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# High-power piezoelectric behavior of acceptor-doped $\langle 001 \rangle$ and $\langle 111 \rangle$ textured piezoelectric ceramics†

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Piezoelectric ceramics with high piezoelectric co-efficient,  $d_{33}$ , and mechanical quality factor,  $Q_m$ , are required in high-power applications.  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured  $\text{Pb}(\text{In}_{1/2}\text{Nb}_{1/2})\text{O}_3\text{-Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-PbTiO}_3$  ceramics were fabricated using templated grain growth method and their high-power electromechanical properties were characterized. It is shown that  $\langle 001 \rangle$  textured ceramics possess higher  $d_{33}$  compared to random and  $\langle 111 \rangle$  textured counterparts, while the  $Q_m$  is strongly enhanced in  $\langle 111 \rangle$  textured ceramics due to less favored polarization rotation.  $\text{MnO}_2$  doping is shown to further improve the  $Q_m$  values for both  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics because of the restricted polarization switching induced by the defect dipole. Doped  $\langle 001 \rangle$  textured ceramics can exhibit the high  $d_{33}$  and moderate  $Q_m$  ( $d_{33} = 725 \text{ pC N}^{-1}$ ,  $Q_m = 716$ ) in comparison with  $\langle 111 \rangle$  textured ceramics exhibiting low  $d_{33}$  and high  $Q_m$  ( $d_{33} = 350 \text{ pC N}^{-1}$ ,  $Q_m = 1495$ ). Owing to the combinatory soft and hard piezoelectric properties, the doped  $\langle 001 \rangle$  textured ceramics exhibit  $1.5\times$  higher vibration velocity ( $\sim 0.90 \text{ m s}^{-1}$ ) in comparison with commercial hard PZTs. Interestingly, a slightly higher vibration velocity ( $\sim 0.94 \text{ m s}^{-1}$ ) can be obtained in doped  $\langle 111 \rangle$  textured ceramics, which is mainly attributed to the high  $Q_m$  and low elastic compliance  $s_{11}$ . These results demonstrate the promise of textured piezoelectric ceramics for high-power applications.

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## 1. Introduction

The lead-free piezoelectric materials have been extensively investigated due to their environmental safety benefits. However, compared to lead-based piezoelectric materials, the lead-free piezoelectric materials have inferior comprehensive properties, limiting their practical applications.<sup>1,2</sup> Lead-based relaxor-PT materials, such as  $\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-PbTiO}_3$  (PMN-PT), are promising candidates for electromechanical devices including actuators, transducers, and sensors, due to their superior piezoelectric properties in comparison to conventional PZT ceramics.<sup>3–5</sup> However, the low phase transition temperatures in PMN-PT, including Curie temperature  $T_c$  and rhombohedral to tetragonal phase transition temperature  $T_{r-t}$ , limit the temperature stability.<sup>6,7</sup> The relaxor ternary system,  $\text{Pb}(\text{In}_{1/2}\text{Nb}_{1/2})\text{O}_3\text{-Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{-PbTiO}_3$  (PIN-PMN-PT), can exhibit higher

phase transition temperatures while retaining comparable piezoelectric properties to that of PMN-PT.<sup>8–10</sup>

For high-power transducer applications, piezoelectric ceramics need to possess high piezoelectric coefficient  $d$  and mechanical quality factor  $Q_m$  in order to maximize vibration velocity ( $v_{\text{rms}} \propto Q_m d$ ) and output power ( $P \propto v^2$ ).<sup>11–13</sup> Prior studies have shown that the piezoelectric constant  $d_{33}$  of PIN-PMN-PT can be significantly improved by texturing along  $\langle 001 \rangle$  crystallographic direction using template grain growth (TGG) method. For example, the  $\langle 001 \rangle$  textured PIN-PMN-PT ceramics can exhibit a high  $d_{33}$  of  $927 \text{ pC N}^{-1}$ , which is  $\sim 2\times$  higher than that of non-textured (random) counterparts.<sup>9</sup> The enhanced  $d_{33}$  of  $\langle 001 \rangle$  textured ceramics can be explained by invoking the piezoelectric anisotropy similar to that shown for piezoelectric single crystals.<sup>14,15</sup> However, the textured PIN-PMN-PT ceramics possess a low  $Q_m$  ( $\sim 100$ ), which restricts their applications in high-power transducer devices.<sup>16</sup> Similar to  $\text{MnO}_2$  doped PIN-PMN-PT single crystal, acceptor doping can be an effective way to improve the  $Q_m$  value of textured PIN-PMN-PT ceramics. In these cases, the acceptor ions substitute on the B-site of the perovskite structure, creating defect dipoles consisting of negatively charged center defect ions paired with positively charged oxygen vacancies.<sup>17–19</sup> These defect dipoles pin the domain wall motion under applied

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electric field, leading to reduced mechanical loss and enhanced  $Q_m$  in piezoelectric ceramics. Prior results show that  $\langle 001 \rangle$  textured  $\text{MnO}_2$ -doped 0.24PIN–0.42PMN–0.34PT piezoelectric ceramics can exhibit an excellent combination of  $d_{33}$  and  $Q_m$  ( $d_{33} = 725 \text{ pC N}^{-1}$ ,  $Q_m = 716$ ).<sup>20</sup> However, the effect of  $\text{MnO}_2$  doping on  $Q_m$  value in polycrystalline ceramics for different crystallographic orientations is not well understood. One of the reasons for this lack of understanding is the difficulty in synthesizing  $\langle 111 \rangle$  textured PIN–PMN–PT ceramics as compared to  $\langle 001 \rangle$  orientation. Here, we address this issue and provide synthesis pathway to consistently realize  $\langle 111 \rangle$  oriented piezoelectric ceramics and use this success in synthesis to provide comprehensive comparative analysis of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented PIN–PMN–PT ceramics.

We have investigated the effect of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  texturing on piezoelectric properties and mechanical quality factor of undoped and  $\text{MnO}_2$ -doped 0.24PIN–0.42PMN–0.34PT ceramics to understand the orientation dependence. Two different types of templates,  $\langle 001 \rangle$  and  $\langle 111 \rangle$   $\text{BaTiO}_3$  (BT) crystals were used to texture 0.24PIN–0.42PMN–0.34PT ceramics along  $\langle 001 \rangle$  and  $\langle 111 \rangle$  directions, respectively. The piezoelectric properties and mechanical quality factor of random,  $\langle 001 \rangle$  oriented, and  $\langle 111 \rangle$  oriented ceramics were measured and compared to understand the differences in their magnitudes as well as influence of  $\text{MnO}_2$  doping. High-power piezoelectric vibration characteristics were measured for both doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics to evaluate their promise for practical applications.

## 2. Experimental procedure

The compositions described by the formulation,  $0.24\text{Pb}(\text{In}_{1/2}\text{Nb}_{1/2})\text{O}_3\text{--}0.42\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3\text{--}0.34\text{PbTiO}_3$  (0.24PIN–0.42PMN–0.34PT) and 2 mol%  $\text{MnO}_2$ -doped 0.24PIN–0.42PMN–0.34PT, were synthesized using two-step columbite precursor method.<sup>17</sup> The  $\langle 001 \rangle$  and  $\langle 111 \rangle$   $\text{BaTiO}_3$  (BT) templates were prepared by topochemical microcrystal conversion (TMC) method.<sup>21,22</sup> The ceramic slurry for tape-casting was prepared by ball-milling the 0.24PIN–0.42PMN–0.34PT or 2 mol%  $\text{MnO}_2$ -doped 0.24PIN–0.42PMN–0.34PT matrix powders with polyvinyl butyral (PVB) binder, toluene solvent and 0.25 wt% CuO. In this ceramic slurry, 2 vol%  $\langle 001 \rangle$  and  $\langle 111 \rangle$  BT templates were mixed by magnetic stirring and the mixture was tape casted at a rate of  $20 \text{ mm s}^{-1}$  using a doctor blade with height of 0.25 mm. The dried green tapes were cut, stacked, and laminated at  $85 \text{ }^\circ\text{C}$  under 20 MPa pressure for 15 min. The green samples were heated to  $600 \text{ }^\circ\text{C}$  with a heating rate of  $0.5 \text{ }^\circ\text{C min}^{-1}$  and fired for 1 h to remove the organic binder, and then cold-isostatically pressed at 200 MPa for 1 min. The 0.24PIN–0.42PMN–0.34PT with 0 vol% BT (random), 0.24PIN–0.42PMN–0.34PT with 2 vol%  $\langle 001 \rangle$  BT ( $\langle 001 \rangle$  textured), and 0.24PIN–0.42PMN–0.34PT with 2 vol%  $\langle 111 \rangle$  BT ( $\langle 111 \rangle$  textured) samples were subsequently embedded in calcined 0.24PIN–0.42PMN–0.34PT powders with 1.5 wt% excess PbO and sintered at  $1220 \text{ }^\circ\text{C}$  for 6 h in air. The 2 mol%  $\text{MnO}_2$ -doped 0.24PIN–0.42PMN–0.34PT with 2 vol%  $\langle 001 \rangle$  BT (doped- $\langle 001 \rangle$  textured) and 2 mol%  $\text{MnO}_2$ -doped 0.24PIN–0.42PMN–0.34PT with 2 vol%  $\langle 111 \rangle$  BT (doped- $\langle 111 \rangle$  textured) samples were embedded in

