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# Direct air capture: process technology, techno-economic and socio-political challenges

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Climate change mitigation scenarios that meet the Paris Agreement's objective of limiting global warming usually assume an important role for carbon dioxide removal and negative emissions technologies. Direct air capture (DAC) is a carbon dioxide removal technology which separates CO<sub>2</sub> directly from the air using an engineered system. DAC can therefore be used alongside other negative emissions technologies, in principle, to mitigate CO<sub>2</sub> emissions from a wide variety of sources, including those that are mobile and dispersed. The ultimate fate of the CO<sub>2</sub>, whether it is stored, reused, or utilised, along with choices related to the energy and materials inputs for a DAC process, dictates whether or not the overall process results in negative emissions. In recent years, DAC has undergone significant technical development, with commercial entities now operating in the market and prospects for significant upscale. Here we review the state-of-the-art to provide clear research challenges across the process technology, techno-economic and socio-political domains.

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## Broader context

Direct air capture (DAC) is an engineered process for removing CO<sub>2</sub> directly from the air. It is technically challenging as CO<sub>2</sub> is present at ~0.04% in the air. This is some 2–3 orders of magnitude lower in concentration than other commonly targeted sources for capturing CO<sub>2</sub>, such as flue gases resulting from energy generation and industrial processes. Nonetheless, DAC has received an increasing amount of attention due largely to development and deployment by a limited number of start-ups. There is also a growing body of research on new materials and processes for DAC, and a need to understand the financial costs and environmental impacts associated with DAC. Moreover, there are emerging questions related to public acceptance, policy requirements, and integration of DAC in the energy system, particularly as related to the energy transition and climate change mitigation. This review article seeks to broadly appraise and interrogate these themes to highlight emerging research challenges across the scientific, engineering, economic, and socio-political domains.

## 1 Introduction

Climate change is the biggest challenge humanity has ever faced. This is due to its effects being both profound and global. Human activities are unequivocally responsible for an increase in atmospheric concentrations of greenhouse gases (GHGs) since the Industrial Revolution (*ca.* 1750).<sup>1</sup> The concentration

of carbon dioxide (CO<sub>2</sub>), the primary GHG responsible for driving climate change, increased from a pre-industrial value of 280 ppm to 412 ppm in 2020, the highest value in at least 2 million years.<sup>2</sup>

Observed global temperature is increasingly higher than that simulated accounting for natural factors alone, with human activity explaining all the deviation (Fig. 1). As a result, mean global surface temperature has increased by 1.07 °C to date and each of the last four decades has been successively warmer than any previous decade since 1850.<sup>3</sup> Global temperature increase has already caused widespread retreat of glaciers and Arctic ice, a sea level increase of ~0.2 m, as well as more frequent and intense heavy precipitation events and hot extremes.<sup>1</sup> All additional warming makes abrupt and irreversible changes in the climate system more likely. These are usually referred to as tipping points.<sup>4</sup>

Unless the global economy is rapidly decarbonised, *i.e.*, GHG emissions are halved in the next decade and net-zero is

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achieved by *ca.* 2050, global mean temperature will increase by at least 2 °C by 2050 compared to the 1850–1900 average. This is projected to result in 1.7 times more frequent heavy precipitation events, 2.4 times more frequent droughts and 13.9 times more frequent hot temperature extremes.<sup>1</sup> Moreover, projected sea level rise will result in the flooding of land used by 100 million people worldwide,<sup>5</sup> and 30–140 million people of the Global South becoming climate refugees.<sup>6</sup>

### 1.1. Strategies for reducing CO<sub>2</sub> emissions

To avoid the worst outcomes of an exacerbated climate change, the Paris Agreement was signed in 2015 with the aim of “holding the increase in the global average temperature to well below 2 °C above pre-industrial levels and pursuing efforts to

limit the temperature increase to 1.5 °C”. With that aim, net emissions of GHGs should halve over the next decade and become net-zero by 2050. Considering that current annual emissions are over 35 billion tCO<sub>2</sub>e,<sup>7</sup> the magnitude of the task becomes evident. Current pledges announced by all countries towards decarbonization would only result in a fall in CO<sub>2</sub> emissions of 40% by 2050.<sup>8</sup> At the time of writing, the most recent UN Climate Change Conference of Parties (COP26) seeks to improve upon these.

To tackle GHG emissions, all sectors must be scrutinized, however, energy-related applications are responsible for over two thirds of total emissions.<sup>9</sup> These are mostly allocated to industry, transport and buildings. Thus, most efforts to curb emissions are aimed at decreasing energy consumption,



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Fig. 1 Change in global surface temperature (annual average) as observed and simulated using human and natural, and only natural factors (both 1850–2020). Taken from Fig. SPM.1 b in ref. 1.

electrification of the energy system, and decarbonizing electricity generation.

**Decreasing energy consumption.** A mere substitution of fossil fuels with renewable energy technologies would miss the benefits of a wholesale ecological transition, including improved energy efficiency, a more circular economy, and more sustainable and environmentally-friendly practices. These factors are taken into account in the models to reach net-zero emissions in 2050 proposed by several institutions.<sup>8,10–13</sup> By combining all of the factors, a significant reduction in final energy consumption compared to current levels can be reached. Reductions of 5–6%,<sup>‡10,11</sup> 8%,<sup>8,12</sup> and 23% are

‡ IPCC “Sustainable energy demand” scenario is considered (S1, based on SSP1).

deemed possible.<sup>§13</sup> Although the smaller reductions may seem negligible, they represent global change after 30 years, including a development of all regions, especially those whose current energy use is insufficient and needs to be increased. On the other hand, ‘business as usual’ scenarios in the same reports project higher energy consumption than today. Degrowth scenarios go further and directly propose reductions in Gross Domestic Product (GDP) trajectories, including sharper reductions in final energy consumption, and ultimately finding a non-economic variable to express quality of life. High energy-GDP decoupling and lower final energy consumption require a slower expansion of renewable energy and deployment of fewer negative emission technologies (NETs). These models claim a lower risk for socio-technical feasibility, but entail a higher risk for socio-political feasibility.<sup>14</sup>

**Electrification of the energy system.** Renewable energy will play a dominant role in 2050 according to virtually all projections. These projections are coherent with current data, since renewables are already the cheapest technology for electricity production,<sup>15</sup> and they account for over 80% of annually installed capacity, with renewable power installed in 2020 being four times higher than the contribution of coal, gas and nuclear plants combined.<sup>16</sup>

During the 1970’s and 1980’s, the share of nuclear in global energy consumption went from 0 to 6.6% in a few decades and hundreds more nuclear reactors were projected worldwide. However, the trend stopped abruptly and the share of nuclear has declined steadily, reaching 4.3% in 2020.<sup>17</sup> Even though alternative coolants, passive cooling, and fast-spectrum and small modular reactors offer improvements over current technology, the future role of nuclear fission in net-zero models is unclear – some studies anticipate significant increases in operating capacity while some others project continued

§ Excluding non-combusted.



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decline.<sup>8,10–13</sup> Apart from social acceptance and proliferation concerns, nuclear power faces two major challenges: the significant time between decision and commissioning of new plants ( $\sim 10$ – $20$  years),<sup>11</sup> and the high cost of the obtained electricity (3–4 times more expensive than solar and wind energy).<sup>15</sup> Even though nuclear power can provide baseload supply, the drawbacks above make a quick and cheap energy transition difficult, eroding the interest of most countries in this technology, which has even been referred to as “the non-solution solution”.<sup>18</sup>

**Carbon capture and storage.** Even considering the best-case scenario (a sharp reduction in energy consumption, significant transition to renewable energies, *etc.*) emissions will likely still occur due to land use, land use change and forestry, agriculture, industry, waste, and other hard-to-abate sectors. Moreover, in the medium term, fossil-fuel power generation facilities may be required for peak load provision. To offset these emissions and reach net-zero goals, additional technologies are needed.

According to the Intergovernmental Panel on Climate Change (IPCC), carbon capture and storage (CCS) processes are necessary to achieve the Paris Agreement goals at lowest cost; a lack of scalable CCS technologies by the end of the century would entail an increase of 29–297% (mean value 138%) in total mitigation costs compared to default technology assumptions (scenarios without CCS but with other low-carbon technologies) to limit the atmospheric CO<sub>2</sub> concentration at 450 ppm (currently the atmospheric concentration is  $\sim 419$  ppm).<sup>¶</sup><sup>11</sup> This increase is significantly higher than that corresponding to any other scenario with a limited availability of technologies (*e.g.*, reduced renewable energy penetration).

CCS technologies are proposed to reduce the rate of release of CO<sub>2</sub> from large, stationary sources by capturing a large portion of CO<sub>2</sub> from gas mixtures destined for the atmosphere, with subsequent storage of CO<sub>2</sub> in geological sites. Thus, they may find application in sectors where CO<sub>2</sub> emissions cannot be avoided as they are inherent to the process, *e.g.*, steel and cement production, and the production of various chemicals, as well as from any remaining fossil-fuel power generation. Carbon dioxide removal (CDR) technologies seek to go further, removing CO<sub>2</sub> already present in the air. If a specific CDR technology results in net-negative CO<sub>2</sub> emissions, *e.g.*, it is powered by renewable energy and the captured CO<sub>2</sub> is stored, then it may be called a NET. Among various NETs, two of them stand out as variations of CCS: bioenergy with carbon capture and storage (BECCS) and direct air carbon capture and storage (DACCS).

## 1.2. Contribution and structure of the review

This review article focusses on the upstream aspect of DACCS, *i.e.*, direct air capture (DAC). To date, DAC has largely been developed by a small number of start-ups. Thus, past reviews of

DAC have focused on materials used in those processes. Instead, here we seek to take a holistic view of DAC to identify research challenges across multiple length and time scales, and therefore disciplines. First, in Section 2, we briefly discuss the advantages and limitations of some photosynthesis-based NETs, to set a context for DAC in terms of costs, energy requirements and interaction with Earth systems. In this section we also consider DAC at a high level, *i.e.*, the potential role of DAC in climate change mitigation, and in CO<sub>2</sub> reuse and utilisation. In Section 3, we appraise the most developed DAC processes to identify the research challenges that have emerged during deployment, and how new materials could be used to address these, or to develop modified processes. Uniquely, we also identify entirely new approaches to DAC that are beginning to appear in the literature, *e.g.*, those relying on electrochemical devices. In Section 4 we assess the cost and sustainability of DAC in detail, reviewing recent work on techno-economic analysis (TEA) and life-cycle analysis (LCA). In Section 5, for the first time, we identify the socio-political challenges that will require consideration if DAC develops as a component of the energy system and climate change mitigation efforts. Finally, we provide concise, high-level research challenges that the science, engineering, economics, and socio-political communities must tackle in the coming years to develop more efficient, sustainable, and societally acceptable DAC technologies.

## 2 Negative emissions technologies and direct air capture

### 2.1. Background on negative emissions technologies

It has been widely suggested that NETs will be necessary to reach climate targets, especially the 1.5 °C goal set by the Paris Agreement.<sup>19–24</sup> In spite of this and the increasing need for NETs, current knowledge is incomplete,<sup>25,26</sup> but is however developing at a fast pace.<sup>23,24</sup> The last IPCC report, AR5, stressed the importance of NETs in order to achieve the 2 °C scenario also; however, it highlighted the uncertainties regarding the availability, scale and possible negative impacts of NETs.<sup>27</sup> Only two NETs have been incorporated into the most recent assessment by the IPCC; BECCS, and afforestation and reforestation (AR).<sup>28</sup> There may be more NETs included in the analysis used for their new assessment report, AR6, which is due to be released in 2022. It is, however, always important to note that NETs are complementary technologies to conventional decarbonisation and climate change mitigation options, not a substitute.<sup>29</sup>

NETs have been described as, “the intentional human efforts to remove CO<sub>2</sub> emissions from the atmosphere”.<sup>24,30,31</sup> A wide variety of NETs have been proposed in literature; some of these technologies are well investigated such as AR, and soil carbon sequestration (SCS), while others are in earlier stages of development.<sup>31,32</sup> NETs can be categorised according to different variables such as technology category, implementation options, their interaction with earth systems, and CO<sub>2</sub> storage medium (Fig. 2). Five of the seven technology categories in

¶ During May 2021 the atmospheric CO<sub>2</sub> concentration averaged 419.13 ppm at the National Oceanic and Atmospheric Administration Mauna Loa Atmospheric Baseline Observatory.



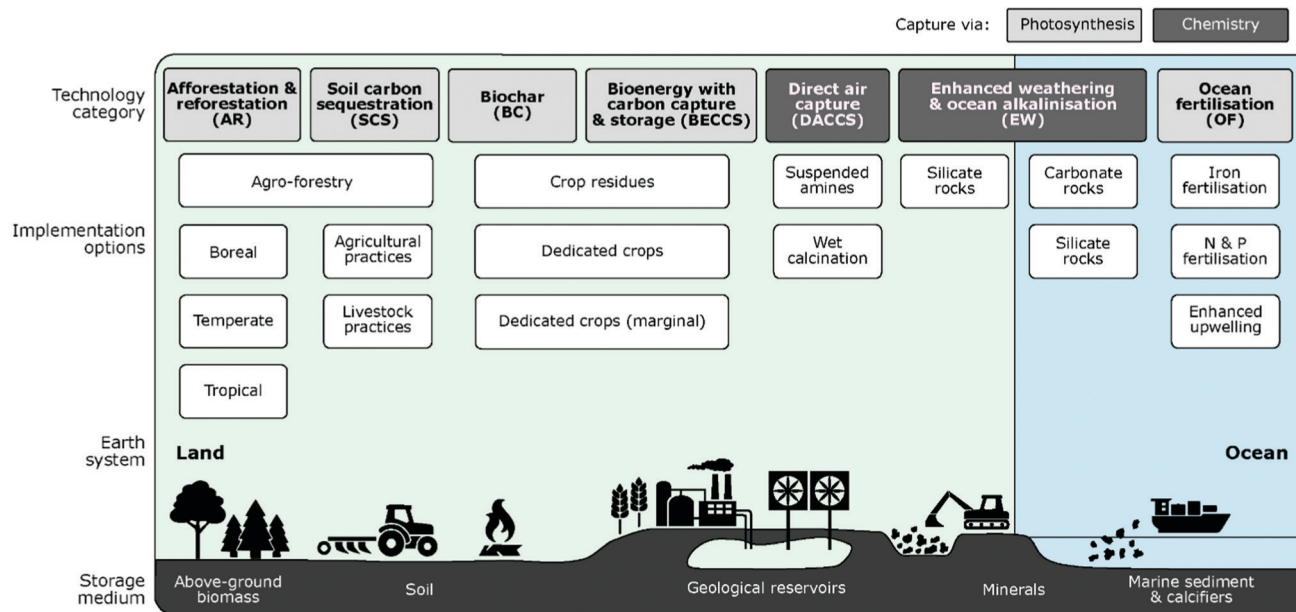


Fig. 2 NET pathways. Taken from Negative emissions – part 1: research landscape and synthesis, ref. 24, licensed under CC BY 3.0.

Fig. 2 (AR, SCS, biochar (BC), BECCS, and ocean fertilisation (OF)) use photosynthesis to capture CO<sub>2</sub> from the air, while DAC, ocean alkalisation (OA) and enhanced weathering (EW) chemically bind CO<sub>2</sub> to synthetic or natural materials, respectively. Other technological divisions can be made, such as whether the technology is land or ocean based, domestic or transboundary, and based on the selected storage medium.<sup>24</sup>

**Afforestation and reforestation.** One of the most studied NETs is AR; both approaches can capture atmospheric CO<sub>2</sub>. Estimated costs for AR range from 2–150 \$ per tCO<sub>2</sub>,<sup>33–36</sup> and the potential for CO<sub>2</sub> capture from 0.5–7 GtCO<sub>2</sub> per year.<sup>37</sup> There are several issues to be considered when implementing AR, including albedo change, biodiversity loss and CO<sub>2</sub> storage timescale.<sup>38–42</sup> There is scientific agreement that deploying AR in high altitude forests is counterproductive due to local warming and the rapid increase of snow and ice loss. However, there are fewer studies on the potential loss of biodiversity that arises from large-scale AR implementation. Instead, individual investigations on a case-by-case basis can be found.<sup>43</sup> AR using native species is superior for biodiversity,<sup>44,45</sup> however, the amount of CO<sub>2</sub> captured by such efforts is generally lower as diverse cultivated areas are less susceptible to climate variations,<sup>46</sup> and may provide more services such as food.<sup>46,47</sup> The residence time of CO<sub>2</sub> stored by AR is much shorter than for geologically stored CO<sub>2</sub>.<sup>48</sup> The time scale varies from centuries when dealing with forests, to thousands of years or longer for geological storage. Moreover, AR implementation may be disturbed naturally (*i.e.*, by fires, pests, and droughts) or by human action (change in land use). These challenges, alongside the fact that it is difficult to monitor the storage potential and global contribution to CO<sub>2</sub> levels in the atmosphere, may deem AR as a less attractive option for climate change mitigation.

**Soil carbon sequestration.** SCS is a well known practice that arises from increasing the organic carbon content of soil, which causes a net CO<sub>2</sub> removal from the atmosphere. SCS is essentially a soil mass balance with carbon inputs (manure, residues, *etc.*) and outputs (soil respiration).<sup>49</sup> There are two schemes for SCS; namely, increasing carbon inputs or decreasing carbon outputs. Possible beneficial effects of SCS implementation are improved soil quality,<sup>50</sup> and higher crop yield.<sup>51</sup> Nonetheless, SCS may also increase CH<sub>4</sub> emissions when manure is used as an additive,<sup>52</sup> and NO<sub>x</sub> emissions when nitrogen-based fertilisers are used.<sup>53</sup>

Key advantages of SCS include that it can be applied without changing land use, and that the practices involved are well understood and can be deployed immediately. Additionally, the water footprint of SCS has been deemed to be relatively minor.<sup>54</sup> The main disadvantage of SCS is sink saturation, *i.e.*, a limited amount of carbon can be stored in soil even with the use of SCS technologies.<sup>55</sup> The initial carbon capture rate is high but it decreases with time to zero, when a new equilibrium is reached.<sup>56,57</sup> The saturation period varies from decades to centuries depending on the technology and soil temperature *etc.*, but the standard saturation period is considered to be ~20 years.<sup>54</sup> Moreover, if the carbon is to remain in the soil these practices need to be maintained after the soil has reached saturation, with an associated cost, otherwise the CO<sub>2</sub> will be released to the atmosphere.<sup>56,58</sup> Finally, the potential storage capacity of SCS varies significantly, depending on where it is applied. Thus, more studies are required to compare and unify criteria, and to address the scarcity of cost estimates (of the few in the literature, ~20–100 \$ per tCO<sub>2</sub> for ~1.4–3.7 GtCO<sub>2</sub> per year).<sup>30</sup>

**Biochar.** The use of BC as a NET again relies on increasing the capacity of soil to absorb CO<sub>2</sub> (noting that it can also



increase soil fertility). Many positive effects have been reported in the literature, including an increase in crop productivity, lower N<sub>2</sub>O and CH<sub>4</sub> emissions (from alternative fertilisation practices), and lower water losses from soil.<sup>59</sup> On the other hand, high BC addition rates can change soil composition, with long-term effects not well understood.<sup>60</sup> The potential release of BC due to wind and soil erosion should also be taken into account as it may decrease air quality.<sup>61,62</sup> One of the main drawbacks, however, is price, which inhibits its large-scale application. Besides, BC must remain in the soil for as long as possible for it to result in long-term storage. Studies suggest a timescale of decades or centuries,<sup>63,64</sup> depending on soil and temperature, with longer times in higher temperature areas,<sup>65</sup> and in acidic soils.<sup>66,67</sup> The traceability of the sequestered carbon may be difficult to measure and monitor; therefore, research efforts should be directed towards solving this challenge.

One of the main challenges for assessing BC use is the lack of field studies; the efficacy of BC is extremely site dependent as soil varies with location, climate, *etc.* Therefore, comprehensive studies on feasibility, CO<sub>2</sub> storage capacity and timescale, soil type, BC materials, and potential side effects are urgently required. Recently, field studies looking at CO<sub>2</sub> emissions on BC treated fields are emerging, showing the potential use of this technology in different areas.<sup>68–71</sup> Another key point that should be carefully considered is the realistic availability of biomass for BC production, as it will have to compete with biomass conversion and combustion for energy production. The estimated capture potential of using BC ranges from 0.6–11.9 GtCO<sub>2</sub> per year depending on biomass availability.<sup>72–74</sup> The projected cost of this technology ranges from 60–120 \$ per tCO<sub>2</sub>, with higher prices for dedicated feedstocks which points towards using waste materials where possible.<sup>54,75,76</sup>

**Bioenergy with carbon capture and storage.** To consider bioenergy processes a net-zero emissions technology, the same amount of CO<sub>2</sub> released during biomass combustion must be fixed by growing biomass. If the combustion emissions are captured and stored (using *e.g.*, typical CCS technology), the overall system (*i.e.*, BECCS) can generate negative emissions.<sup>77–80</sup>

The main limiting factors for the large-scale deployment of BECCS are land, biomass and storage availability.<sup>26,78,81</sup> Side effects of BECCS include the emissions derived from land use change, such as those produced from deforestation, and land use change induced by economic markets. Additionally, as with other NETs, the albedo effects of cultivating biomass for BECCS should be considered. For example, at higher altitudes, biomass cultivation can lead to a reduction in the area of reflective snow surfaces.<sup>82</sup> Land competition should be carefully investigated as well, as BECCS could have an impact on biodiversity, water use, and nutrient availability/distribution.<sup>80,83–86</sup> Mass deployment of BECCS may also pose a threat to food security and potentially lead to higher food prices.<sup>87,88</sup> Recently, integrating BECCS with algae-based processes has been proposed, which will be discussed further below. This biomass alternative

has a high photosynthetic efficiency and high yields,<sup>89</sup> and it may also help in reducing land competition.<sup>90</sup>

Even with the challenges presented, BECCS still has significant potential to contribute to the energy transition, with an estimated energy production in 2050 of 60–1548 EJ per year.<sup>91–94</sup> The estimated cost of BECCS ranges from 15–400 \$ per tCO<sub>2</sub>.<sup>95–97</sup> Note that the issues around BECCS described here are complex, and inter-dependent, and have thus been the subject of more detailed discussion than is suitable here.<sup>98–101</sup>

**Non-photosynthesis-based negative emissions technologies (ocean alkalisation and enhanced weathering).** Non-photosynthesis-based NETs can be likened to DAC on the basis that they rely on the chemical binding of CO<sub>2</sub> in the air. OA, also known as ocean liming, is based on the addition of alkaline solids (*e.g.*, calcium hydroxide) to marine environments to increase the CO<sub>2</sub> capacity of the ocean.<sup>102,103</sup> The potential for OA has been estimated to be 0.1–10 GtCO<sub>2</sub> per year with a cost range of 14–500 \$ per tCO<sub>2</sub>.<sup>102</sup> Few studies have investigated OA and the results are still in the early stages of modelling. Thus, more research is needed to elucidate whether OA could be implemented at scale, and what the potential benefits and side effects are. EW generally involves the spreading of pulverized alkaline materials on to the Earth's surfaces (including the oceans, *i.e.*, OA) to mimic and/or accelerate natural weathering processes. The materials employed include silicate and carbonate minerals,<sup>104</sup> and waste materials like mine tailings and industrial by-products. As there are significant synergies between these non-photosynthesis-based NETs and DAC, we will consider these throughout the review.

## 2.2. The potential role of direct air capture in climate change mitigation

The use of DAC for climate change mitigation was first introduced by Lackner in the 1990's.<sup>105</sup> In the following years many studies and comments aimed to assess the practical relevance of DAC in reducing atmospheric CO<sub>2</sub> levels.<sup>106–115</sup> Experimental works were published too, but their number only increased significantly a decade or so after the concept of DAC was introduced.

DACCS is often compared with CCS due to their similarity. While the goal of CCS is to reduce the rate of CO<sub>2</sub> emissions from a specific process (or group of processes), DACCS targets the removal of CO<sub>2</sub> that is already in the atmosphere. Thus, CCS technologies are typically proposed for large, stationary sources of CO<sub>2</sub>, but not for distributed and mobile sources. However, as distributed sources account for approximately half of global CO<sub>2</sub> emissions, DACCS is increasingly proposed as a NET. Thus, DACCS and CCS technologies should be considered as complementary, with DAC offering some unique potential advantages. For example, DAC facilities process air, which typically has lower amounts of contaminants present in flue gases (SO<sub>2</sub>, NO<sub>x</sub>, *etc.*) that usually reduce the performance and life span of CO<sub>2</sub> sorbents. Moreover, DAC is not limited to locations with large, stationary CO<sub>2</sub> sources; in principle, it can be applied anywhere (however, ideally this would be in proximity with both an energy source and CO<sub>2</sub> storage site). This can



potentially lead to multiple advantages: existing industries that operate on a relatively small scale do not need to modify their processes; CO<sub>2</sub> producing facilities that are geographically remote do not require extensive CO<sub>2</sub> transport infrastructure; DAC facilities can be co-located with renewable energy generation facilities to reduce transmission losses, and/or with CO<sub>2</sub> storage facilities to minimise transport costs and infrastructure.

