

# Long-chain aliphatic polyesters from plant oils for injection molding, film extrusion and electrospinning†

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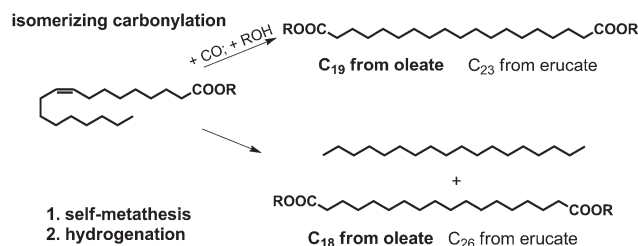
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## Introduction

Dicarboxylic acids derived from plant oils are attractive intermediates for the synthesis of polymer materials.<sup>1</sup> Similar to polyethylene, the incorporation of long methylene sequences enables polymer crystallization and renders polyesters hydrophobic. Long-chain aliphatic polyesters that incorporate the full length of the plant oil methylene sequences possess high melting points ( $T_m > 100$  °C) and crystallization temperatures, suitable for thermoplastic processing. This differs from shorter chain analogs. Here, the incorporation of aromatic comonomers such as terephthalic acid is required in order to improve dimensional stability, heat distortion temperature and mechanical properties of aliphatic polyesters.<sup>2</sup>

More recently, entirely chemical catalytic conversions of plant oils have complemented the existing approach of bio-

The polycondensation of long-chain  $\alpha,\omega$ -diesters with long-chain  $\alpha,\omega$ -diols, prepared by means of catalytic conversion of plant oils, affords linear aliphatic polyesters. They contain both long crystallizable polyethylene-like hydrocarbon segments and ester moieties in the backbone. In a convenient catalytic one-step process a high-purity polycondensation grade dimethyl-1,19-nonadecanedioate monomer is obtained directly from the technical grade methyl ester of high oleic sunflower oil. Likewise, dimethyl-1,23-tricosanedioate is derived from methyl erucate. The successful scale-up renders both intermediates available on a 100 g scale. Injection molded parts of polyester-19.19 and -23.23 with a number average molecular mass of  $M_n = 3 \times 10^4$  g mol<sup>-1</sup> possess an elongation at break of >600% and a Young's modulus of 400 MPa. Electrospinning produces non-woven meshes. The polyesters prepared even enable film extrusion and represent new blend components for a variety of thermoplastics including polyethylene.



**Scheme 1** Main products of the isomerizing carbonylation and self-metathesis, respectively, of unsaturated fatty acid esters.

technological  $\omega$ -oxidation as a route to long-chain aliphatic monomers.<sup>3,4</sup>

Self-metathesis<sup>5–9</sup> generates (after subsequent double bond hydrogenation) a long-chain  $\alpha,\omega$ -diacid ester along with a stoichiometric amount of linear hydrocarbon as the main products (Scheme 1). In this context, the implementation of a commercial-scale refining of palm oil to chemicals by metathesis with 1-butene is notable.<sup>10,11</sup> Due to the specifics of the process and of olefin metathesis in general, a significant amount of self-metathesis will occur as a side reaction to yield 1,18-octadecene dioate.<sup>12</sup>

A different route has recently been found with isomerizing alkoxy carbonylation (Scheme 1).<sup>13–15</sup> Other than metathesis, the long-chain methylene sequence of the fatty acid feedstock is fully incorporated into the  $\alpha,\omega$ -diacid ester product. This is a result of the highly kinetically controlled outcome of the isomerizing carbonylation reaction *vs.* the equilibrium product distribution from metathesis.<sup>16</sup>

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Polycondensation reactions are well established and used widely in industry for the synthesis of, amongst others, polyesters. Nonetheless, obtaining sufficient molecular weight for achieving entanglement and mechanical strength is not trivial for a given set of monomers. Typically, polyester molecular weights are in the range of  $10^4$  to  $5 \times 10^4$  g mol<sup>-1</sup> in order to prevent embrittlement and premature mechanical failure on straining. Molecular weights of polyesters or polyamides prepared by step-growth polycondensation are highly sensitive to the presence of impurities and require a high purity and accurate stoichiometry of difunctional monomers. Obtaining a material with useful mechanical properties from a new type of monomer is always precarious, and there is no generic protocol. For example, most A<sub>2</sub> + B<sub>2</sub> syntheses of polyester materials employ a diol which is volatile to a relevant extent under polycondensation conditions such that it can be used in excess in the initial reaction mixture. This does not apply to the polyesters studied here. Due to these and other general limitations only little is known about the materials properties of such entirely long-chain aliphatic polyesters based on symmetric  $\alpha,\omega$ -functionalized monomers. We now report on the mechanical properties and processing including blending of recently reported<sup>14,15</sup> entirely aliphatic semicrystalline polyesters based on linear long-chain dicarboxylic acids and diols.