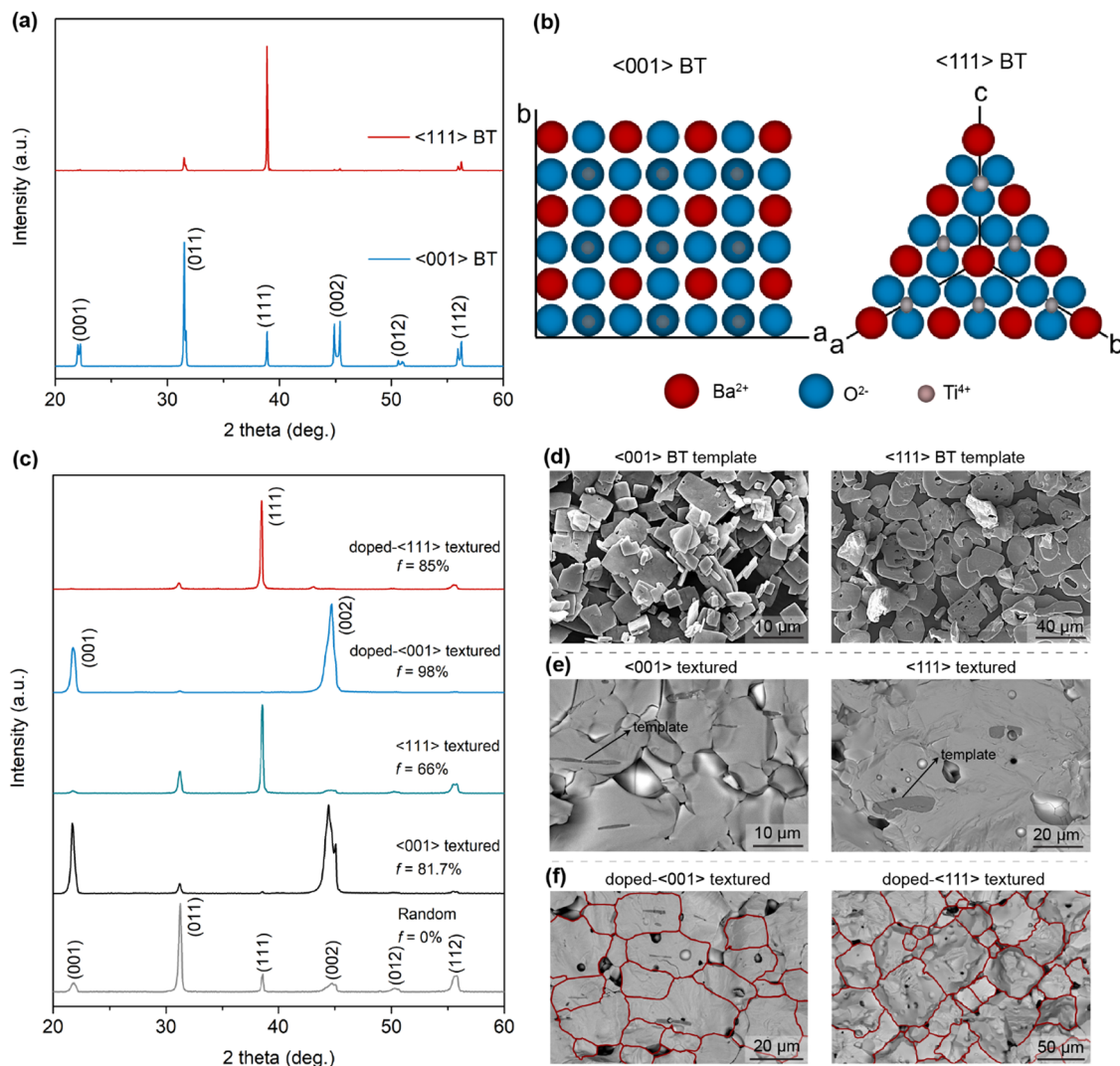
calcined 2 mol%  $\text{MnO}_2$ -doped 0.24PIN–0.42PMN–0.34PT powders with 1.5 wt% excess PbO and sintered at  $1200 \text{ }^\circ\text{C}$  for 6 h in air. The sintered samples were polished to remove residual powders. The sintered densities were measured by Archimedes' method, as listed in Table S1 (ESI†).

The phases and microstructures were determined using X-ray diffraction (XRD, PANalytical Empyrean) and field-emission scanning electron microscopy (FESEM Apreo) in combination with electron backscatter diffraction (EBSD), respectively. The  $\langle 001 \rangle$  and  $\langle 111 \rangle$  texture degree  $F$  was evaluated by Lotgering factor method according to the X-ray diffraction patterns in the 2-theta range of  $20\text{--}60^\circ$ .<sup>23,24</sup> The piezoelectric coefficient  $d_{33}$  was measured by using a quasi-static  $d_{33}$  meter (YE2730A, APC Products). The dielectric permittivity  $\epsilon_r$  as a function of temperature was measured at 1 kHz by a multifrequency LCR meter (HP4284A). Ferroelectric  $P$ – $E$  hysteresis loops and the piezoelectric unipolar strains were measured at 1 Hz using a Precision Premier II ferroelectric Tester (Radiant Technologies). The mechanical coupling coefficient  $k$  and mechanical quality factor  $Q_m$  were determined by resonance and anti-resonance technique using impedance analyzer (Keysight E4990A). Piezoresponse force microscopy (PFM) mode in Bruker Icon II instrument was used to characterize the domain structure and microscopic piezoresponse. The high-power piezoelectric vibration characteristics of commercial hard PZT (APC 841) sample, and  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics were measured in the transverse 31 mode using a laser vibrometer (PSV-500 by Polytec).

## 3. Results and discussion

### 3.1. Fabrication of $\langle 001 \rangle$ and $\langle 111 \rangle$ -textured ceramics

Fig. 1a shows X-ray diffraction (XRD) patterns for  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented BT templates after the topochemical conversion reaction. It can be found that both  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented BT templates exhibit tetragonal perovskite phase. The scanning electron microscopy (SEM) images of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  BT templates are shown in Fig. 1d. Both  $\langle 001 \rangle$  and  $\langle 111 \rangle$  BT templates possess high-aspect ratio plate-like morphologies. The length and thickness of  $\langle 001 \rangle$  BT templates are in the ranges of  $5\text{--}10 \text{ }\mu\text{m}$  and  $0.2\text{--}1.2 \text{ }\mu\text{m}$ , respectively, while the  $\langle 111 \rangle$  BT templates have a larger size with  $20\text{--}30 \text{ }\mu\text{m}$  in length and  $1.5\text{--}3 \text{ }\mu\text{m}$  in thickness. Fig. 1b shows the schematic illustration of  $\text{Ba}^{2+}$  and  $\text{O}^{2-}$  ions arrangement along  $\langle 001 \rangle$  and  $\langle 111 \rangle$  directions for BT templates, which demonstrates that  $\langle 111 \rangle$  BT has higher atomic packing density compared to  $\langle 001 \rangle$  BT. The XRD patterns of random and textured ceramics are shown in Fig. 1c. All samples exhibit perovskite phase, while the  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics exhibit enhanced intensities of  $(00l)$  and  $(11l)$  diffraction peaks, respectively, in comparison with random counterpart, indicating the strong  $\langle 001 \rangle$  or  $\langle 111 \rangle$  orientation of grains. The calculated Lotgering factors  $F_{00l}$  and  $F_{11l}$  for  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics are 81.7% and 66%, respectively. After  $\text{MnO}_2$  doping, both doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics can exhibit much higher  $F_{00l}$  of 98% and  $F_{11l}$  of 85%, respectively, indicating that the  $\text{MnO}_2$  dopant can effectively promote the  $\langle 001 \rangle$  or  $\langle 111 \rangle$  texture development in