Despite the potential advantages of DAC, there are also uncertainties. For example, as with CCS, the environmental risks and uncertainties associated with CO<sub>2</sub> storage (cost, long-term monitoring, induced seismicity, and leakage) should be addressed,<sup>116</sup> as well as specific DAC-related concerns on the financial, energy and materials requirements, as well as socio-political acceptance. All these topics are discussed in detail in later sections of this review.

### 2.3. Direct air capture and CO<sub>2</sub> use/utilisation

Although geological storage of CO<sub>2</sub> should be the primary aim for climate change mitigation strategies (*i.e.*, DACCS), CO<sub>2</sub> captured from the air can also be used directly or utilised as a feedstock in the production of valuable products such as chemicals or fuels. The use or utilisation of CO<sub>2</sub> in this way can lower the net costs of DAC technologies and recycle a useful material that otherwise would be stored in deep reservoirs.<sup>117</sup> A number of routes can be followed to use or utilise CO<sub>2</sub>,<sup>118–120</sup> with a selection of these introduced to provide context for later discussions.

**Enhanced oil recovery.** Captured CO<sub>2</sub> is already being used to recover oil from semi-depleted oil fields through enhanced oil recovery (EOR), a type of tertiary oil recovery. EOR can recover up to 15–20% of the original field, with the US producing around 3.5% of their annual domestic oil output using EOR.<sup>121</sup> According to the International Energy Agency (IEA), for every oil barrel produced using captured CO<sub>2</sub>, a net 0.19 metric tons CO<sub>2</sub> are stored.<sup>122</sup> However, it seems counterintuitive to use captured CO<sub>2</sub> to extract more oil that will generate CO<sub>2</sub> *via* combustion, particularly if the CO<sub>2</sub> is captured from the air *via* DAC. In this line, the IEA has recently pointed out that no new investments in fossil fuels should be made in order to comply with the Paris Agreement goals,<sup>123</sup> so it is necessary to find other uses for CO<sub>2</sub> that are both profitable and clean.

**CO<sub>2</sub> conversion to fuels and chemicals.** Obtaining fuels (gasoline, diesel and jet fuel) and chemicals (methanol, methane, formic acid, and formaldehyde) from captured CO<sub>2</sub> is arguably a more promising alternative to EOR in certain situations.<sup>124</sup> These products have the capability of displacing conventional fossil fuels directly or indirectly. In the case of fuels, current transport infrastructure can still be used and besides, they could help to decarbonize hard-to-abate sectors such as maritime transport and aviation. To convert CO<sub>2</sub> to such compounds, CO<sub>2</sub> must be reduced *via* thermodynamically unfavourable reactions due to the high stability of CO<sub>2</sub>. Two main routes can be followed: hydrogenation and electrochemical reduction. These technologies are also known as ‘Power to X’ (where X is the molecule of interest) since they are also proposed as a route to storing surplus renewable electricity.

The use of captured CO<sub>2</sub> would generate an interesting synergy to aid decarbonization efforts: storing renewable energy, reducing CO<sub>2</sub> emissions, and obtaining fuels for transportation.

Syngas, a mixture of H<sub>2</sub> and CO, is an intermediate used in the production of synthetic ammonia and methanol, among other compounds. Steam reforming of fossil gas is currently the most widespread route to obtain syngas. This process emits CO<sub>2</sub> to the atmosphere. CO<sub>2</sub> reforming (also known as dry reforming) is an alternative method of producing syngas by reacting CO<sub>2</sub> and methane.<sup>125</sup> Dry reforming requires high temperatures (900–1200 K) and the deposition of soot deactivates the catalyst, so it is not yet widely utilised.<sup>126</sup>

Methanol is an important building block in the synthesis of olefins, dimethyl ether, and fuels, and is thus capable of displacing fossil fuels.<sup>127,128</sup> Besides, methanol can be used as an energy carrier. As a liquid, it can be handled and transported more easily than gases or solids.<sup>129</sup> Methanol is currently produced from syngas that, in turn, is obtained from fossil fuels. However, it can also be produced from CO<sub>2</sub> in one of the simplest processes available to convert CO<sub>2</sub> into liquid products.<sup>127</sup> Electrochemical reduction,<sup>130–132</sup> and catalytic hydrogenation,<sup>133,134</sup> processes can be used. Large plants show more potential, with facilities producing as much as 50 000 tMeOH and using 71 600 tCO<sub>2</sub> per year suggested as being feasible.<sup>134</sup>

Methane is currently used to produce electricity, heat, and chemicals. Methane is primarily obtained from natural gas, and is referred to as substitute natural gas (SNG) when obtained sustainably.<sup>135</sup> SNG has a high purity and can be injected directly into the natural gas grid. As above with methanol, methane can be synthesised by two main paths: electrochemical reduction,<sup>136–138</sup> and catalytic hydrogenation (methanation),<sup>139,140</sup> of CO<sub>2</sub>.

Gasoline, diesel, and kerosene are classically obtained *via* the Fischer–Tropsch process using H<sub>2</sub> and CO to obtain alkanes, which are subsequently upgraded.<sup>141</sup> Alternatively, clean methanol can be transformed into fuels by means of industrial processes such as olefin synthesis, oligomerization, and hydrotreating,<sup>141</sup> or dimethyl ether can be transformed into high-octane gasoline.<sup>142</sup>

**Products from microalgae.** Biological carbon fixation is the conversion of CO<sub>2</sub> into organic carbon through photosynthesis by autotrophic organisms, such as algae.<sup>143</sup> Photosynthesis occurring in the ocean accounts for 40% of all carbon fixed annually.<sup>144</sup> Thus, algae could be cultivated and employed in engineered processes, either in a DAC process or with CO<sub>2</sub>-enriched air. Microalgae present ten times higher solar energy conversion efficiency into biomass than terrestrial plants,<sup>89</sup> and they grow quickly, *e.g.*, doubling their population on the time-scale of a few hours. They are deemed as a promising CO<sub>2</sub> sink as 1.83 kg of CO<sub>2</sub> can be fixed by cultivating one kg of microalgae.<sup>145</sup> Moreover, several products of interest can be obtained from microalgae, such as food, biofuels, and cosmetics, *etc.*<sup>146</sup> However, the main limitation is mass transfer from the air to the medium.<sup>147,148</sup> Other parameters affect the CO<sub>2</sub> capture capacity of algae, namely, temperature and light intensity. Higher temperatures and high light intensity have been linked to higher CO<sub>2</sub> fixation rates.<sup>145,149</sup>



New engineered concepts using algae are emerging. First, ABECCS (algae and bioenergy with CCS) has been proposed, where land biomass is used in a combustion process to produce electricity, and a portion of the captured CO<sub>2</sub> is used for algae cultivation, whilst the rest can be stored.<sup>90</sup> Second, microbial carbon capture cells (MCCs) have also been investigated for mitigating CO<sub>2</sub> emissions, where the off gas is transferred to an algal cathode chamber, which leads to waste water treatment, algal growth and electricity generation by a voltage shift without energy input.<sup>150,151</sup>

### 3 Direct air capture process technology; state of the art and opportunities

#### 3.1. Chemical separation processes and application to CO<sub>2</sub> separation

The production of key global resources such as chemicals, fuels, foods, and medicines routinely involves separation processes. These may be based upon distillation, drying, evaporation, extraction, sorption, membranes and crystallisation (presented in approximate descending order of energy-intensity and from thermal to non-thermal processes).<sup>152</sup> Due to the ubiquity of separation processes and the extensive use of energy-intensive, thermal separation processes, separations currently account for ~10–15% of the world's energy consumption.<sup>153</sup>

**History of gas separation processes.** Gas separation processes are employed in the production of fuel gases (*e.g.*, CH<sub>4</sub>, H<sub>2</sub> *etc.*), industrial gases (*e.g.*, N<sub>2</sub>, O<sub>2</sub> *etc.*), and noble gases (*e.g.*, Ar, He *etc.*). They are also at the core of many emissions control technologies (*e.g.*, CO<sub>2</sub>, SO<sub>x</sub>, *etc.*). An extremely brief history of gas separation is useful to frame the following discussion on DAC materials and processes.

Distillation has been practiced for centuries and is now ubiquitous in the petrochemical industry for *e.g.*, ethylene recovery following steam cracking of saturated hydrocarbons. Distillation at cryogenic temperatures for air separation was developed in the late 19th century and is still the most economically competitive technology for the production of high-purity N<sub>2</sub>, O<sub>2</sub>, and Ar at the largest scales.<sup>152</sup> Rare gases (Ne, Kr, Xe *etc.*) are almost exclusively produced *via* cryogenic distillation. Sorption-based gas separation processes appeared in the early 20th century for flue-gas desulfurization,<sup>154</sup> and more recently for *e.g.* H<sub>2</sub> production in the sorbent-enhanced water-gas shift reaction following steam-methane reforming.<sup>155</sup> Gas separation membranes were commercialised in the second half of the 20th century and are now available for the purification of CH<sub>4</sub>, and for H<sub>2</sub> and O<sub>2</sub> production. Contemporary developments have been in electrochemical devices for, and biological routes to, gas separation. All these gas separation processes (distillation, sorption, membranes, electrochemical and biological) have been studied, and in some cases deployed, for CO<sub>2</sub> separation, as part of CCS processes.

**State-of-the-art in CO<sub>2</sub> separation from 'concentrated' sources.** Typically, CCS processes target gas mixtures containing 'concentrated' CO<sub>2</sub>, such as point sources (*e.g.*, power

plants) or clusters of emitters (*e.g.*, industrial regions). In these locations, CO<sub>2</sub> is found over a wide concentration range (~5–95%) in gas mixtures containing N<sub>2</sub>, O<sub>2</sub>, H<sub>2</sub>, CH<sub>4</sub>, and CO *etc.* Often the goal is to separate and concentrate CO<sub>2</sub>, as the resulting CO<sub>2</sub> may then be used directly, transformed (chemically or biologically), or stored geologically, with high efficiency. For separation (usually termed capture) at the most frequently studied sources, *i.e.*, power plants where flue gas streams contain ~5–15% CO<sub>2</sub>, a 90% capture rate is arbitrarily assumed and very often a high final CO<sub>2</sub> purity (>90%) is targeted. Higher than 90% capture rates can be economical and are technically possible using existing separation processes.<sup>156–158</sup> Such an approach could reduce the burden on NETs, like DAC, that are currently proposed to deal with residual emissions.

The pre-eminent ('TRL9 – Commercial') CO<sub>2</sub> separation process is a sorption one which uses aqueous amine solutions to absorb CO<sub>2</sub>. It is currently applied, in a relatively small number of locations,<sup>98</sup> as a post-combustion separation process at power plants and for natural gas processing. Polymeric membranes have also recently been demonstrated ('TRL7 – Demonstration') for CO<sub>2</sub> separation from syngas and during natural gas processing, whilst several other sorption and membrane processes span 'TRL3 – Proof of Concept' to 'TRL7 – Demonstration'.<sup>98</sup> Numerous high-quality review articles cover the development of CO<sub>2</sub> separation processes from concentrated sources,<sup>98,159–163</sup> with recent articles providing a detailed history of the pre-eminent aqueous amine sorption process,<sup>156</sup> and a TEA of the most mature absorption, adsorption and membrane processes.<sup>164</sup>

**CO<sub>2</sub> separation from the air; comparison with 'concentrated' sources.** Considering the separation of CO<sub>2</sub> from air, the most obvious difference is the concentration of CO<sub>2</sub> at the source (~0.04% or ~419 ppm in air),<sup>†</sup> some 2 to 3 orders of magnitude lower than that found in the previously mentioned sources. It follows that the kinetics of any gas separation process will be less favourable, and that the thermodynamic challenge is heightened (*i.e.*, it is more difficult to produce the same output CO<sub>2</sub> purity from air as compared to more concentrated sources of CO<sub>2</sub> like flue gases). Thus, it would be expected that the energy input required to separate and concentrate the CO<sub>2</sub> to the same output purity will increase. For example, to produce a 1 bar stream of CO<sub>2</sub> captured from air instead of from a more concentrated source (*e.g.*, flue gas at 12%), the intrinsic thermodynamic penalty increases by approximately a factor of 3.7, arriving at ~0.44 GJ per tCO<sub>2</sub> as a first estimate of the minimum energy requirement for DAC. A further ~0.28 GJ per tCO<sub>2</sub> would then be required to compress the 1 bar stream to 150 bar for *e.g.*, storage (*i.e.*, DACCS).<sup>165</sup> The general point to be made however, is that for DAC (and particularly separations where a large volume of low-value material is processed), any real process will require more energy than the thermodynamic minimum. For example, note that capture from concentrated sources today requires ~2–4 GJ per tCO<sub>2</sub>,<sup>98</sup> and that a range of estimates have been made from ~1–10 GJ per tCO<sub>2</sub> for DAC.<sup>111,166,167</sup>





On financial cost, a simple empirical relationship observed for separations generally (Sherwood's plot) suggests costs might be expected to increase from  $\sim 10^1$  \$ per tCO<sub>2</sub> to  $\sim 10^3$  \$ per tCO<sub>2</sub> when comparing CO<sub>2</sub> capture from concentrated sources to DAC.<sup>168</sup> It is worth noting that recent DAC demonstrations claim (or target) lower costs ( $< 10^2$  \$ per tCO<sub>2</sub>) due to the oversimplification of Sherwood's plot. Additionally, a case can be made that any costs should be weighed against the social cost of CO<sub>2</sub> emissions, for which estimates are now available ( $\sim 10^2$  \$ per tCO<sub>2</sub>).<sup>169</sup>

Detailed reviews of techno-economic and socio-political considerations are provided below, but for now it is important to acknowledge that no DAC process will ever be energetically or economically competitive with capture from more concentrated sources if similar capture conditions are considered (*i.e.*, percent captured and final CO<sub>2</sub> purity *etc.*).<sup>168,170</sup> However, it is important to note that DAC does not necessarily have to achieve

high percent capture or high final purity to be useful in the context of CDR; any amount of capture results in removal from the atmosphere. To achieve negative emissions, however, it is likely that a high final purity will be required for permanent geological storage, due to considerations around storage efficiency, phase behaviour and pipeline corrosion *etc.* Moreover, a detailed life-cycle analysis is required to account for *e.g.*, emissions from energy inputs to the system (however, we note that there are many low-carbon energy sources that can be used to achieve negative emissions from DACCS).<sup>171</sup> Additionally, for utilisation, which can achieve close to carbon neutrality if low-carbon energy is used, high purity CO<sub>2</sub> would permit the use of existing catalysts and endow favourable kinetics in reaction engineering scenarios *etc.*

DAC technologies have been demonstrated, or are planned to be demonstrated soon, using several different process configurations (Table 1). It is notable, as compared to other

**Table 1** Examples of DAC-related companies and projects. Note that with the rapid development of DAC, we do not seek to be comprehensive here

Company, project	Process technology	Ref.
Antecy, Carbon from Air (CAIR™)	Solid carbonate sorbent, temperature swing	177
Carbon Capture™	Zeolite molecular sieves, temperature-vacuum swing	178
Carbon Collect, MechanicalTrees™ for Passive Direct Air Capture (PDAC™)	Solid ion-exchange resin tiles, moisture swing	179
Carbon Engineering	Aqueous alkali hydroxide solution, oxy-fired circulating fluidised bed calcination	180
Carbon Engineering & Greyrock Energy, AIR TO FUELS™, Direct Fuel Production™, GreyCat™	Carbon Engineering DAC with Fischer–Tropsch catalysis	180
Carbon Engineering & Storegga Geotechnologies	Carbon Engineering DAC with geological storage	181
Carbon Engineering & 1PointFive (Oxy Low Carbon Ventures & Rusheen Capital Management)	Carbon Engineering DAC licensed to 1PointFive with EOR and geological storage	182
Carbyon	Thin-film sorbent on porous membrane, temperature swing	183
Climeworks	Amine-functionalised solid sorbent, temperature-vacuum swing	184
Climeworks in partnership with Northern Lights	Climeworks DAC with geological storage	184
Climeworks in partnership with Carbfix, Orca	Climeworks DAC with geological storage	185
CO <sub>2</sub> Circular	Membrane gas absorption with liquid absorbent and concentration by membrane electrolysis	186
DACCITY	Surface-activated porous carbon composite ceramic monoliths	187
Global Algae	DAC and flue gas capture with algae production	188
Global Thermostat	Solid amine sorbent on honeycomb ceramic monoliths	189
Heirloom	Solid oxide sorbent derived from minerals, passive contacting	190
Highly Innovative Fuels	DAC with water electrolysis and fuel synthesis	191
Hydrocell	Solid amine sorbent for indoor air quality control	192
Mission Zero Technologies	DRIVE: Direct Removal (of CO <sub>2</sub> ) <i>via</i> Innovative Valorisation using Emissions	193
Mosaic Materials	Metal–organic framework sorbents for indoor air quality control	194
Nordic Electrofuel	Climeworks and Sunfire technologies for synfuel production	195
Noya	Retrofit of building cooling towers with “non-toxic CO <sub>2</sub> -absorbing chemical blend”	196
Origen Power	Lime-based sorbents with solid oxide fuel cell and oxy-fired calcination	197
Prometheus Fuels	Water electrolysis and fuel synthesis using nanotube membranes, for zero-net-carbon fuels	198
Rolls-Royce	Small modular nuclear reactors to power DAC and fuel synthesis (aviation fuel)	199
Skytree	Derived from International Space Station air scrubber technology, deployed in electric vehicles	200
Soletair Power	Hydrocell DAC with water electrolysis and fuel synthesis, for capturing CO <sub>2</sub> in buildings	201
Sunfire	Climeworks DAC with co-electrolysis for syngas production and fuel synthesis	202
Sustaera	Solid alkali metal sorbent on ceramic monoliths	203
Verdox	Solid quinone sorbent, electro-swing adsorption	204
Zenid Fuel	Climeworks DAC with co-electrolysis for syngas production and fuel synthesis (aviation fuel)	205



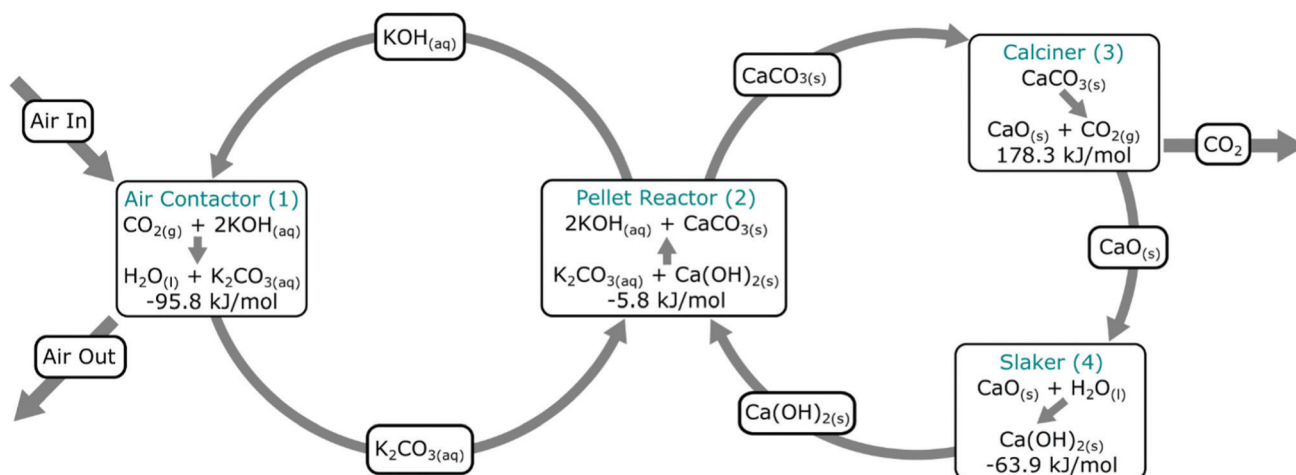
technologies, that to date this has largely been through a limited number of start-ups seeking to validate scalable business models. Thus, there is still significant potential to improve the materials and processes used for DAC, which is the subject of this section of the review. Here we make a concerted effort to provide an update, and to broaden the scope, from previous review articles on DAC materials and processes,<sup>172–176</sup> particularly to highlight publications in the previous  $\sim 5$  years, and with coverage of a wider range of processes and materials (for detail on the initial development of DAC, readers are referred to prior reviews).<sup>172–176</sup> Here, we first identify research challenges emerging from the deployment of the most well-established DAC technologies, *i.e.*, those based on sorption processes. We identify challenges at both the materials and process scales and highlight emerging materials, and process modifications, that appear to show promise in addressing these. This includes aspects unique to DAC, *i.e.*, the design of air contactors, sorbent regeneration, and the production of high-purity CO<sub>2</sub>. Subsequently, we shift our focus to alternative process options proposed for DAC and the materials advances required to realise these, *e.g.*, gas separation membranes and electrochemical devices *etc.* Finally, we explore very recent efforts related to catalytic and biological approaches for integrating DAC with CO<sub>2</sub> conversion and new concepts related to the idea of passive DAC contactors integrated with existing civil and industrial infrastructure. Throughout, we highlight relevant research challenges.

### 3.2. The development of established sorption-based direct air capture technologies and emerging research challenges

The vast majority of DAC development has been focussed on sorption processes,<sup>206</sup> with the largest demonstrations using hydroxide- or amine-based (*i.e.*, base) chemistry in the sorption stage, applied either as liquid sorbents (*e.g.*, Carbon Engineering) or as functionalised solid sorbents (*e.g.*, Climeworks),

respectively (Table 1). In these processes, sorbents are cycled between ‘loaded’ and ‘unloaded’ states, where in a first stage CO<sub>2</sub> is ab/adsorbed and in the second it is desorbed. Such cycling provides one distinction with other non-photosynthesis-based NETs introduced above, *i.e.*, in DAC the materials are used and re-used after regeneration multiple times, whereas in other NETs such as EW the capacity of the sorbent is only used once. The sorption (‘loading’) and desorption (‘unloading’) is mediated by a ‘swing’ process, where pressure, temperature, and/or humidity *etc.* is modulated in a cyclic manner (either temporally or spatially). Sorbents can be deployed in fixed-, moving- or fluidised-beds, or supported on high surface area supports such as monoliths or fibres. This overall approach has the general advantage of shifting the major energy requirement of the process to the desorption stage where CO<sub>2</sub> is more concentrated (as compared to cooling, heating or compressing the entire stream).<sup>173</sup>

**3.2.1. Liquid sorbents employed in existing direct air capture technology and potential for process modification and alternative materials.** Aqueous alkali hydroxide solutions have been used in DAC demonstrations (Carbon Engineering) (Fig. 3).<sup>167</sup> In the first stage (the air contactor), an alkali hydroxide solution reacts with CO<sub>2</sub> to form a solution containing alkali carbonate species. This solution is then contacted with Ca(OH)<sub>2</sub>, to form a carbonate precipitate which is calcined to release CO<sub>2</sub> and return CaO. CaO is slaked to regenerate the Ca(OH)<sub>2</sub>. Sorbent regeneration is the most energy-intensive aspect of the process, and therefore electrochemical regeneration routes (as opposed to thermal) have recently been proposed.<sup>207,208</sup> First, following contacting, the aqueous solution of alkali carbonate (in this case K<sup>+</sup>, CO<sub>3</sub><sup>2-</sup> and HCO<sub>3</sub><sup>-</sup>) is fed to a bipolar membrane electrodialysis stack with acidic and basic compartments separated by an anion-exchange membrane (Fig. 4).<sup>207</sup> In the basic compartment, alkali hydroxide is regenerated, whilst in the acidic compartment gaseous



**Fig. 3** Carbon Engineering DAC process. An aqueous alkali hydroxide solution is used for CO<sub>2</sub> capture from air in the contactor, which is subsequently contacted with Ca(OH)<sub>2</sub> to form CaCO<sub>3</sub> and regenerate the aqueous alkali hydroxide solution. CO<sub>2</sub> is produced in a second cycle, which also produces CaO, which is slaked to regenerate CaCO<sub>3</sub>. Taken from ref. 167. Reprinted from Keith *et al.*, A process for capturing CO<sub>2</sub> from the atmosphere, *Joule*, **2**, 1573–1594, Copyright (2018), with permission from Elsevier. <https://www.sciencedirect.com/journal/joule>.