## Results and discussion

### Monomer and polymer synthesis

As an access to long-chain linear aliphatic diesters and diols, we utilized isomerizing alkoxycarbonylation. High oleic sunflower oil methyl ester (Dakolub MB9001) or technical grade methyl erucate, respectively, was used as a starting material. A well-defined catalyst precursor, [1,2-bis((di-*tert*-butylphosphino)methyl)benzene palladium ditriflate],<sup>15</sup> was employed. It is significantly more efficient in comparison with catalysts obtained by mixing a palladium source and the diphosphine *in situ*, which require a five-fold excess of the diphosphine.<sup>17,18</sup> As a prerequisite for the studies of polyesters reported here, this monomer synthesis was investigated on an enhanced scale in a 1 L pressure reactor (Table 1). No adverse effects on productivity, selectivity or product purity vs. smaller scale syntheses<sup>15</sup> were observed. Upon crystallization from methanol, used as the reaction medium, the linear C<sub>19</sub> and C<sub>23</sub>

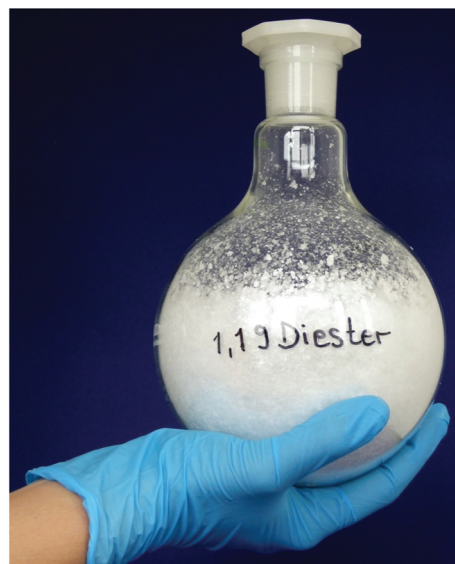


Fig. 1 Photograph of dimethyl 1,19-nonadecanedioate as obtained from entry 1, Table 1.

diesters were obtained on a 100 g scale in >99% purity (Fig. 1). The residual filtrate predominantly consists of (isomerized) starting material and in principle can be reused again. Even the  $\alpha,\beta$ -unsaturated carbonyl compounds which represent the most stable isomer can be reacted to the desired linear products.<sup>13</sup>

Long-chain  $\alpha,\omega$ -diol monomers were generated by reduction of the aforementioned diesters, stoichiometrically with LiAlH<sub>4</sub> or by catalytic hydrogenation with Saudan's<sup>19</sup> ruthenium catalyst. Previous work by our laboratory demonstrated that polycondensation of stoichiometric amounts of these difunctional A<sub>2</sub> + B<sub>2</sub> monomers catalyzed by titanium alkoxides afforded the corresponding long-chain aliphatic polyesters, namely poly[1,19-nonadecadiyl-1,19-nonadecanedioate] (PE-19.19) and poly[1,23-tricosadiyl-1,23-tricosanedioate] (PE-23.23).<sup>14</sup> In order to elucidate the polyesters' materials properties, increased quantities of polymer were required. Thus polymerizations were typically performed on a scale of 20 mmol of either monomer, affording between 10 and 15 g of polyester (Table 2).§ Optimized reaction conditions essentially comprised 0.04 mol% of Ti(OBu)<sub>4</sub> and stirring for 16 hours at 200 °C and 0.01 mbar with a helicon stirrer (*cf.* Experimental section). Polymerization under these conditions and on this scale yielded polyesters with a number average molecular weight of  $M_n$   $3.0 \times 10^4$  g mol<sup>-1</sup> as determined by both <sup>1</sup>H-NMR quantification of end-groups and high temperature size exclusion chromatography (SEC) relative to polyethylene standards. In view of the largely polyethylene-like character of the polymer chains, SEC vs. polyethylene standards appears most appropriate in comparison with other common standards.