**Fig. 1** (a) XRD patterns and (b) schematic diagrams of ion arrangement for  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented BT templates. (c) XRD patterns of PIN-PMN-PT with 0 vol% BT (random), PIN-PMN-PT with 2 vol%  $\langle 001 \rangle$  oriented BT (abbreviated as  $\langle 001 \rangle$  textured), PIN-PMN-PT with 2 vol%  $\langle 111 \rangle$  oriented BT ( $\langle 111 \rangle$  textured), 2 mol%  $\text{MnO}_2$ -doped PIN-PMN-PT with 2 vol%  $\langle 001 \rangle$  oriented BT (doped- $\langle 001 \rangle$  textured), and 2 mol%  $\text{MnO}_2$ -doped PIN-PMN-PT with 2 vol%  $\langle 111 \rangle$  oriented BT (doped- $\langle 111 \rangle$  textured) ceramics. (d) SEM images of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented BT templates. (e) Cross-sectional SEM images of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics. (f) Cross-sectional SEM image of doped- $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics (The visible grain boundaries are marked by red lines).

PIN-PMN-PT ceramics. Fig. 1e and f show the cross-sectional SEM images for undoped and doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics, respectively. The epitaxial grain growth of PIN-PMN-PT matrix on  $\langle 001 \rangle$  and  $\langle 111 \rangle$  BT templates (black areas) can be observed in this figure. In addition, it can be found that the doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics can exhibit textured microstructures with dense grain structure. The enhanced grain growth induced by  $\text{MnO}_2$ -doping has also been found in PZT-PZN piezoelectric ceramics, which is assumed to be caused by diffusion of oxygen vacancies.<sup>25</sup> The oxygen vacancies induced by  $\text{MnO}_2$ -doping can facilitate the lattice diffusion, leading to the enhanced grain growth.<sup>20,25</sup> Considering the different sizes of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  BT templates, it is worth noting that there is still space to further improve the  $\langle 111 \rangle$  texturing degree of PIN-PMN-PT ceramics by optimizing the tape-casting parameters (*e.g.* blade

gap height and tape-casting speed). This presents opportunities for future studies.

Fig. 2 compares the grain growth behavior of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented PIN-PMN-PT matrix grains. The EDS maps indicate the excellent stability of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  BT templates inside the PIN-PMN-PT matrix during the template grain growth process at high temperatures. It is interesting to note that  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented grains exhibit different shapes. Specifically, the  $\langle 001 \rangle$  oriented PIN-PMN-PT grains grown from the  $\langle 001 \rangle$  BT template exhibit a rectangular cross-section, while the  $\langle 111 \rangle$  oriented counterparts display a diamond shape cross-section (Fig. 2a and b). The different grain morphologies in doped- $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics can also be observed in Fig. 1f. Fig. 2c shows the schematic diagrams describing the different grain growth behavior of  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented grains. For the



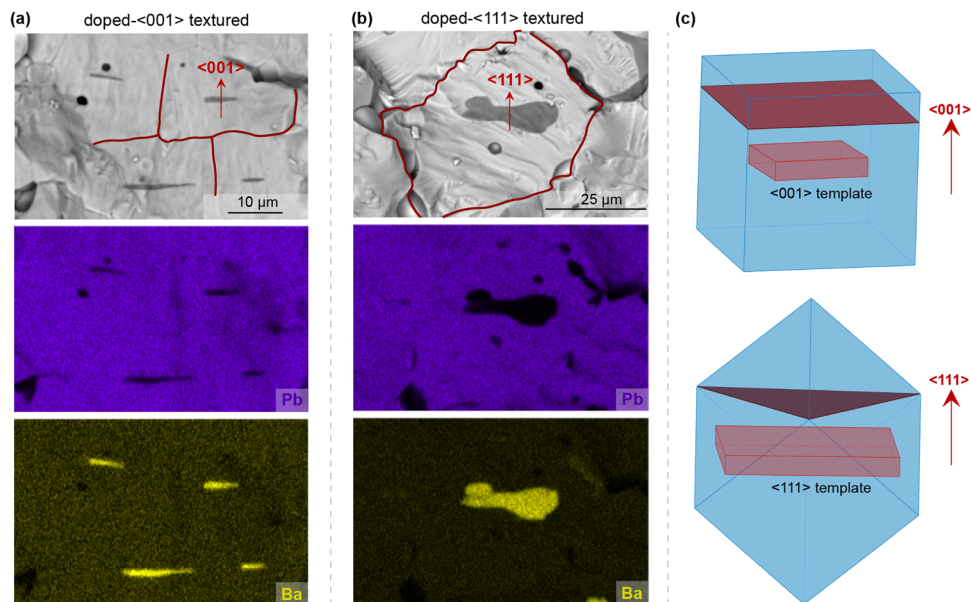


Fig. 2 (a) and (b) Cross-sectional SEM images and the corresponding EDS element mapping of doped-⟨001⟩ and ⟨111⟩ textured ceramics. (c) Schematic diagrams of ⟨001⟩ and ⟨111⟩ oriented grain growth of PIN–PMN–PT matrix on ⟨001⟩ and ⟨111⟩ BT templates.

grains grown on the surface of ⟨001⟩ template, they will follow a layer-by-layer growth mode to form {001}-faced cuboids. This is due to the fact that the perovskite phase have the lowest energy along {001} surface and the ⟨001⟩ template has plate-like morphologies.<sup>21,26</sup> Compared to the ⟨001⟩ oriented grains, the ⟨111⟩ oriented grains grown on the surface of ⟨111⟩ template will grow fastest along ⟨111⟩ direction due to the high surface energy of {111} planes, leading to the absence of {111} surfaces in the

final shape and forming triangular bi-pyramids with low-energy density {001} surfaces.

The SEM images of polished surface and the corresponding EBSD images for random and textured ceramics are shown in Fig. 3. The doped ⟨111⟩ textured ceramics possess much larger grain size compared to doped ⟨001⟩ textured ceramics. As shown in Fig. 1d, the ⟨111⟩ BT templates have much larger crystal size compared to ⟨001⟩ BT templates. Since the total BT