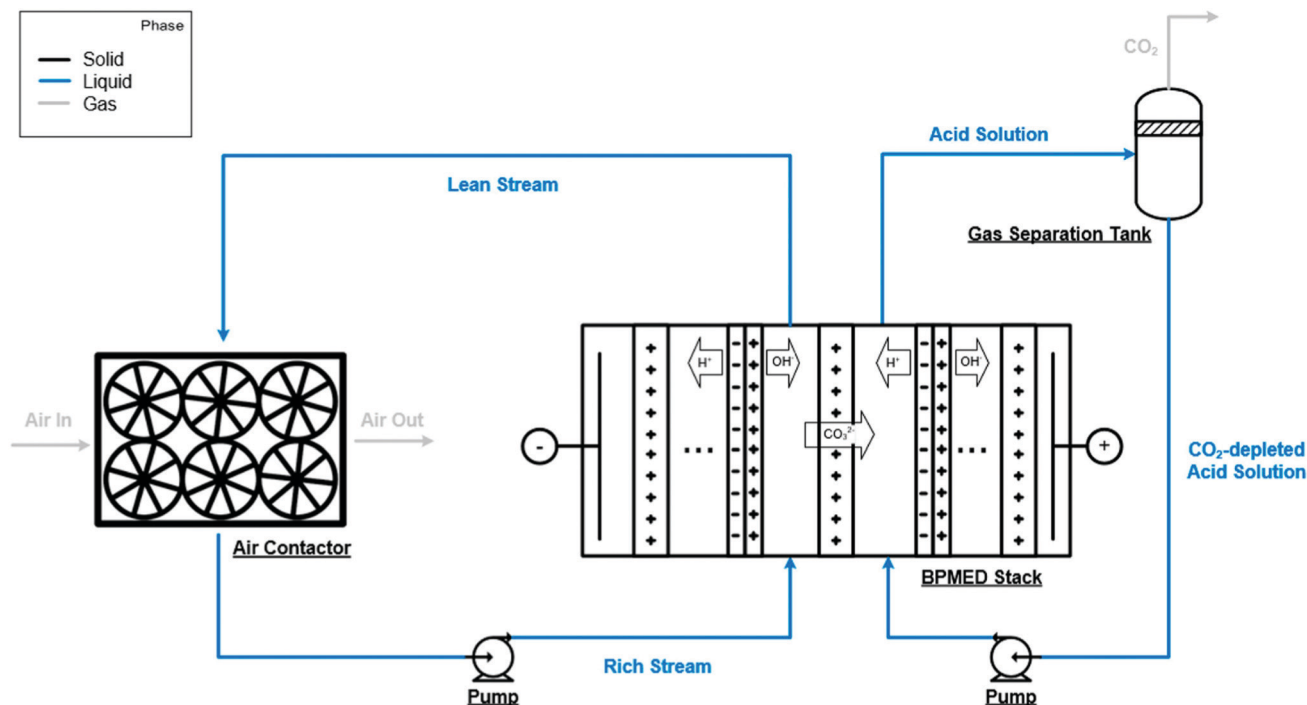


Fig. 4 An alternative aqueous alkali hydroxide solution regeneration strategy. Instead of precipitation of solid carbonates, this approach relies on a bipolar membrane electrodes stack employing anion-exchange membranes to regenerate aqueous alkali hydroxide solution and to produce  $\text{CO}_2$ . Taken from Evaluation of a direct air capture process combining wet scrubbing and bipolar membrane electrodes, ref. 207, licensed under CC-BY-NC-ND 4.0.

$\text{CO}_2$  is produced. Such a regeneration process was found to be less energy-intensive than the Carbon Engineering demonstration pilot plant. Additionally, it avoids solids handling and only relies on electricity (as opposed to electricity and heat), which could, in principle, be renewable. However, due to the high costs of the membrane materials it was not economically-competitive with current Carbon Engineering demonstrations ( $\sim 3$  times more expensive on a \$ per  $\text{tCO}_2$  basis).<sup>167</sup> In another electrochemical regeneration arrangement with a  $\text{H}_2$ -recycling electrochemical cell and a cation-exchange membrane, protons from  $\text{H}_2$  oxidation at the anode decrease the pH of the capture solution, such that carbonic acid ( $\text{H}_2\text{CO}_3$ ) is formed, and upon further pH decrease gaseous  $\text{CO}_2$  is evolved.<sup>208</sup> Sodium hydroxide ( $\text{NaOH}$ ) is regenerated at the cathode. This system can theoretically achieve a lower minimum energy consumption than the two prior systems, however this has not been experimentally demonstrated.

*Potential for and limitations of alternative liquid sorbents for direct air capture.* Aqueous amine solvents are at the core of commercial absorption processes for the capture of  $\text{CO}_2$  from concentrated sources, having been used since  $\sim 1930$ ,<sup>209</sup> yet there are few studies on their application in DAC.<sup>210–215</sup> Screening of aqueous amines has shown that numerous amines can achieve a similar percentage capture as compared to commonly suggested liquid sorbents for DAC (e.g. hydroxides), but with the potential for energy saving due to their lower regeneration temperature.<sup>212</sup> The rapid and high-yield formation of amine

carbamate (as opposed to e.g. carbonates and bicarbonates) in sterically unhindered amines provides the highest percentage capture from air. However, the decomposition of carbamate in the regeneration stage is slow, and therefore, during rapid cycling, the capacity (or percentage capture under the same capture conditions) can decrease. The use of a catalyst added to the amine to aid regeneration appears to help rectify this situation.<sup>213</sup> It is important to note however, that early appraisals of DAC with amine solvents highlighted that the evaporative loss of amines, which are poorly stable in air, would lead to intolerable economics (and in some cases, toxic emissions).<sup>165</sup> Indeed, recent process modelling work on DAC showed that additional plant would be required to reduce such evaporative losses, and that new amines with negligible vapour pressures are necessary to reduce capital costs from initial estimates on the order of  $10^3$  \$ per  $\text{tCO}_2$ .<sup>216</sup> New amines are under development for DAC, however, the focus thus far has been on hydrophobic amines to tackle water co-absorption issues (which leads to a higher energy requirement during regeneration of the amine).<sup>214,215</sup>

To overcome some of the issues above, aqueous amino acids have been investigated for DAC, as they are non-volatile and environmentally friendly.<sup>217–221</sup> The approach generally relies on the crystallisation of a guanidinium carbonate salt of low aqueous solubility, which upon heating regenerates the amino acid sorbent (guanidine) and releases  $\text{CO}_2$ . As this stage is endothermic, concentrated solar power has been used as an energy input, to try to improve the sustainability of the



process.<sup>218</sup> Recent work has taken advantage of the structural diversity offered by the platform to improve the cyclic capacity of the system, with initial regeneration energy requirements on the order of  $10^0$  GJ per tCO<sub>2</sub>.<sup>222,223</sup>

Ionic liquids (ILs) can have high CO<sub>2</sub> capacities and offer negligible volatility; however, their high viscosities impose challenges for handling and gas-liquid mass transfer limitations. Thus, there have been very few studies for DAC-related applications.<sup>224,225</sup> In an attempt to overcome the challenges above, the 1-ethyl-3-methylimidazolium 2-cyanopyrrolide IL was encapsulated and tested for application in indoor air quality control (> 1000 ppm CO<sub>2</sub>).<sup>224</sup> Encapsulation increased the gas-liquid interfacial area and will likely permit simpler handling. The encapsulated ILs show comparable sorption capacities to a standard zeolite (13X), but with significantly lower regeneration temperatures and with better stability under humidity (and selectivity over water). To improve absorption rates, which is particularly important for DAC, as compared to capacity,<sup>226</sup> the same IL was also mixed with ethylene glycol to form a deep eutectic solvent with lower viscosity.<sup>225</sup> For ILs to be a reasonable option for DAC, more work on these major limitations would first be necessary.

**3.2.2. Solid sorbents employed in existing direct air capture technology and associated materials challenges.** Solid-supported amines have received significant attention for DAC due to their stability under moisture in the air, low-temperature regeneration conditions (~50 to 120 °C) and the flexibility in choice of low-cost supports (typically mesoporous silicas). They are used in commercial DAC processes, *i.e.*, Climeworks (Table 1). These materials are covered in depth in previous reviews,<sup>172,173,176</sup> with a large amount of prior work focussed on poly(ethylenimine) (PEI) on mesoporous silica due to PEI's high amine content and commercial availability. The most recent work on sorbent development has focussed on understanding and mitigating oxidative degradation and urea formation in silica-supported amines, which have been found to occur during elevated-temperature sorbent regeneration and in CO<sub>2</sub>-rich atmospheres, respectively.<sup>227–231</sup> This has involved the use of functionalisation which modifies the distribution of primary, secondary and tertiary amines,<sup>229</sup> and to remove oxidation-catalysing metal ions,<sup>232</sup> which together results in an order of magnitude decrease in deactivation rate compared to the archetypal PEI on mesoporous silica. The use of hierarchical silica structures with meso- and macro-porosity, which may be more suitable for scale-up, results in increased CO<sub>2</sub> capacity under DAC conditions with PEI,<sup>233</sup> whilst replacing PEI with poly(propylenimine) (PPI) on mesoporous silicas results in increased capacity and higher resistance to oxidative degradation (Fig. 5).<sup>227,228</sup> A number of other amines are under investigation,<sup>234,235</sup> but further work is needed to understand their potential benefits over the PEI and PPI systems.

Other recent works with amine-based solid sorbents have considered issues relevant to scale-up, such as sorbent lifetime,<sup>236</sup> fabrication of contactors,<sup>237</sup> alternative silica supports,<sup>238</sup> and detailed process modelling.<sup>239</sup> For example, PPI-silica sorbents aged under air for 2 years showed minimal

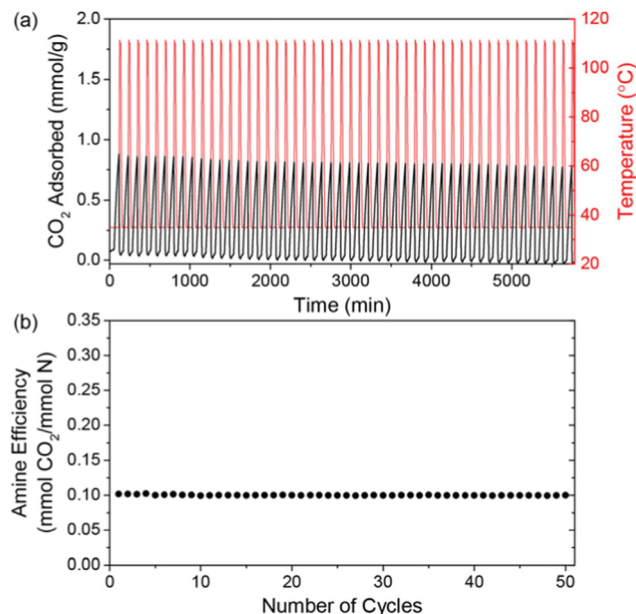


Fig. 5 CO<sub>2</sub> capacity and amine efficiency of a PPI-silica solid sorbent during temperature-swing cycles. (a) Adsorption was carried out under 400 ppm CO<sub>2</sub>/N<sub>2</sub> at 35 °C for 60 minutes, with desorption under N<sub>2</sub> at 110 °C for 10 minutes and, (b) amine efficiency as a function of cycle number. Taken from Oxidatively-Stable Linear Poly(propylenimine)-Containing Adsorbents for CO<sub>2</sub> Capture from Ultradilute Streams, ref. 227.

degradation (~20% drop in CO<sub>2</sub> capture from air capacity), although accelerated oxidation had a more significant impact on the sorbents applied to DAC compared to those applied to capture from more concentrated sources (a ~40% drop in capacity after 12 hours under ~0.04% CO<sub>2</sub>) (Fig. 6).<sup>236</sup> PEI-infused cellulose acetate-silica fibres have also been studied as a proof-of-concept for scalable, structured DAC contactors.<sup>237</sup> Using a combined temperature-vacuum swing regeneration, with dry air as an input, 98% CO<sub>2</sub> was produced. With a wet air input ~65% CO<sub>2</sub> was produced (co-captured water would have to be condensed in a real process to produce high-purity CO<sub>2</sub>).

In terms of alternative silica supports, silica gels offer lower costs and are available in larger quantities compared to the ordered mesoporous silica frameworks typically employed in DAC studies, but due to their lower surface areas would be expected to perform poorly. However, recent work has shown that the addition of water during the amine grafting process (to generate surface hydroxyl groups for amine attachment) results in sorbents that appear to be competitive with those employing mesoporous frameworks.<sup>238</sup> Similarly, water also plays a significant role during capture; for example, the amine-based sorbent Lewatit® VP OC 1065 (a polystyrene matrix with amine groups “believed to be (very similar to) the adsorbent that Climeworks uses in their first-generation DAC process”)<sup>239</sup> shows humidity-enhanced sorption of CO<sub>2</sub>. Recently, detailed water and CO<sub>2</sub> (co-)adsorption isotherm models have been developed for a DAC system based upon such solid amine sorbents, which is an important step to enable the benchmarking of sorbents and more accurate process modelling.<sup>239</sup>





Fig. 6 Effect of accelerated oxidation on CO<sub>2</sub> capacity of PPI-silica solid sorbents under (A) 10% CO<sub>2</sub> and (B) ~0.04% CO<sub>2</sub>, showing a more significant impact on sorbent capacity under DAC conditions. Taken from ref. 236. Reprinted (adapted) with permission from Rosu *et al.*, Effect of extended aging and oxidation on linear poly(propyleneimine)-mesoporous silica composites for CO<sub>2</sub> capture from simulated air and flue gas streams, *ACS Appl. Mater. Interfaces*, **12**, 38085–38097. Copyright 2012 American Chemical Society.

*Opportunities and challenges for other amine-functionalised solid direct air capture sorbents.* In an attempt to address perceived issues related to capacity, hydrothermal stability (*e.g.*, during steam regeneration of sorbents), and limited multi-cycle durability of amine-based silica sorbents, exfoliated mixed-metal oxides (MMOs) (derived from layered-double hydroxides) and layered-double hydroxides have also been tested for DAC.<sup>240,241</sup> The unique nanostructure of MMOs (slit-shaped mesopores and broad pore-size distribution) results in uniform dispersion of the amines and good accessibility for CO<sub>2</sub>.<sup>240</sup> The strong interaction between the MMO surface and amine results in good thermal, chemical and hydrothermal stability, with initial multi-cycle studies showing good durability.<sup>241</sup> Future work on metal oxide-supported amines will need to carefully consider the role that the support

plays (as compared to silicas), as it has been noted that *e.g.* basicity impacts surface speciation, amine-amine interactions and heats of adsorption *etc.*<sup>242</sup>

Metal-organic frameworks (MOFs) are of interest for gas separations generally due to the tunability of their chemistry (of the framework, and for post-synthetic modification).<sup>243</sup> For application as chemisorbents in DAC they must offer durability under moisture, which is atypical for MOFs generally, and be amenable to amine functionalisation. MIL-101(Cr) has been studied as it is water stable and offers multiple avenues for amine functionalisation (adsorption of amines onto metal sites or physical impregnation with liquid amines). A balance between low CO<sub>2</sub> uptake with low amine loading, and high CO<sub>2</sub> uptake but poor kinetics due to pore blockage or loss of amines at high amine loading has to be considered.<sup>244</sup> The Mg<sub>2</sub>(dobpdc) family of MOFs capture CO<sub>2</sub> using a cooperative insertion mechanism whereby CO<sub>2</sub> is inserted into the metal-amine bond to form ammonium carbamate chains. Therefore, the metal-amine bond strength is a tuneable parameter, where the framework metal, or the attached amine can be varied (Fig. 7).<sup>245,246</sup> Although the mmen-Mg<sub>2</sub>(dobpdc) MOF has

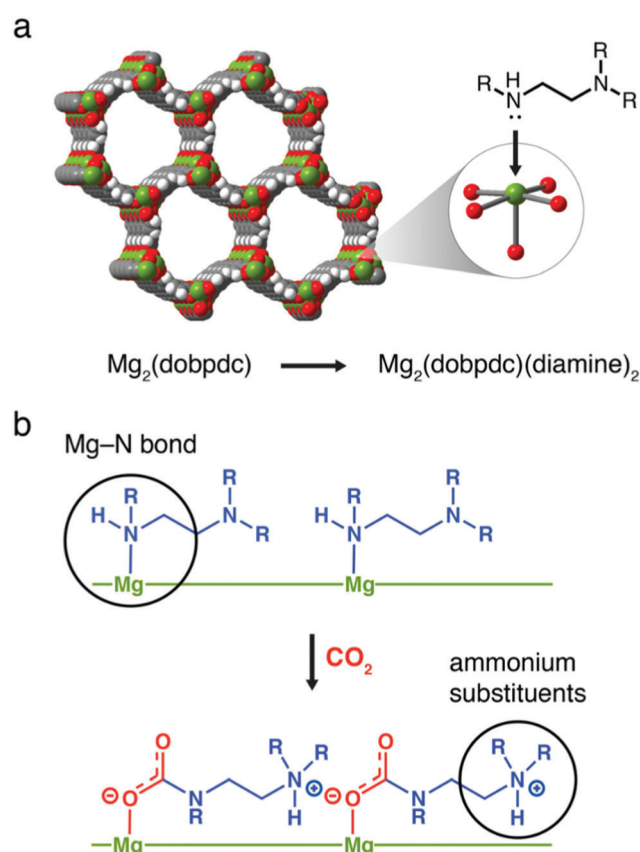


Fig. 7 Cooperative insertion mechanism in Mg<sub>2</sub>(dobpdc) MOFs. (a) Structure of Mg<sub>2</sub>(dobpdc) and, (b) the formation of ammonium carbamate chains by cooperative insertion of CO<sub>2</sub>. Taken from ref. 245. Reprinted (adapted) with permission from Siegelman *et al.*, Controlling cooperative CO<sub>2</sub> adsorption in diamine-appended Mg<sub>2</sub>(dobpdc) metal-organic frameworks, *J. Am. Chem. Soc.*, **139**, 10526–10538. Copyright 2017 American Chemical Society.



shown very high adsorption capacities under equilibrium isotherm studies at  $\sim 0.04\%$ , the unique adsorption isotherm shape and kinetic factors significantly reduce the capacity under more realistic flow geometries, strongly suggesting that adsorption isotherms alone can have limited utility in predicting behaviour in realistic DAC systems.<sup>247</sup> Furthermore, the stability of powders under humidity is an issue, although strategies related to preparing composites with hydrophobic binders are beginning to appear, which may also help address issues related to *e.g.*, pressure drop and handling during application.<sup>248</sup> Finally, it has been suggested that the current cost of MOFs makes their use in DAC prohibitively expensive.<sup>173</sup> Notably, however, Mosaic Materials are developing CO<sub>2</sub> capture and indoor air quality control technologies based upon the use of MOFs (Table 1).

*Alternative solid CO<sub>2</sub> sorbents and the opportunities they offer for developing new direct air capture technologies.* Polymeric ionic liquids (PILs) offer similar synthetic flexibility to ILs but with stability akin to macromolecular frameworks. The introduction of CO<sub>3</sub><sup>2-</sup> ions into quaternary-ammonium-based PILs results in a sorbent which captures CO<sub>2</sub> when dry and releases it when wet, opening the possibility of a moisture or humidity swing approach (as opposed to *e.g.*, pressure or temperature). Thermodynamic analysis implies that as the hydration sphere of the CO<sub>3</sub><sup>2-</sup> ion decreases, it becomes favourable to form HCO<sub>3</sub><sup>-</sup> and OH<sup>-</sup> ions, which in turn bind less water than the CO<sub>3</sub><sup>2-</sup> ion. Thus, when dry, more OH<sup>-</sup> ions are available to capture CO<sub>2</sub>.<sup>249,250</sup> Recent direct experimental evidence (NMR) has challenged this mechanism, stating that as the sorbent dries, water is released from the hydration sphere of OH<sup>-</sup> ions, and CO<sub>2</sub> reacts with OH<sup>-</sup> ions to form HCO<sub>3</sub><sup>-</sup>.<sup>251</sup> Regardless, as water and CO<sub>2</sub> sorption are now opposing, this offers the possibility of avoiding heating or cooling the contactor. In fact, the release of water from the sorbent as CO<sub>2</sub> binds results in a cooling of the sorbent, a somewhat counter-intuitive ‘spontaneous cooling absorption’ phenomenon (Fig. 8).<sup>252</sup> An increase in CO<sub>2</sub> concentration of two orders of magnitude (compared to air) has been shown to be possible, and the release of free energy as a result of water evaporation drives the process.<sup>173</sup> The general approach may have limited utility in cold and humid weather, as due to the underlying mechanism water could condense on the surface.<sup>253</sup> The choice of anion (*e.g.* CO<sub>3</sub><sup>2-</sup>, F<sup>-</sup>, C<sub>2</sub>H<sub>3</sub>O<sub>2</sub><sup>-</sup>, *etc.*) impacts upon whether the resulting sorbents are more suitable for moisture-swing DAC, or thermal regeneration in more conventional scenarios,<sup>254</sup> and the choice of amine functional group also impacts performance.<sup>255</sup> Porous (as opposed to dense), high aspect-ratio fibres have been investigated as a sorbent support structure for application in DAC,<sup>256</sup> with ongoing work seeking to use biomass-derived materials as lower-cost and more sustainable supports.<sup>257,258</sup> Overall, the general strategy has largely been developed by Lackner as a moisture-swing sorbent approach, with ion-exchange resins as the basis for the planned MechanicalTrees™ demonstration which aims to produce 95% CO<sub>2</sub>.<sup>179</sup>

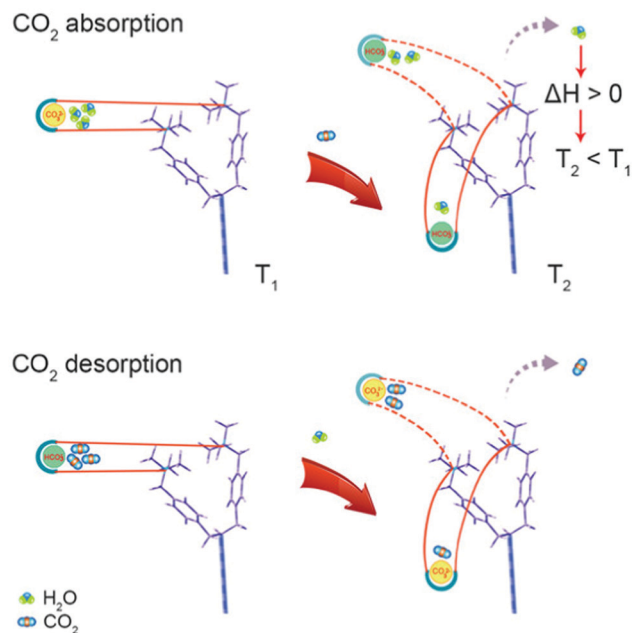


Fig. 8 ‘Spontaneous cooling absorption’ phenomenon in polymeric ionic liquids with quaternary ammonium ions. As CO<sub>2</sub> is absorbed, the desorption of water results in a release of free energy and a decrease in temperature. Taken from ref. 252. Reprinted (adapted) with permission from Wang *et al.*, Spontaneous cooling absorption of CO<sub>2</sub> by a polymeric ionic liquid for direct air capture, *J. Phys. Chem. Lett.*, **8**, 3986–3990. Copyright 2017 American Chemical Society.

Calcium looping, (CaL), the cyclic carbonation and calcination of lime-based sorbents, is a promising strategy for CO<sub>2</sub> capture from concentrated sources, particularly in the cement industry due to spent-sorbent recycling synergies.<sup>162,259</sup> The bulk carbonation of lime-based sorbents (*i.e.*, absorption of CO<sub>2</sub> into the bulk of CaO),<sup>260</sup> occurs at ambient conditions, with water playing a key role; negligible carbonation of CaO is observed in packed-bed reactors without both the pre-hydration of CaO to form Ca(OH)<sub>2</sub>, and the use of air with high relative humidity.<sup>261</sup> Similar observations have been made for the regeneration of spent CaO discharged from the calciner of traditional CaL; moisture in the air ‘passively’ reactivates the sorbent for CO<sub>2</sub> sorption by forming Ca(OH)<sub>2</sub> and modifying surface and pore characteristics.<sup>262</sup> Adopting this ‘passive pre-hydration’ strategy, whereby lime was exposed to a controlled humidity environment before DAC, it has been shown that the higher the relative humidity during lime storage/pre-treatment, the greater the degree of CO<sub>2</sub> capture.<sup>263</sup> In fact, only after high relative humidity storage is significant carbonation observed; at low relative humidity CO<sub>2</sub> is likely captured by dissolution in physisorbed water on the surface of lime. Also, in a fluidized bed arrangement, significant pre-hydration of lime improved its fluidisation behaviour. Note that these tests were performed with dry CO<sub>2</sub> at 0.04% to study the effect of pre-hydration in isolation. Calcination conditions have also been studied at pilot-scale using a high water vapour (21 and 35% vol) content gas as a fluidisation medium.<sup>264</sup> The calcined materials were subsequently exposed to ambient air reaching a carbonation



conversion of 55% after 14 days. Under simpler DAC conditions, *i.e.*, without humidity control and with lime exposed to the air as a thinly spread layer, again the importance of the humidity of the air was noted, with differences in the rate and extent of carbonation found for sorbent applied indoors (low relative humidity) and outdoors (high relative humidity).<sup>265</sup> Granulated and pre-hydrated lime achieved 50% conversion to  $\text{CaCO}_3$  after  $\sim 170$  h, compared to  $\sim 450$  h for lime. On the scale of weeks or months, high  $\text{CaCO}_3$  conversions were noted ( $\sim 75\%$ ), suggesting that like EW strategies, large areas of land would be required.