§ For polyester-19.19 prepared on a larger scale of 50 mmol, essentially identical molecular weights and tensile properties were observed.

Table 1 Monomer synthesis by isomerizing alkoxycarbonylation<sup>a</sup>

| Entry | Substrate      | Conversion <sup>b</sup> | Selectivity <sup>b</sup> | Isolated yield of pure product |
|-------|----------------|-------------------------|--------------------------|--------------------------------|
| 1     | Methyl oleate  | 89%                     | 89%                      | 115 g (76%)                    |
| 2     | Methyl erucate | 72%                     | 84%                      | 96 g (54%)                     |

<sup>a</sup> Conditions: 430 mmol substrate, 0.86 mmol [(dtbpx)Pd(OTf)<sub>2</sub>] (dtbpx = 1,2-bis((di-*tert*-butylphosphino)methyl)benzene), 550 mL MeOH, 20 bar CO, 90 °C, 120 h. <sup>b</sup> Determined by GC analysis of the crude reaction mixture.



Table 2 Polycondensation to polyesters

|          | $T_m^a/^\circ\text{C}$ | $T_c^a/^\circ\text{C}$ | $M_{n,\text{NMR}}^b/\text{g mol}^{-1}$ | $M_{n,\text{GPC}}^c/\text{g mol}^{-1}$ | $M_w/M_n^c$ |
|----------|------------------------|------------------------|--|--|-------------|
| PE-19.19 | 102                    | 83                     | $2.9 \times 10^4$                      | $3.0 \times 10^4$                      | 2.6         |
| PE-23.23 | 107                    | 86                     | $3.9 \times 10^4$                      | $3.9 \times 10^4$                      | 2.4         |

<sup>a</sup> Determined by DSC with a heating/cooling rate of  $10 \text{ K min}^{-1}$ .

<sup>b</sup> Determined by end-group analysis from  $^1\text{H}$  NMR spectroscopy. <sup>c</sup> GPC at  $160^\circ\text{C}$  in trichlorobenzene versus polyethylene standards.

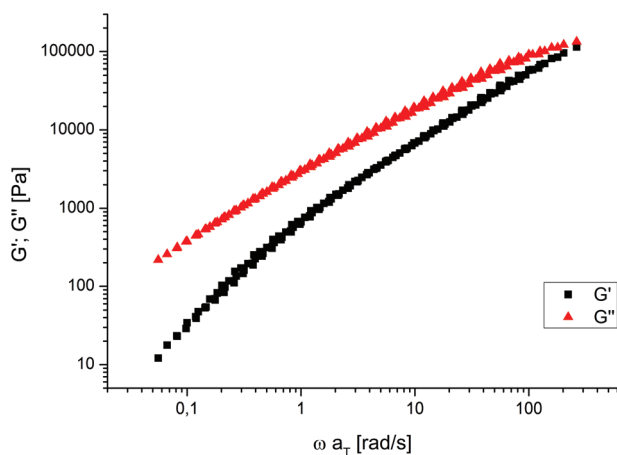


Fig. 2 Master curves of  $G'$  and  $G''$  for PE-19.19 (from measurements at  $130, 140, 150, 160$  and  $170^\circ\text{C}$ ). Shifting temperature:  $150^\circ\text{C}$ .

In view of melt processing, required amongst others for the preparation of samples for tensile testing (*vide infra*), it is worth noting that the polyesters prepared display a simple rheological behavior (Fig. 2 and ESI†). The storage modulus ( $G'$ ) and loss modulus ( $G''$ ) can be superimposed only by horizontal shifts along the frequency axis.<sup>20</sup> This shows that no undesired chemical or physical changes occur in the melt, such as changes of molecular weight by degradation, further reactions of end-groups, or crosslinking.

### Tensile properties

Concerning the mechanical properties of long-chain  $A_2B_2$ -type polyesters, Cho *et al.* investigated polyester-30,30 from polycondensation of diethyl-1,30-tricontanedioate and tricontane-1,30-diol.<sup>21</sup> However, an elongation at break of only 5% was found, indicating that the molecular weight of the material was likely insufficient to enable effective chain entanglement.

For tensile testing of PE-19.19 and -23.23 generated by the above protocol, dumbbell test specimens were obtained by injection molding using a mini-compounder (Experimental section and ESI†).