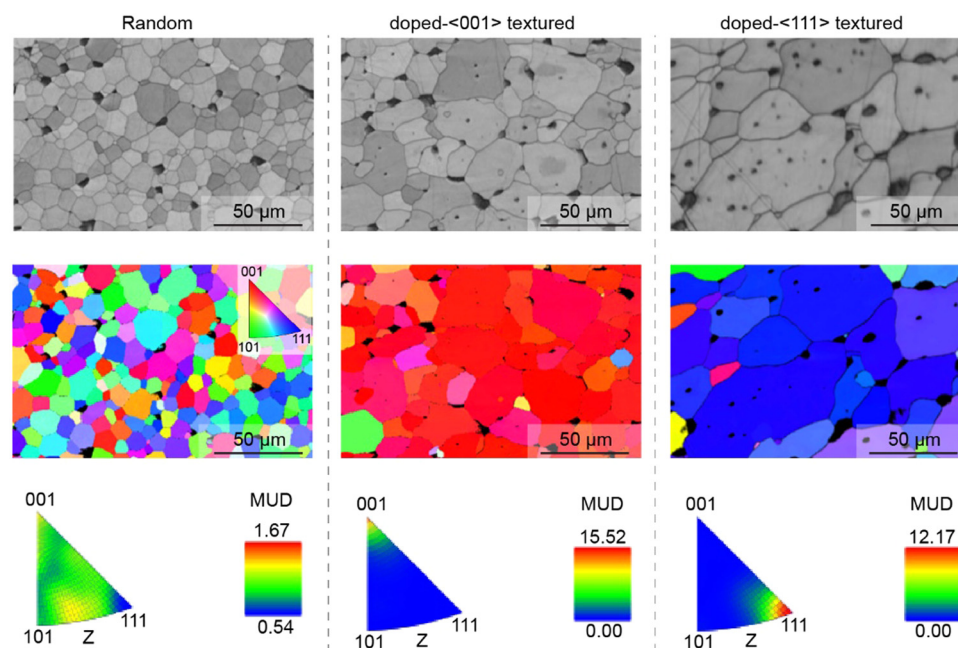


Fig. 3 SEM images of polished surface and the corresponding EBSD images of random, doped-⟨001⟩ and ⟨111⟩ textured ceramics. In EBSD, MUD (multiple of uniform density) is a parameter used for the statistical description of the intensity of texture. MUD value of 1 indicates randomly oriented gains and MUD value significantly  $> 1$  indicates textured grains.

template content inside the PIN-PMN-PT matrix is fixed for  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics,  $\langle 111 \rangle$  textured ceramics will have lower number of the templates ( $f_T$ ) inside the PIN-PMN-PT matrix compared to  $\langle 001 \rangle$  textured ceramics. As a result,  $\langle 111 \rangle$  oriented grains have longer crystal growth length ( $x_T$ ) before impinging on surrounding textured grains, based on the relationship  $x_T = \left(\frac{6}{\pi f_T}\right)^{\frac{1}{3}}$ ,<sup>27</sup> leading to the larger grain sizes. The EBSD mapping further provides the evidence for strong  $\langle 001 \rangle$  and  $\langle 111 \rangle$  orientation of grains in textured ceramics.

### 3.2. Dielectric and piezoelectric properties of $\langle 001 \rangle$ and $\langle 111 \rangle$ -textured ceramics

Fig. 4a shows the dielectric constant as a function of temperature for random,  $\langle 001 \rangle$  textured, and  $\langle 111 \rangle$  textured ceramics. First, two dielectric peaks at approximately 118 °C and 219 °C, corresponding to rhombohedral to tetragonal ( $T_{r-t}$ ) and tetragonal to cubic ( $T_c$ ) phase transitions can be found in random ceramic. Both  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics have  $T_c$  value around 219 °C, indicating that the presence of 2 vol% BT template has little influence on the transition temperature. After MnO<sub>2</sub> doping, the Curie temperature  $T_c$  slightly decreases to 204 °C for doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics. Similar phenomenon induced by Mn doping has also been reported in PSZTN system.<sup>28</sup> Fig. 4b compares the unipolar strain response measured at the electric field of 30 kV cm<sup>-1</sup> for random,  $\langle 001 \rangle$  textured, and  $\langle 111 \rangle$  textured ceramics. The strain values follow the trend,  $S_{\langle 001 \rangle} > S_{\text{Random}} > S_{\langle 111 \rangle}$  at 30 kV cm<sup>-1</sup>, which is

consistent with the trend of measured small signal  $d_{33}$  values for random and textured ceramics in Table 1. From the  $P$ - $E$  hysteresis loops shown in Fig. 4c, it is interesting to note that both MnO<sub>2</sub>-doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics possess higher remnant polarization ( $P_r$ ) compared to undoped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  counterparts. The lower  $P_r$  values of undoped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics can be understood from the impedance spectra shown in Fig. 4d. It is known that the maximum impedance phase angle  $\theta_z$  in impedance spectra is related to the poling degree of piezoelectric ceramics.<sup>29,30</sup> The undoped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics exhibit lower  $\theta_z$  values of 75° and 72°, respectively, compared to doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured counterparts with high  $\theta_z$  values of 89° and 88°, respectively, indicating the low poling degree of undoped textured ceramics. The low poling degree implies insufficient polarization switching under electric field, resulting in low  $P_r$  value of piezoelectric ceramics. In addition to the different polarization values, the apparent horizontal shift in the  $P$ - $E$  hysteresis loops of MnO<sub>2</sub>-doped textured ceramics can be observed in comparison with undoped textured counterparts (Fig. 4c), suggesting the existence of internal bias field  $E_i$  induced by the well oriented defect dipoles. The  $E_i$  value can be calculated by the equation  $E_i = (E_{c+} + E_{c-})/2$ , where  $E_{c+}$  and  $E_{c-}$  are the intersections of  $P$ - $E$  hysteresis loops with the positive and negative  $E$  field axis, respectively.<sup>31</sup> The  $E_i$  value is calculated to be 1.10 kV cm<sup>-1</sup> and 1.31 kV cm<sup>-1</sup> for doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics, respectively.

The detailed dielectric and piezoelectric properties of random,  $\langle 001 \rangle$  textured, and  $\langle 111 \rangle$  textured ceramics can be found

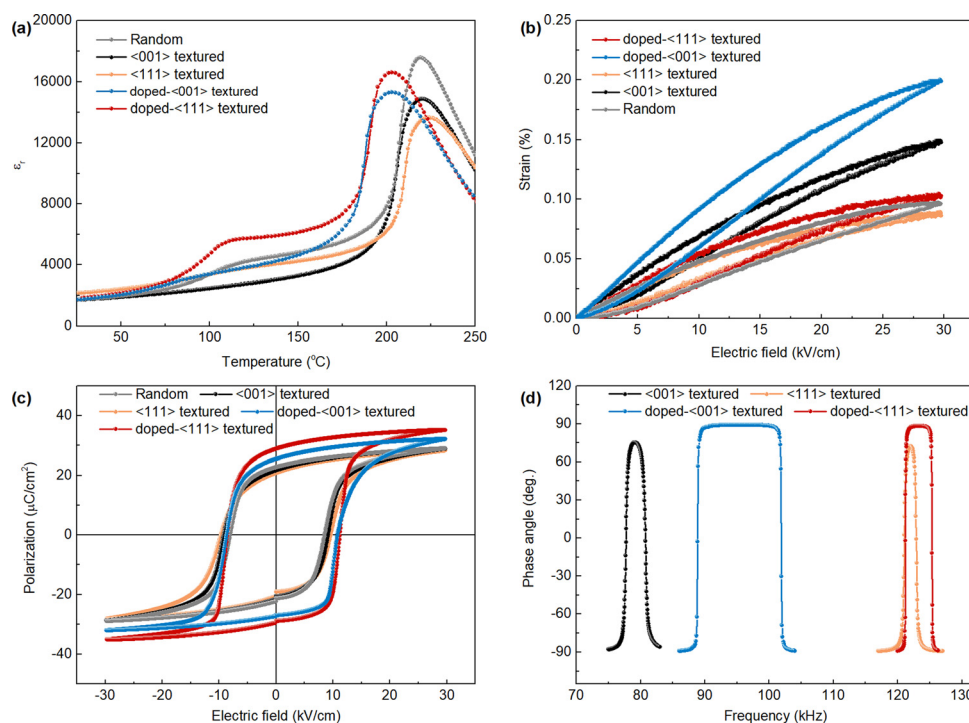


Fig. 4 (a) Dielectric permittivity (measured at 1 kHz) and (b) unipolar  $S$ - $E$  curves (measured at 1 Hz) for random,  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured, and doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics. (c)  $P$ - $E$  hysteresis loops (measured at 1 Hz) and (d) phase angle spectra (measured with the voltage amplitude of 500 mV) for random,  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured, and doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics.