Modified  $\text{CaO}$ -based materials have also been investigated for DAC. Ethanol treated sorbent was exposed to air to assess its  $\text{CO}_2$  uptake potential. Different variables such as the effect of pre-milling, exposure time and the addition of alkaline water were investigated.<sup>266</sup> The ethanol-treated material presented a carbonation yield of 20.4% compared to 2.4% for commercial lime after 7 days. The authors also observed that increasing the liquid to solid ratio leads to a higher  $\text{CO}_2$  uptake, but a trade-off should be considered between the solvent used and the desired carbonation conversion. Milling the slurry or adding alkaline water to the material improved the carbonation yield even further. Magnesium hydroxide ( $\text{Mg}(\text{OH})_2$ ) has also been considered for this application. Magnesite ( $\text{MgCO}_3$ ) is calcined to produce pure  $\text{CO}_2$  and magnesium oxide. However, the mechanism of this reaction and the effect of different factors such as humidity, temperature and particle size has not been fully described for DAC. Therefore, more research is needed to assess the suitability of magnesite for DAC, particularly as the

enthalpy of decarbonisation is 66% lower than that of limestone.<sup>267</sup>

Recent work sought to model the integration of lime-based DAC with a solid-oxide fuel cell (SOFC) where the high-grade heat from the SOFC is used to calcine the sorbent before DAC.<sup>268</sup> This system has the benefit of providing high-efficiency power and DAC, which gives an opportunity to meet costs *via* electricity sales and carbon taxes. The importance of the choice of lime-based material was highlighted as it impacted on the thermal efficiency, the extent of CDR, and whether a 'once-through' (as was studied) or cyclic process would be more suitable. A range of further research avenues were provided,<sup>268</sup> and it appears that a similar process is being developed by Origen Power (Table 1).<sup>197</sup> Finally, it is also important to highlight that other related solid oxide, hydroxide and carbonate systems are under investigation for cyclic absorption DAC processes.<sup>269–271</sup>

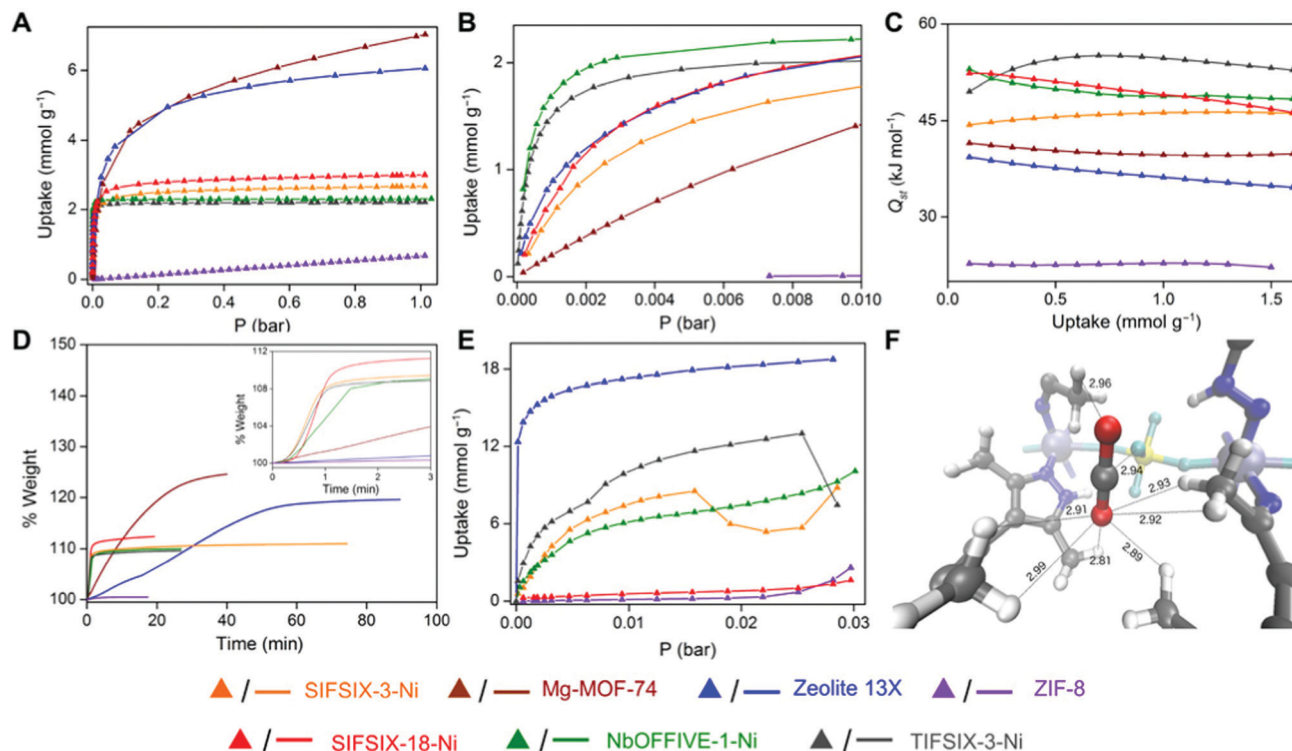
*Challenges for physisorbents in direct air capture and inspiration for improvements from enzymes and drug binding.* All deployed sorbents for DAC to date are chemisorbents. However, physisorbents have been used to pre-treat air (to remove  $\text{CO}_2$  and water) prior to *e.g.*, cryogenic air separation technologies. Thus, early work on a number of physisorbents for DAC found that the major limitation is the poor  $\text{CO}_2$  selectivity with respect to water,<sup>272</sup> and that water vapour leads to sorbent degradation during *e.g.*, sorbent storage in specific cases.<sup>273</sup> Additionally the capacity for  $\text{CO}_2$  is typically low (due to the low heat of adsorption).<sup>173</sup>

The control of pore size and chemistry has been highlighted as a key route to improving physisorbent DAC performance (Fig. 9).<sup>274</sup>



Fig. 9 Benchmark metal–organic framework materials investigated for DAC. The synthetic flexibility, control over pore size and pore chemistry can be harnessed to produce MOF-based physisorbents that overcome issues related to selectivity for  $\text{CO}_2$  over water. Taken from ref. 274. Republished with permission of The Royal Society (UK), from Flue-gas and direct-air capture of  $\text{CO}_2$  by porous metal–organic materials, Madden *et al.*, **375**, 2084, 2017; permission conveyed through Copyright Clearance Center, Inc.





**Fig. 10** Low-pressure CO<sub>2</sub> capture using porous frameworks. (A and B) Low-pressure CO<sub>2</sub> isotherms at 298 K, (C) Isosteric heat of adsorption profiles for CO<sub>2</sub>, (D) gravimetric CO<sub>2</sub> uptake at 1.0 bar with time at 303 K, (E) dynamic vapour sorption isotherms for water at 298 K and, (F) CO<sub>2</sub> binding sites in SIFSIX-18-Ni-β determined by *ab initio* periodic computation. SIFSIX-18-Ni-β has reasonable CO<sub>2</sub> sorption capacity (A and B) as compared to other physisorbents, but fast kinetics (D) and low water uptake (E), which taken together provides promise for its use as a physisorbent for low-pressure CO<sub>2</sub> capture. Taken from Trace CO<sub>2</sub> capture by an ultramicroporous physisorbent with low water affinity, ref. 275, licensed under CC BY-NC 4.0.

Indeed, work with hybrid ultramicroporous (<0.7 μm) materials (HUMs, similar to MOFs but using both organic and inorganic linkers, hence hybrid) has shown that the combination of strong electrostatic interactions with CO<sub>2</sub> along with hydrophobicity in ultramicropores may be a fruitful strategy to pursue.<sup>275</sup> For example, in SIFSIX-18-Ni-β, the introduction of hydrophobic methyl moieties to the SIFSIX framework supplemented the strong interactions between C (of CO<sub>2</sub>) and F moieties (of SIFSIX) to break the typical selectivity issue (Fig. 10). Notably, this work tested separation of CO<sub>2</sub> from sources with CO<sub>2</sub> concentrations of >1000 ppm, *i.e.*, targeted for indoor air quality control where faster and less energy-intensive regeneration of sorbents may be beneficial and indeed necessary.

It has been highlighted that physisorbent materials like those above mimic the ribulose-1,5-bisphosphate carboxylase/oxygenase (Rubisco) enzyme (the primary CO<sub>2</sub> acceptor in plants) by exploiting multiple binding sites optimised from both a kinetic (pore size) and thermodynamic (polarizability) perspective.<sup>272</sup> The general approach, precisely endowing porous frameworks with complex arrangements of moieties to break the selectivity issue,<sup>276</sup> has also been investigated for CO<sub>2</sub> capture from more concentrated sources.<sup>277</sup> Here, 'pockets' which reject water but adsorb CO<sub>2</sub> were termed 'adsorbaphores' (from pharmacophores for drug binding), with large-scale screening of databases of hypothetical structures used to guide synthesis of promising candidates. Approaches such as

these could conceivably aid in guiding the design of entirely new frameworks, or in improving porous frameworks that appear to show promise for DAC (but which have yet to be tested in situations containing water vapour).<sup>278,279</sup> Alternatively, recent work has shown that preparing well-dispersed MOF nanocrystals on hydrophobic supports improves the adsorption efficiency of MOFs under DAC conditions, whilst also reducing water adsorption by ~25% (Fig. 11).<sup>280</sup> These composite sorbents were prepared on a kilogram scale and underwent 2000 DAC cycles (with humid air), showing only ~1% degradation in capacity, suggesting promise. A recent perspective on MOFs for low-pressure CO<sub>2</sub> capture provides more detail.<sup>243</sup>

**3.2.3. Air contacting and regenerating CO<sub>2</sub> sorbents for high-purity CO<sub>2</sub> production; technology status and opportunities.** A key issue for all DAC technologies is moving large volumes of air in such a way that sufficient contact occurs between the CO<sub>2</sub> molecules in the air and the surfaces of the material or device that mediates capture. This stage of DAC is referred to as contacting. Almost all of the work on contactors for DAC has been for sorbent-based processes due to their relatively advanced stage of development. Similarly, and as discussed above, the production of high-purity CO<sub>2</sub> is also an important consideration for any DAC process, and again, almost all the work to date here has focussed on sorbent regeneration strategies to achieve this. In this section, the







Fig. 11 Preparation of composite sorbent containing NbOFFIVE-1-Ni MOF and polyacrylate beads. The porous, hydrophobic polyacrylate beads prevent water from entering the inner structure of the sorbent which contains the NbOFFIVE-1-Ni MOF. Such an approach seeks to protect the MOF from water vapour in the air, whilst also dispersing MOF nanocrystals. Taken from ref. 280. Reprinted (adapted) with permission from Guo *et al.*, A highly efficient and stable composite of polyacrylate and metal–organic framework prepared by interface engineering for direct air capture, *ACS Appl. Mater. Interfaces*, **13**, 21775–21785. Copyright 2021 American Chemical Society.

commercial scale DAC processes that use liquid sorbents (Carbon Engineering) and solid sorbents (Climeworks) are considered in terms of contacting and sorbent regeneration, highlighting recent research on alternative strategies for both.

*General contactor considerations for direct air capture application.* First, it is important to note that a contactor with a high

exposed specific surface area per unit volume can use a weaker sorbent to achieve the same amount of capture for a given contactor volume, *i.e.*, there is a trade-off between the strength of the sorbent interaction with CO<sub>2</sub> and the exposed surface area of the sorbent (noting of course that the strength of the sorbent interaction with CO<sub>2</sub> also impacts sorbent regeneration conditions).<sup>175</sup> Regardless of the nature of the sorbent, electrical fans (*i.e.*, forced draft) have been required in all examples of commercial scale DAC, to overcome pressure drop in contactors. Thus, optimisation has been required between pressure drop and the quantity of CO<sub>2</sub> removed, and between operating and capital costs (high air flows increase forced-draft costs but necessitate smaller contactors). Thus, pressure drop per unit surface area is a central concern for any DAC contactor; it has been described as “arguably the single most important efficiency metric”.<sup>281</sup>

*Contactor design; comparison of innovation in liquid and solid sorbent contactors.* In the most developed liquid sorbent system (*i.e.*, Carbon Engineering),<sup>167,281</sup> a high surface area contactor is continually renewed with a thin layer of aqueous alkali hydroxide solution that is pumped over a hydroxide-resistant PVC packing surface (Fig. 12). The high surface area is required to maximise air–liquid interfacial area, and the thin layer of liquid sorbent reduces liquid-phase diffusion resistance. Due to the low concentration of CO<sub>2</sub> in air, the required liquid-to-gas flow ratio is far lower than is typical for gas separations, which reduces the liquid pumping requirements but gives rise to difficulties in keeping the packing surface wetted (which can be overcome by pulsing the liquid flow).<sup>281</sup> The gas flow is

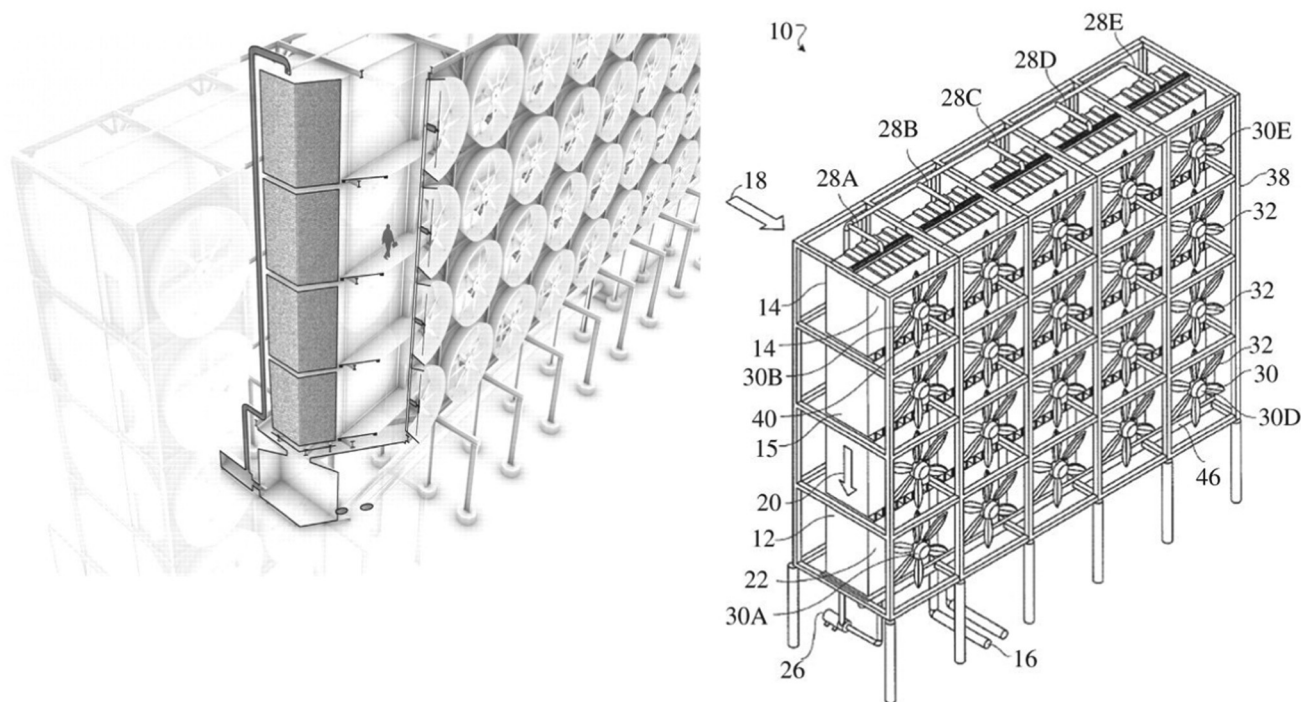


Fig. 12 The Carbon Engineering contactor design featuring forced-draft fans and structure packing with cross-flow gas and a liquid feed. Taken from ref. 281. Republished with permission of The Royal Society (UK), from An air–liquid contactor for large-scale capture of CO<sub>2</sub> from air, Holmes and Keith, 370, 1974, 2012; permission conveyed through Copyright Clearance Centre, Inc.



horizontal whilst the liquid flow is vertical (cross-flow). This unusual final design feature is described as a “crucial enabler of cost-effective DAC” due to the high cost of traditional counter-flow alternatives.<sup>167</sup> As will be discussed below, the design of contactors for DAC requires a detailed design assessment, and the lack of air–liquid contactor designs in the literature is thus notable. For example, although membrane contactors can intensify gas–liquid sorption processes by providing an order of magnitude reduction in plant size compared to traditional solvent contactors (or a similar increase in surface area to volume ratio),<sup>282</sup> the authors are not aware of studies on their application in DAC to date. Notably, however, they appear to be planned for use in commercial projects.<sup>186</sup> Similar comments could be made for rotating-packed beds.

By contrast, for solid sorbent DAC systems, contactors of monolithic,<sup>283,284</sup> fibre,<sup>237,256</sup> fluidized-bed,<sup>285</sup> fixed-bed,<sup>206,286–292</sup> and moving-bed designs,<sup>293,294</sup> have all been investigated for DAC. The monolithic, fibre, fluidized-bed and fixed-bed concepts involve a temporal change in conditions to mediate sorption and desorption of captured CO<sub>2</sub>. Alternatively, a fixed-bed may be continuously replaced to create a moving bed, and fluidized beds can also be operated in a circulating mode, which spatially segregates sorption and desorption. In the final two arrangements there is always sorbent in sorption ‘mode’, at the expense of more complex sorbent handling mechanics. Having multiple fixed beds can of course also ensure that a portion of the sorbent is continually in sorption ‘mode’.<sup>287</sup>

Parallel channel cellular monoliths can offer low pressure drops and high mass transfer rates, with important considerations

including cell density, cell wall thickness and sorbent loading/film thickness (Fig. 13). Thin cell walls are desirable, as they reduce the energy requirement during desorption (*i.e.*, a smaller mass of ‘non-active’ component is heated). For similar reasons, a thicker sorbent film reduces the energy requirement during desorption (the same mass of ‘non-active’ component is heated but more CO<sub>2</sub> is released).<sup>284</sup> However both approaches are challenging during manufacture, due to the stability of the monolith and adhesion of the sorbent, respectively. As an alternative to a thicker sorbent film, a sorbent with a higher equilibrium capacity could, in principle, be used (noting that equilibrium sorption capacity is not always useful to assess a sorbent’s use in practice).<sup>239</sup>

Fibre contactors have also been shown to offer low pressure drops in DAC using solid sorbents.<sup>237</sup> A direct comparison with a packed bed of the same sorbent material and with a comparable void fraction highlighted that packed beds give rise to high, intolerable pressure drops at the air velocities likely required for DAC. Similarly, fluidised beds can give rise to high pressure drops, as there may be an additional contribution to lifting (and, in some arrangements, circulating) the sorbent. Also, as pressure drop is proportional to the length of the sorbent bed, a small bed length may be necessary, which can be challenging to achieve with fluidised beds for a variety of reasons.<sup>286</sup>

It is important to highlight that the arguments presented above are somewhat simplistic, as changes in sorbent particle size, reaction kinetics, packing surface area *etc.* can all be modulated in such a way to claim an advantage over an alternative design. In all cases a detailed design assessment is required. As an example, the majority of early work by Steinfeld on DAC contactors for solid-supported amine sorbents focussed on fixed-bed arrangements,<sup>288–292</sup> which later became the basis of the Climeworks contactor. More recently, moving-bed arrangements have been considered by others to avoid very low height/diameter ratios of contactors (a common design feature for the reasons identified above) and to reduce pressure drop and improve adsorption performance (Fig. 14).<sup>286,293,294</sup> Here the sorption stage is mediated in a radial flow contactor, where air crosses the sorbent bed in the radial direction. Radial flow contactors first appear promising as they combine high volumetric adsorption rates to minimize contactor size and costs, and low pressure drops, which tackle capital and operating costs, respectively. But the point to be made, is that although such a contactor can be operated in a moving-bed arrangement, batch operation (akin to fixed-bed operation) appears to offer better capture efficiency in most DAC situations due to the high air velocity, highlighting again the complexity involved in contactor assessment.<sup>294</sup>

*Sorbent regeneration strategies in the laboratory compared to practical direct air capture application where high-purity CO<sub>2</sub> is usually required.* As above, it is also important to consider the production of high-purity CO<sub>2</sub> following contacting, *i.e.*, sorbent regeneration. We also know that it is inefficient to cool, heat or compress the entire air stream entering a DAC

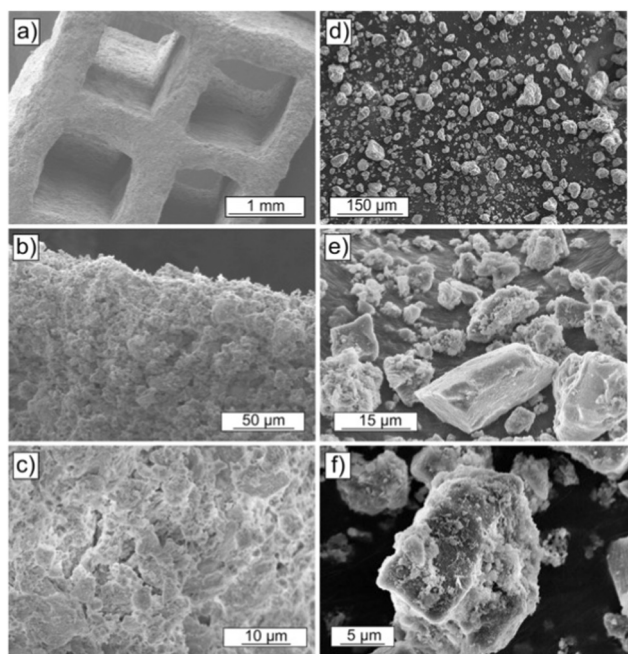


Fig. 13 Comparison of the morphologies of monolith (a–c) and powder (d–f) (formed by grinding pieces of monolith) of a PEI-alumina DAC sorbent. Taken from, Poly(ethyleneimine)-functionalized monolithic alumina honeycomb adsorbents for CO<sub>2</sub> capture from air, ref. 283.





Fig. 14 Moving-bed contactor. Blue arrows indicate gas flow and red arrows indicate solid sorbent flow. Taken from CO<sub>2</sub> Capture from air in a radial flow contactor: Batch or continuous operation? ref. 294, licensed under CC BY 4.0.

process.<sup>173</sup> Thus, in a majority of cases the air entering a sorbent-based DAC process is at ambient or near-ambient conditions with the change in conditions to produce high-purity CO<sub>2</sub> enacted during the sorbent regeneration stage. This approach excludes certain regeneration strategies that may be appropriate for capture from more concentrated sources. For example, a vacuum or pressure swing desorption (VSD or PSD) process would have to operate at <0.4 mbar during the regeneration stage, which is not a practical vacuum level to employ in a real process.<sup>295,296</sup> Furthermore, any weakly-bound CO<sub>2</sub> (e.g., physisorbed on a solid sorbent) would be desorbed from the sorbent during evacuation of the adsorption chamber to remove residual air (effectively 'wasting' capacity of the sorbent). Laboratory-scale research on sorbent processes for DAC has generally utilised temperature-swing desorption (TSD) with an inert gas purge to regenerate the sorbent and produce high purity CO<sub>2</sub>. The limitations of such an approach are discussed briefly here

with comparisons made to the regeneration strategies employed in commercial DAC processes.

In practice, TSD would involve a significant energy requirement as the large mass being heated involves 'non-active' components of the DAC system. In the case of liquid sorbents, the specific heat capacity of water is important, as the amine and hydroxide solutions employed are mostly water. Whereas heating such a liquid sorbent is often an appropriate regeneration strategy for capture from more concentrated sources, heating of liquid sorbents has not been used in commercial DAC technologies. Instead, precipitation and heating of the resulting solid at high temperatures is favoured in the Carbon Engineering technology (ultimately delivering ~97% CO<sub>2</sub> at ~150 bar).<sup>167</sup> As above, electrochemical methods for liquid sorbent regeneration are also in development,<sup>207,208</sup> and thus it seems likely that new liquid sorbent regeneration approaches will be a key opportunity for efficiency gains.