Following a linear and nonlinear viscoelasticity regime (I), a neck region with strain softening (II) and plastic flow (III), strain hardening (IV) is also observed as concluded from the characteristic changes of slope in the stress-strain curves (Fig. 3 and ESI†).<sup>22</sup> That is, the polyesters prepared clearly

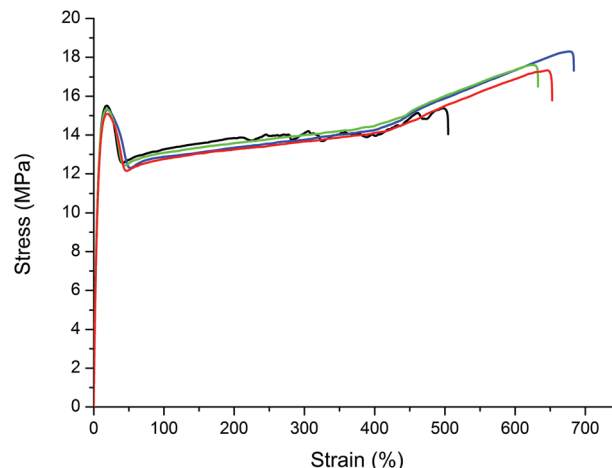


Fig. 3 Stress-strain curves of PE-19.19.

Table 3 Tensile properties (Young's modulus, yield stress, yield strain, tensile stress at break and tensile strain at break) of polyesters<sup>a</sup>

|          | Young's modulus [MPa] | Yield stress [MPa] | Yield strain [%] | Tensile stress at break [MPa] | Tensile strain at break [%] |
|----------|-----------------------|--------------------|------------------|-------------------------------|-----------------------------|
| PE-19.19 | 408                   | 15.3               | 18.3             | 15.9                          | 619                         |
| PE-23.23 | 436                   | 16.7               | 19.7             | 17.0                          | 678                         |

<sup>a</sup> True stress at break calculated after cross-section area correction.

show typical properties of a polymeric material rather than a brittle wax-like behavior.

Both polyesters show Young's moduli around 400 MPa and an elongation at break of more than 600% (Table 3). In detail, PE-23.23 displays a slightly higher modulus *vs.* PE-19.19, as expected due to the higher crystallinity<sup>14</sup> arising from the longer methylene sequences. These tensile properties are similar to those of polyesters  $[\text{O}(\text{CH}_2)_n\text{C}(\text{O})]_x$  generated by ring opening chain growth polymerization of naturally occurring pentadecalactone ( $n = 15$ )<sup>23–25</sup> or AB-polycondensation of 14-hydroxytetradecane carboxylic acid from enzymatic  $\omega$ -hydroxylation of myristic acid ( $n = 14$ ).<sup>26</sup> By comparison, high density polyethylene (HDPE) from linear insertion chain growth typically displays a Young's modulus of *ca.* 1 GPa.<sup>27</sup>

Shore D hardness increases with increasing chain length of the repeat units' hydrocarbon segments from 54 for PE-19.19 to 56 for PE-23.23. This approaches the hardness of 60 to 70 reported for HDPE.<sup>28</sup>

Major application areas for conventional polyethylene particularly in the food sector are packaging materials. For this application, low density polyethylene is blow molded or extruded to produce films. As shown in Fig. 4, both PE-19.19 and PE-23.23 were successfully extruded by means of a twin-screw mini-extruder to produce films. This is quite remarkable as film breaking during extrusion is a frequently encountered problem. Apparently, the combination of melt stability (viscosity) and solidification behaviour is sufficient here. With





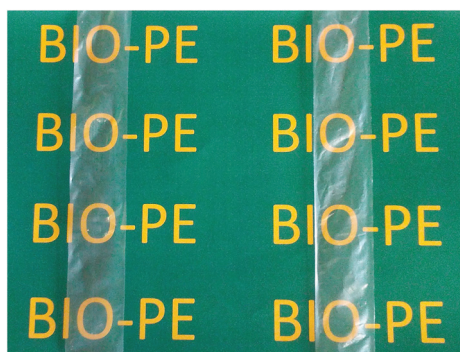


Fig. 4 Photograph of melt-extruded films of PE-19.19 (left) and PE-23.23 (right).

