

Depleted uranium catalysts for chlorine production†

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This study demonstrates depleted uranium as a remarkable heterogeneous catalyst for the oxidation of HCl to Cl₂. This reaction comprises a sustainable approach to valorise byproduct HCl streams in the chemical industry. Bulk α -U₃O₈ showed an outstanding stability against chlorination, which is crucial for its durability in catalytic tests. UO₂ and γ -UO₃ transformed into α -U₃O₈ under reaction conditions. Uranium deposition on different carriers by dry impregnation concluded the superiority of zirconia as support. HAADF-STEM investigations revealed that the uranium oxide on the surface of this carrier is present in the form of a film-like nanostructure with a thickness ranging from a monolayer to 1 nm as well as atomic dispersion. The effect of variables (temperature, feed O₂/HCl ratio, metal loading, and Cl₂ co-feeding) on the performance of U₃O₈/ZrO₂ has been studied. The HCl conversion over this catalyst increased with reaction time as a likely consequence of *in situ* re-dispersion of the original uranium phase into atomically dispersed UO_x. As demonstrated by H₂-TPR, the uranium in the generated UO_x phase is more oxidised than in the original U₃O₈. Such a highly dispersed active phase is produced faster in the uncalcined sample. The extraordinary stable Cl₂ production over U₃O₈/ZrO₂ at 773 K for 100 h on stream indicates its potential for application in high-temperature HCl oxidation. Under these conditions, other known catalytic materials suffer from significant deactivation.

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Introduction

Uranium compounds have been used as heterogeneous and homogeneous catalysts.^{1,2} Their suitability for redox reactions is related to the wide range of oxidation states that uranium can assume (from II to VI), which in turn derives from the ability of its 5f-electrons to hybridise.³ Specifically for the heterogeneous catalysis field, uranium oxides (mostly U₃O₈) have been recognised since the 1920s for reactions of industrial relevance such as the oxidation of hydrocarbons and the partial oxidation of ethanol.^{4–6} Later efforts extended the scope of uranium-catalysed transformations to comprise the oxidative destruction of volatile chlorinated hydrocarbons,^{7,8} the oxidative coupling of ethylene, acetylene, and acetaldehyde,³ the esterification of formaldehyde,³ and NO_x reduction.⁹ Relevantly, uranium-based materials were once used in industry for the hydrocracking of shale oil (UO₃/Al₂O₃, UO₃/CoMoO₄)¹⁰ and in the ammoxidation of propylene to acrylonitrile (USb_xO_y).^{11–13}

Natural uranium consists of three isotopes, ²³⁸U, ²³⁵U, and ²³⁴U, in the relative abundance of 99.275, 0.720, and 0.005%, respectively.¹⁴ ²³⁸U and ²³⁴U are α -ray emitters, while ²³⁵U emits both α - and low-energy γ -rays. Alpha particles are much less

penetrating than other forms of radiation, thus rendering uranium only a little hazardous (mainly from the γ -rays). Depleted uranium (DU), which is produced as a waste in the uranium enrichment process, is even considerably less radioactive (*ca.* 0.2–0.4% ²³⁵U) and, thus, less harmful. To generate the carbon-neutral energy source, the demand of enriched uranium as a fissile nuclear fuel can be expected to increase,² which represents a strong incentive for the development of novel applications of DU.

The heterogeneously catalysed oxidation of HCl to Cl₂ (Deacon reaction)¹⁵ is an attractive route to recycle chlorine from byproduct HCl streams in the chemical industry, namely in the production of polyurethanes and polycarbonates.^{16–18} Two industrial catalysts based on RuO₂, featuring high activity at a relatively low temperature and remarkable stability, have been recently introduced: RuO₂/SiO₂/TiO₂-rutile (by Sumitomo) and RuO₂/SnO₂-Al₂O₃ (by Bayer).^{19–27} The wide use of ruthenium catalysts for HCl oxidation is hindered by its high and fluctuating market price.¹⁶ This drawback triggered research efforts to develop alternative cost-effective systems. CeO₂-based catalysts represent tangible steps along this direction.^{28,29}

Uranium oxide-based catalysts for HCl oxidation have recently been patented.^{30,31} High single-pass HCl conversion at high temperature and practically negligible active phase loss have been claimed as the key characteristics of these systems. To assess the real potential of uranium-based catalysts for industrial application, further knowledge needs to be gathered. The optimal combination of active phase and support will be

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derived only based on a deeper understanding of activity and stability descriptors. The catalyst performance should be then put into perspective with respect to other known catalytic systems and evaluated in an industrially relevant time frame. Herein, we systematically investigated uranium oxides in bulk and supported forms for HCl oxidation. Catalytic tests at ambient pressure in a continuous flow fixed-bed reactor combined with detailed characterisation of the catalysts prior to and after reaction have been applied to gather a solid knowledge of the Deacon chemistry of these materials.

Results and discussion

Bulk uranium oxides

As starting point, the main binary oxides of uranium were considered in this study, namely, UO_2 , U_3O_8 , and UO_3 . The X-ray diffractograms of the solids as well as their corresponding structures are displayed in Fig. 1a and b. According to the XRD phase analysis, the catalysts were identified as uranium dioxide (JCPDS 05-0550), α -triuranium octoxide (JCPDS 31-1424), and γ -uranium trioxide (JCPDS 31-1422) with small amounts of β - and α -forms. The crystal structure of UO_2 is of fluorite type with face-centred cubic atomic arrangement. Uranium and oxygen atoms are octa- and tetrahedrally coordinated, respectively.¹⁴ α - U_3O_8 , one of the two forms (α , β) of this oxide which are stable at ambient temperature,³ crystallises in an orthorhombic structure. All of the uranium atoms are coordinated with oxygen atoms forming pentagonal pyramids.¹⁴ γ - UO_3 , the most stable of the seven crystalline phases (α , β , δ , ϵ , γ , ζ , and η) of this oxide,³ belongs to the tetragonal crystal system and is characterised by octa- and dodecahedral coordination of uranium to oxygen. All of the three oxides possess a very low total surface area (S_{BET} , Table 1).