In the case of solid sorbents (typically solid-supported amines), as well as the specific heat capacity of the sorbent itself, 'non-active' components such as sorbent binders and the sorbent support structure/packing will impact the energy requirements during regeneration,<sup>175</sup> and therefore should be considered during design. As laboratory-scale studies typically use an inert gas purge during TSD solid sorbent regeneration, this results in a dilute output stream with an unrecoverable fraction (the inert gas) and faster kinetics during desorption (due to the lower partial pressure of CO<sub>2</sub> in the output stream).<sup>287,297</sup> Such an approach can provide unrealistically optimistic results (unless low-concentration CO<sub>2</sub> output streams are of interest).<sup>298</sup>

The combination of temperature and vacuum swing desorption (TVSD) can be used in practice to produce high purity CO<sub>2</sub> following DAC,<sup>295</sup> and is employed in the Clime-works technology (Fig. 15).<sup>299</sup> Here, following adsorption the contactor is closed to ambient air, heat is delivered at <100 °C, and vacuum (at practically achievable levels) is applied to collect the CO<sub>2</sub> and co-adsorbed water. Following condensation, CO<sub>2</sub> is ultimately delivered at >99% at slightly elevated pressure.<sup>299</sup> Steam-assisted TVSD (S-TVSD) utilises a steam purge to further lower the partial pressure of CO<sub>2</sub>, in turn providing a larger driving force for CO<sub>2</sub> desorption.<sup>297</sup> As the process operates under vacuum, steam can be generated at <100 °C, which opens the possibility of using solar energy or waste heat.<sup>296</sup> For both TVSD and S-TVSD, complex relationships emerge between e.g., evacuation pressure, productivity, power and heat requirements, and capital and operating costs *etc.* which necessitates multi-dimensional optimisation.<sup>296,297,300,301</sup>

It is also important to highlight that although equilibrium sorption capacity is useful to compare sorbents at the laboratory scale, this metric is not very useful in assessing their use in practice, due to differences in the shapes of sorption isotherms and their dependency on temperature.<sup>239</sup> Complex relationships emerge between e.g., sorbent working capacity, desorption temperature, productivity and energy requirements *etc.*, again necessitating complex multi-dimensional



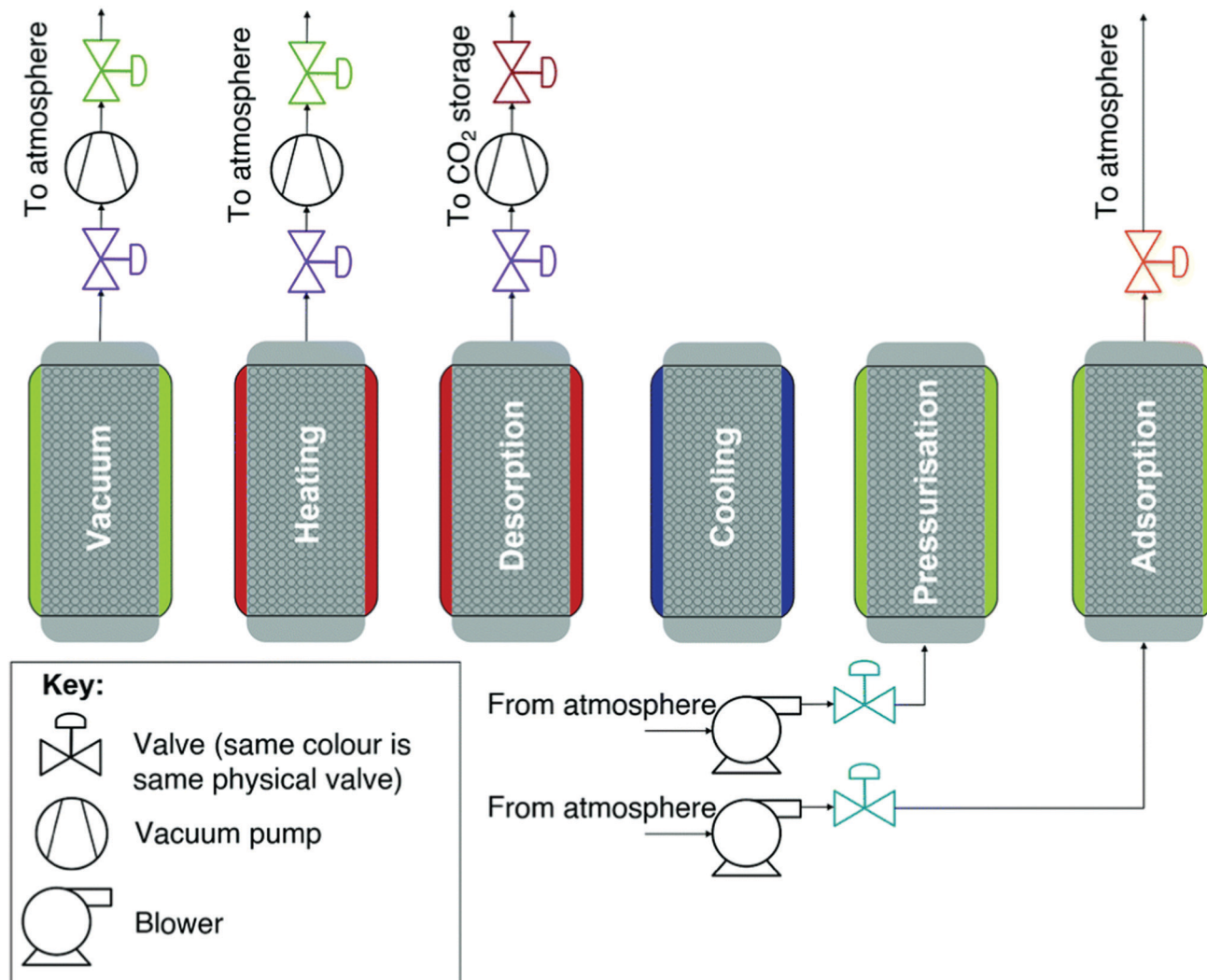


Fig. 15 A schematic of a simple temperature and vacuum swing DAC process. A full cycle includes evacuation of the adsorbent chamber, heating, a second heating step where CO<sub>2</sub> is extracted for storage, cooling to protect the sorbent from oxidative degradation, exposure to the atmosphere and adsorption. Reproduced from ref. 239 with permission from the Royal Society of Chemistry.

optimisation.<sup>239,287,300</sup> Additionally, weather conditions (humidity, ambient temperature *etc.*) can strongly affect performance.<sup>253,265,287,295</sup> Overall, common laboratory sorbent regeneration strategies and sorbent capacity measurements have clear limitations when they are translated to practical DAC application.

### 3.3. Assessment of alternative processes for direct air capture

Whilst sorption-based DAC is now relatively well-established, there are several other process technologies at earlier stages of development for DAC. Here we assess those based on distillation, gas separation membranes, and electrochemical devices, highlighting areas where innovation is required and where such devices might be able to make an impact. We also assess very early-stage work on the direct conversion of CO<sub>2</sub> from the air using engineered biological systems and chemical catalysis, comparing these to natural systems and catalytic processes using concentrated streams of CO<sub>2</sub> following DAC, respectively.

Finally, we reconsider contacting of CO<sub>2</sub> in the air, seeking to assess scenarios where 'passive' contacting might be economically viable through *e.g.*, integration with buildings.

In Table 2 we attempt to summarise key figures of merit for various NETs and DAC processes, noting the difficulty in doing so rigorously due to the enormous variations in assumptions made across the different studies summarised. This is perhaps best captured by a quote related to the relatively well-established Carbon Engineering DAC process which states, "CE has spent several tens of millions of dollars developing DAC technology, yet our performance and cost estimates still carry substantial uncertainty."<sup>167</sup> Readers are therefore directed to the numerous caveats presented in the caption of Table 2 and the original cited works in all cases.

**Potential integration of direct air capture with cryogenic- and distillation-based air separation and energy storage processes.** Cryogenic gas separation processes separate mixtures by exploiting the condensation and desublimation properties of



**Table 2** An indicative range of figures of merit for some DAC processes and their comparison with selected NETs. NETs are coloured red, high TRL DAC is coloured orange, low TRL DAC is coloured blue. All the values presented are likely subject to significant uncertainty and differing assumptions due to e.g., considered process boundary, and approach to economic assessment etc. Readers are therefore strongly advised to consult the original cited work in all cases and not to interrelate quoted values as a 'like for like' comparison is often unavailable. Additionally for a small number of methods, values are quoted from different studies. In these cases, the authors strongly advise against interrelation as the original cited works may have used different sets of assumptions. Throughout, where references are not provided, content is based on the author's assessment. Section 4 discusses many of these figures of merit in more detail. For an extremely comprehensive comparison of figures of merit for NETs (including DAC), interested readers are referred to ref. 24, 30 and 31

Method	Method Description	Energy Cost <sup>a</sup> /GJ/tCO <sub>2</sub>	Abatement Cost <sup>a</sup> /\$/tCO <sub>2</sub> <sup>a</sup>	CO <sub>2</sub> Removal Potential/GtCO <sub>2</sub> /year <sup>b</sup>	Technology Readiness Level <sup>c</sup>	Selected Challenges <sup>d</sup>
Afforestation and reforestation	Tree planting	Very low relative to DAC	2–150 [ <sup>33–36</sup> ]	0.5–7 [ <sup>37</sup> ]	8–9	Significant land use and change; albedo change; biodiversity loss; CO <sub>2</sub> storage security, timescale, and monitoring
Soil carbon sequestration	Increasing organic carbon content of soil	Very low relative to DAC	20–100 [ <sup>30</sup> ]	1.4–3.7 [ <sup>30</sup> ]	7–9	Sink saturation; soil maintenance and permanence; CO <sub>2</sub> storage monitoring and verification; permanence
Biochar	Addition of biochar to soil	Low relative to DAC	60–120 [ <sup>54,75,76</sup> ]	0.6–11.9 [ <sup>72–74</sup> ]	6–7	Changes to soil composition; maintenance and permanence; lack of field studies; CO <sub>2</sub> storage monitoring and verification; biochar price/availability
Bioenergy with carbon capture and storage	CO <sub>2</sub> emissions from biomass combustion captured and stored	Low relative to DAC	15–400 [ <sup>95–97</sup> ]	2.4–69.7 [ <sup>24</sup> ]	6–7 (Industry); 3–5 (Power) [ <sup>98</sup> ]	Land, biomass, and CO <sub>2</sub> storage availability; albedo change; land use change emissions and competition; food security and price
Ocean alkalisation	Addition of alkaline solids to seawater	Low relative to DAC	14–500 [ <sup>102</sup> ]	0.1–10 [ <sup>102</sup> ]	3–5	Unintended biogeochemical impacts; trace metal accumulation; need for mining; grinding energy consumption
High-temperature DAC	Carbon Engineering process	8.81 ("of natural gas [...] depending on financial assumptions, energy costs, and the specific choice of inputs and outputs") [ <sup>167</sup> ]	94–232 for a 1 MT CO <sub>2</sub> facility ("depending on financial assumptions, energy costs, and the specific choice of inputs and outputs") [ <sup>167</sup> ]	Current scale, <sup>e</sup> 10 <sup>7</sup> (174)	6–7	Fully optimizing least-cost design; all-electric variant that eliminates natural gas input; all liquid-phase regeneration system; full life cycle assessment [ <sup>167</sup> ]
Low-temperature DAC	Climeworks process	10 <sup>0</sup> [ <sup>175</sup> ]	500–600 (current), 100 (10-year target) [ <sup>175</sup> ]	Current scale, <sup>e</sup> 10 <sup>6</sup> [ <sup>175</sup> ]	6–7	Integration of waste heat or e.g., heat pumps (sorbet regeneration); potential of moving-bed adsorbers; sorbet manufacture scale-up; full life-cycle assessment
Low-temperature DAC	Global Thermostat process	Not reported [ <sup>175</sup> ]	Not reported [ <sup>175</sup> ]	Current scale, <sup>e</sup> 10 <sup>6</sup> [ <sup>175</sup> ]	5–6	Difficult to assess due to lack of information
Passive DAC	Using DAC sorbents in existing infrastructure (e.g., in buildings)	10 <sup>0</sup> including recycling, transport, CO <sub>2</sub> storage etc [ <sup>306</sup> ]	140–340 ("depending on assumed cost values for fuel, land use, structural materials manufacture & transport, and process and project contingencies") [ <sup>306</sup> ]	10 <sup>0</sup> (assumes 10 <sup>9</sup> buildings) [ <sup>307</sup> ]	3–5	Challenges associated with wind and natural atmospheric convective currents; intermittency; infrastructure availability (for DAC sorbents and their regeneration/recycling)
Solid-oxide fuel cell DAC	Integrated calciner and solid-oxide fuel cell	5.8 (provided by author)	149 for limestone which reduces to 41.2 if net electricity sold to grid (see original work for detailed discussion/assumptions around e.g., carbon taxes and electricity prices) [ <sup>268,308</sup> ]	<sup>e</sup>	2–5	Integration between power, heat, and industrial sectors; feasibility of closed-loop operation; carbonation extent of sorbet
Aqueous Amine DAC	Absorption of CO <sub>2</sub> from air in aqueous amines	10 <sup>1</sup> [ <sup>216</sup> ]	10 <sup>2</sup> –10 <sup>3</sup> ("depending on different economics parameters such as electricity (\$20–\$200/MWh) and heat price (\$2–\$20/GJ), plant life (15–25 years) and capital expenditure (±30%)") [ <sup>216</sup> ]	<sup>e</sup>	3–4	Evaporative losses of amines/amines with negligible vapour pressures; water co-absorption; requirement for carbamate decomposition catalyst; toxic emissions
Aqueous Amino Acid DAC	Absorption of CO <sub>2</sub> from air in aqueous amino acids	10 <sup>0</sup> [ <sup>222,223</sup> ]	Not reported	<sup>e</sup>	3–4	Sorbent stability and lifetime; techno-economic and life-cycle analyses
MOF DAC	Sorption of CO <sub>2</sub> from air using metal-organic-frameworks	2.6–3.3 ("minimum energy requirements") [ <sup>284</sup> ]	60–190 ("The overall DAC cost is sensitive to adsorbent purchase cost and lifetime as well as cycle parameters such as adsorption and desorption times") [ <sup>284</sup> ]	<sup>e</sup>	3–4	Sorbent stability and lifetime; tolerance to water; sorbet cost; supporting and contacting designs
Bipolar membrane electrodialysis DAC	Electrochemical regeneration of hydroxide capture solutions	5.4 [ <sup>207</sup> ]	773 (largely driven by high cost of membrane materials) [ <sup>207</sup> ]	<sup>e</sup>	3–4	High cost of membranes renders process uneconomical; need for development of electrochemical DAC processes generally
Cryogenic DAC	Condensation/sublimation of CO <sub>2</sub> from air, or integration with liquefied air energy storage (LAES)	10 <sup>1</sup> –10 <sup>2</sup> when operating as a standalone DAC process [ <sup>303–305</sup> ]	Very high when operating as a standalone DAC process; potential for revenue from LAES [ <sup>309</sup> ]	10 <sup>1</sup> –10 <sup>0</sup> when integrated with LAES under a highly-idealised energy storage scenario [ <sup>309</sup> ]	2–4	Unavoidable, very high energy costs necessitating construction of renewable power generation at massive scale; dependency on very widespread use of LAES
Membrane DAC	Membrane separation of CO <sub>2</sub> from air using high-performance membrane materials	10 <sup>1</sup> (first-order optimised energy requirement) [ <sup>310</sup> ]	10 <sup>3</sup> –10 <sup>4</sup> [ <sup>310</sup> ]	<sup>e</sup>	2–3	Selectivity-permeability trade-off; need for multi-stage modules; unrealistic feed-to-permeate pressure ratios; low recovery; pressure drop and concentration polarisation effects



<sup>a</sup> Note that these values are subject to significant change depending on the boundary conditions selected, amongst other concerns; it is therefore not straightforward to compare across rows given the enormous variation in the assumptions made across the different studies summarised here. Where  $10^x$  is provided, this implies 'on the order of'. <sup>b</sup> CO<sub>2</sub> flux values are subject to significant changes depending on *e.g.*, point in time. <sup>c</sup> Studies may inconsistently apply TRL definitions; for this reason, the different entries are not always comparable. Where references are not provided, these values are based on the authors' assessment and definitions used in ref. 98. <sup>d</sup> Some challenges will be common across options, *e.g.*, at low TRL, raising R&D funding and successful demonstration will be essential, whereas at higher TRL, all options will require investment and supportive business and policy models, and will need to address public acceptance to obtain a social license to operate. CO<sub>2</sub> storage will, across all relevant cases, be affected by regulation, compliance, and liability considerations. In this column we therefore highlight areas where the challenges are different from one option to the next. <sup>e</sup> In principle, limited by CO<sub>2</sub> storage capacity and energy supply.

different gases. For CO<sub>2</sub> separation from concentrated sources, they can achieve higher percent capture (~99.99%) and final purity (~99.99%) than competing technologies and thus, in principle, the exhaust streams exiting cryogenic carbon capture units could contain a lower concentration of CO<sub>2</sub> than is in the air (which would reduce the burden on NETs like DAC).<sup>302</sup> Their potential benefits include the lack of requirement for additional chemicals, and the direct production of compressed (liquid) CO<sub>2</sub> suitable for geological storage. Cryogenic processes are most appropriate when the CO<sub>2</sub> containing target stream is already at elevated pressure or concentration (clearly not the conditions of DAC) and are generally only more economically-competitive than other capture technologies when low-cost cold energy sources (*e.g.*, liquified natural gas) are available.<sup>302</sup> Nonetheless, inspired by the CO<sub>2</sub> ice cap on Mars's South Pole,<sup>||</sup> cryogenic-based DAC processes have been tested at the bench scale and modelled for application in the Antarctic.<sup>303–305</sup> Results indicate that energy requirements are on the order of  $10^1$ – $10^2$  GJ per tCO<sub>2</sub>, far higher than other methods. In turn, this would necessitate the construction of renewable power generation facilities at scales multiple orders of magnitude larger than has been achieved previously.

Notably, however, CO<sub>2</sub> has a relatively high freezing temperature (−78 °C for CO<sub>2</sub>, compared to −210 °C for N<sub>2</sub> and −220 °C for O<sub>2</sub>). Thus, CO<sub>2</sub> and water are currently removed from air to protect downstream cryogenic plant during cryogenic air separation (to produce high-purity N<sub>2</sub>, O<sub>2</sub>, and Ar) as they would freeze and cause plugging. This removal has been mediated by aqueous alkali solutions, physisorption and molecular sieving. Similarly, in liquified air energy storage, where air is cooled to −196 °C, CO<sub>2</sub> must first be removed from the air to protect the plant. Recent work has suggested that the potential value of CO<sub>2</sub> removed from the air may influence the design of liquified air energy storage systems, *i.e.*, encouraging the construction of larger plants near CO<sub>2</sub> storage or utilisation facilities. Such systems could, in principle, contribute to CDR targets (on the order of  $10^{-1}$  to  $10^0$  Gt per year).<sup>309</sup> It is important to note that this work assumed a highly idealised energy storage scenario, where all energy storage was *via* air liquefaction or compression (amongst many other assumptions) to provide a first-order feasibility assessment.

**Innovation requirements to realise gas separation membrane-based direct air capture.** Despite showing promise for CO<sub>2</sub> separation from more concentrated sources,<sup>161,311</sup> and with numerous promising materials under investigation,<sup>312–314</sup>

membranes for DAC have scarcely been investigated. An appraisal of DAC technology options by Keith *et al.* highlights the major limitations of such an approach.<sup>165</sup> First, the driving force for permeation of CO<sub>2</sub> from the air is around 40 Pa. This is some 3 to 4 orders of magnitude lower than would be required (and practically achievable) for economical capture from more concentrated sources using membranes.<sup>161</sup> Thus, in the absence of compressing the air source to higher pressures than is typical for existing gas separation membrane processes (a pressure ratio of ~5–15), the flux through commercial membrane materials would be vanishingly low. Secondly, considering the volume of air to be processed, a 'sweeping' gas arrangement would require a similarly large volume of sweep gas, and would result in a permeate stream with a CO<sub>2</sub> concentration lower than that of air (unless applied in combination with an absolute pressure driving force). Additionally, most gas separation membranes suffer from a trade-off in permeability and selectivity, which can limit their general utility, particularly in situations where high performance is necessitated.

A recent engineering parametric study investigated the impact of materials performance, process design and operating conditions on membrane-based DAC.<sup>310</sup> The study concluded that with existing commercial membrane materials, the maximal CO<sub>2</sub> output concentration from a single-stage separation would be ~2%. A similar two-stage process could increase this to ~50%, noting that O<sub>2</sub> and water would be co-permeated. High-performance materials (not commercialised) could achieve ~12% in a single stage, and up to ~99% with two stages. For these high-performance materials in a two-stage process, costs would be on the order of  $10^3$  to  $10^4$  \$ per tCO<sub>2</sub> with a first-order optimised energy requirement on the order of  $10^1$  GJ per tCO<sub>2</sub>. Whilst deleterious effects such as pressure drop and concentration polarization may reduce this modelled performance further, clearly multi-stage membrane modules would be required to produce high purity outputs (Fig. 16). It is also very important to note that these results were achieved with very high feed-to-permeate pressure ratios (on the order of 100) and with a vanishingly low recovery, conditions very far from existing gas separation membrane processes and with large energy costs. Indeed, similar modelling work notes a multi-stage membrane process with materials offering a combination of very high permeability selectivity, as well as a pressure ratio >30, would all be required for a 1000-fold increase in CO<sub>2</sub> concentration.<sup>315</sup> Note that in this second work the permeability and selectivity values were taken from two different membrane materials, highlighting again the difficulty in

<sup>||</sup> Note that the atmosphere of Mars is ~95% CO<sub>2</sub> at the surface.





Fig. 16 Schematic of a multi-stage membrane DAC process. Taken from A new strategy for membrane-based direct air capture, ref. 315, licensed under CC BY 4.0.

achieving high permeability and selectivity in a single membrane material.

Facilitated-transport membranes (membranes containing carriers that ‘shuttle’ gas molecules) may provide opportunities to improve membrane performance in DAC, as they can achieve both high permeability and selectivity in a single membrane and are therefore particularly suited to dilute separations. However, work with fixed-carrier systems has thus far only resulted in output streams of 0.8% CO<sub>2</sub> with a 3 bar air feed pressure.<sup>316</sup> Very recent work on a mobile carrier system appears promising, and likely represents an important avenue for future development.<sup>317</sup>

**The significant potential of electrochemical processes and devices for direct air capture.** Electrochemical gas separation processes can offer higher efficiencies than thermal- or pressure-based separation processes, as they act directly on the target molecules rather than the molecules and the medium they are within. Thus, they can eliminate inefficiencies associated with *e.g.*, energy wasted during heating of solvents, or pressurising a feed gas.<sup>318</sup> Furthermore, they will likely integrate well with a future electrified industry, and are appropriate for tackling CO<sub>2</sub> capture at different scales due to their modularity. Reviews of the general area (electrochemical capture of CO<sub>2</sub> from a range of sources) highlight key advantages which include the direct targeting of CO<sub>2</sub> (instead of the ‘non-active’ components of *e.g.*, a contactor), the lack of requirement for sources of heat or pressure/vacuum, modularity, and the possibility of integration with electrochemical utilisation reactions.<sup>319–321</sup> Here we focus on select examples that specifically target DAC application.

Further to the electrochemical membrane examples for DAC involving an SOFC,<sup>268</sup> and ion-exchange membranes to recover CO<sub>2</sub> from liquid capture solutions presented above,<sup>207,208</sup> a

small number of electrochemical sorption approaches to DAC have been studied.<sup>318,322–325</sup> These may be direct or indirect, where either the sorbent itself or a second species is redox active. In the latter case, the redox-active species competes with CO<sub>2</sub> for sorbent affinity (thus releasing CO<sub>2</sub> as it instead binds with the sorbent). As with chemical sorption methods, sorbent affinity for CO<sub>2</sub> strongly influences the energetics, *e.g.*, for weak adsorption, small potentials are required which leads to low faradaic efficiency. One recent example involves the reductive addition of CO<sub>2</sub> to quinones, which has been tested with CO<sub>2</sub> down to 0.6%, showing < 30% loss of capacity after 7000 cycles (Fig. 17).<sup>318</sup> In another arrangement, water electrolysis is used to produce hydroxide ions which combine with calcium ions from dissolved CaCO<sub>3</sub> to generate Ca(OH)<sub>2</sub>. Upon contacting the Ca(OH)<sub>2</sub> slurry with air, CaCO<sub>3</sub> is regenerated. The protons generated from water electrolysis result in the liberation of CO<sub>2</sub> from CaCO<sub>3</sub>, the regeneration of water and the continuous supply of calcium ions to close the loop.<sup>322</sup> Additionally, examples are beginning to appear where electrochemically-driven pH swing methods are used to reversibly generate and consume hydroxide,<sup>323–325</sup> and where electrochemical methods are used to separate CO<sub>2</sub> from water or seawater as a potential alternative to DAC.<sup>326–330</sup>

To further develop electrochemical processes for DAC generally, key challenges include reducing the cost of the materials employed within the devices (particularly the case for membranes), understanding the impact of other components of air (particularly O<sub>2</sub>), and gaining a deeper knowledge of molecular scale mechanism to further iterate materials design.