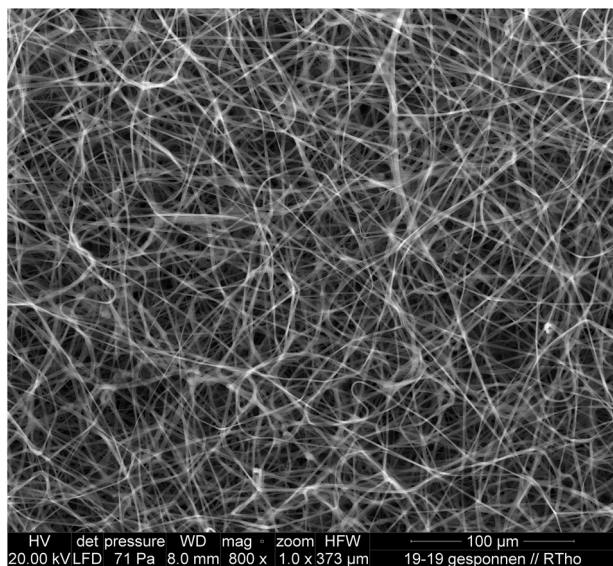


Fig. 5 SEM image of electrospun PE-19.19 fibers.

an average film thickness of 60 microns, they showed little opacity (Fig. 4). Hence, applications such as bio-based packaging films and bags appear feasible.

Applications of thermoplastics in such diverse areas as clothing textiles and filters require non-wovens. To this end, a further preliminary insight into processing beyond the injection molding of samples for tensile testing was provided by electrospinning. Spinning from a pre-heated 7.5 wt% solution which was stabilized with 1 wt% ( $\pm$ )- $\alpha$ -tocopherol in 1,1,2,2-tetrachloroethane $\ddagger$  yielded non-woven meshes of polyester-19,19 fibers with average diameters on the order of a few microns (Fig. 5).

$\ddagger$ Electrospinning from more environmentally benign non-chlorinated solvent such as decaline may be possible. However, this requires higher temperatures to ensure solubility of the polymer, not accessible with the electrospinning setup available.

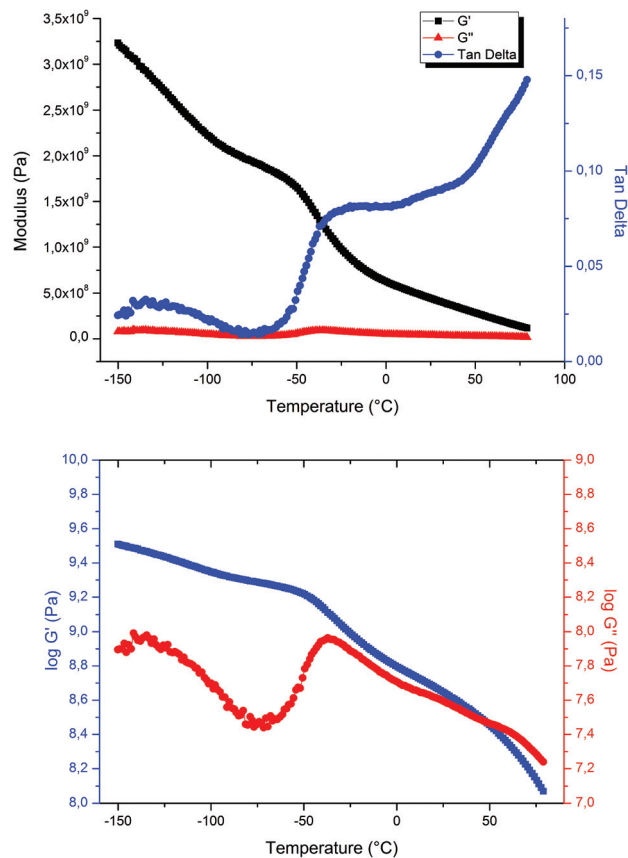


Fig. 6 Dynamic mechanical analysis of PE-19.19.