The reducibility of these materials was studied under a diluted H_2 flow up to 1100 K (Fig. 1c). The reduction profile of UO_2 shows a little H_2 consumption at ca. 880 K. As the XRD

pattern of the reduced sample (Fig. S1 in the ESI†) was unaltered with respect to that of the fresh solid, this feature was attributed to the removal of oxygen species that are known to accommodate in the lattice of the fluorite structure of UO_2 upon exposure to air.¹ For α - U_3O_8 , a single and broad peak centred at ca. 975 K was evidenced, which is assigned to the reduction of U_3O_8 to UO_2 .⁸ The reduction profile of γ - UO_3 displays a broad signal composed by two main contributions at ca. 880 and 963 K, due to the transitions $\text{UO}_3 \rightarrow \text{U}_3\text{O}_8$ and $\text{U}_3\text{O}_8 \rightarrow \text{UO}_2$, respectively (Fig. 1c).³² The formation of UO_2 from both α - U_3O_8 and γ - UO_3 was confirmed by XRD (Fig. S1 in the ESI†).

These bulk uranium oxides were tested in the gas-phase oxidation of HCl at $T_{\text{bed}} = 773$ K and $\text{O}_2/\text{HCl} = 2$ for 3 h. The rates of Cl_2 production were stable at ca. $2 \text{ mol Cl}_2 \text{ h}^{-1} \text{ mol U}^{-1}$ for UO_2 and α - U_3O_8 and ca. $3 \text{ mol Cl}_2 \text{ h}^{-1} \text{ mol U}^{-1}$ for γ - UO_3 . Normalisation of the rates by S_{BET} of the fresh samples gives the values as 7×10^{-3} , 8×10^{-3} , and $3.4 \times 10^{-3} \text{ mol Cl}_2 \text{ h}^{-1} \text{ m}^{-2}$ for α - U_3O_8 , UO_2 , and γ - UO_3 , respectively. However, due to transformation of the latter two oxides into the former during reaction (*vide infra*), rates normalised by the S_{BET} of the used sample are more relevant and lead to a value of $4 \times 10^{-3} \text{ mol Cl}_2 \text{ h}^{-1} \text{ m}^{-2}$ in all cases. The dependence of the activity of these oxides on temperature was investigated between 673 and 823 K at $\text{O}_2/\text{HCl} = 2$. The reaction rate scaled linearly with the temperature in the whole range. The apparent activation energy ($E_{\text{a}}^{\text{app}}$) was estimated from the Arrhenius plots at 52, 54, and 40 kJ mol^{-1} for UO_2 , α - U_3O_8 , and γ - UO_3 , respectively.

The used catalysts were characterised by the same techniques applied to the fresh samples in order to assess possible structural changes upon exposure to reaction conditions. Remarkably, XRD analysis indicated the absence of chlorinated phases in any of the used catalysts. However, we observed the complete conversion of UO_2 and γ - UO_3 into α - U_3O_8 (Fig. 1b). It is suggested that such transformation is due to oxidation by the excess gas-phase O_2 for the former oxide and reduction by feed

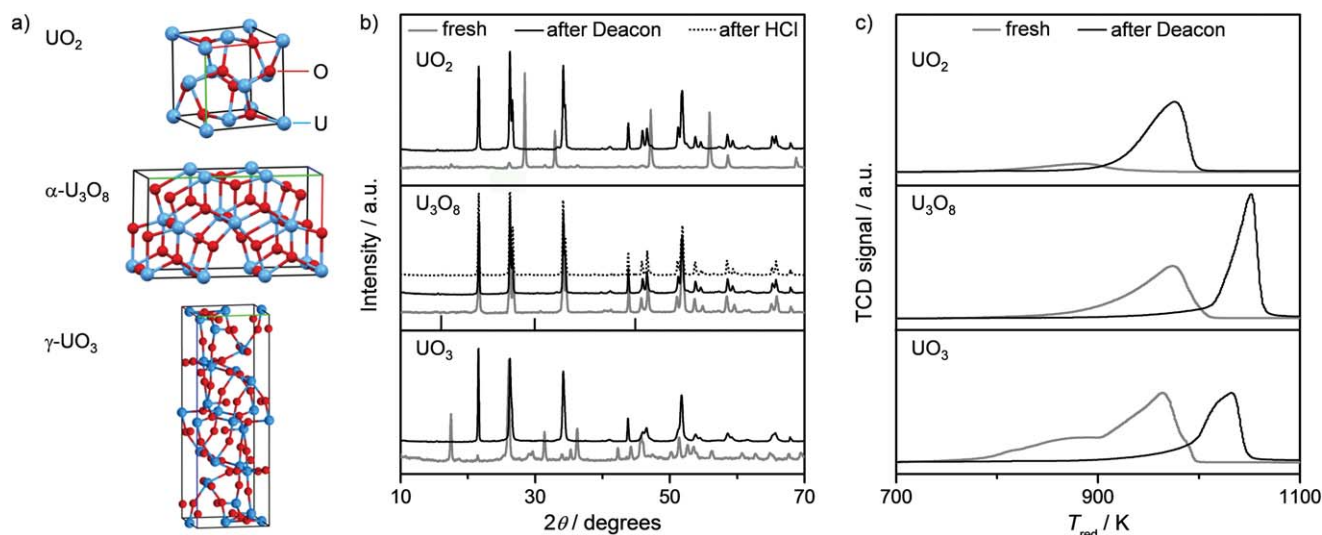


Fig. 1 Structure of the uranium oxides (a) and characterisation results from powder XRD (b) and H_2 -TPR (c) of the samples in fresh form (blue lines), after HCl oxidation at 773 K (black lines), and after HCl treatment at 823 K (dotted lines). Vertical lines at the bottom of the U_3O_8 pattern show the positions of most intense reflections of UCl_4 .