**Engineered biological direct air capture systems to overcome limitations of analogous natural processes.** A commonly raised natural analogy for DAC technologies is AR. However, extremely large areas of land would be required to deal with a



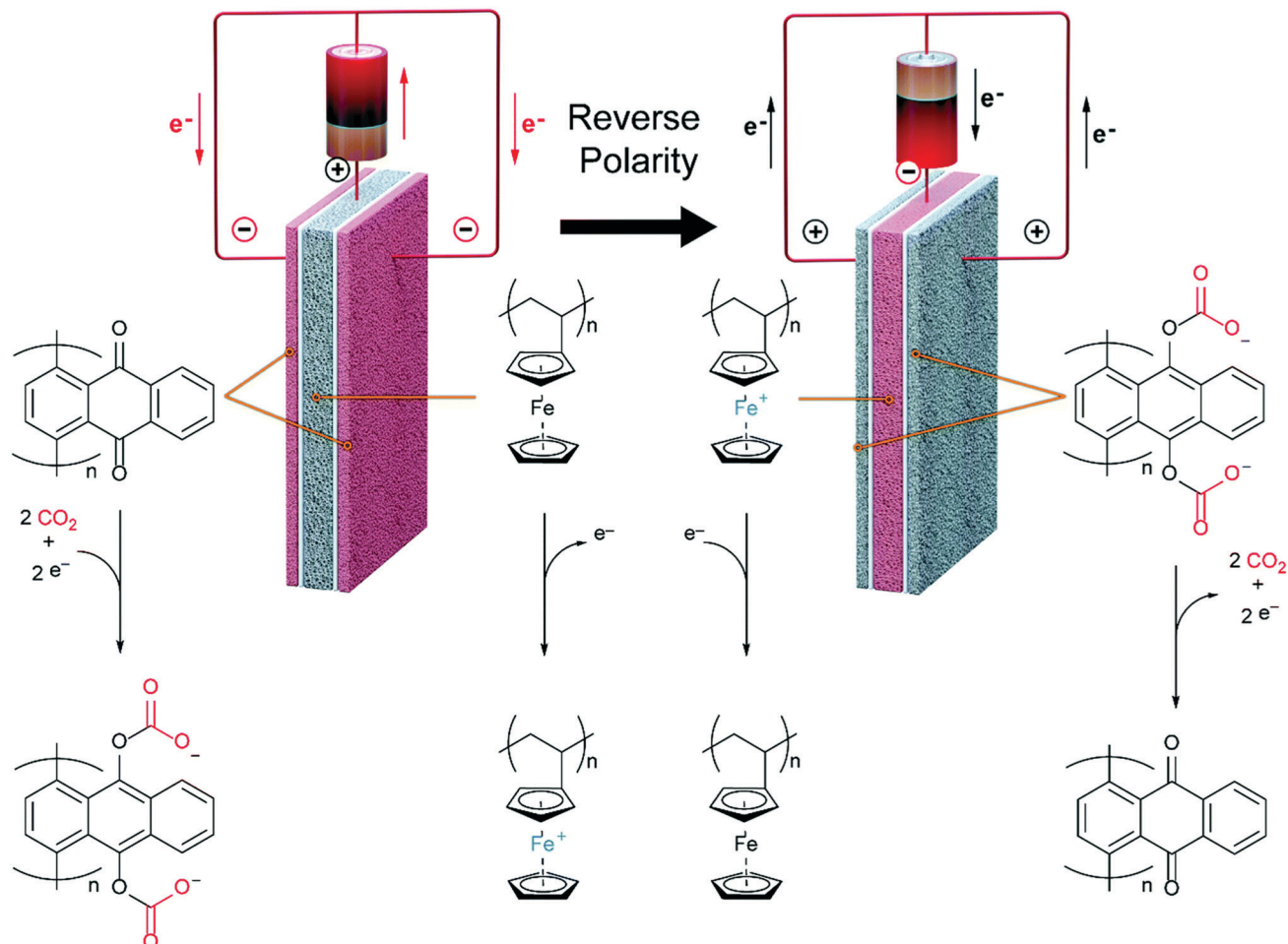


Fig. 17 Electro-swing adsorption of CO<sub>2</sub>. Following the application of a reducing potential, carboxylation of quinone captures CO<sub>2</sub>. CO<sub>2</sub> is released when the polarity is reversed. The inner polyvinylferrocene-containing electrode acts as an electron source and sink. Reproduced from ref. 318 with permission from the Royal Society of Chemistry.

relatively small quantity of emissions; by some estimates  $\sim 10\%$  of the Earth's surface is required to remove  $\sim 20$  years of CO<sub>2</sub> emissions.<sup>\*\* 331</sup> Whilst debate continues about the area required, it will necessarily be multiple orders of magnitude higher than that required for technological approaches to DAC.<sup>332</sup> A potentially more feasible nature-based, engineered DAC approach is to consider plant-like species in Earth's waters. Although the area required may not be very significantly reduced, there is a larger potential deployment area for which there is less competition with *e.g.*, farming, crop growth and housing. For example, microalgae (single-celled photosynthetic microorganisms) can convert dissolved inorganic carbon (*e.g.*, HCO<sub>3</sub><sup>-</sup>) into CO<sub>2</sub> by photosynthesis at ambient conditions and fix the CO<sub>2</sub> into biomass, with high photosynthetic efficiency (approximately an order of magnitude more efficient than terrestrial plants).<sup>89</sup>

Microalgae can survive in saline, alkaline and waste water, but high pH conditions increase the gas-liquid mass transfer

rate of CO<sub>2</sub> and biomass productivity, potentially increasing the feasibility of DAC (*e.g.*, in nature, soda lakes encourage such microalgae processes).<sup>333,334</sup> Suspension-based techniques, *e.g.*, open ponds or photobioreactors, can have large land, water, energy and maintenance requirements, and significant gas-liquid mass transfer limitations. Open pond systems, however, are easily scalable and offer lower costs and energy requirements than alternative arrangements, with such an approach being piloted by Global Algae (Table 1).<sup>188</sup> Recently, to tackle gas-liquid mass transfer limitation issues, carbonic anhydrase (CA) enzymes have been used to catalyse the gas-liquid reaction (CO<sub>2</sub> to HCO<sub>3</sub><sup>-</sup>), by cross-linking CA with glutaraldehyde and encapsulation into buoyant calcium alginate beads (Fig. 18).<sup>335</sup> The buoyant beads float at the air-water interface of an open pond, ensuring that the enzyme is close to the interface. Encapsulation also protects CA from biodegradation and ensures that it is in a recoverable form. The use of encapsulated CA resulted in improved CO<sub>2</sub> fixation rates and reduced water evaporation compared to controls. Alternatively, microalgae can be immobilised on a support, with recent work showing a significant enhancement in CO<sub>2</sub> absorption rate and

\*\* Readers should note the large number of comments and responses to this publication challenging the assumptions of the calculations related to the required land area.



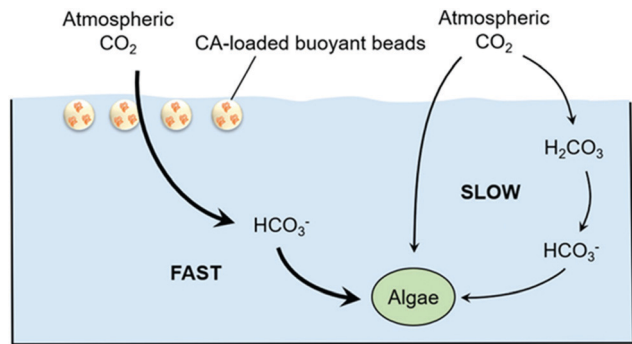


Fig. 18 DAC by microalgae, catalysed by carbon anhydrase. Buoyant beads containing carbonic anhydrase float at the gas–liquid interface, acting as a catalyst for the  $\text{CO}_2$  to bicarbonate reaction. Taken from ref. 335. Reprinted (adapted) with permission from Xu *et al.*, Direct air capture of  $\text{CO}_2$  by microalgae with buoyant beads encapsulating carbonic anhydrase, *ACS Sustainable Chem. Eng.*, **9**, 9698–9706. Copyright 2021 American Chemical Society.

substantially reduced water use when microalgae were immobilised on fabrics, as compared to suspension controls (note that this work tested the approach using  $\sim 5\%$   $\text{CO}_2$ ).<sup>336</sup>

**Combining catalytic and direct air capture functionality for integrated capture and conversion.** Whilst  $\text{CO}_2$  that has been captured from air can later be catalytically converted (*i.e.*, using the concentrated  $\text{CO}_2$  output from a DAC process), direct conversion of  $\text{CO}_2$  from air is also possible. Such an approach, like the biological processes introduced above, blurs the distinction between DAC and carbon capture and utilisation (CCU), as it achieves both in an integrated process. Thus, the limited number of reports on this concept are included here for completeness.

The first report on direct conversion of  $\text{CO}_2$  from the air used a homogeneous metal-catalysed approach to produce methanol.<sup>210</sup> Air was bubbled through a pentaethylenhexamine (PEHA) solution, with a Ru-based hydrogenation catalyst (with  $\text{H}_2$  at 50 bar) used to mediate conversion to methanol. Up to 79% of the captured  $\text{CO}_2$  was converted to methanol. Later work developed a biphasic system to enable the efficient recovery and recycle of the amine and catalyst (again tested for DAC) (Fig. 19).<sup>337</sup> An amine-free system (using the same Ru-

based catalyst) employed an alkali hydroxide in ethylene glycol, and achieved quantitative conversion to methanol after 20 h at  $140^\circ\text{C}$  with  $\text{H}_2$  at 70 bar.<sup>338</sup> The addition of ethylene glycol enabled the conversion to methanol, as previous work with an alcohol-free system had resulted in formate formation.<sup>339</sup> Other non-Ru-based catalysts systems have also been studied, but appear to suffer from poor selectivity for methanol,<sup>340</sup> or are targeting more complex high-value chemicals.<sup>215</sup> A full account of work in this area is available, highlighting that ongoing research seeks to develop the approach in a flow-system geometry to enable continuous production of methanol from air.<sup>341</sup>

Inspired by the high reactivity of hydrides with  $\text{CO}_2$  under mild conditions, ILs with  $\text{BH}_4^-$  ions have also been studied for capture and conversion of  $\text{CO}_2$  directly from air.<sup>342,343</sup> Competition between hydrolysis of the  $\text{BH}_4^-$  and  $\text{CO}_2$  reduction is observed, with significant conversion to products taking a number of days. Recovery of the IL is possible by introducing hydrochloric acid to form formic acid.

Approaches which integrate solid sorbents and heterogeneous catalysis appear to be in the early stages of development.<sup>344–346</sup> Early examples involved a DAC sorption stage followed by methanation of  $\text{CO}_2$  over a Ru catalyst.<sup>347,348</sup> However, a ‘dual function material’ has recently been proposed which combines DAC and methanation functionality in a single material, potentially avoiding penalties associated with *e.g.*, a temperature swing and subsequent catalytic conversion.<sup>346</sup> In this case, NaO and Ru are dispersed on an  $\text{Al}_2\text{O}_3$  support, acting as capture and conversion agents respectively. At  $\sim 320^\circ\text{C}$   $\text{CO}_2$  is adsorbed and upon addition of  $\text{H}_2$ , converted to  $\text{CH}_4$ . A similar process using a Ni/Na- $\gamma$ - $\text{Al}_2\text{O}_3$  dual-function material has also been proposed; 100 ppm  $\text{CO}_2$  feeds were converted to 11.5%  $\text{CH}_4$  in a cyclic sorption and hydrogenation process.<sup>349</sup>

**Opportunities for passive contacting with  $\text{CO}_2$  in the air, and leveraging existing civil and industrial infrastructure.** ‘Passive’ contactors have been proposed as novel DAC technologies suitable for specific applications. This includes in commercial projects.<sup>179,186</sup> These take inspiration from *e.g.*, the carbonation reactions of cement in buildings and within alkaline waste heaps, or from carbon fixation in plants and from other NETs like OA and EW, with the distinction being that here they are always purpose-built, engineered structures for DAC. A further key distinction is that the structures are regenerable, meaning that they are potentially more efficient in terms of land use than some of the processes they take inspiration from. In the case of ‘passive’ contacting, where fans are substituted for ambient wind, it will always be important to consider whether the capital costs associated with the overall DAC process are sufficiently high that the potential intermittency of ‘passive’ contacting would result in intolerable overall capture costs.<sup>281</sup>

Lackner’s moisture-swing sorbents are currently being commercialised as MechanicalTrees™, whereby tiles made from moisture-swing sorbents are raised in a column to capture  $\text{CO}_2$  from the air. Once saturated with  $\text{CO}_2$ , the tiles are lowered into the base of the column for recovery before subsequent

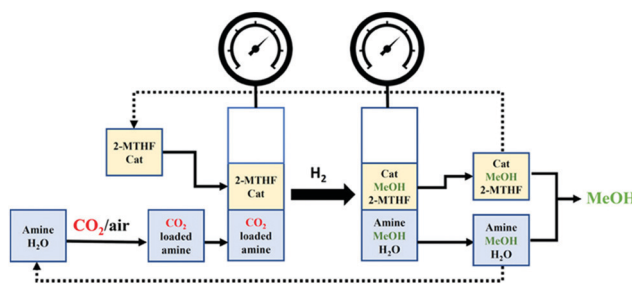


Fig. 19 Schematic of a biphasic  $\text{CO}_2$  to methanol system, where  $\text{CO}_2$  is captured and converted from the air and the amine and catalyst are recyclable. Taken from ref. 337. Reprinted (adapted) from Kar *et al.*, Integrative  $\text{CO}_2$  capture and hydrogenation to methanol with reusable catalyst and amine: Toward a carbon neutral methanol economy, *J. Am. Chem. Soc.*, **140**, 1580–1583. Copyright 2018 American Chemical Society.



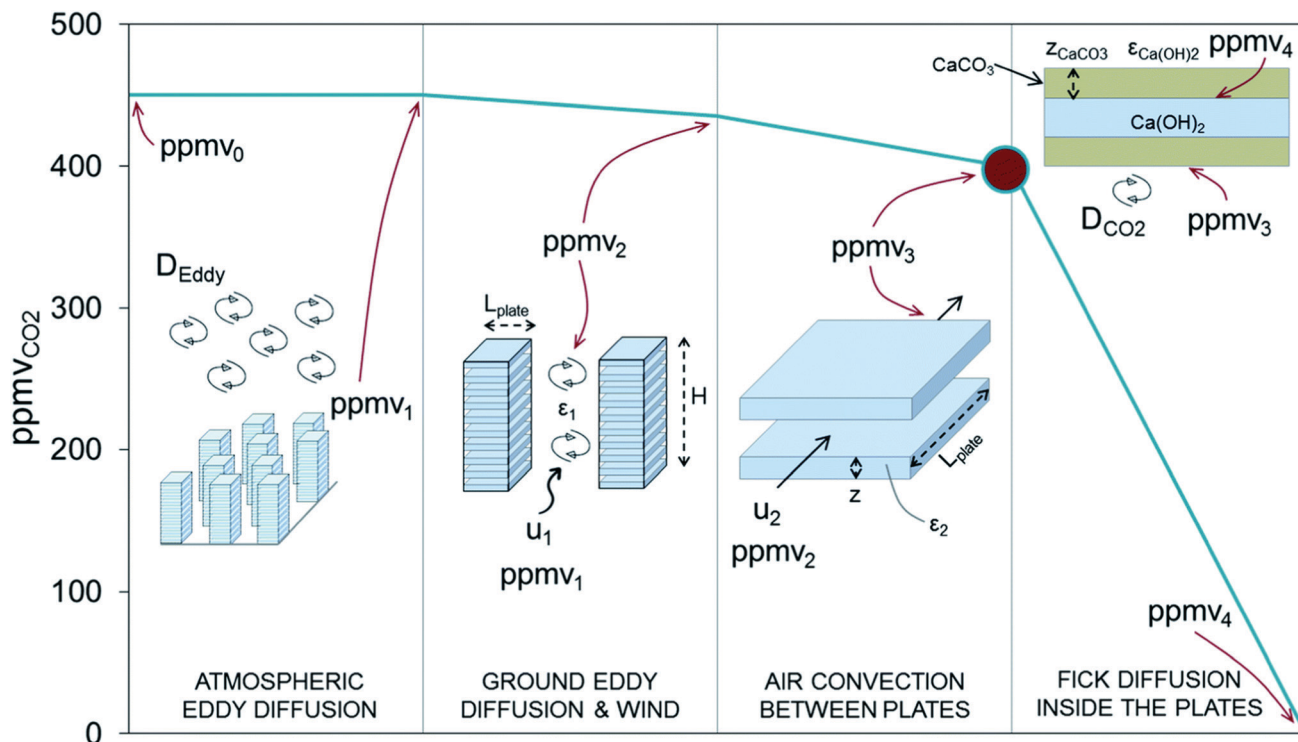


Fig. 20 Evolution of  $\text{CO}_2$  concentration at various scales within porous  $\text{Ca}(\text{OH})_2$  plates fabricated into large structures. From right to left: interior of plate, between plates, stacked plates, and installation of stacked plates. Reproduced from ref. 306 with permission from the Royal Society of Chemistry.

water and  $\text{CO}_2$  separation. It is claimed that up to 95%  $\text{CO}_2$  can be produced.<sup>179</sup> In another arrangement, ‘shading devices’ fabricated from the moisture-swing sorbents are envisaged as components of building facades that both mediate DAC and reduce the solar heat gain of buildings.<sup>307</sup> Such an arrangement may enable DAC in congested cities. However, as the sorbent is now static, the moisture-delivery system must move (like an automated window-cleaning system). It is suggested that many buildings using this design, on the order of  $10^5$ , would be required to achieve capture rates on the order of  $10^0$  Gt per year.

$\text{Ca}(\text{OH})_2$  panels have been envisaged as being deployed as recyclable components of buildings or as components of larger, centralised installations in open fields (Fig. 20).<sup>306</sup> The volume of these structures would be 1 to 2 orders of magnitude larger than those of typical DAC contactors (on a  $\text{m}^3$  per  $\text{tCO}_2$  basis), but with the advantage that the materials are available at very low cost, and the recycling to produce concentrated  $\text{CO}_2$  and return the  $\text{Ca}(\text{OH})_2$  relies on existing technology (oxy-fuel combustion to calcine  $\text{CaCO}_3$  to  $\text{CaO}$ , which is hydrated to produce  $\text{Ca}(\text{OH})_2$ ). A first order cost estimate was proposed as  $10^2$  \$ per  $\text{tCO}_2$  for the overall technology (*i.e.*, including fabrication, installation, transport, recycling and  $\text{CO}_2$  transport and storage *etc.*), which appears to be competitive with other DAC technologies, although with (as above) much larger contactor volumes.

Leveraging existing industrial infrastructure may also be able to provide passive air contacting (note that one of the commercial designs for contacting liquid solvents with air was

derived from wet cooling tower technology).<sup>167</sup> For example, it has been proposed that natural draft dry cooling towers could, in principle, reduce the electrical energy requirement of mechanical fans to move air.<sup>350</sup> Similarly, solar updraft towers may be able to provide high flowrates of air without an electricity input, and as such their use in a DAC system has also been considered recently (Fig. 21).<sup>351</sup>

Finally, passive contactors appear in somewhat related dilute separations, including in uranium recovery from seawater ( $\sim 3$  ppb). As there is  $\sim 4$  Gt of uranium in seawater, efficient extraction could have profound effects on the nuclear industry.<sup>352</sup> The proposed technology relies on amidoxime functionalised polymers which are braided and attached to a weight. The weights are sunk, with the braids floating vertically and exposed to sea currents, which mediate mass transfer (Fig. 22). The best estimates of current technology costs are on the order of  $10^6$  \$ per tU, which is more than an order of magnitude more expensive than the current market price of uranium (not significantly dissimilar to DAC).<sup>352</sup> Recent work highlights that modification of the braids with electrochemically-mediated sorbents may be able to reduce current technology costs to a level where they would compete with traditional sources of uranium.<sup>353</sup> Regardless, the overall concept supports the idea of passive contactors for dilute separations, and it is not difficult to envisage an above-ground DAC equivalent, *e.g.*, ‘sails’ or canopies fabricated using, for example, the fabric-supported microalgae discussed above.<sup>336</sup>



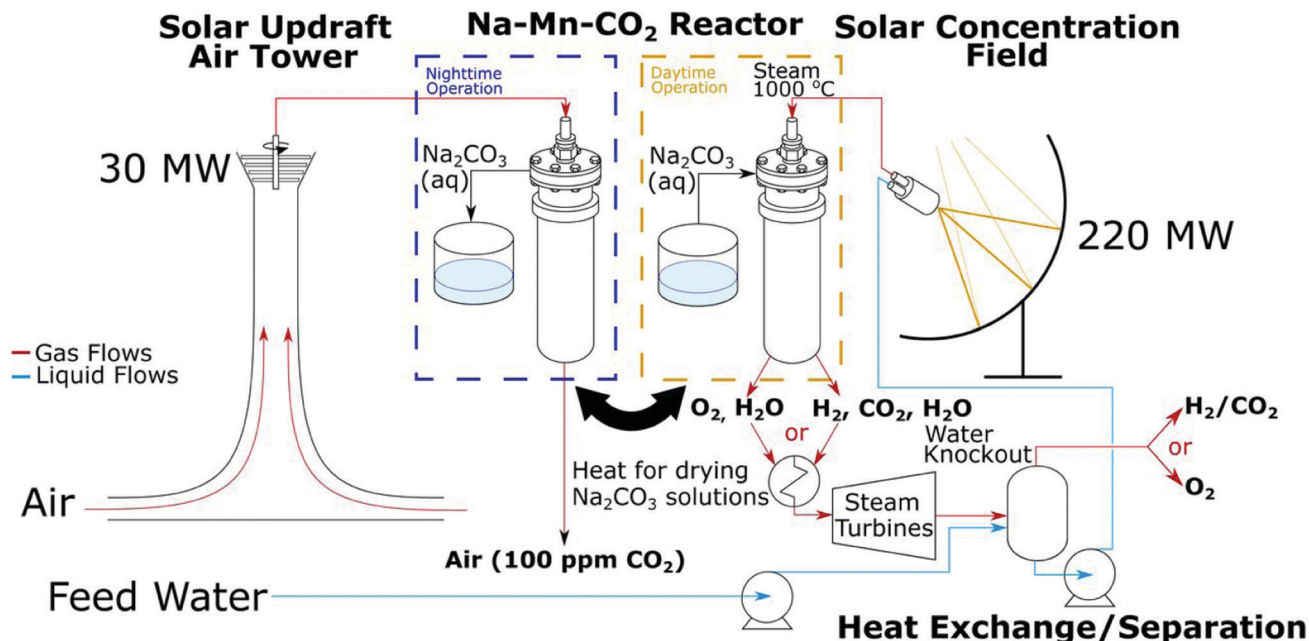


Fig. 21 Schematic of an integrated thermochemical water splitting and DAC process, using a solar updraft air tower for passive contacting. Taken from Integration of thermochemical water splitting with CO<sub>2</sub> direct air capture, ref. 351, licensed under CC-BY-NC-ND 4.0.



Fig. 22 Schematic of a braided adsorber system for uranium removal from seawater. Taken from ref. 352. Reprinted from Dungan *et al.*, Uranium from seawater – Infinite resource or improbable aspiration? *Progress in Nuclear Energy*, **99**, 81–85, Copyright 2017, with permission from Elsevier.

## 4 Feasibility of direct air capture; techno-economic analysis and life-cycle assessment

### 4.1. Techno-economic analysis

Early estimates of DAC costs indicated that the technology may not be economically viable. One of the first estimates for high-temperature DAC was provided by Duong and Keith,<sup>354,355</sup> who

assumed CO<sub>2</sub> is removed from the air using hydroxides, such as NaOH and Ca(OH)<sub>2</sub>. Their work indicated that the cost of CO<sub>2</sub> removal may reach 500 \$ per tCO<sub>2</sub>, but potential reductions to 150–250 \$ per tCO<sub>2</sub> were expected in the long run. In this vein, work by Stolaroff *et al.* confirmed that the cost of CO<sub>2</sub> removal for a similar NaOH-based system that used a spray tower as a contactor would reach 53–127 \$ per tCO<sub>2</sub>.<sup>356</sup> Nikulshina *et al.* showed that using Ca(OH)<sub>2</sub> to remove CO<sub>2</sub> directly from the air can be a technically viable HT-DAC route.<sup>357</sup> They assumed that the sorbent is regenerated using solar energy at a high temperature (>900 °C). They reported the expected cost of CO<sub>2</sub> removal to be in the range of 160–200 \$ per tCO<sub>2</sub>. Such a figure is in line with the predictions by Lackner for low-temperature DAC, who claimed that the first designs of DAC can break 200 \$ per tCO<sub>2</sub> for the system based on direct bicarbonate formation on resins.<sup>113</sup> However, the study by House *et al.*<sup>168</sup> dismissed the potential for low-cost DAC, as they estimated that the early cost estimates for CO<sub>2</sub> removal would reach around 1000 \$ per tCO<sub>2</sub>. Consequently, the cost estimates for DAC are subject to large uncertainties and depend on the considered process boundary and approach to economic assessment. Therefore, we explore high-temperature and low-temperature DAC in more detail before also assessing their sustainability (*i.e.*, recent TEA and LCA work in the literature).

**High-temperature direct air capture.** Stolaroff *et al.* considered the spray-based contactor for contact of NaOH with CO<sub>2</sub> in the air. Their study focused solely on the design of the contactor for DAC and excluded the solution recovery and CO<sub>2</sub> conditioning parts of the DAC chain (Fig. 23).<sup>356</sup> It aimed to verify whether using off-the-shelf technology is viable for DAC. The fan energy requirement was shown to vary between 4.3–8.9 GJ per tCO<sub>2</sub> which was not deemed to be prohibitive.