**Table 1** Dielectric and piezoelectric properties for both random, ⟨001⟩ and ⟨111⟩ textured piezoelectric ceramics

| Specimen                          | Template        | $F_{001}$ [%] | $\epsilon_{33}^T/\epsilon_0$ | $s_{11}$ [ $\mu\text{m}^2 \text{N}^{-1}$ ] | $\tan \delta$ [%] | $d_{33}$ [ $\text{pC N}^{-1}$ ] | $d_{31}$ [ $\text{pC N}^{-1}$ ] | $k_{31}$ | $Q_m$ |
|-----------------------------------|-----------------|---------------|------------------------------|--|-------------------|---------------------------------|---------------------------------|----------|-------|
| Random <sup>a</sup>               | 0               | 0             | 1836                         | 12.39                                      | 0.96              | 304                             | 101                             | 0.22     | 147   |
| ⟨001⟩ textured                    | 2 vol% ⟨001⟩ BT | 81.7          | 1727                         | 14.44                                      | 0.9               | 412                             | 138                             | 0.29     | 165   |
| ⟨111⟩ textured                    | 2 vol% ⟨111⟩ BT | 66            | 2097                         | 11.20                                      | 0.7               | 274                             | 82                              | 0.18     | 385   |
| Doped-⟨001⟩ textured <sup>a</sup> | 2 vol% ⟨001⟩ BT | 98            | 1498                         | 15.90                                      | 0.42              | 725                             | 247                             | 0.54     | 716   |
| Doped-⟨111⟩ textured              | 2 vol% ⟨111⟩ BT | 85            | 1850                         | 9.90                                       | 0.5               | 350                             | 116                             | 0.29     | 1495  |
| Commercial APC 841                | 0               | 0             | 1152                         | 11.24                                      | 0.5               | 312                             | 108                             | 0.33     | 1050  |

<sup>a</sup> Ref. 20.

in Table 1. The piezoelectric coefficient  $d_{33}$  of ⟨001⟩ textured ceramics is higher than that of random ceramics, while the ⟨111⟩ textured ceramics show the lowest  $d_{33}$  value.

For perovskite ferroelectrics, the piezoelectric coefficient  $d_{33}$  is proportional to  $Q_{33}P_S\epsilon_{33}$ .<sup>32–34</sup> The electrostrictive coefficient  $Q_{33}$  of perovskite ferroelectrics exhibits orientation dependent behavior. The maximum  $Q_{33}$  is along the ⟨001⟩ direction, while the minimum value is along the ⟨111⟩ direction.<sup>34</sup> In addition, the anisotropy of  $Q_{33}$  is not sensitive to the ferroelectric phases. As a result, the ⟨001⟩ textured ceramics will exhibit the highest  $d_{33}$  value compared to random and ⟨111⟩ textured ceramics. Although the highest  $d_{33}$  value can be obtained in ⟨001⟩ textured ceramics, the percentage enhancement in  $d_{33}$  coming from the ⟨001⟩ texturing is less than 40% (from 304  $\text{pC N}^{-1}$  in random ceramics to 412  $\text{pC N}^{-1}$  in ⟨001⟩ textured ceramics) due to the incomplete template grain growth of ⟨001⟩ textured ceramics ( $F_{001} \sim 81.7\%$ ).

As shown in Table 1, the ⟨111⟩ textured ceramics possess much higher mechanical quality factor  $Q_m$  of 385 in comparison with ⟨001⟩ textured ceramics exhibiting  $Q_m$  value of 165, indicating the orientation dependence of  $Q_m$  in PIN-PMN-PT ceramics. This is different from the softening and hardening effects induced by dopants in piezoelectric ceramics. It is known that the polarization rotation under external electric field will result in high magnitude of mechanical loss ( $\tan \gamma$ ) in ferroelectrics.<sup>35,36</sup> When an electric field is applied to poled piezoelectric sample with multi-domain configuration, the torque per unit volume for the polarization rotation can be expressed as:<sup>37</sup>

$$M = \frac{q\vec{E} \times \vec{l}}{V} = \frac{qEl \sin \varphi}{V} = \left(\frac{ql}{V}\right) \cdot E \cdot \sin \varphi = PE \sin \varphi \quad (1)$$

where  $q$  represents the charge of polarization  $P$ ,  $l$  is the effective distance between the negative charge and positive charge point,  $V$  is the unit cell volume, and  $\varphi$  is the angle between the polarization  $P$  and external electric field  $E$ . It can be found that a larger angle  $\varphi$  will favor the polarization rotation under the external electric field, leading to the high mechanical loss (low  $Q_m$ ). As shown in Fig. S1 (ESI<sup>†</sup>), the  $\varphi$  value is around 54.7° and 0° for ⟨001⟩ and ⟨111⟩ oriented samples, respectively. This implies that the ⟨111⟩ oriented samples will possess lower mechanical loss (high  $Q_m$ ) compared to ⟨001⟩ oriented counterparts, which is consistent with our experimental results.

After MnO<sub>2</sub> doping, the  $d_{33}$  of ⟨001⟩ textured ceramics exhibit significant improvement from 412  $\text{pC N}^{-1}$  to 725  $\text{pC N}^{-1}$ , which is due to the improved ⟨001⟩ texturing degree ( $F_{001}$  value from

81.7% to 98%) and poling degree ( $\theta_z$  value from 75° to 89°) induced by MnO<sub>2</sub> doping effect. The ⟨111⟩ textured ceramics also exhibit similar trend, where the  $d_{33}$  value increases from 274  $\text{pC N}^{-1}$  to 350  $\text{pC N}^{-1}$  due to the improved poling degree ( $\theta_z$  value from 72° to 88°). The low poling degree of piezoelectric ceramics is usually caused by different losses, including mechanical loss  $\tan \gamma$ , dielectric loss  $\tan \delta$ , and piezoelectric loss  $\tan \theta$ .<sup>37–39</sup>

These three losses can be obtained by simulating the impedance spectra using the loss incorporated equivalent circuit.<sup>39,40</sup> As shown in Fig. 5a–d, the simulation results demonstrate that both ⟨001⟩ and ⟨111⟩ textured ceramics possess much higher loss in comparison with doped ⟨001⟩ and ⟨111⟩ textured counterparts. The simulation results in Fig. 5e–g and Fig. S2 (ESI<sup>†</sup>) show the effect of different magnitudes and different types of loss on phase angle  $\theta_z$  of ⟨001⟩ and ⟨111⟩ textured ceramics, respectively. It was found that both dielectric loss  $\tan \delta$ , and piezoelectric loss  $\tan \theta$  have minimal effect on phase angle  $\theta_z$ , while mechanical loss  $\tan \gamma = 1/Q_m$  shows the significant effect on  $\theta_z$  in both ⟨001⟩ and ⟨111⟩ textured ceramics. A lower mechanical loss  $\tan \gamma$  (high  $Q_m$ ) will lead to higher phase angle  $\theta_z$ , which is consistent with our experimental results where doped textured ceramics show higher  $\theta_z$  value than undoped counterparts due to the reduced mechanical loss  $\tan \gamma$  (high  $Q_m$ ). The doped ⟨001⟩ textured ceramics still exhibits much higher piezoelectric response  $d_{33}$  in comparison with doped ⟨111⟩ textured counterparts due to the orientation dependent behavior of  $d_{33}$  as discussed before.

In addition to the intrinsic contribution from the piezoelectric anisotropy, it is known that the domain size and morphology can strongly affect the piezoelectric properties.<sup>41–43</sup> Thus, piezo-response force microscopy (PFM) was applied to observe the domain structures for both doped ⟨001⟩ and ⟨111⟩ textured ceramics. As shown in Fig. 6a and b, both doped ⟨001⟩ and ⟨111⟩ textured ceramics have an island-type domain structure, while the doped ⟨001⟩ textured ceramic exhibits a smaller and homogeneous domain than that of doped ⟨111⟩ textured counterpart. The domain size  $D$  is proportional to the domain wall energy  $\gamma$  based on the relationship  $D \propto \sqrt{\gamma}$ .<sup>44</sup> The smaller domains with reduced domain wall energy in doped ⟨001⟩ textured ceramic can facilitate the domain wall motion and domain switching under the external electric field, leading to the enhanced extrinsic piezoelectric contributions. Thus, the domain size may be a factor responsible for the high piezoelectric response of doped ⟨001⟩ textured ceramic. Previous domain size studies on Pb(Zr,Ti)O<sub>3</sub> and BaTiO<sub>3</sub> systems find that the domain size increases with increasing grain size.<sup>45</sup> We also observe the similar grain-domain size relation in textured