Table 1 Characterisation and catalytic data of uranium-based catalysts

Sample	U ^a (wt%)	S _{BET} (m ² g ⁻¹)	r ^b (mol Cl ₂ h ⁻¹ mol U ⁻¹)	E _a ^{app} (kJ mol ⁻¹)
UO ₂	88.1	1	2.2	52
γ-UO ₃	83.1	3	2.9	40
α-U ₃ O ₈	84.8	1	2.0	54
U ₃ O ₈ /ZrO ₂	9.8	35 (47) ^c	63.5	50
U ₃ O ₈ /SiO ₂	9.5	136 (193)	45.4	46
U ₃ O ₈ /TiO ₂	9.4	30 (52)	28.6	54
U ₃ O ₈ /Al ₂ O ₃	9.6	131 (191)	27.3	57

^a Determined by ICP-OES. ^b Conditions: *W* = 0.5 g (bulk oxides) or 0.25 g (supported catalysts), *T*_{bed} = 773 K, O₂/HCl = 2, *F*_T = 166 cm³ STP min⁻¹, and *t* = 3 h (bulk oxides) or 1 h (supported catalysts). ^c Surface area of the supports in brackets.

HCl for the latter. Indeed, treatment of UO₂ and γ-UO₃ in 20 vol % O₂/N₂ at 773 K for 3 h caused the complete transformation of UO₂ into α-U₃O₈, while it did not affect the state of γ-UO₃ (confirmed by XRD, Fig. S2 in the ESI†). All of the H₂-TPR profiles of the uranium oxides after reaction feature a single reduction peak, attributed to the transformation of U₃O₈ into UO₂ (Fig. 1c), in line with the identical bulk composition of the samples after HCl oxidation. The appearance of the peak at higher reduction temperature for used γ-UO₃ and α-U₃O₈ is likely related to certain degree of surface chlorination and/or sintering. With regard to the former, the bulk α-U₃O₈ catalyst after Deacon reaction was calcined in static air at 773 K for 5 h (aimed at removing surface chlorine species) and then measured by H₂-TPR. A reduction profile equivalent to that of the fresh α-U₃O₈ sample was obtained (Fig. S3a†), which confirmed that the change in reducibility is mainly due to surface chlorination. Further, TEM of α-U₃O₈ in fresh form and after Deacon indicated a slight increase in overall particle size for the latter (Fig. S3b and c†). Since calcination of U₃O₈ after Deacon reproduced the reduction profile of the fresh sample, the effect of sintering on reducibility of U₃O₈ seems to be negligible.

α-U₃O₈ was further assessed under harsher conditions, *i.e.* at O₂/HCl = 0.5 and 0 (without gas-phase O₂) at 823 K for 2 h on stream to evaluate its resistance to bulk chlorination and metal loss. The weight of the reactor before and after the tests remained practically unchanged, suggesting no loss of uranium. Furthermore, the diffractograms of the samples after these treatments indicated the preservation of a pure oxidic phase (Fig. 1b). The endothermic nature of the penetration of Cl atoms to deeper layers (*ca.* 2 eV) has been already found as a key reason for the robustness of RuO₂ against bulk chlorination.^{22,28} Similar property could be responsible for the stability of α-U₃O₈ against bulk chlorination. In this line, chlorination of UO₂ (which also revealed the absence of any chloride phase upon testing in O₂/HCl = 0 at 823 K for 2 h), by Cl₂ to form UCl₄ has been reported highly endothermic (Δ*G* = 148.9 kJ mol⁻¹).³³ Thus, bulk uranium oxide represents an exceptionally stable high-temperature catalyst for HCl oxidation. This finding is particularly striking since CuO, Cr₂O₃, CeO₂, and RuO₂ undergo structural changes at high temperatures. In particular, after testing at 823 K and O₂/HCl = 0.5 for 2 h, strong chlorination

was detected (XRD analysis) for the first three oxides, while RuO₂ underwent partial transformation into volatile RuO₄ (*ca.* 20 wt% RuO₂ loss).¹⁶ It is worth noting, though, that RuO₂ is an outstanding low-temperature (473–673 K) catalyst and is extremely stable under its optimised operating conditions.^{20,34}

Supported U₃O₈ catalysts

Based on the very promising performance of bulk α-U₃O₈, the next step of the work consisted of finding a suitable support for this uranium-based active phase. Monoclinic ZrO₂, γ-Al₂O₃, SiO₂, and TiO₂-anatase were considered as carriers. The synthesis protocol comprised dry impregnation of these oxides with a uranium precursor (in an amount corresponding to a nominal loading of 10 wt% U), followed by calcination under the same conditions applied for the preparation of bulk α-U₃O₈ (see Experimental section).

The supported U₃O₈ catalysts were screened in HCl oxidation at O₂/HCl = 2 in the temperature range of 673–823 K (Fig. 2a). Blank experiments confirmed that the Deacon activity of the pure carriers was negligible under the conditions applied. The HCl conversion displayed a steady increase with the temperature for all supported catalysts, reaching values comprised between 21 and 47% at 823 K. U₃O₈/ZrO₂ was the most active catalyst, followed by U₃O₈/SiO₂ and, finally, U₃O₈/TiO₂ and U₃O₈/Al₂O₃, which were comparably active. With respect to the bulk oxide, only the zirconia- and silica-supported materials offered improved performances (Fig. 2a). Still, as α-U₃O₈ was tested using twice the catalyst amount, a better comparison was drawn on the basis of the reaction rates per mol of U at 773 K. Accordingly, it appeared evident that any of the supports employed determined an activity enhancement, overall leading to 14–30 times higher rates (Table 1). As shown in the same table, the *E*_a^{app} values (at 723–823 K and O₂/HCl = 2) determined from the Arrhenius plots were in the range of 46–57 kJ mol⁻¹ for the supported catalysts, thus being similar to α-U₃O₈. The dependence of the activity on the relative O₂ content in the feed was studied over the two most promising catalysts, U₃O₈/ZrO₂ and U₃O₈/SiO₂ (Fig. 2b). In both cases, the HCl conversion increased upon raising the feed O₂/HCl ratio and the formal reaction order of O₂ was calculated as *ca.* 0.3. This behaviour is common to the vast majority of Deacon catalysts^{24,28} and