### Dynamic mechanical analysis (DMA)

As a result of the high degree of crystallinity ( $\chi$ ) of about 70% for PE-19.19 and 75% for PE-23.23 as determined by wide-angle X-ray scattering,<sup>14</sup> even upon rapid cooling or heating in DSC no glass transitions could be observed reliably due to the small portion of amorphous polymer subject to vitrification or softening, respectively. Dynamic mechanical analyses (DMA, at a frequency of 1 Hz) were more conclusive to this end. For PE-19.19 from the loss modulus *vs.* temperature a  $T_g$  of  $-37^\circ\text{C}$  was observed (Fig. 6). The longer-chain aliphatic polyester PE-23.23 exhibits a slightly higher glass-transition temperature of  $-27^\circ\text{C}$  (*cf.* ESI $^\dagger$ ). This difference can be ascribed to the enhanced crystallinity due to the longer methylene sequences and the resulting stronger restriction in mobility.<sup>29</sup> ||

Besides the relaxation due to the glass transition, both polymers show a second relaxation phenomenon at around  $-130^\circ\text{C}$ , which can be ascribed to the motion of the methylene sequences of the polyester main chain.<sup>30,31</sup>

### Polyester melt compounding

Polymer blends offer the opportunity to expand the property profiles of polymeric materials. In fact, when appropriate com-

|| For poly( $\omega$ -hydroxyl tetradecanoic acid) (PE-14) a  $T_g$  of  $-30^\circ\text{C}$  has been reported,<sup>26</sup> and for poly( $\omega$ -pentadecalactone) (PE-15) a  $T_g$  of  $-27^\circ\text{C}$ .<sup>31</sup>



Table 4 Thermo-mechanical properties of talcum-filled polyesters

|          | Filler content/<br>wt% | $T_m^a$ /<br>°C | $T_c^a$ /<br>°C | $G'$ (RT) <sup>b</sup> /<br>MPa | $G''$ (RT) <sup>b</sup> /<br>MPa |
|----------|------------------------|-----------------|-----------------|---------------------------------|----------------------------------|
| PE-19.19 | 0                      | 102             | 83              | 1100                            | 84                               |
| PE-19.19 | 25                     | 108             | 87              | 1510                            | 130                              |
| PE-19.19 | 45                     | 107             | 88              | 1908                            | 180                              |
| PE-23.23 | 0                      | 107             | 86              | 880                             | 60                               |
| PE-23.23 | 25                     | 108             | 91              | 1950                            | 150                              |
| PE-23.23 | 45                     | 109             | 95              | 2830                            | 200                              |

<sup>a</sup> Determined by DSC with a heating/cooling rate of 15 K min<sup>-1</sup>.

<sup>b</sup> Determined by DMA (1 Hz, 0.1% deformation).

patibility is assured, polymer blends exhibit new properties which substantially deviate from the properties expected from just taking into account the properties and the mixing ratio of the individual blend components.<sup>32</sup> Moreover, blends with commodity polymers are attractive with respect to improving cost efficiency.

Blending of the long-chain polyesters (PE-19.19 and PE-23.23) with various types of thermoplastics was studied. For this purpose 5 and 15 wt%, respectively, of these polyesters were melt-compounded for 3 min at 150 rpm in a twin-screw mini-extruder with 1 wt% of ( $\pm$ )- $\alpha$ -tocopherol added as a stabilizer. DMA test specimens were produced by means of subsequent injection molding. Thermal properties were determined by means of both DMA and DSC measurements. As hydrocarbon blend components we investigated linear low density polyethylene (LLDPE, Affinity 8200G) and high density polyethylene (HDPE, Hostalen GC 7260), as well as a thermoplastic elastomer (SEBS, Kraton G1643 MS). According to the thermal and mechanical properties (see ESI†) all blends had a rather poor compatibility of both components. This was also observed for blends with a biodegradable aliphatic-aromatic polyester (Ecoflex F Blend C1200, BASF). Long-chain polyesters were successfully melt-compounded with talcum as a filler. Talcum is well established as a filler of engineering thermoplastics, especially in automotive applications.<sup>33,34</sup> Talcum efficiently reinforces PE-19.19 und PE-23.23 (Table 4). The addition of 25 wt% talcum doubles the storage modulus. On increasing the talcum content to 45 wt%, a three-fold increase of the storage modulus was achieved with respect to the bulk polyester.

## Summary and conclusions

These findings show that useful and attractive materials properties can be achieved for aliphatic polyesters generated by polycondensation of long-chain aliphatic diacids with long-chain diols. This is relevant, amongst others, as melting and crystallization temperatures of these new materials are advantageously high in comparison with existing shorter chain aliphatic polyesters. At the same time, the required monomers are accessible from plant oils in one or two steps only *via* self-metathesis or isomerizing alkoxycarbonylation as two comp-

lementary approaches. Here, we also demonstrate that polymerization grade long-chain  $\alpha,\omega$ -diacid ester monomers can be obtained conveniently on a 100 g scale in polycondensation grade purity using standard laboratory equipment by isomerizing alkoxycarbonylation.

