $0.1\ \text{nm}$ , a typical value for such an erbium-doped fiber laser

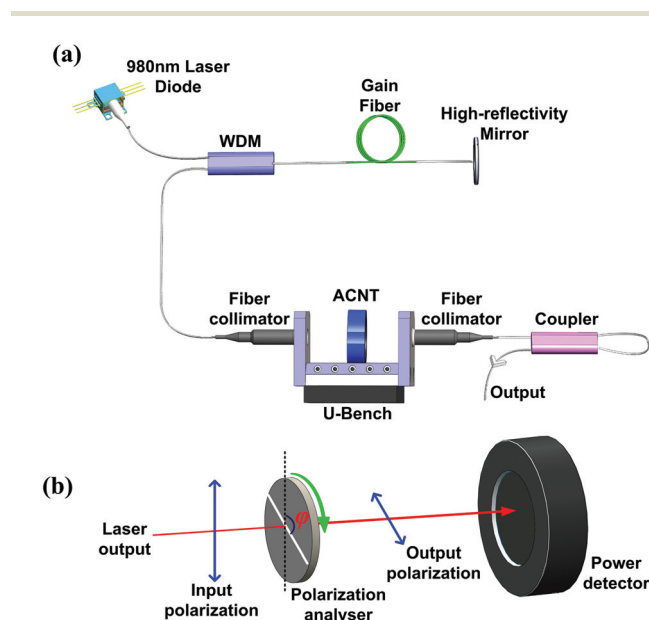


Fig. 4 (a) Fiber laser setup for both  $1$  and  $1.5\ \mu\text{m}$  laser systems, (b) laser polarization performance characterization system.

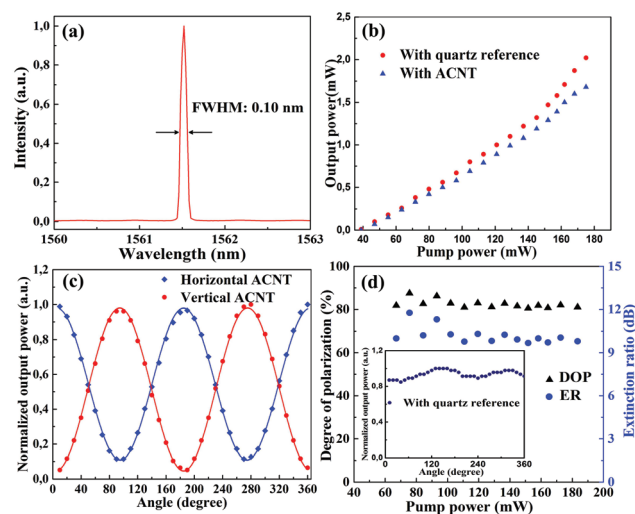


Fig. 5 Experimental results at  $1.5\ \mu\text{m}$ : (a) output spectrum, (b) output power as a function of pump power (with the quartz reference and our ACNT device), (c) normalized output power as a function of polarization analyser angle of our ACNT laser output, and the cosine function fitting of the experimental data. (d) DOP and ER versus pump power, and the inset figure is the normalized output power of the laser with a quartz reference as a function of polarization analyser angle.



without mode-selection. The output power as a function of the pump power is shown in Fig. 5(b). The output power presents linear characteristics for both situations, while the slope efficiency decreased when the ACNT device was inserted. It is because the ACNT device in the cavity also introduces additional small attenuation to the laser cavity. The laser threshold of pump power was  $\sim 34$  mW. The maximum output power decreased from  $\sim 2.0$  to  $\sim 1.6$  mW under the highest pump power of  $\sim 180$  mW (the maximum output power from the laser diode), after replacing the quartz reference with the ACNT device in the cavity. Further increase of the laser output power is possible, as the output power linearly increases with the pump power with no sign of saturation.