However, the drop coalescence (reduced CO<sub>2</sub> adsorption efficiency) and water loss (30 molH<sub>2</sub>O/molCO<sub>2</sub>) were indicated as factors that could limit the deployment of this technology. Their work showed that the full-scale contactor will result in the cost of CO<sub>2</sub> captured of 96 \$ per tCO<sub>2</sub>. This figure can vary between 53–127 \$ per tCO<sub>2</sub> depending on the droplet mean size that was varied between 50 μm and 150 μm, respectively. However, their assessment considered a social discount rate, which reflects how much today's society needs to invest to mitigate the future impacts associated with climate change, resulting in the capital charge rate of 6.5%. This is significantly lower than the capital charge, which corresponds to the rate of return required by the investors of the capital, of 15% commonly used for the commercial processes. Moreover, their approach to economic assessment assumed overnight investment, which implies the investment was made and built within a single year and did not account for the cost variation throughout the process lifetime.

Fasihi *et al.* has performed a comprehensive economic assessment and comparison of the near-commercial DAC plants.<sup>358</sup> In contrast to the study by Stolaroff *et al.*,<sup>356</sup> they considered the full DAC plant, including the air contactor and sorbent regeneration steps. For HT-DAC systems, Fasihi *et al.*<sup>358</sup> considered the process design developed by Carbon Engineering (Fig. 3). Their model assumed that CO<sub>2</sub> was removed in a continuous process, comprising air contactor, causticizer, slaker and calciner. Potassium hydroxide (KOH) was used as a solvent for CO<sub>2</sub> capture and Ca(OH)<sub>2</sub> for caustic solvent recovery. They also assumed that the energy demand for calcination

is met with electricity, at 5.5 GJ per tCO<sub>2</sub>. Their economic assessment of HT-DAC, which assumed the weighted average cost of capital of 7% (capital charge of 9.4% at 20 years lifetime), indicated that a first-of-a-kind plant would result in the cost of CO<sub>2</sub> removal of 815 € per tCO<sub>2</sub> in 2020. As the technology matures, the costs were forecasted to reduce to 211–378 € per tCO<sub>2</sub> in 2030, 122–265 € per tCO<sub>2</sub> in 2040 and 93–222 € per tCO<sub>2</sub> in 2050, assuming a conservative learning rate of 10–15%. Note that the original work presents a 94–233 \$ per tCO<sub>2</sub> value.<sup>167</sup> Similarly to work by Stolaroff *et al.*,<sup>356</sup> Fasihi *et al.* assumed overnight investment and did not account for the cost variation throughout the process lifetime.<sup>358</sup>

Zeman considered HT-DAC based on Ca(OH)<sub>2</sub> as sorbent.<sup>359</sup> Such an approach is deemed to avoid the challenges with sintering in conventional CaL cycles.<sup>360</sup> Their work estimated that the amount of heat required to sustain the reaction in the calciner *via* oxy-fuel combustion is 6.7 GJ per tCO<sub>2</sub> and the electrical energy requirement of 1.7 GJ per tCO<sub>2</sub>. It also estimated the cost of CO<sub>2</sub> avoided would be 580 \$ per tCO<sub>2</sub>. Yet, this figure was obtained based on the assumption that the electricity is supplied from the unabated natural gas combined cycle (NGCC) that emits 610 kgCO<sub>2</sub> per MW h and supplies electricity at 71 \$ per MW h. As such an approach is not sustainable, Zeman<sup>359</sup> considered the electricity supplied from a NGCC with post-combustion CCS (107 \$ per MW h, 43 kgCO<sub>2</sub> per MW h) and a coal-fired power plant with post-combustion CCS (139 \$ per MW h, 121 kgCO<sub>2</sub> per MW h). Despite the increase in the unit cost of electricity associated with CCS, the

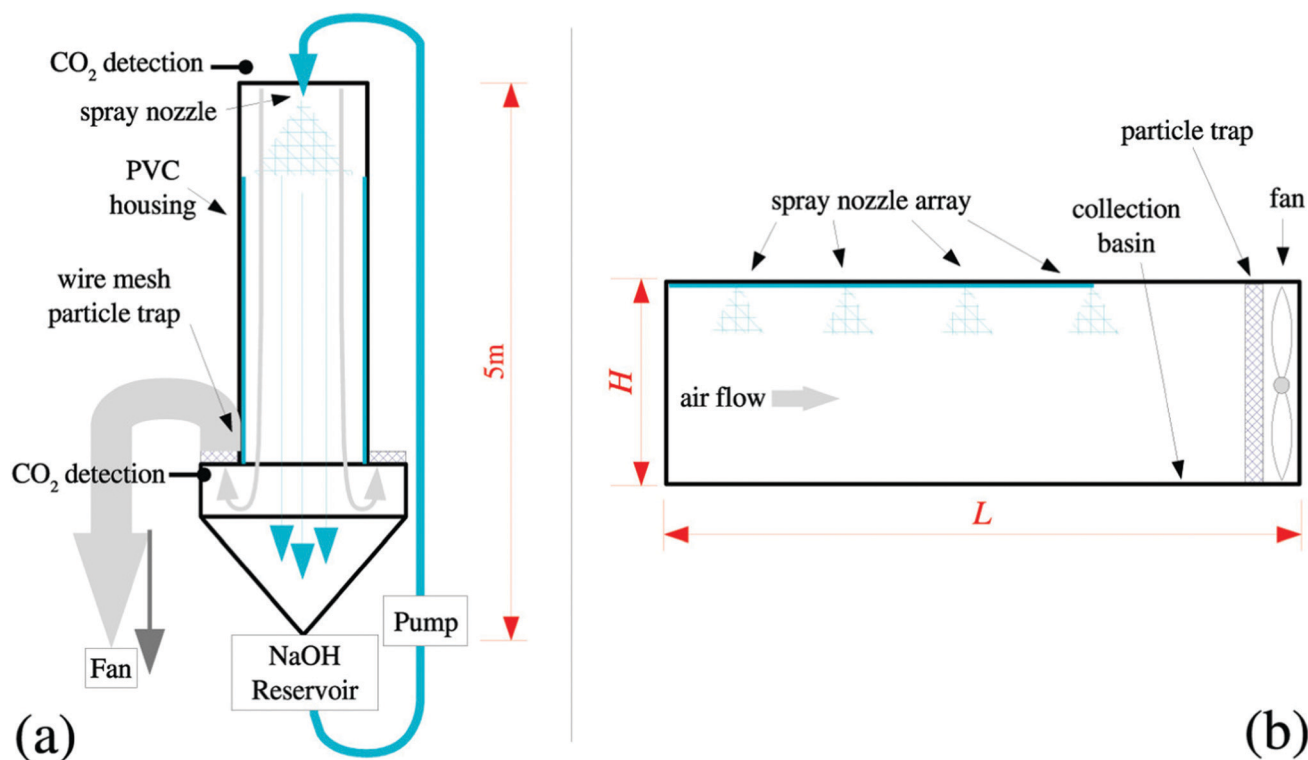


Fig. 23 Representation of off-the-shelf spray contactor for DAC. Taken from ref. 356. Reprinted (adapted) with permission from Stolaroff *et al.*, Carbon dioxide capture from atmospheric air using sodium hydroxide spray, *Environ. Sci. Technol.*, **42**, 2728–2735. Copyright 2008 American Chemical Society.



overall cost of CO<sub>2</sub> avoided reduced to 437 \$ per tCO<sub>2</sub> and 470 \$ per tCO<sub>2</sub>. Importantly, a significant reduction in the cost of CO<sub>2</sub> avoided was obtained on heat integration (3% reduction) and use of a plastic packing rather than a stainless-steel packing in the contactor (30% reduction). Nevertheless, such an approach to DAC relies on fossil fuels and may not be seen as sustainable in the long term. Moreover, the validity of their cost estimates needs to be verified, as a limited amount of information on the assumptions used in the economic assessment was provided.

Hanak *et al.* assessed the techno-economic performance of producing natural solid sorbents using an integrated calciner and solid-oxide fuel cell for DAC.<sup>268,308</sup> In contrast to previous designs, this study assumed that the process is a once-through system and the produced metal oxides (CaO, MgO) will be spread in the open environment for CO<sub>2</sub> removal from the air. In this way, the costs associated with a contactor were avoided. Moreover, this study used the net present value approach to economic assessment, considering the lifetime costs of DAC. The net present value was performed at 8.8% discount rate over the period of 25 years, yielding the capital charge of 10%. This study showed that the cost of CO<sub>2</sub> removal would be 149 £ per tCO<sub>2</sub> for limestone, 129.1–150.5 £ per tCO<sub>2</sub> for dolomite and 368.8 £ per tCO<sub>2</sub> for magnesite. Importantly, if the net amount of electricity produced in the SOFC was sold to the grid at 50 £ per MW h, the cost of CO<sub>2</sub> removal reduced to 41.2 £ per tCO<sub>2</sub> for limestone, 39.2–74.9 £ per tCO<sub>2</sub> for dolomite and 312.1 £ per tCO<sub>2</sub> for magnesite.

It needs to be emphasised that the HT-DAC designs presented above still relied on the use of fossil fuels for sorbent regeneration in the calciner. Sabatino *et al.* considered an alternative route for KOH-based solvent regeneration.<sup>207</sup> Rather than using the calcium-based Kraft process, which is used in the Carbon Engineering design, they considered bipolar membrane electro dialysis (Fig. 4). In this process, CO<sub>2</sub> is liberated from the solvent *via* ion transport through the membrane. This process is driven by the difference in electric potential across the membrane cells. Sabatino *et al.* used the levelized approach to estimate the CO<sub>2</sub> removal cost, assuming the capital charge of 12.5%.<sup>207</sup> Their study showed that the use of bipolar membrane electro dialysis could reduce total capital cost by about 27%. Moreover, the energy requirement for regeneration was reduced from 7.7 GJ per tCO<sub>2</sub> to 5.4 GJ per tCO<sub>2</sub> compared to the process used by Carbon Engineering. However, for the same system scale, the CO<sub>2</sub> capture cost for the bipolar membrane electro dialysis was reported to be 773 \$ per tCO<sub>2</sub>, compared to 232 \$ per tCO<sub>2</sub> reported for the Carbon Engineering design. This is mostly associated with the high cost of energy used to drive the electro dialysis process and the need for regular membrane replacement.

**Low-temperature direct air capture.** In addition to assessing the HT-DAC, Fasihi *et al.* also considered low-temperature DAC (LT-DAC) to compare their performance under the same economic basis.<sup>358</sup> For LT-DAC systems, this study considered the process design developed by Climeworks and Global Thermostat. Such a process usually assumes that adsorption and desorption occur in a single reactor, following cyclic operation (Fig. 24). Their study assumed that the sorbent is regenerated



Fig. 24 Representation of low-temperature DAC by Global Thermostat and Climeworks. Taken from Techno-economic assessment of CO<sub>2</sub> direct air capture plants, ref. 358, license under CC BY 4.0.

*via* temperature swing, requiring 0.9 GJ per tCO<sub>2</sub> of electricity (fans and control) and 6.3 GJ per tCO<sub>2</sub> of low-grade heat to regenerate the amine-based sorbent at 80–100 °C. Their economic assessment of LT-DAC indicated that a first-of-a-kind plant will result in the cost of CO<sub>2</sub> removal of 730 € per tCO<sub>2</sub>, at 7% discount rate (capital charge of 9.4% at 20 years lifetime). As the technology matures, the costs are forecasted to reduce to 189–338 € per tCO<sub>2</sub> in 2030, 110–237 € per tCO<sub>2</sub> in 2040, and 84–199 € per tCO<sub>2</sub> in 2050, assuming a conservative learning rate of 10–15%. Importantly, if the LT-DAC is heat integrated with the fuels and chemicals production, the costs of CO<sub>2</sub> removal were forecasted to reduce significantly to 133 € per tCO<sub>2</sub> in 2020, 60 € per tCO<sub>2</sub> in 2030, 40 € per tCO<sub>2</sub> in 2040, and 32 € per tCO<sub>2</sub> in 2050. Such figures imply that LT-DAC should offer better economic performance compared to the HT-DAC and, therefore, may become a preferred option in the long term.

Sinha *et al.* evaluated the economic viability of MOFs for DAC *via* the temperature vacuum swing cycle (TVSC).<sup>284</sup> The considered process assumes that CO<sub>2</sub> adsorption takes place on monolith structures coated with MOF films (60 μm). Their study considered two of the most promising MOFs, MIL-101(Cr)-PEI-800 and mmen-Mg2(dobpdc). The considered process comprised of 5 cycles (Fig. 25), including adsorption, channel evacuation, channel pressurisation to atmospheric pressure, desorption, and cooling. The adsorption takes place at 298 K and 1 atm, whereas the desorption takes place at 373 K and 1 atm. The heat for desorption is supplied with saturated steam at 65 bar and 408 K that is produced using fossil energy. Their study showed that these sorbents would require a minimum of 3.3 GJ per tCO<sub>2</sub> and 2.6 GJ per tCO<sub>2</sub> of primary fossil energy.†† With the maximum energy use that would result in negative CO<sub>2</sub> emissions of 10.2 GJ per tCO<sub>2</sub>, the CO<sub>2</sub> emitted

†† Note that the authors of the original work use MJ mol<sup>-1</sup> and MJ mol<sup>-1</sup> of CO<sub>2</sub> inconsistently. We have assumed all cases of MJ mol<sup>-1</sup> in their work refer to MJ mol<sup>-1</sup> of CO<sub>2</sub>.





Fig. 25 Temperature vacuum swing adsorption for DAC. Taken from ref. 284. Reprinted (adapted) with permission from Sinha *et al.*, Systems design and economic analysis of direct air capture of CO<sub>2</sub> through temperature vacuum swing adsorption using MIL-101(Cr)-PEI-800 and mmen-Mg<sub>2</sub>(dobpdc) MOF adsorbents, *Ind. Eng. Chem. Res.*, **56**, 750–764. Copyright 2017 American Chemical Society.

from fossil fuel combustion would be lower than that removed from the air, resulting in net negative CO<sub>2</sub> removals.<sup>††</sup> However, it needs to be stressed that the CO<sub>2</sub> separation from the fossil fuel combustion is exponentially less energy intensive and should be, therefore, prioritised. Also, reliance on fossil fuels to drive DAC does not support its primary goal, which is to remove CO<sub>2</sub> from the air. The high-level economic assessment performed by Shina *et al.* assumed the equipment lifetime of 10 years and the sorbent lifetime of 1–3 years.<sup>284</sup> They have not provided details and assumptions behind the method used to perform the economic analysis. Their work showed that the TVSAC DAC using MOFs should result in the cost of CO<sub>2</sub> removal of 75–140 \$ per tCO<sub>2</sub> for MIL-101(Cr)-PEI-800 and 60–190 \$ per tCO<sub>2</sub> for mmen-Mg<sub>2</sub>(dobpdc). Although such performance would make DAC an attractive option for CDR, it is difficult to assess the accuracy and uncertainty behind these estimates.

Arazabadi and Lackner were the first to develop the comprehensive net present value (NPV) model for economic assessment of the sorbent-based DAC systems.<sup>361</sup> Their approach to economics accounted for the degradation of the sorbent capacity with number of cycles. Their cost calculations assumed that the operation lifetime of the DAC device was equal to one lifetime of the sorbent, and that its scrap value was equal to the initial purchase price. Their model was set up to optimise the sorbent performance with the DAC performance, correlating the price of sorbent with the cost of CO<sub>2</sub> removal. They applied their model to assess the DAC system based on temperature vacuum swing adsorption and using MOF-based sorbents (MIL-101(Cr)-PEI-800 and mmen-Mg<sub>2</sub>(dobpdc)) that were initially evaluated by Sinha.<sup>284</sup> Assuming the discount rate of 5%, their work showed that under particular conditions, MOF-based sorbents could result in the cost of CO<sub>2</sub> removal lower than 100 \$ per tCO<sub>2</sub>. Namely, for MIL-101(Cr)-PEI-800 (sorbent cost

15 \$ per kg), the minimum cost of CO<sub>2</sub> removal was shown to be 75 \$ per tCO<sub>2</sub>, with a cycle time of 22–39 min. For the mmen-Mg<sub>2</sub>(dobpdc) (sorbent cost 50 \$ per kg), the minimum cost of CO<sub>2</sub> capture would be 82 \$ per tCO<sub>2</sub> with a cycle time of 79 min. Such performance confirms the figures estimated by Sinha,<sup>284</sup> and further demonstrate that LT-DAC can be more cost effective than HT-DAC.

Finally McQueen *et al.*<sup>362</sup> considered LT-DAC that used a monolith contactor with functionalised solid-sorbent. Similarly to Sinha *et al.*,<sup>284</sup> they considered a 5-step TVSAC process, but their economic assessment focused on understanding how different sources of waste heat can influence DAC viability. Their study showed that the cost of CO<sub>2</sub> capture varied between 205 \$ per tCO<sub>2</sub>, 223 \$ per tCO<sub>2</sub> and 233 \$ per tCO<sub>2</sub> for the system driven by geothermal, natural gas, and nuclear plant, respectively. Despite similar costs, the geothermal and nuclear cases resulted in a significantly lower carbon footprint of the process, reducing the carbon intensity from 0.65 tCO<sub>2,emitted</sub>/tCO<sub>2,captured</sub> to 0.29 tCO<sub>2,emitted</sub>/tCO<sub>2,captured</sub>. This implies that for DAC systems to truly fulfil their design intent, these need to be driven *via* low-carbon energy sources.

#### 4.2. Life-cycle analysis

Despite being considered as one of the technologies that will need to be deployed to maintain the atmospheric CO<sub>2</sub> concentration in line with the agreed environmental targets, the assessment of the life-cycle GHG emissions is still limited in the current literature. The life-cycle performance of DAC is often considered as a part of the power-to-gas system,<sup>363–365</sup> rather than as a standalone process. de Jonge *et al.*<sup>366</sup> were the first to assess the environmental LCA of a DAC process. Their study considered HT-DAC using NaOH as a solvent, based on the Carbon Engineering design including an oxy-fired kiln. Their functional unit was 1 Mt CO<sub>2</sub> removed from the air per year. Yet, the methodology used for the LCA study was not specified in detail. Their study showed that the majority of the life-cycle GHG emissions for the considered DAC process stem from the heat and electricity demand. The life-cycle carbon efficiency was shown to be 62% under the baseline case that considered natural gas as a source of energy for DAC. This means that for each Mt of CO<sub>2</sub> removed from the air, 0.38 Mt of CO<sub>2</sub> is emitted from natural gas combustion in the kiln. This can be improved to 92% if renewable energy and heat recovery are used to drive DAC. It is worth mentioning that if DAC is driven *via* a coal-fired power plant, the life-cycle carbon efficiency will reduce to 10%. This implies that the DAC would still be carbon negative, even though such a solution would not be sustainable as it would drive further use of fossil fuels.

Deutz and Bardow assessed the LCA performance of the LT-DAC based on the Climeworks design.<sup>299</sup> Their work considered a range of solid sorbents, including amines supported on oxides, alkali carbonates, and anionic resins. Their LCA approach relied on the ISO14040/14044 standards and considered the end use of CO<sub>2</sub>. The environmental impacts were assessed considering the Environmental Footprint 2.0 as the life-cycle impact assessment method. Their functional unit was



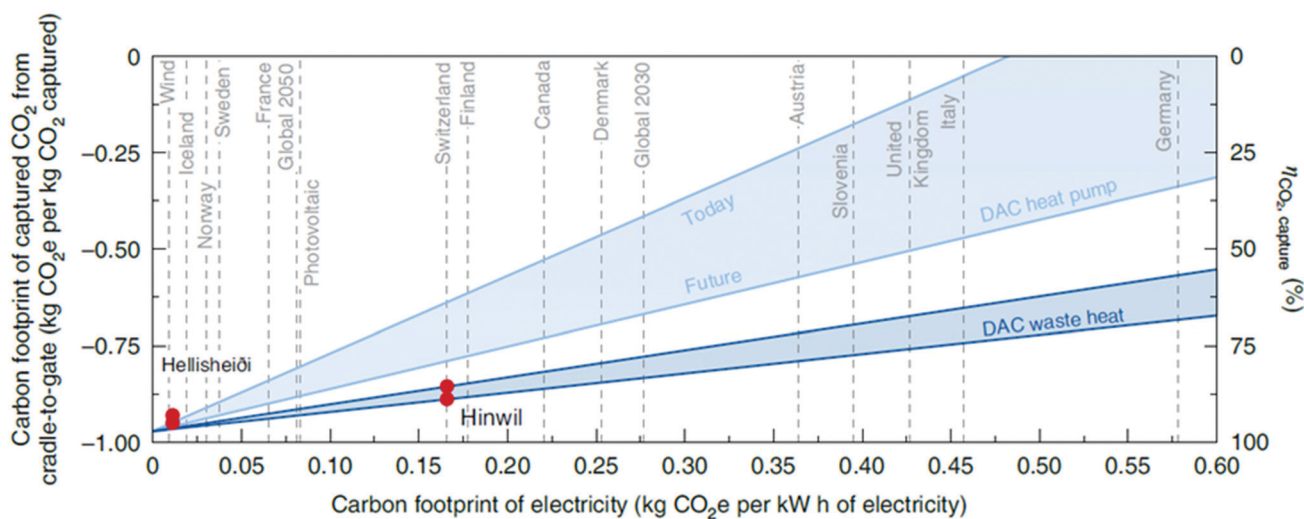


Fig. 26 Effect of carbon footprint of electricity supply on carbon footprint of low-temperature DAC. Taken from ref. 299. Reprinted by permission from Springer Nature Customer Service Centre GmbH: [Springer Nature] [Nature Energy] [Life-cycle assessment of an industrial direct air capture process based on temperature-vacuum swing adsorption, Sarah Deutz & André Bardow], Copyright 2021.

"1 kg CO<sub>2</sub> captured". Their study revealed that LT-DAC using an amine-based adsorbent could achieve negative emissions, with the life-cycle carbon efficiency higher than 95% for the process driven *via* waste heat or low-carbon electricity. Importantly, a direct relationship between the carbon footprint of an electricity source and the carbon footprint of the DAC was derived (Fig. 26). Importantly, their work emphasised that CO<sub>2</sub> from DAC can produce almost carbon-neutral fuels over the entire life cycle but requires low-carbon electricity. A comparison of several promising adsorbents indicated that there was no preferred option when all environmental impact categories were considered. For example, amine on alumina sorbent may appear to be the most optimum sorbent from the LCA perspective, but alumina manufacturing will cause higher human toxicity. Similarly, carbonate-based adsorbents had similar average LCA performance but resulted in enhanced eutrophication of freshwater due to K<sub>2</sub>CO<sub>3</sub> production. This emphasises the importance of considering the LCA performance at the DAC design stage.

Finally, Terlouw *et al.*<sup>171</sup> presented the first comprehensive assessment of the life-cycle emissions of DAC driven by low-carbon energy sources (Fig. 27). Their study, for the first time, considered the emissions associated with the carbon storage stage. Their LCA approach relied on the ISO 14040 standard and considered the ILCD 2.0 (2018) methodology to represent climate change, ecosystem quality, human health, and resources impact categories, and the ReCiPe (2016) methodology was used to assess the water depletion impact category. Their functional unit was "gross removal of 1 ton CO<sub>2</sub> from the atmosphere *via* the use of a DAC plant combined with geological CO<sub>2</sub> storage". The DAC plant was represented based on the Climeworks technology (LT-DAC). Their study showed that for DAC to achieve life-cycle carbon efficiencies of >90%, the electricity and heat should be of low-carbon origin (Fig. 28). This can be the case for countries like Iceland or Norway, whose electricity grids are already highly decarbonised. High life-cycle carbon efficiencies of >85% are achievable worldwide for autonomous systems driven by

solar PVs. For grids relying mostly on fossil fuels, such as in the case of Greece or Mexico, the use of grid electricity and heat pumps to drive DAC would yield life-cycle carbon efficiencies of only 9% and 17%, respectively. Although DAC in these countries will still result in net negative emissions, the cost of net CO<sub>2</sub> removal will be significantly higher than that reported in previous sections. This implies that for DAC to be viable from environmental and economic standpoints, the electricity supply must be first fully decarbonised.

#### 4.3. Comments on feasibility assessments of direct air capture

To date, only a handful of comprehensive TEAs and LCAs were performed to quantify the economic and environmental viability of DAC. More importantly, the data presented in the current literature show a large discrepancy in the economic viability of DAC. This is mostly because of the lack of standardised method, set of assumptions and benchmarks for DAC. The TEAs reviewed use different discount rates and project lifetimes, as well as methods, to estimate the cost of CO<sub>2</sub> captured (or avoided), making a direct comparison of different DAC options challenging. Most figures reported do not account for the variation in operating cost associated with DAC, for example due to inflation or energy cost changes, over its lifetime. Although the LCA has been standardised and ISO14040/14044 standards were considered, the studies that assessed the life-cycle carbon efficiency of DAC used different approaches to life-cycle inventory analysis.