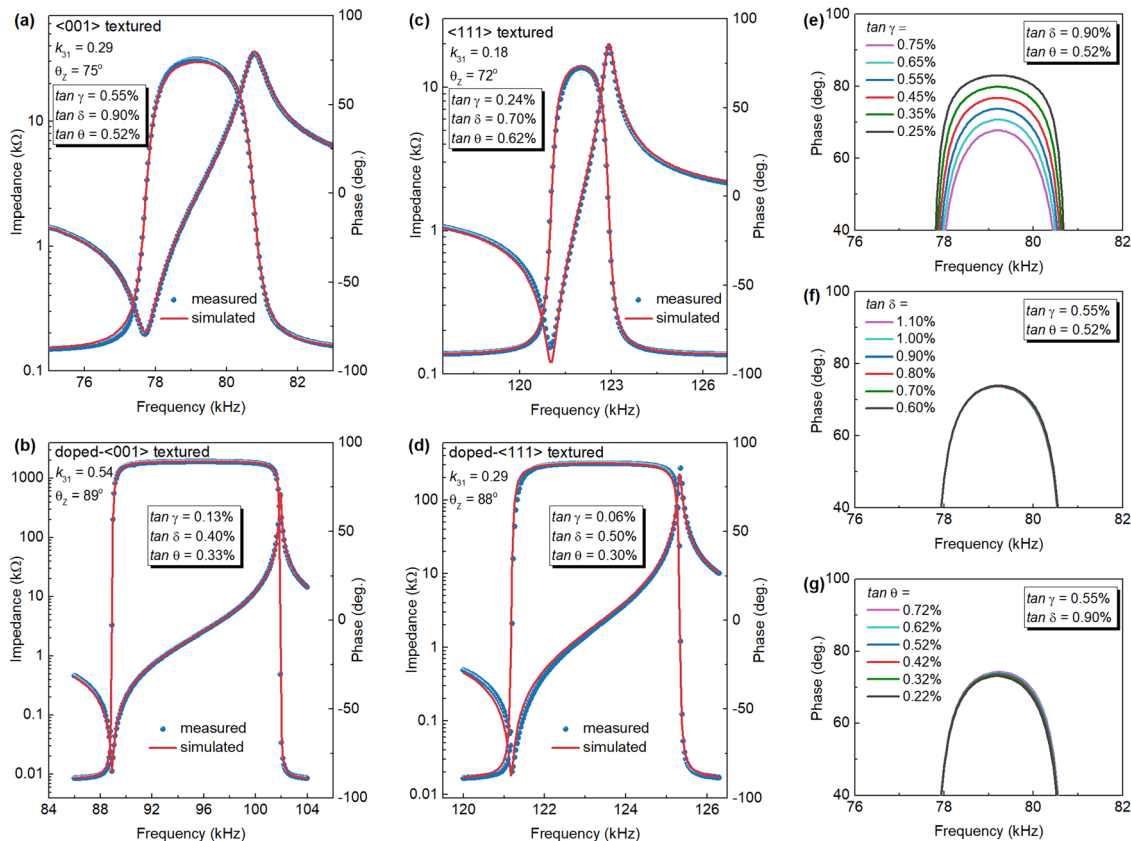


Fig. 5 Impedance and phase angle spectra for (a)  $\langle 001 \rangle$  textured and (b) doped- $\langle 001 \rangle$  textured ceramics. Impedance and phase angle spectra for (c)  $\langle 111 \rangle$  textured and (d) doped- $\langle 111 \rangle$  textured ceramics (the mechanical loss  $\tan \gamma$ , dielectric loss  $\tan \delta$ , and piezoelectric loss  $\tan \theta$  were fitted using loss incorporated equivalent circuit). (e)–(g) Simulated phase angle spectra for  $\langle 001 \rangle$  textured ceramic with different loss factors.

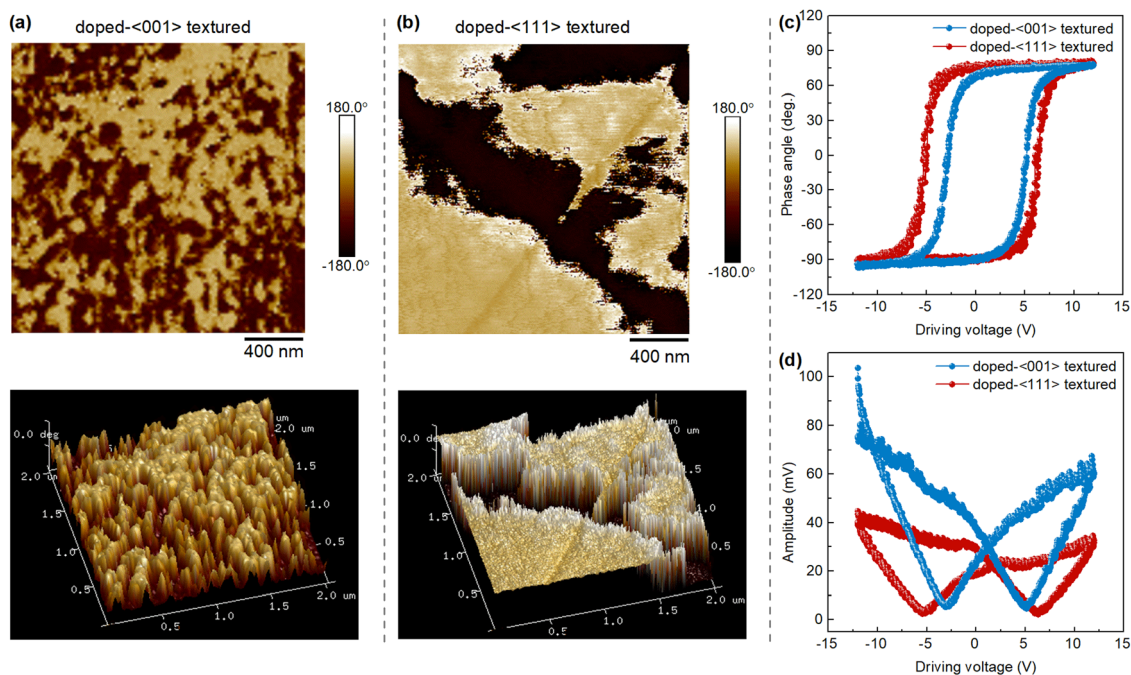


Fig. 6 (a) and (b) 2D and 3D PFM phase images of domain structure for doped- $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics. (c) Microscopic piezoresponse hysteresis loops and (d) butterfly-shaped amplitude versus driving voltage curves for doped- $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics.

ceramics where doped  $\langle 111 \rangle$  textured ceramics with larger grain size can exhibit larger domain size in comparison with doped  $\langle 001 \rangle$  textured counterparts. In addition, it has been reported that the strain induced by the template-matrix interface in textured ceramics constrains the domain size, leading to the fine domain structure.<sup>24,46</sup> Based on SEM results, the  $\langle 111 \rangle$  BT templates have lower frequency inside the PIN–PMN–PT matrix than  $\langle 001 \rangle$  BT templates. Thus, the strain effect on domain structure induced by the template-matrix interface is smaller in doped  $\langle 111 \rangle$  textured ceramics compared to doped  $\langle 001 \rangle$  textured ceramics.

To further understand the effect of crystallographic orientation on microscopic piezoresponse, both phase-voltage hysteresis loops and amplitude-voltage butterfly curves were measured at local positions in  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured grains by applying a sequence of DC voltage from  $-12$  V to  $12$  V with a superimposed AC signal of  $5$  V to the PFM tip (Fig. 6c and d). The phase hysteresis loops exhibit nearly  $180^\circ$  phase reversal, indicating the sufficient polarization switching of doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics. However, the average amplitude of piezoresponse in doped  $\langle 001 \rangle$  textured ceramic is much higher than that of doped  $\langle 111 \rangle$  textured ceramic (Fig. 6d), which is consistent with the trend of measured macroscopic piezoresponse for doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics.