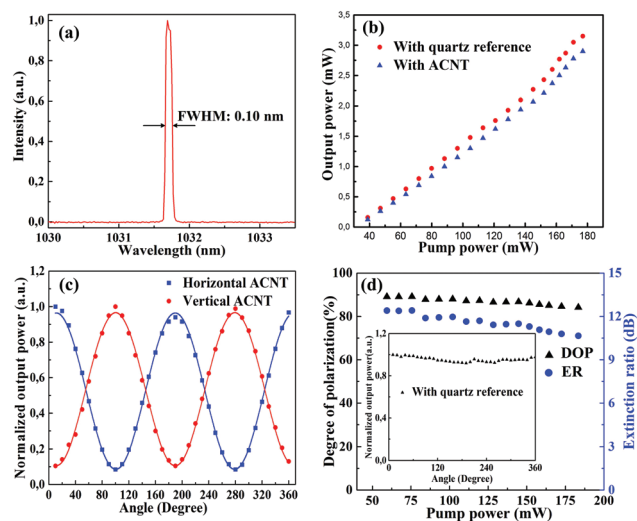
To investigate the polarization dynamics of our ACNT device in the laser resonator, we experimentally measured the laser output power after the polarization analyzer, as shown in Fig. 4(b). At first, we inserted the ACNT device into the laser resonator and fixed the alignment direction of ACNT vertical to the horizontal plane in the free space, without changing any experimental conditions. After that, the output laser power after the polarization analyzer was recorded by changing the angle  $\varphi$  (shown in Fig. 4(b)) from  $0^\circ$  to  $360^\circ$ . The experimental results are illustrated in Fig. 5(c), fitted well with the cosine function, *i.e.*, the minimum output power was close to zero at the angle  $\varphi$  of  $0^\circ$ , while the maximum power was located at the angle  $\varphi$  of  $90^\circ$ . It shows that the output polarization of the laser was changed from the random-polarization state to the linear-polarization state, after insertion of our ACNT device into the laser cavity. In order to fully study the performance of intra-cavity polarization control of the ACNT device, the CNT alignment direction was rotated from vertical to horizontal orientation for comparison. The corresponding results are also shown in Fig. 5(c). It is observed that the whole curve shifts  $90^\circ$  when compared to the one with the vertical placement case of the ACNT device. The result suggests that the laser output with the ACNT device was linearly-polarized, and the polarization direction rotates with the rotation of the ACNT device. This shows that the polarization state of our laser output can be simply controlled by rotating the intra-cavity ACNT device. Fig. 5(d) summarizes the degree of polarization (DOP) and ER of our ACNT laser *versus* pump power. The DOP and ER are defined as  $\text{DOP} = (P_{\max} - P_{\min}) / (P_{\max} + P_{\min})$ ,  $\text{ER} = P_{\max} / P_{\min}$ , where  $P_{\max}$  and  $P_{\min}$  are the maximum and minimum output power given by the measured results shown in Fig. 5(c). The maximum DOP of our ACNT laser is 87.5% at the pump power of  $\sim 75$  mW, 10-time higher than the DOP of the laser with the quartz reference ( $\sim 8\%$ , as shown in the inset of Fig. 5(d)). The corresponding ER of our ACNT laser is  $\sim 12$  dB, around 8-time higher than the value of the laser with the quartz reference ( $\sim 1.5$  dB). The ER is  $\sim 9.8$  dB (with 81% of DOP) at the maximum output power of 1.6 mW. The DOP and ER performance is pretty unchanging when the pump power is high ( $>100$  mW). This is because the anisotropic absorption of ACNT dominates the laser output polarization performance at the high pump power. No performance degradation is observed during the 1.5 hours experiment. We also carry out

the same polarization control experiment with a traditional prism based polarizer (Thorlabs, GL10) for comparison. The comparison of results are given in Fig. S2 of the ESI,<sup>†</sup> which shows that the polarization performance of our ACNT laser is comparable ( $\sim 8\%$  difference) to the laser using the traditional prism based polarizer. It is worth noting that our ACNT fabrication method is compatible to other photonic devices (*e.g.*, fibers and silicon devices), which can offer huge flexibility to be integrated into various photonic platforms (*e.g.*, waveguides) for a large range of photonic applications.

#### 4.2 $1\ \mu\text{m}$ Yb-doped fiber laser (YDFL)

In our ACNT based YDFL, the output spectrum is shown in Fig. 6(a). The peak wavelength is  $\sim 1032$  nm with FWHM of  $\sim 0.1$  nm, typical for an YDFL without any wavelength selection component in the cavity. The spectrum is similar to the laser system with a pure quartz reference. Fig. 6(b) illustrates the results of laser output power under the same conditions with the quartz reference and our ACNT device. The threshold for the laser system with ACNT (27 mW) was slightly higher than that (24 mW) with the quartz reference. With the increase of the pump power, the output power increased linearly. The highest output power for the laser with the quartz reference is  $\sim 3.2$  mW, while for the laser with the ACNT device, the output power is  $\sim 2.75$  mW.