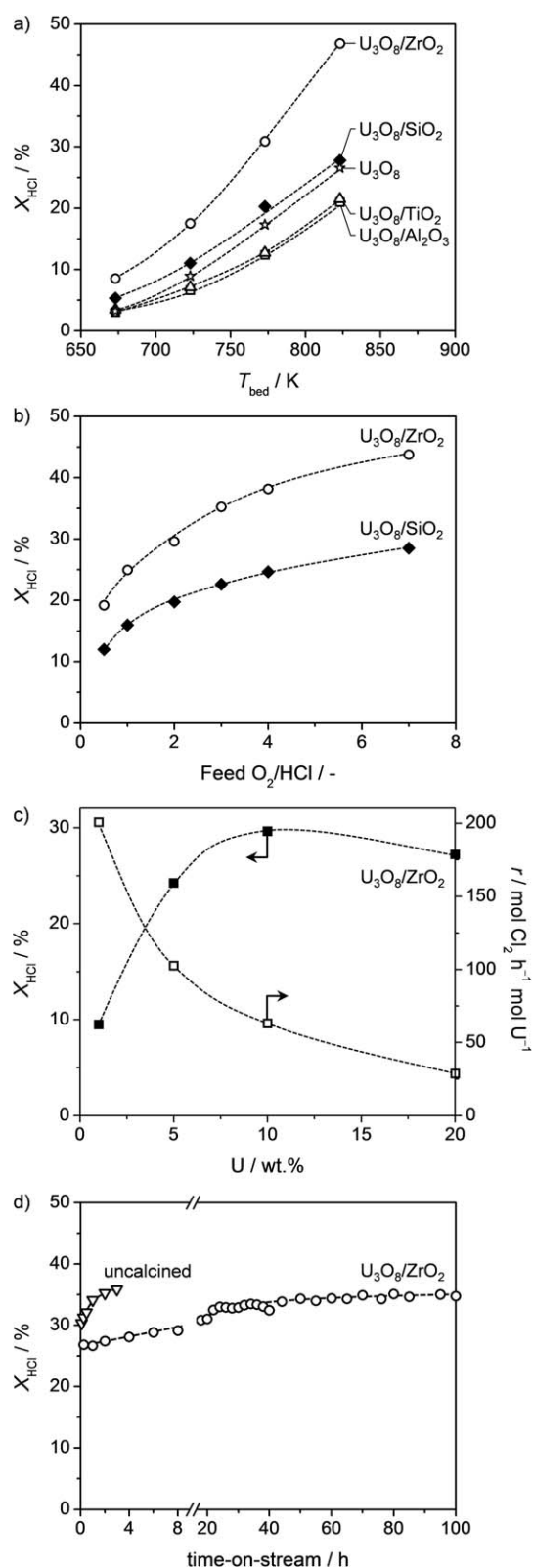


Fig. 2 HCl conversion over U_3O_8 -based catalysts versus (a) bed temperature at $O_2/HCl = 2$ and (b) O_2/HCl ratio at 773 K. HCl conversion and U-specific rate over U_3O_8/ZrO_2 versus the uranium loading (c) and HCl conversion over U_3O_8/ZrO_2 and an as-impregnated zirconia-supported catalyst (uncalcined) versus time-on-stream (d) at 773 K and $O_2/HCl = 2$. Data were acquired after 1 h under each condition for a–c. Other conditions are detailed in the Experimental section.

indicates that catalyst re-oxidation is the limiting step.²⁷ It is worth noting that the HCl conversion over U_3O_8/ZrO_2 remained higher than that of U_3O_8/SiO_2 at all O_2/HCl ratios. Overall, the catalytic results indicate that zirconia is the most suitable carrier for uranium oxide.

In order to rationalise the activity differences, the supported U_3O_8 catalysts were characterised in fresh form and after use in the Deacon reaction. The uranium content, as determined by ICP-OES, was close to the nominal value of 10 wt% for all of the catalysts and remained unchanged in the used samples, indicating negligible uranium loss during HCl oxidation. The fresh alumina- and silica-based catalysts featured *ca.* 4 times larger S_{BET} than the zirconia- and titania-based materials (Table 1). This deviation reflects the difference in surface area of the pure carriers, which was depleted to a similar extent upon uranium incorporation in all cases, likely due to pore blockage. The S_{BET} of the catalysts was also unaltered upon use. Accordingly, the activity trend cannot be explained by differences and/or changes in the active phase content or textural characteristics.

XRD analysis of the fresh materials evidenced the formation of α - U_3O_8 over all supports with exception of titania (Fig. 3). In this latter case, a mixed $UTiO_5$ phase was detected (JCPDS 49-1397).³⁵ Furthermore, reflections specific to both the anatase and rutile forms of titania were observed, indicating that partial transformation of the carrier structure occurred during the high-temperature thermal activation of the as-impregnated solid. Thus, the loss in the support's surface area during catalyst preparation could be additionally ascribed to phase changes and structural reconstructions for U_3O_8/TiO_2 . Based on the much lower intensity of its diffraction lines, the uranium phase is supposed to be present in form of smaller nanostructures on ZrO_2 compared to the other carriers, especially titania. The diffractograms of the samples after reaction revealed the absence of bulk chlorides (Fig. 3), extending the stability of

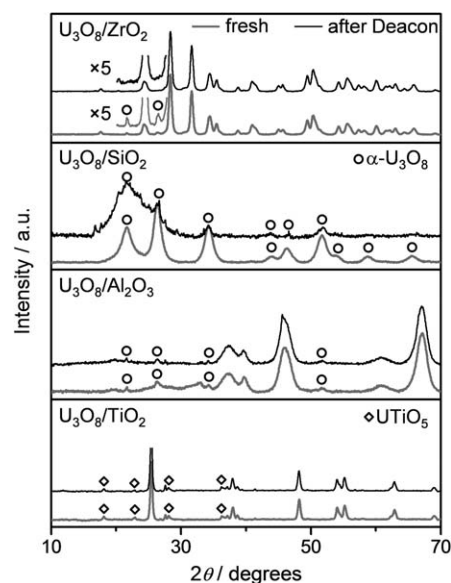


Fig. 3 XRD patterns of supported U_3O_8 samples in fresh form (blue lines) and after Deacon reaction (black lines). Unmarked reflections belong to the corresponding carriers.