### 3.3. Crystallographic orientation dependence of high-power properties

The mechanical quality factor for doped textured ceramics also exhibits anisotropic behavior, where the  $\langle 111 \rangle$  textured ceramics possess much higher  $Q_m$  value of  $1495$  in comparison with doped  $\langle 001 \rangle$  textured ceramics exhibiting  $Q_m$  value of  $716$  (Table 1). As shown in Table 1, the enhancement of  $Q_m$  after  $\text{MnO}_2$  doping can be found in both  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured

ceramics. For  $\text{MnO}_2$ -doped piezoelectric ceramics, acceptor ions like  $\text{Mn}^{2+}$  or  $\text{Mn}^{3+}$  will substitute on B-site of perovskite structure, replacing higher valent  $\text{Ti}^{4+}$  and  $\text{Nb}^{5+}$  due to the similar ionic radius, resulting in the formation of defect dipoles consisting of negatively charged acceptor ions and positively charged oxygen vacancies,  $\text{Mn}_{\text{Ti}}'' - \text{V}_{\text{O}}^{\bullet\bullet}$ .<sup>28,35</sup> The formation of defect dipoles in  $\text{MnO}_2$ -doped textured ceramics can restrain the oxygen vacancy  $\text{V}_{\text{O}}^{\bullet\bullet}$  migration (higher activation energy  $E_a$  of the conduction) and decrease in the electrical conductivity, as shown in Fig. 7, leading to the lower dielectric loss  $\tan \delta$  in doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics (Table 1).

On the other hand, the  $\text{Mn}^{2+} - \text{V}_{\text{O}}^{\bullet\bullet}$  defect dipoles will induce defect polarization  $P_D$ , which can be represented by:

$$P_D = \frac{\sum p_D}{V} = \frac{cp_D}{V} \quad (2)$$

where  $p_D$  is the defect dipole moment of  $\text{Mn}_{\text{Ti}}'' - \text{V}_{\text{O}}^{\bullet\bullet}$  and  $V$  is the lattice volume. The defect polarization  $P_D$  will prefer to align in the same direction of spontaneous polarization  $P_S$  based on the symmetry conforming short-range ordering (SC-SRO).<sup>47,48</sup> When an external electric field  $E$  is applied to the sample, the spontaneous polarization  $P_S$  prefers to switch to the same direction of  $E$ , while the defect dipole induced polarization  $P_D$  will remain along its original direction since the  $P_D$  switching requires  $\text{V}_{\text{O}}^{\bullet\bullet}$  diffusion, and the polarization switching under electric field is diffusion-less process.<sup>17</sup> The  $P_D$  will then generate a restoring force to constrain the  $P_S$  switching under electric field, as shown in Fig. 8a. To further confirm the constrained  $P_S$  switching in  $\text{MnO}_2$ -doped textured ceramics, the activation energy  $E_a$  for polarization switching for both undoped and  $\text{MnO}_2$ -doped textured ceramics is calculated and compared. For piezoelectric ceramics, the back-switching polarization  $P_{bc}$  will increase with

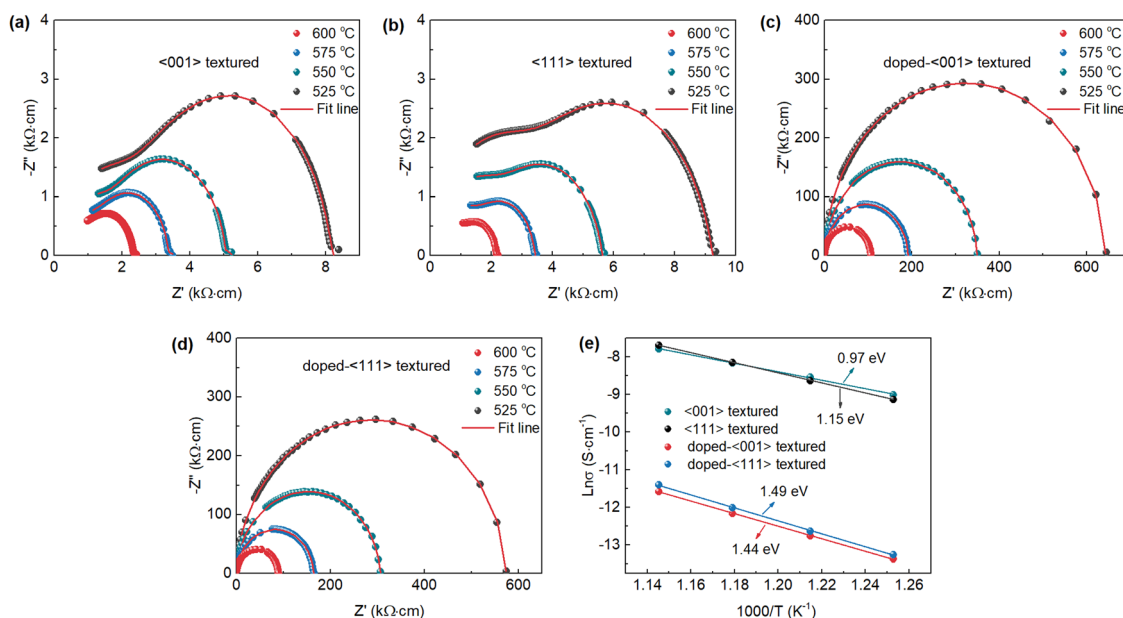


Fig. 7 (a)–(d) Temperature dependent complex impedance spectra and (e) corresponding Arrhenius plots of ionic conductivities for  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured, and doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics.





Fig. 8 (a) Schematic diagram of restricted polarization rotation induced by defect polarization  $P_D$  in acceptor-doped piezoelectric materials. (b) Plot of  $\ln(P_{bc})$  versus inverse temperature for  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured and doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics.

temperature following the Arrhenius Law:<sup>35,49,50</sup>

$$P_{bc} = P_0 \exp\left(\frac{-E_a}{k_B T}\right) \quad (3)$$

where  $P_0$  is the fitting constant and  $E_a$  is the activation energy of polarization switching. The activation energy is determined to be 0.153 eV and 0.135 eV for doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics, respectively, which is much higher than that of undoped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics (0.032 eV and 0.050 eV, respectively), as shown in Fig. 8b, experimentally demonstrating the constrained  $P_s$  switching in  $\text{MnO}_2$ -doped textured ceramics. The constrained  $P_s$  switching will lead to low magnitude of mechanical loss  $\tan \gamma$  (high  $Q_m$ ).

In addition to the hardening effects induced by  $\text{MnO}_2$  dopant, the different engineered domain configurations can also play an important role in affecting  $Q_m$  value. The poled  $\langle 111 \rangle$  oriented sample exhibits monodomain configuration (1R), thus, the low mechanical loss and high  $Q_m$  can be expected. For poled  $\langle 001 \rangle$  oriented sample, it exhibits four equivalent engineered domains (4R), leading to the enhanced polarization rotation and higher mechanical loss (lower  $Q_m$ ). Thus, the doped  $\langle 111 \rangle$  textured ceramics will possess much