## 5 Social implications of direct air capture systems and policy

### 5.1. Stakeholder concerns over development and deployment of direct air capture at scale

Unlike more widely discussed CDR options such as BECCS and AR, many key stakeholders have yet to develop a coherent



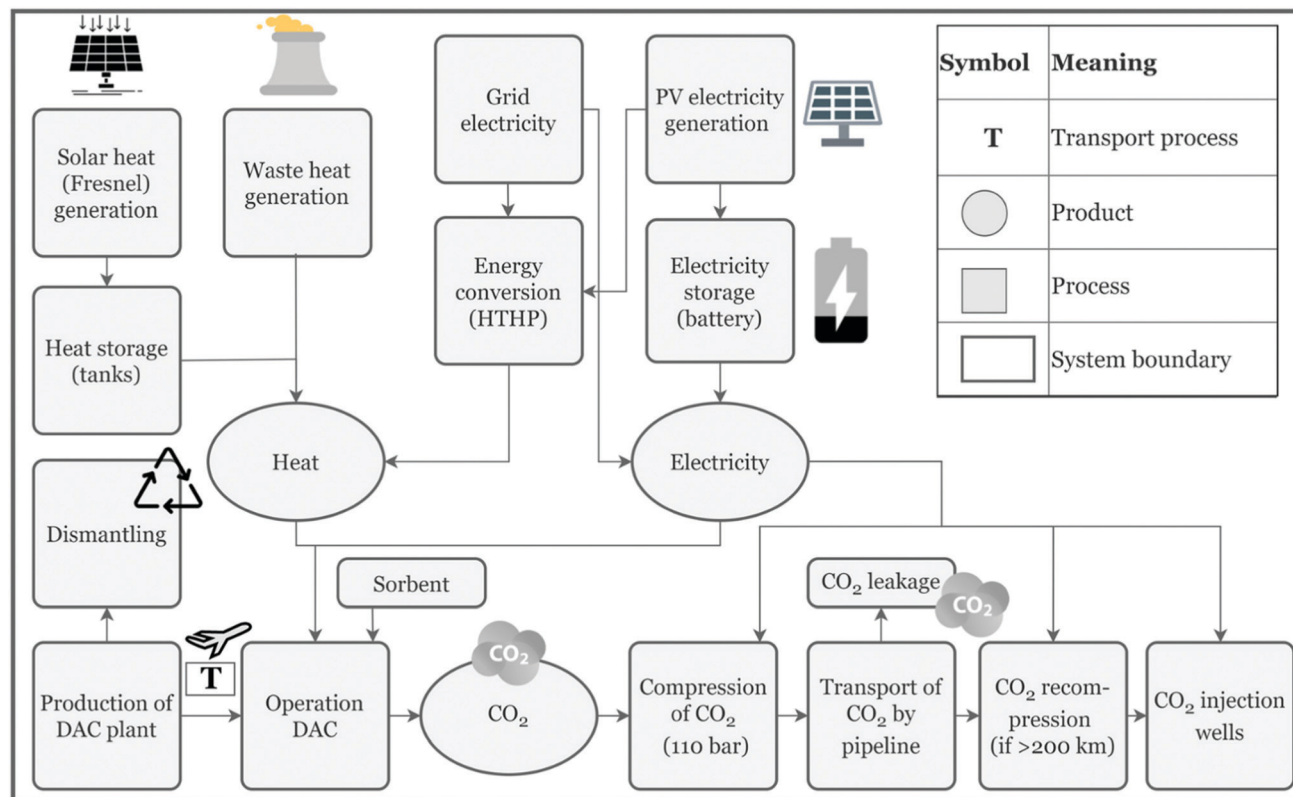


Fig. 27 Superstructure of the process boundaries for life-cycle emissions of DAC. Taken from ref. 171. Reprinted (adapted) with permission from Terlouw et al., Life cycle assessment of direct air carbon capture and storage with low-carbon energy sources, *Environ. Sci. Technol.*, **55**, 11397–11411. Copyright 2021 American Chemical Society.

position towards DAC. To the extent that stakeholders have devoted attention to this still-nascent technology, the prisms they have deployed have been economic, technological, risk-based, and moral.

For many national governments and private actors who have taken an interest, the chief concern is cost. The costs associated with DAC infrastructure, energy generation, transport, storage, monitoring and maintenance,<sup>367,368</sup> renders DAC significantly more expensive than other leading CDR and mitigation options.<sup>30,369</sup> Although economies of scale are expected with upscaling, at present, the limited number of large-scale demonstrations and uncertainties in cost estimates pose strong disincentives for potential investors.<sup>367,370</sup>

Although some industry-leading firms have taken an interest in DAC to meet internal commitments, market demand is unlikely to cover longer-term deployment costs,<sup>371</sup> given the large gap between DAC costs and other options. Moreover, private actors are generally reluctant to provide the required investment without public intervention.<sup>372</sup> Yet governments are also hesitant because, in addition to the high cost, they do not want to appear to be picking winners.<sup>31</sup>

Moreover, the rollout of relevant components or analogous technologies such as CCS,<sup>373</sup> and BECCS,<sup>374</sup> has been stymied by numerous cases of public opposition, failures and aborted projects, which casts doubts over the credibility of DAC projects.<sup>375</sup> On the other hand, countries with ample renewable

and CO<sub>2</sub> storage capacity may look more positively on DAC because they can take advantage of relevant technical knowledge and infrastructure investments. Given the massive energy and heat demands, both the potential technology pairings and the resulting geopolitics are important considerations for locating DAC plants. Iceland, with ample hydro and geothermal resources was identified by Climeworks for its Orca project. Similarly, EDF Energy recently secured funding to explore using low-carbon heat for DAC from its future nuclear power station at Sizewell C.<sup>376</sup>

Proponents of DAC tend to emphasize two main options for addressing cost concerns. First, a major claimed advantage of DAC over the other CCS-based CDR option (BECCS) is that it can be deployed proximate to storage and renewable energy facilities, significantly reducing transport costs.<sup>166,377,378</sup> As discussed below, public attitudes towards CCS show that concern about the local effects of CO<sub>2</sub> storage (such as leakage and seismic activity) as well as the pipelines needed to take the CO<sub>2</sub> from the source to the storage site can sometimes obstruct projects from being deployed.<sup>379</sup> Some contend that the ability to situate DAC away from host communities (*e.g.*, offshore or in remote locations) could prove to be a key advantage in securing social license to operate,<sup>380,381</sup> although, as with CCS more broadly, not all countries would have access to such sites and storage capacity would likely become scarce with upscaling.<sup>367,382</sup>





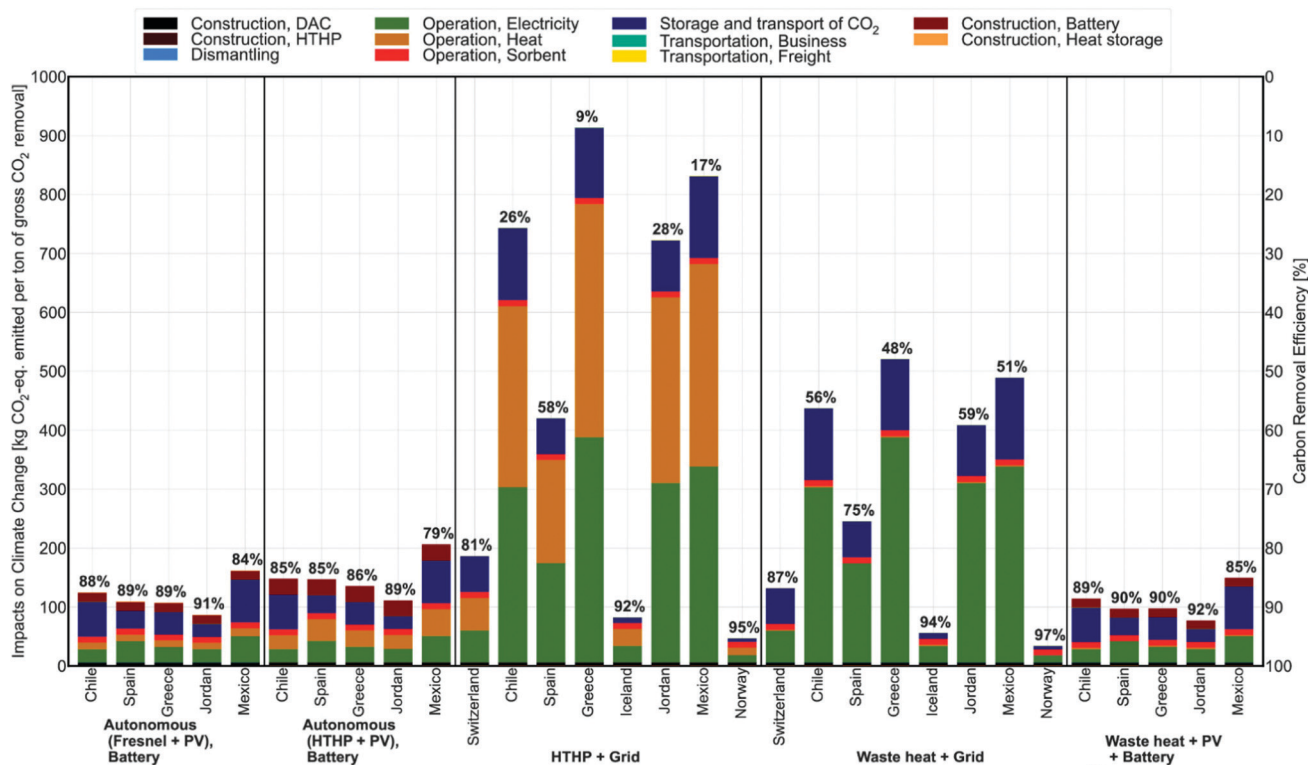


Fig. 28 Carbon removal efficiencies (%) and life-cycle greenhouse gas emissions for various DAC systems in different locations. Taken from ref. 171. Reprinted (adapted) with permission from Terlouw *et al.*, Life cycle assessment of direct air carbon capture and storage with low-carbon energy sources, *Environ. Sci. Technol.*, **55**, 11397–11411. Copyright 2021 American Chemical Society.

Another incentive for potential investors is the possibility of using or utilising the captured CO<sub>2</sub> in commercially viable end use industries such as carbonated drinks, synthetic fuels and, most prominently, EOR.

Two key industries have demonstrated a keen interest in CCS: Energy and utility companies have focused on the possibility of combining DAC with existing energy facilities, notably with the oil and gas industry seeking to employ captured CO<sub>2</sub> for EOR. Stakeholders in transport and aviation have also engaged with CCU options for producing low-carbon synthetic fuels for air and road transport,<sup>377,378,383</sup> yet there is a fundamental risk that re-releasing the captured CO<sub>2</sub> through utilisation will result in net increases rather than reductions.<sup>384,385</sup> While a small number of existing DAC deployments involve long-term storage such as, for example, the United Airlines 1Point5 Project,<sup>386</sup> or utilise the captured CO<sub>2</sub> in permanent end-products such as building materials,<sup>387</sup> most leading commercial DAC start-ups such as Carbon Engineering and Global Thermostat, supported by the venture arms of firms such as Occidental Petroleum and ExxonMobil, focus on EOR or other forms of CO<sub>2</sub> utilisation and, therefore, do not qualify as genuine NETs. While CCU can only play a limited role in mitigation efforts (perhaps 0.5% of the mitigation challenge by 2050),<sup>385</sup> the association between DAC and fossil fuel industries seems to validate environmentalist concerns that large-scale deployment could obstruct mitigation and ‘lock-in’ fossil fuel energy.<sup>388–390</sup> Some describe DAC as a “societally uncontentious

long-term prospect, but only if the relatively high energy demand is met by electricity from renewable sources”.<sup>391,392</sup>

As long as DAC projects continue to prioritise CCU over permanent storage, moral hazard concerns, that CDR could detract from mitigation,<sup>393,394</sup> are likely to become harder to dispel and increase negative perceptions among commercial stakeholders and publics. Indeed, one study even quantified “a risk of assuming that DACCS can be deployed at scale” contributing to additional warming of up to 0.8 °C if DAC was later found unavailable.<sup>166</sup> A related concern is that DAC is premised on accepting the inevitability of overshoot and in so doing predestines such an outcome.<sup>392</sup>

Another attraction is DAC’s potential to avoid some of the critical resource pressures and side-effects (*e.g.*, ecosystem damage and rising food prices) associated with other leading NETs. Land requirements are expected to be several orders of magnitude smaller than that of other CDR options.<sup>26,166,371,377,395</sup> Yet recent research suggests that this resource advantage may not be as large as earlier studies estimate. For example, while DAC requires much less land than BECCS and AR, accounting for water loss from evapotranspiration of unirrigated bioenergy crop cultivation,<sup>54</sup> and water-rebound effects,<sup>382</sup> suggests that water use is likely to be comparable to land-based NETs at scale. In addition, as noted, climatically-relevant deployment would eventually encounter limitations as suitable storage sites (such as deep saline formations, depleted hydrocarbon fields and coal





As DAC emerges from the R&D phase, governments will have different policy levers at their disposal for incentivizing DAC and driving down costs. Technology mandates could ensure DAC is deployed in key industries such as energy and transport, although such mandates would need to be designed to avoid simply prolonging the use of old, high-carbon plants.<sup>30,371,422</sup> Tax breaks and capital grants have played a key role in supporting other low-carbon technologies such as offshore wind and solar PV, providing another option for mitigating the risks associated with large-scale DAC demonstrations.<sup>423,424</sup> In addition, government procurement of DAC-based applications such as low-carbon fuels or construction materials could stimulate demand for DAC.<sup>421</sup>

Most forecasts involving large-scale CDR assume a much higher carbon price to internalize the effects of CO<sub>2</sub> on the climate system. Taxing carbon emissions could effectively become a subsidy for negative emissions, which, at climatically relevant scale, would require massive expenditures (as much as a third of general government spending in advanced economies).<sup>372</sup> Political reactions to taxes and subsidies for renewables suggest that relying on carbon taxes or negative emission subsidies will become increasingly challenging as DAC grows.<sup>371</sup> Moreover, carbon pricing alone would not induce the needed global transition away from fossil fuels and optimal CDR deployment as both outcomes are likely to require different prices.<sup>370</sup>

The fundamental issue facing all of these policy options is that, currently, carbon pricing does not reward CDR, which renders alternative decarbonization options significantly cheaper than NETs in general and DAC in particular.<sup>408</sup> Several experts propose that accounting based on storage, rather than emissions, could provide the necessary incentives for upscaling CDR applications of CCS-based technologies.<sup>382,407,408,410</sup> Dag-gash and MacDowell, for example, propose a negative emissions credit – payment for each ton of CO<sub>2</sub> removed, which would also reduce overall end-prices.<sup>408</sup> Similarly, Jenkins *et al.* propose the concept of a ‘carbon takeback obligation’ (CTO) to shift accounting away from the polluter pays principle, which is based on counting emissions, to producer storage, which involves counting storage.<sup>407</sup> In order to be effective, such proposals would need to be accompanied by comprehensive regulatory mechanisms for managing risks, long-term storage and verification spanning up and downstream flows, and be integrated with complementary frameworks for overseeing interactions with other priorities such as food supply, energy security and sustainable development.<sup>400,425</sup>

#### 5.4. Social implications of scaling up

As DAC plants have moved from the drawing board to larger demonstration plants, the technologies (and respective start-ups) have attracted greater media attention and interest by firms as customers, as well as greater scrutiny for the wider systemic role it might play. For example, large firms such as Shopify, Audi, Microsoft and Swiss Re have become customers for Orca, the largest DACCS project launched by Climeworks and Carbfix, which will remove 4000 tons of CO<sub>2</sub> per year.<sup>426</sup>

Carbon Engineering is planning a megaton scale plant in West Texas (that will also be used for EOR) by 2024 and a second facility in Scotland by 2026.<sup>427</sup>

Public interest has also increased as a result. For example, as measured by Google Trends, after first appearing in 2010, searches for ‘direct air capture’ were only intermittent until 2017 when there began to be a steadier, if low-level, interest and by 2019 searches began to increase substantially. Attention shot up even more dramatically in 2021 (Fig. 29).<sup>428</sup>

Ultimately, the social viability of any policy instrument depends on a nation’s political economy, social values, norms and priorities.<sup>409</sup> The history of energy transitions shows that low-carbon energy technologies tend to be more successful in eliciting public support when opportunities are provided for stakeholders to voice concerns about potential side-effects and risks and influence the creation of local incentives.<sup>410,429</sup> Distributing responsibility for upscaling DAC and other CDR options will inevitably be politically contentious and require attention at both the national and international level to questions of equity.<sup>430,431</sup> Most cost-optimal pathways to net-zero are based on deploying BECCS and AR at scale in countries where the potential for negative emissions is highest.<sup>11,432</sup> Yet even if international assistance (*e.g.*, technology transfers and funds) is available to help with deployment, this would effectively mean that ideally-situated host countries, which might have minimal responsibility for historical emissions, would bear most of the burden for dealing with the adverse consequences of CDR such as integrating new energy flows with existing (often fragile) infrastructure, substantial land use changes and displacement.<sup>374,410,429,433</sup> The ability of DAC to facilitate location-independent sourcing of CO<sub>2</sub> could thus prove critical for enabling advanced economies with geological storage capacity and greater willingness to shoulder more of the

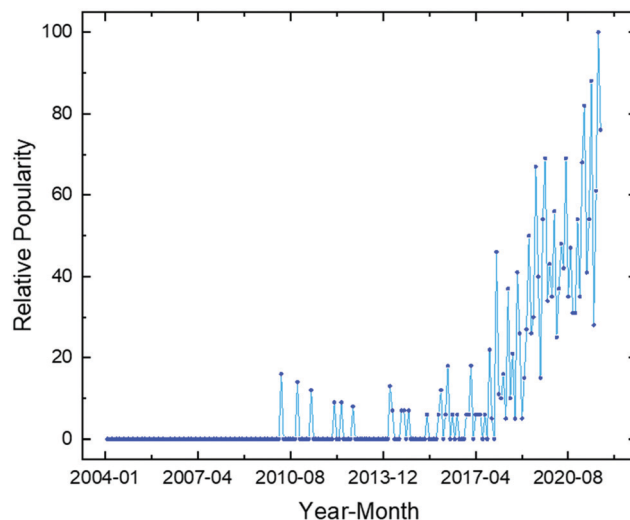


Fig. 29 Google Trends data on worldwide searches for search term “Direct air capture” from January 2004 to September 2021. Each data point is generated by dividing the number of searches by the total searches in the same geography and time. This ratio is then normalised so that peak popularity is equal to 100.



burden by hosting NET projects with permanent storage outcomes.<sup>371</sup>

## 6 Conclusions

We have reviewed the state-of-the-art in DAC across the commercial and research sectors, seeking to provide clear research challenges in the science, engineering, economics, and socio-political domains. The development and deployment of DAC will continue to provide research challenges as the technology has to date been developed by a limited number of start-ups. This has resulted in a somewhat narrow focus; in the first decade or so after DAC was proposed, almost all research focussed on developing sorbents and a limited number of process configurations. Whilst continued improvement of these materials and processes is warranted, particularly in understanding their integration with the energy system, their evolving costs, and their sustainability from a wider frame of reference, a focus on new materials and processes for DAC will provide new opportunities, and the development of DAC will raise challenges in the socio-political domain also. To conclude, we discuss high-level challenges that researchers could address soon to improve our understanding of DAC, unlock new levels of efficiency and sustainability, and increase societal acceptance.

Climate change will require adaptation and mitigation on a massive scale (Section 1). This will involve changes to human practices and behaviours, structural and physical adaptation, a broad portfolio of clean energy generation technologies, as well as technologies to mitigate GHG emissions. The need for, and interaction between these aspects of adaptation and mitigation will evolve with time and thus efforts at understanding the complexity, inter-dependencies, pace, and scale involved will continue to be of the highest importance.

DAC (and other NETs) are not a substitute for *e.g.*, improved energy efficiency, the development of a circular economy, conventional decarbonisation, and more sustainable practices (Section 2). However, DAC offers some unique advantages amongst various NETs and other CCS-related technologies. These advantages should be exploited, yet there is much more that can be done. For example, in almost all cases of DAC deployment, CO<sub>2</sub> utilisation is a crucial technology enabler. However, it is also known that CO<sub>2</sub> utilisation (as compared to storage) is sub-optimal in terms of climate change mitigation. Thus, DAC coupled with geological storage (*i.e.*, DACCS) should be pursued as a deployment priority. Scenarios where CO<sub>2</sub> utilisation is economically favourable should not serve as a distraction but may prove useful to demonstrate DAC technology in the near-term.

CCS processes are only beginning to be deployed at the scale required for meaningful climate change mitigation, whilst DAC is still very much in its infancy (Section 3). Increases in capture rates (*i.e.*, beyond 90%) in CCS processes will reduce the burden on DAC and other NETs and is therefore a research and deployment priority. The most developed DAC processes rely

on sorbents, either liquid or solid. For liquid sorbents, electrochemical regeneration methods appear to show promise for reducing energy requirements, if they can be demonstrated at a suitable scale, with sufficient reliability and reduced materials costs. New liquids with lower regeneration energy requirements will always be beneficial, and it is notable that there is a lack of work on liquid-air contacting. For solid sorbents, several challenges have emerged during deployment, as discussed above. These deserve attention to improve existing processes, as does the development of entirely new sorbents (and associated understanding of structure–activity relationships). However, in all cases, consideration should be given to manufacturing of sorbents at scale and it is also prudent to highlight the disparity between laboratory-scale investigations (sorbent regeneration practices, measurement of equilibrium sorption capacity *etc.*) and the realities involved with deployment. Entirely new DAC processes (*i.e.*, those not relying on sorbents) may offer bespoke options for specific scenarios and, importantly, inspiration for entirely new ways to approach DAC. As DAC is a relatively new technology, investment in ‘blue skies research’ here is likely to provide significant return. Amongst those emerging technologies discussed, electrochemical devices show significant promise, yet they have scarcely been investigated. Passive DAC contacting and the design of physiosorbents has taken inspiration from nature; it would seem foolish not to explore the nexus between natural and engineered DAC systems much further.

A limited amount of reliable data is presented in the literature on both techno-economic and life-cycle environmental performance of DAC (Section 4). To date, only a handful of comprehensive technology assessments have been published to accurately establish the economic and environmental viability of DAC. In the most optimistic scenarios, the long-term cost of CO<sub>2</sub> removal was shown to vary between 40–80 € per tCO<sub>2</sub> for low-temperature DAC and 45–90 € per tCO<sub>2</sub> for high-temperature DAC. It needs to be stressed that there is a large discrepancy in the reported economic viability of DAC, and the cost of CDR up to 400–800 € per tCO<sub>2</sub> that has been reported. Such discrepancies result from a lack of standardised assessment methods and reliable benchmarks for DAC. From the life-cycle emissions perspective, DAC was shown to achieve life-cycle carbon efficiencies of 85–95% when driven by low-carbon energy sources. However, if DAC is driven by electricity from grids relying on fossil fuels, the life-cycle efficiencies can be as low as 9–17%. This means that for each 1 kg of CO<sub>2</sub> removed from the air, 0.83–0.91 kg of CO<sub>2</sub> is released into the atmosphere from the combustion of fossil fuels, negating the true potential of DAC. Importantly, although the LCAs presented in the literature follow the standardised assessment procedures, different approaches to life-cycle inventory analysis and data sources were used. Consequently, past TEAs and LCAs rely on different sets of assumptions, making reliable benchmarking of reported results difficult, if not impossible. It is, therefore, important to derive a set of standardised guidelines and benchmarks that would enable a reliable comparison of DAC.



There are many policy challenges including how to finance demonstration projects and then scale up DAC technologies in the hopes of bringing costs down sufficiently to the point where it is a viable option even with respect to other NETs (Section 5). Most mechanisms have been developed in the more general context of supporting CDR and CO<sub>2</sub> storage, but increasingly there have been more DAC-specific initiatives. There are many attractions of DAC including its greater flexibility in plant location and ability to address overshoot and scale up without some of the social and political constraints faced by other CDR and climate change mitigation options. On the other hand, the attention given to CCU and the association of several of the first major projects with the oil and gas industry, though valuable at providing financing at an early stage, has also led to concerns that DAC will detract from other mitigation options and ensure overshoot. Public and even stakeholder awareness has been low, but as the first large-scale projects have been deployed, DAC has begun to receive greater scrutiny. As interest in DAC has risen, some governments have begun to fund programmes to support early-stage DAC projects and set ambitious targets to bring down the costs of DAC.

Ultimately, DAC is in its infancy, with its place in the energy system and climate change mitigation efforts yet to be clearly defined. Regardless, the challenges associated with DAC forces us to redouble our efforts on climate change mitigation through more conventional efforts and, importantly, to continue to be creative in tackling apparently intractable problems.

## Disclaimer

The content of this article does not reflect the official opinion of the European Union. Responsibility for the information and views expressed herein lies entirely with the author(s).

## Author contributions

All authors contributed individual sections during writing – original draft. All authors were involved in writing – review and editing. All authors were responsible for their respective funding acquisition, where applicable. GAM was responsible for overall project administration.

## Conflicts of interest

There are no conflicts to declare.

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