α - U_3O_8 against chlorination also to the supported form. No changes were detected in the patterns of the TiO_2 and Al_2O_3 -supported catalysts upon use, while the reflections specific to α - U_3O_8 became less intense for $\text{U}_3\text{O}_8/\text{SiO}_2$ and disappeared for $\text{U}_3\text{O}_8/\text{ZrO}_2$. Since uranium was not lost upon reaction, these alterations might be substantiated by fragmentation of the α - U_3O_8 phase in tinier structures.

In order to further tackle this point and as the XRD analysis hints to differences in the dispersion of the supported active phase as a possible main parameter for determining the activity levels, the two most active catalysts ($\text{U}_3\text{O}_8/\text{ZrO}_2$ and $\text{U}_3\text{O}_8/\text{SiO}_2$) were further investigated by electron microscopy (EM, Fig. 4 and 5). For fresh $\text{U}_3\text{O}_8/\text{ZrO}_2$, aggregates of 20–30 nm sized support grains are visualised by HRTEM (Fig. 4a). However, inspection of surface regions even at higher magnification does not reveal a distinct uranium phase. Thus, based on the significant difference in the atomic numbers of U and Zr ($Z_{\text{U}} = 92$ versus $Z_{\text{Zr}} = 40$), HAADF-STEM with Z-contrast was applied as a suitable tool to get information about the distribution of uranium-based phases (Fig. 5). Indeed, the uranium oxide species in the fresh $\text{U}_3\text{O}_8/\text{ZrO}_2$ are clearly visualised as bright rim or spots (Fig. 5a and b). The presence of uranium in these rims was confirmed by EDXS analysis. Investigation of the surface structure at the edges and on the surface revealed that two types of uranium oxide dispersions are present in the fresh $\text{U}_3\text{O}_8/\text{ZrO}_2$, namely, (i) a film-like nanostructure with a thickness ranging from a monolayer to 1 nm (Fig. 5a) and (ii) atomically dispersed uranium oxide as identified by bright spots (encircled) on the ZrO_2 support (Fig. 5b). Moreover, analysis of the complete structure of these spots is not possible on the basis of HAADF-STEM and would require more specific methods such as STEM coupled with electron energy loss spectrometer (EELS).³⁶ Nonetheless, based on the studies on identification of single atoms,³⁶ the bright spots seem to be composed of a single uranium atom (likely with some O atoms bound to it) and therefore, in this study they are referred to as atomically dispersed UO_x . Upon exposure to reaction conditions (for 5 h), the catalyst morphology seems to be altered. A film-like nanostructure is less visible and a concentration of bright spots of UO_x appears to be increased (Fig. 5c), suggesting the

transformation into tinier, better dispersed uranium oxide. Thus, uranium oxide on zirconia likely undergoes partial re-dispersion during reaction. This explains the disappearance of the α - U_3O_8 peaks in the XRD pattern of the used sample (Fig. 3). α - U_3O_8 on SiO_2 appears to be carried as nanoparticles of ca. 5 nm in the fresh catalyst (Fig. 4b). Upon use in HCl oxidation, the average particle size was reduced to ca. 2.5 nm (Fig. 4c, inset in b), supporting a certain degree of re-dispersion of the uranium phase. This agrees with the XRD results (Fig. 3). The origin of the active phase re-dispersion phenomenon, apparently common to both the zirconia- and silica-supported catalysts, is not fully understood. It is proposed that disaggregation of the uranium oxide structures might be induced by HCl and Cl_2 . The latter has been reported to produce such an effect on supported noble metal particles by generation of chlorides which readsorb on the solid carrier and are then reduced by the reaction environment.^{37,38} In our case, it is possible that uranium oxychloride species (UO_2Cl_2 , melting point = 843 K)³⁹ are formed to some extent. As they are highly unstable and readily re-oxidise under conditions similar to those applied in HCl oxidation,⁴⁰ uranium will not be lost, but a certain degree of metal migration could be possible. This will ultimately improve the dispersion of the supported phase. Thus, based on the XRD and EM results, the activity differences seem to mainly depend on the uranium oxide dispersion. Still, the possibly different intrinsic activity of the chemical forms of uranium stabilised by the carriers might also play a role.

In view of its potential practical application, the $\text{U}_3\text{O}_8/\text{ZrO}_2$ system was further studied in terms of optimisation of the active phase content as well as durability. Thus, catalysts with U loading comprised between 1 and 20 wt% were prepared and tested at 773 K and $\text{O}_2/\text{HCl} = 2$ (Fig. 2c). The HCl conversion was found to raise with increasing U contents up to 10 wt%, while a loading of 20 wt % resulted in slightly lower activity. On the contrary, the U specific activity (*i.e.* reaction rate per mol of U) was the highest for the 1 wt% U catalyst and progressively diminished at increased U loadings. Hence, as a compromise between these parameters, a 5–10 wt% U content turns out to be optimal.

The robustness of U_3O_8 (10 wt% U)/ ZrO_2 in HCl oxidation was tested in a long catalytic run (Fig. 2d). The HCl conversion

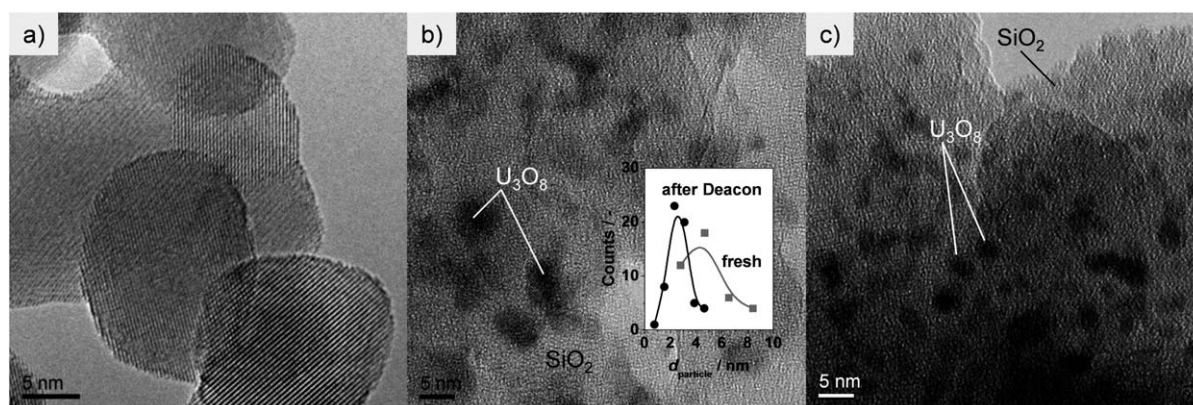


Fig. 4 HRTEM of fresh $\text{U}_3\text{O}_8/\text{ZrO}_2$ (a), $\text{U}_3\text{O}_8/\text{SiO}_2$ in fresh form (b) and after Deacon (c). Inset in (b) shows the particle size distribution of the fresh and used $\text{U}_3\text{O}_8/\text{SiO}_2$ sample.