We have demonstrated that long-chain all-aliphatic polyesters meet the demands of injection molding, film extrusion and even electrospinning to produce non-woven meshes. High Young's moduli and elongation at break are attainable. Polyesters-19.19 and -23.23 were phase-separated from selected polymer matrices, while filling with talcum enhances the storage modulus significantly. This offers prospects for novel bio-based packaging materials, non-wovens and moldings.

## Experimental section

### Materials and general considerations

Methanol was distilled from magnesium turnings and iodine prior to use. Toluene was distilled from sodium and THF from sodium/benzophenone. All other solvents were used in technical grade as received. Carbon monoxide (3.7) and hydrogen (5.0) were supplied by Air Liquide. [Pd(dtbpx)(OTf)<sub>2</sub>] was prepared according to a reported procedure.<sup>15</sup> High oleic sunflower oil methyl ester (92.5% of methyl oleate) supplied by Dako AG and methyl erucate (>90%) from TCI were degassed prior to use. Sodium methoxide (95%), titanium(IV) butoxide ( $\geq 97\%$ ) and ( $\pm$ )- $\alpha$ -tocopherol (synthetic,  $\geq 96\%$ ) were purchased from Sigma Aldrich.

NMR spectra were recorded on a Varian Inova 400. <sup>1</sup>H and <sup>13</sup>C chemical shifts were referenced to the solvent signals. High-temperature NMR measurements of polymers were performed in 1,1,2,2-tetrachloroethane-*d*<sub>2</sub> (Euroisotop) at 130 °C. DSC analyses were performed on a Netzsch Phoenix 204 F1 instrument with a heating and cooling rate, respectively, of 10 K min<sup>-1</sup>. Data reported are from second heating cycles. GPC analyses of polymers were carried out in 1,2,4-trichlorobenzene at 160 °C at a flow rate of 1 mL min<sup>-1</sup> on a Polymer Laboratories 220 instrument equipped with Olexis columns with differential refractive index, viscosity, and light-scattering (15° and 90°) detectors. Data reported were determined directly against linear PE standards. Gas chromatography was carried out on a PerkinElmer (PE) Clarus 500 instrument with an autosampler and FID detection on a PerkinElmer Elite-5 (5% diphenyl-95% dimethylpolysiloxane) Series capillary columns (length: 30 m, inner diameter: 0.25 mm, film thickness: 0.25 mm), using helium as a carrier gas at a flow rate of 1.5 mL min<sup>-1</sup>. The injector temperature was 300 °C. After injection the oven was kept isothermal at 90 °C for 1 min, heated at 30 K min<sup>-1</sup> to 280 °C, and kept isothermal at 280 °C for 8 min.

### Monomer synthesis

Alkoxycarbonylations of unsaturated long-chain fatty acid esters were carried out in a mechanically stirred 1.1 L stainless steel pressure reactor, equipped with a heating/cooling jacket



supplied with a thermostat controlled by a thermocouple dipping into the reaction mixture. Prior to alkoxycarbonylation experiments the reactor was evacuated and purged with nitrogen several times.

**Dimethyl-1,19-nonadecanedioate.**<sup>15</sup> Methyl oleate (150 mL, Dakolub MB 9001) was dissolved in 500 mL of methanol and cannula transferred into the pressure reactor under a nitrogen atmosphere. A solution of the catalyst precursor [(dtbpx)Pd-(OTf)<sub>2</sub>] (687 mg, 0.86 mmol) in another 50 mL of methanol was added, and the reactor was pressurized with 20 bar of CO and heated to 90 °C. A constant CO pressure was maintained by periodic replenishing. After 120 h the reactor was cooled to room temperature and vented. The crude product was dissolved in methylene chloride and filtered over a Buchner funnel to remove solid residues. Removal of the solvent *in vacuo* and recrystallization from methanol yielded pure dimethyl-1,19-nonadecanedioate (115.0 g, 76%, purity 99.5% from GC, confirmed by <sup>1</sup>H- and <sup>13</sup>C-NMR spectroscopy\*\*).