Fig. 6(c) presents the polarization control results of our  $1\ \mu\text{m}$  YDFL with the ACNT device. Similar to the EDFL experiment, we firstly inserted the ACNT device into the resonator, and used the experimental procedures (identical to what we



**Fig. 6** Experimental results at  $1\ \mu\text{m}$ : (a) output spectrum, (b) output power as a function of pump power (with the quartz reference and our ACNT device), (c) normalized output power as a function of angle with the polarization analyser, and the cosine function fitting of the experimental data, (d) DOP and ER *versus* pump power, and the inset figure is the normalized output power of the laser with the quartz reference as a function of polarization analyser angle when the laser is with the quartz reference.



employed in EDFL) to study the polarization state of the laser output. The result is shown in Fig. 6(c). As expected, the output of our laser with ACNT became linearly polarized, and the polarization state can be controlled by the rotation of the ACNT alignment direction. After that, we also measured the laser output power change after the polarization analyzer with the quartz reference, as illustrated in the inset figure of Fig. 6 (d). The output power remains almost unvarying with a fluctuation of  $\sim 5.8\%$ , which indicates that the output of our laser with the quartz reference is randomly-polarized, similar to what we observed with the laser working at  $1.5\ \mu\text{m}$ . Fig. 6(d) summarizes the DOP and ER *versus* pump power. The DOP reaches  $\sim 89\%$  at the pump power of  $59.4\ \text{mW}$  (in contrast to the DOP of  $2.9\%$  with the quartz reference in the laser cavity). It decreased slightly as we increased the pump power, which also confirms good polarization dynamics control of our  $1\ \mu\text{m}$  fiber laser with the ACNT device. The maximum ER is  $\sim 12.4\ \text{dB}$ , comparable to the result achieved with the EDFL. Similarly, we conducted the polarization control experiment with a prism based polarizer (Thorlabs, GL10) for comparison, depicted in the ESI Fig. S2.† The result illustrates that the polarization performance of our ACNT laser is comparable ( $\sim 7\%$  difference) to the one using the traditional prism based polarizer and also these were typically published with FBGs (*e.g.*, ER of  $15\ \text{dB}^{42}$ ). We also did not observe any device damage during our experiment.

## 5. Conclusions

We introduce a simple method to fabricate an ACNT device for broadband polarization control in laser systems (at  $1$  and  $1.5\ \mu\text{m}$ ). The anisotropic properties of ACNTs were confirmed with various characterization methods (*e.g.*, optical microscopy, SEM, and Raman spectroscopy). By integrating the ACNT device into the fiber laser system, we obtained a linearly-polarized light output with DOP up to  $89.1\%$  and  $87.5\%$  with the corresponding ER of  $12.4$  and  $\sim 12\ \text{dB}$  in  $1$  and  $1.5\ \mu\text{m}$  laser systems, respectively. Our experimental results exhibit that the ACNT device can be potentially employed as a polarization controller for a broad range of photonic applications (nonlinear frequency conversion,<sup>52,53</sup> beam combination,<sup>54</sup> material processing, polarization diversity detection in communications *etc.*), where linear polarization output is required.

## Author contribution

Z. S., H. Y., B. F. and D. L. conceived and designed the laser experiments. Z. S., Y. T., Y. C., and M.M. performed the characterization experiments. Z. Y. and Q. L. fabricated the ACNT device. R. L. performed the TEM measurement; A. H. performed the sample thickness measurement with AFM. I. T., Z. R., J. B., Q. L., E. K., H. L., and Z. S coordinated the experiments. All authors contributed to the writing of the manuscript and to the discussion.

## Acknowledgements

The authors acknowledge funding from Teknologiaateollisuus TT-100, Academy of Finland (grants: 276160, 276376, 284548, 285972), the European Union's Seventh Framework Programme (REA grant agreement No. 631610), the National Natural Science Foundation of China (grants: 61377039, 61177059), the China Scholarship Council, and Aalto University (Finland). The authors also thank the provision of facilities and technical support by Aalto University at the Micronova Nanofabrication Centre.

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