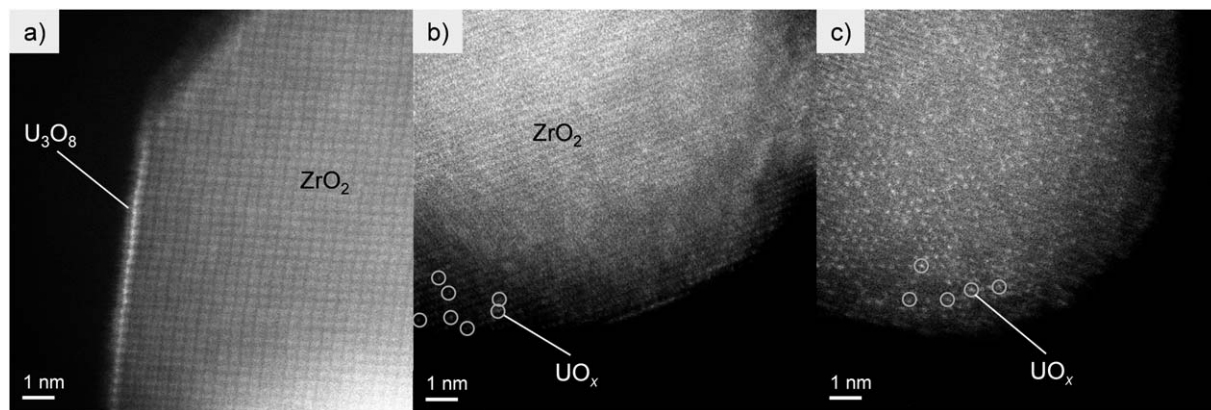


Fig. 5 HAADF-STEM of $\text{U}_3\text{O}_8/\text{ZrO}_2$ in fresh form (a and b) and after Deacon reaction for 100 h (c). Bright spots (some of which are encircled) in b and c corresponds to atomically dispersed UO_x .

moderately increased from 27 to 35% in the first 85 h on stream, remaining then stable up to a reaction time of *ca.* 100 h. Overall, this result evidences outstanding longevity, offering bright perspectives for an industrial application of zirconia-supported uranium catalysts in chlorine production. Still, the progressive catalyst activation indicates an alteration of the material's properties upon use. According to the above discussion of the characterisation data, this might originate from an increase in the dispersion of the active phase induced by the exposure to the reaction mixture. To further explore this point, samples after 5, 10, and 100 h on stream were collected and characterised by HAADF-STEM and H_2 -TPR (Fig. 5 and 6). While an increase in the uranium dispersion to certain extent has been already discussed for the sample after 5 h reaction (*vide supra*), HAADF-STEM of the sample after 100 h reaction evidenced that the uranium on ZrO_2 carrier is mainly present as atomically dispersed UO_x (Fig. 5c). The latter would be characterised by the highest dispersion of uranium oxide. This result provides a direct evidence for the dependence of activity on degree of dispersion.

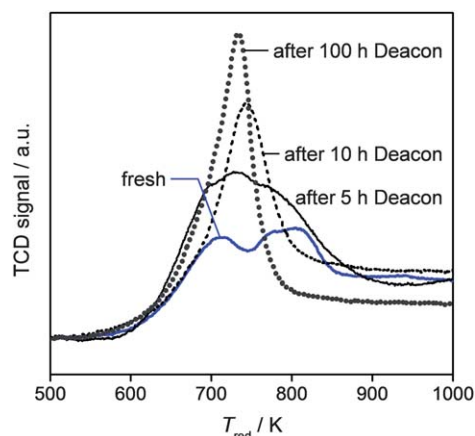


Fig. 6 H_2 -TPR profiles of $\text{U}_3\text{O}_8/\text{ZrO}_2$ in fresh form and after Deacon reaction for different times.

Additional support was derived from the H_2 -TPR analysis. The reduction profile of fresh $\text{U}_3\text{O}_8/\text{ZrO}_2$ features two main peaks at *ca.* 710 and 800 K (Fig. 6), which could be consistent with the presence of uranium oxide structures of different size (Fig. 5a and b), namely, thin layer (high-temperature signal) and atomic dispersion (low-temperature signal). For the sample collected after 5 h, a broad and more intense reduction peak centred at *ca.* 730 K with low- (695 K) and high-temperature (775 K) shoulders was visualised, while that taken after 10 h of reaction produced a single, symmetric, and sharper signal with maximum at 740 K. The curve of the catalyst unloaded at the end of the run displays an even narrower and more intense peak, slightly shifted to lower temperature (710 K). The depletion of the high-temperature signals with reaction time and the strengthening of a single peak at lower temperature supports a change in the morphology of α - U_3O_8 phase towards the formation of more uniformly-sized atomically dispersed nanostructures (UO_x), in line with the HAADF-STEM results. The latter actually represents the predominant uranium distribution after 100 h on stream (Fig. 5c). Still, considering the modifications in peak position and shape, along with the significant increase in H_2 consumption, the presence of more oxidic uranium in UO_x than in the original α - U_3O_8 phase cannot be excluded. Based on the structural equivalence between the zirconia support and β - UO_3 (both monoclinic, the latter having about double cell parameters with respect to the former),¹ it could be possible that α - U_3O_8 undergoes transformation into this oxide during reaction. Although α - U_3O_8 is the most stable bulk oxide under HCl oxidation conditions and γ - UO_3 is converted into it during reaction, it is plausible that, when the incipient uranium oxychloride is oxidised by the O_2 excess, the structural matching offered by the support could stabilise β - UO_3 as an oxidation product rather than α - U_3O_8 . However, this phase is not detected by XRD owing to its very small size. Thus, from increased H_2 uptake and development of atomically dispersed UO_x with reaction time, it can only be suggested that uranium generated *in situ* as UO_x is in higher oxidation state than in the original α - U_3O_8 and the transformation of α - U_3O_8 to UO_x is