**Dimethyl-1,23-tricosanedioate.** Employing methyl erucate (175 mL) rather than oleate in an otherwise identical procedure yielded pure dimethyl 1,23-tricosanedioate (96.0 g, 54%, purity 99.6% from GC, confirmed by <sup>1</sup>H and <sup>13</sup>C NMR spectroscopy).

Catalytic reduction of the  $\alpha,\omega$ -diesters was performed analogously to a previously reported procedure.<sup>15</sup> In brief, reduction (50 bar H<sub>2</sub>, 100 °C) was performed here on a scale of *ca.* 12 g of diester in THF solvent to yield, after recrystallization, pure diol in *ca.* 85% yield.

## Polycondensation

Polyesters were prepared in a 100 mL two-necked Schlenk tube equipped with an overhead stirrer. Efficient mixing of the highly viscous polymer melt was achieved by a helical agitator. Under a static argon atmosphere the monomers (20.0 mmol of dimethyl 1,19-nonadecanedioate or diethyl-1,23-tricosanedioate, respectively, and 20.0 mmol of the corresponding  $\alpha,\omega$ -diol) were filled into the reaction vessel and melted by heating to 120 °C. A 0.6 mL aliquot of a 0.028 M titanium(IV) butoxide solution in toluene was injected, and the temperature was raised to 200 °C over the course of 8 h. Finally, the polymer melt was stirred for about 16 h at this temperature under reduced pressure (0.01 mbar).

## Tensile testing

Dogbone-shaped sample bars for tensile testing (75 × 12.5 × 2 mm<sup>3</sup>; ISO 527-2, type 5A) were prepared *via* melt compounding at 180 °C and 150 rpm for 3 min, using a DSM Xplore Micro 5cc Twin Screw Compounder and a DSM Xplore Micro 4cc Injection Molding Machine. In order to prevent oxidative degradation the polymers were stabilized with 1 wt% of ( $\pm$ )- $\alpha$ -tocopherol. For producing the polyester films a DSM Xplore Film device was used.

After preconditioning the samples overnight at 23 °C tensile tests were performed on a Zwick Z005 instrument according to ISO 527 (crosshead speed 50 mm min<sup>-1</sup>). The Zwick test Xpert software version 11.0 was used to collect and analyze the results. Young's modulus, yield stress, yield strain, tensile stress at break and tensile strain at break were obtained by averaging the data from several test specimens.

## Shore D Hardness

Measuring Shore D Hardness (according to DIN 535054) was performed with a Zwick 3150 H04 instrument at room temperature. For determination of hardness 12.5 × 12.5 × 4 mm test specimens were used. Values given are the average of six independent measurements.

## Dynamic mechanical analysis (DMA)

Dynamic-mechanical analyses (DMA) were recorded on melt compounded rectangular specimens (length × width × thickness = 25 × 6 × 2 mm<sup>3</sup>) using a Triton Technology TTDMA instrument equipped with single cantilever geometry. Measurements were performed from -150 °C to 80 °C at a heating rate of 3 °C min<sup>-1</sup> and a frequency of 1 Hz. The Triton Technology DMA software was used to acquire and process the data. Glass transition temperatures (*T*<sub>g</sub>) were determined from the temperature position of the maximum in loss modulus (*G''*).

Dynamic-mechanical analyses on the polymer compounds were performed using a TA Instruments Q 800 with single cantilever geometry. Measurements were performed from -60 °C to 10 °C under the melting point of the compounds investigated at a heating rate of 3 °C min<sup>-1</sup>, a deformation of 0.1% and a frequency of 1 Hz.

## Rheological studies

Rheological measurements were carried out with an Advanced Rheometric Expansion System (ARES) from Rheometric Scientific. Test specimens (25 mm diameter) were prepared with a Dr Collin vacuum press 200 PV at 180 °C, and a pressure of 30 bar was sustained for 30 minutes. Polymers were stabilized with 1 wt% of ( $\pm$ )- $\alpha$ -tocopherol. Specimens were analyzed using a plate/plate geometry (25 mm diameter). The frequency was varied between 0.1 and 100 rad s<sup>-1</sup>. The temperature was raised from 110 to 180 °C during the measurement.

Shifting of isothermal curves was performed only in a horizontal dimension, leading to *b*<sub>T</sub> = 1. The Carreau-Yasuda equation was used to extrapolate data to obtain the zero shear viscosity (*cf.* ESI†).

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