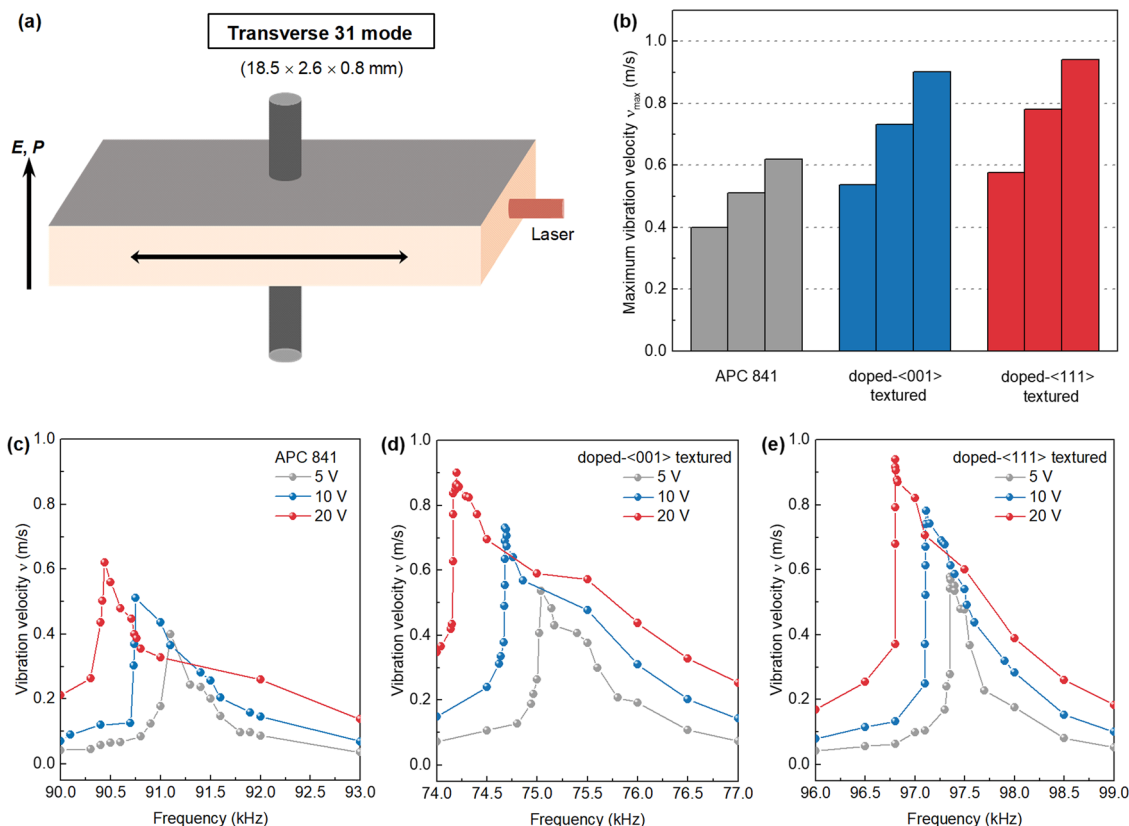
higher  $Q_m$  value in comparison with doped  $\langle 001 \rangle$  textured ceramics (Fig. 9a). As shown in Fig. 9b, the doped  $\langle 001 \rangle$  textured ceramics exhibit the high  $d_{33}$  and moderate  $Q_m$  value in comparison with  $\langle 111 \rangle$  textured ceramics exhibiting low  $d_{33}$  and high  $Q_m$ . Since the  $\langle 110 \rangle$  oriented sample exhibits the two equivalent engineered domains (2R), lying between  $\langle 001 \rangle$  and  $\langle 111 \rangle$  oriented samples (4R and 1R, respectively), it is expected that the doped  $\langle 110 \rangle$  textured ceramics can exhibit good combination of  $d_{33}$  and  $Q_m$ .

#### 3.4. Enhanced high-power vibration characteristics in $\langle 001 \rangle$ and $\langle 111 \rangle$ -textured ceramics

To demonstrate the effectiveness of doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics in high-power applications, we measured the high-power piezoelectric vibration characteristics for both doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics under the transverse length (31) mode using a laser vibrometer, as shown in Fig. 10a. These vibration characteristics were then compared with that of the commercial hard PZT ceramic (APC 841). Fig. 10c and d show the vibration velocity as a function of the measured frequencies under the constant driving voltage of 5  $V_{p-p}$ , 10  $V_{p-p}$  and 20  $V_{p-p}$  for doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics



Fig. 9 (a)  $Q_m$  values of undoped and doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics. (b)  $Q_m$  vs.  $d_{33}$  for doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics.



**Fig. 10** (a) Schematics of the measured piezoelectric sample geometries ( $k_{31}$  mode), where electric field  $E$ , polarization  $P$ , and vibrometer laser beam directions are indicated by arrows. (b) Comparison of maximum vibration velocities at 5  $V_{p-p}$ , 10  $V_{p-p}$  and 20  $V_{p-p}$  for APC 841, doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics. (c–e) Vibration velocity as a function of the measured frequency under the constant driving voltage of 5  $V_{p-p}$ , 10  $V_{p-p}$  and 20  $V_{p-p}$  for APC 841, doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics, respectively (the measured vibration velocities of APC 841 are from ref. 18).

and APC 841 sample, respectively. The peak values of the measured vibration velocity at 5  $V_{p-p}$ , 10  $V_{p-p}$  and 20  $V_{p-p}$  for these samples were compared in Fig. 10b. Under the same driving voltage, the maximum vibration velocity  $v_{\max}$  of both  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics is much higher than that of the APC 841 sample. Specifically, the doped  $\langle 001 \rangle$  textured ceramic can exhibit around  $1.5\times$  higher  $v_{\max}$  ( $\sim 0.90$   $\text{m s}^{-1}$ ) in comparison with commercial hard PZT samples ( $\sim 0.62$   $\text{m s}^{-1}$ ) at 20  $V_{p-p}$ . The enhanced vibration velocity in doped  $\langle 001 \rangle$  textured ceramic can be understood in terms of its combinatory soft and hard piezoelectric properties, as shown in Table 1. Interestingly, a slightly higher  $v_{\max}$  ( $\sim 0.94$   $\text{m s}^{-1}$ ) can be obtained in doped  $\langle 111 \rangle$  textured ceramic. Compared to both doped  $\langle 001 \rangle$  ceramic and APC 841 sample, the higher vibration velocity in doped  $\langle 111 \rangle$  textured ceramic should be attributed to its high  $Q_m$  and low elastic compliance  $s_{11}$  (Table 1) since the vibration velocity of piezoelectric ceramics is proportional to the figure of merit  $\frac{d_{31} \cdot Q_m}{s_{11}^{1.5}}$ .<sup>13</sup> It is known that the output power of high-power device is proportional to  $v^2$ . Thus, both doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics will show over  $2\times$  higher output power in comparison with APC 841 sample. The experimental results here clearly demonstrate the promise of doped  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured piezoelectric ceramics for replacing conventional random ceramics in high-power applications.

## 4. Conclusion

In summary, both  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured PIN-PMN-PT ceramics were successfully fabricated through TGG method to investigate the effects of the crystallographic orientation on high-power properties of PIN-PMN-PT ceramics. Interestingly, we found that both piezoelectric properties and mechanical quality factor exhibit crystallographic orientation dependent behavior in PIN-PMN-PT ceramics. The  $\langle 001 \rangle$  textured PIN-PMN-PT ceramics possess higher piezoelectric constant  $d_{33}$  and coupling factors  $k_{31}$  in comparison with both random and  $\langle 111 \rangle$  textured counterparts, while the mechanical quality factor  $Q_m$  was enhanced in  $\langle 111 \rangle$  textured ceramics due to the less favored polarization rotation in  $\langle 111 \rangle$  oriented sample with monodomain configuration (1R). The  $d_{33}$  of  $\langle 001 \rangle$  textured ceramics can be further improved from  $412$   $\text{pC N}^{-1}$  to  $725$   $\text{pC N}^{-1}$  because of the improved  $\langle 001 \rangle$  texturing degree and poling degree induced by  $\text{MnO}_2$  doping. In addition, the  $Q_m$  values for  $\langle 001 \rangle$  and  $\langle 111 \rangle$  textured ceramics were significantly improved by  $\text{MnO}_2$  doping effect. The doped  $\langle 001 \rangle$  textured ceramics exhibit high  $d_{33}$  and moderate  $Q_m$  ( $d_{33} = 725$   $\text{pC N}^{-1}$ ,  $Q_m = 716$ ) in comparison with  $\langle 111 \rangle$  textured ceramics exhibiting low  $d_{33}$  and high  $Q_m$  ( $d_{33} = 350$   $\text{pC N}^{-1}$ ,  $Q_m = 1495$ ). Compared to commercial hard PZT samples, the doped  $\langle 001 \rangle$  textured ceramics exhibit around  $1.5\times$  higher vibration velocity ( $\sim 0.90$   $\text{m s}^{-1}$ ), which is

mainly attributed to its high soft and hard piezoelectric properties. In addition, owing to the high  $Q_m$  and low elastic compliance  $s_{11}$ , the doped (111) textured ceramics possess higher vibration velocity ( $\sim 0.94 \text{ m s}^{-1}$ ). Our experimental results demonstrate the promise of textured piezoelectric ceramics to replace conventional random ceramics in high-power applications.

## Conflicts of interest

There are no conflicts to declare.

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