accompanied by an enhancement of the dispersion. Since the presence of some UO_x is evidenced already for the fresh catalyst (Fig. 5b and 6), it could even be possible that a part of the uranium is already stabilised as UO_x during calcination and the atomic dispersion (Fig. 5b) rendering it undetectable by XRD (Fig. 3). An increase of uranium oxide dispersion during HCl oxidation was also evidenced for $\text{U}_3\text{O}_8/\text{SiO}_2$ (Fig. 3, 4b and c). However, from a similar H_2 consumption of fresh and used catalyst (not shown), it appears that *in situ* oxidation of the uranium phase does not occur on silica. This could be related to a specific property of the carrier and its interaction with the active phase. Thus, it seems that the support determines the degree of redispersion and reoxidation characteristics of the uranium phase. An in-depth understanding of these complex phenomena will require deeper characterisation studies, which are beyond the scope of this paper.

Finally, we tested under the same HCl oxidation conditions an as-impregnated catalyst sample with equal U loading (*i.e.* no calcination applied after impregnating the U-precursor). This material reached a similar HCl conversion level (*ca.* 36%) to $\text{U}_3\text{O}_8/\text{ZrO}_2$ after only 3 h on stream (Fig. 2d). On the basis of this outcome and of the resemblance of the HAADF-STEM images and XRD pattern of the two catalysts after use (not shown), it is suggested that UO_x can be directly created *in situ* from the uranium precursor and with much faster kinetics. The latter is probably related to the ease of altering an amorphous and unstable deposit rather than a well-crystallised and stable phase.

Comparison with other systems

The performance of $\text{U}_3\text{O}_8/\text{ZrO}_2$ was contrasted with other known supported HCl oxidation catalysts, namely, $\text{RuO}_2(2 \text{ wt}\% \text{ Ru})/\text{SnO}_2\text{-Al}_2\text{O}_3$,²⁰ $\text{CeO}_2(9 \text{ wt}\% \text{ Ce})/\text{ZrO}_2$,²⁹ and $\text{CuO}(15 \text{ wt}\% \text{ Cu})/\text{SiO}_2$ (synthesised by dry impregnation, followed by calcination at 823 K for 10 h). Fig. 7a displays the dependence of the HCl conversion level on temperature for these materials. The equilibrium HCl conversion (dashed line) is reported as a reference. The activity of $\text{RuO}_2/\text{SnO}_2\text{-Al}_2\text{O}_3$ increases with the temperature and reaches a HCl conversion close to the equilibrium value at 673 K. Beyond this temperature the active phase of this catalyst starts to form volatile RuO_4 .¹⁶ This indicates that the optimal high temperature boundary for RuO_2 -based catalysts is 673 K. CuO/SiO_2 possesses a volcano-shaped activity profile. A strong deactivation above 723 K is due to huge copper loss in the form of CuCl and CuCl_2 .⁴¹ Differently, $\text{U}_3\text{O}_8/\text{ZrO}_2$ and $\text{CeO}_2/\text{ZrO}_2$ show a steady increase of the HCl conversion with temperature. The difference of activity between these two systems is relatively low (*ca.* 30 K). Cl_2 co-feeding at comparable initial HCl conversion levels (attained by adjusting T_{bed} , Experimental section) also displays a very similar inhibition of HCl oxidation activity (Fig. 7b). Still, $\text{CeO}_2/\text{ZrO}_2$ was observed to undergo bulk chlorination and, thus, deactivation at low O_2 excess.²⁹ Accordingly, $\text{U}_3\text{O}_8/\text{ZrO}_2$ stands as the most robust catalyst among all and belongs to the category of high-temperature catalysts, similar to $\text{CeO}_2/\text{ZrO}_2$. However, the former offers a superior resistance to bulk chlorination.

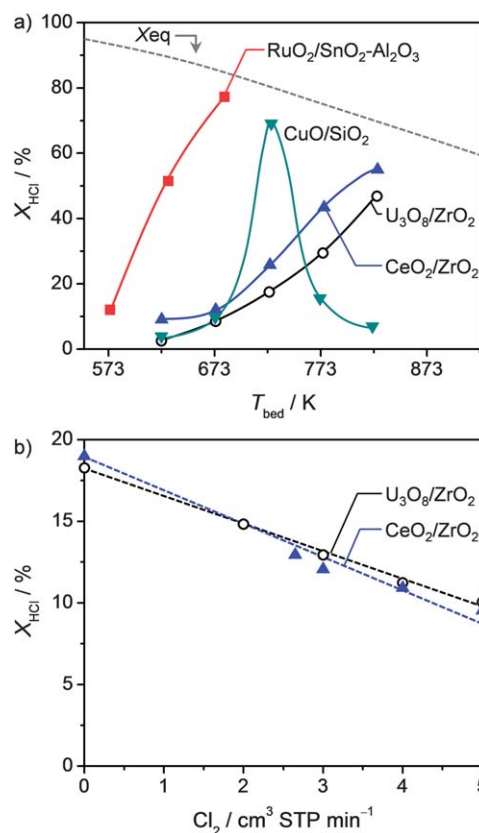


Fig. 7 Steady-state HCl conversion versus bed temperature (a) and amount of Cl_2 co-fed (b) at $\text{O}_2/\text{HCl} = 2$. Other conditions are detailed in the Experimental section.

Conclusions

Uranium catalysts have been successfully evaluated for HCl oxidation to Cl_2 . Extraordinary resistance of bulk uranium oxides against chlorination demonstrates their suitability as a stable active phase for this reaction. While $\alpha\text{-U}_3\text{O}_8$ maintains its oxidation state, UO_2 and $\gamma\text{-UO}_3$ tend to transform into $\alpha\text{-U}_3\text{O}_8$ under reaction conditions. The support of the uranium phase plays a very important role on its performance. ZrO_2 allows depositing of the oxidic uranium phase in the form of film-like nanostructures and atomic dispersion, thus leading to a superior catalyst. $\text{U}_3\text{O}_8/\text{ZrO}_2$ activates under reaction conditions before reaching a stable performance after *ca.* 85 h on stream. The catalyst activation is related to *in situ* re-dispersion and gradual transformation of the original $\alpha\text{-U}_3\text{O}_8$ phase into a more oxidic and atomically dispersed UO_x . An uncalcined sample allows faster generation of this highly dispersed UO_x . The unique robustness of ZrO_2 supported uranium oxide under the harsh reaction conditions and stable Cl_2 production for more than 100 h on stream justifies its consideration as a high-temperature HCl oxidation catalytic technology. Uranium materials are less sensitive to metal loss and sintering than other known catalysts and are cost-effective since they can be prepared from waste produced in the uranium-enrichment processes.



Experimental

Materials

ZrO₂-monoclinic (Saint-Gobain NorPro, 99.8%), γ -Al₂O₃ (Alfa Aesar, catalyst support, 43855), SiO₂ (ABCR, 99%), and TiO₂-anatase (Aldrich, nanopowder, 99.7%) were calcined at 773 K (10 K min⁻¹) for 5 h prior to their use. The starting uranium compounds UO₂ and UO₂(NO₃)₂·6H₂O (International Bio-Analytical Industries) derive from depleted uranium sources and were used as received. The most important precaution for the safe handling of uranium compounds is to avoid their access to the body, through direct contact with the skin and/or inhalation, and dispersal in the environment. In the present case, personal protective equipment such as impervious gloves, boots, and an apron were worn to prevent skin contact. U₃O₈ and UO₃ were prepared by thermal decomposition of UO₂(NO₃)₂·6H₂O in static air following existing protocols.^{8,42} U₃O₈ was obtained by two-step calcination of UO₂(NO₃)₂·6H₂O. The uranyl nitrate was treated at 573 K (5 K min⁻¹) for 1 h and then, without intermediate cooling, at 1073 K (5 K min⁻¹) for another 3 h. UO₃ was synthesised by calcination of the uranyl nitrate at 723 K (5 K min⁻¹) for 3 h. Supported catalysts were prepared by dry impregnation of the carriers with an aqueous solution of uranyl nitrate (nominal 1–20 wt% U), followed by drying at 338 K for 12 h and calcination, according to the same protocol applied for the synthesis of bulk U₃O₈. Unless stated otherwise, the supported catalysts, denoted as U₃O₈/support, contain 10 wt% U.

Characterisation techniques

Powder X-ray diffraction (XRD) was measured in a PANalytical X'Pert PRO-MPD diffractometer. Data were recorded in the 10–70° 2 θ range with an angular step size of 0.017° and a counting time of 0.26 s per step. N₂ sorption at 77 K was performed in a Quantachrome Quadrasorb-SI gas adsorption analyser. Prior to the measurement, the samples were evacuated at 473 K for 12 h. Temperature-programmed reduction with hydrogen (H₂-TPR) was measured in a Thermo TPDRO 1100 unit. The samples were loaded in a quartz micro-reactor (11 mm i.d.), pre-treated in He (20 cm³ STP min⁻¹) at 473 K for 30 min, and cooled to 323 K in He. The analysis was carried out in 5 vol% H₂/N₂ (20 cm³ STP min⁻¹), ramping the temperature from 323 to 1173 K at 10 K min⁻¹. High-resolution transmission electron microscopy (HRTEM) measurements were undertaken on a FEI Tecnai F30 microscope (field emission gun), operated at 300 kV. High-angle annular dark field scanning transmission electron microscopy (HAADF-STEM) investigations were performed on an aberration-corrected Hitachi HD-2700CS microscope, operated at 200 kV and equipped with an energy-dispersive X-ray spectrometer (EDXS, EDAX) for elemental analysis. The incorporated probe correction system (CEOS) enables a resolution of below 0.1 nm to be achieved.⁴³

Catalytic tests

The gas-phase oxidation of hydrogen chloride was studied at ambient pressure in a continuous-flow set up⁴⁴ composed of mass-flow controllers to feed HCl (Messer, purity 2.8, anhydrous), O₂ (Pan Gas, purity 5.0), Cl₂ (Messer, purity 2.8,

anhydrous), and N₂ (Pan Gas, purity 5.0), a home-made electrically heated oven hosting a 8 mm i.d. quartz micro-reactor, and a Mettler Toledo G20 Compact Titrator for quantitative Cl₂ analysis in the product stream. The catalysts were loaded in the tubular reactor and pre-treated in N₂ at 673 K for 30 min. Thereafter, steady-state experiments at variable bed temperatures ($T_{\text{bed}} = 673\text{--}823$ K), inlet O₂/HCl ratios (0.5–7), and catalyst amounts ($W = 0.25$ or 0.5 g for supported or bulk catalysts, respectively) were carried out. The inlet HCl concentration and total volumetric flow (F_T) were fixed at 10 vol% and 166 cm³ STP min⁻¹, respectively. The O₂/HCl dependence was measured by increasing the O₂ content in the inlet mixture from 5 to 70 vol% with N₂ as balance gas. The influence of Cl₂ co-feeding on the rate of HCl oxidation was studied by introducing variable amounts (2–5 cm³ STP min⁻¹) of Cl₂ to the inlet feed with O₂/HCl = 2 at 733 K and 703 K over U₃O₈/ZrO₂ and CeO₂/ZrO₂, respectively. Used samples were collected for characterisation after rapidly cooling down the reactor to room temperature in N₂ flow. The percentage of HCl conversion was determined as $X_{\text{HCl}} = (2 \times \text{mole Cl}_2 \text{ at the reactor outlet} / \text{mole HCl at the reactor inlet}) \times 100$.

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