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A critical review of technologies, costs, and projects for production of carbon-neutral liquid e-fuels from hydrogen and captured CO₂

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Hydrogen production along with CCUS (carbon capture, utilization, and storage) are two critical areas towards decarbonization and transition to net-zero from the current fossil fuel-based energy system. Although some technical challenges and relatively high costs of these technologies are the limiting factors for their wide-scale use in the short term, the other challenge in the mass-adoption of these technologies is the lack of the hydrogen- and CO₂-compatible midstream (transport, pipelines, storage, etc.) and downstream (engines, turbines, etc.) infrastructure, especially as it is related to the scale required for their wide adoption. The widespread infrastructure to support the large-scale hydrogen (H₂) economy with CCUS is not expected to be ready before 2030 in any part of the world, although the social and legal obligations to decarbonize energy and other infrastructure-heavy sectors are moving much faster. The lack of compatible midstream and downstream infrastructure is limiting the large-scale utilization of H₂, and captured CO₂ can be partially offset by producing sustainable liquid electro-fuels (e-fuels) derived from H₂ and captured CO₂. The carbon-neutral liquid e-fuels derived from H₂ and captured CO₂ are attractive for multiple reasons, which include (i) being compatible with existing infrastructure for storage and transportation, (ii) being compatible with existing internal combustion engines in aviation, shipping, freight, etc., without requiring any modification to the engine or other equipment, (iii) being low in sulfur and being also able to be mixed with kerosene produced using fossil fuel, and (iv) huge transport market for their fossil fuel-based counterparts, with potential for greater long-term returns in view of their contribution in reducing carbon emissions from this sector. In terms of the technology readiness level and the field experience, liquid e-fuels have been produced at various pilot and industrial scales worldwide without any technical barriers. This study reviews a large number of technologies for H₂ production (16 technologies), CO₂ capture (7 technologies), their performance data, and the costs. Further, this study reviews the processes, including reactions, catalysts, and costs, to produce two liquid e-fuels (e-methanol and e-kerosene) that can be used as carbon-neutral alternatives to their fossil fuel-based conventional counterparts. The current and future projects for commercial production of liquid e-methanol and e-kerosene are also reviewed. Finally, the outlook and challenges to produce liquid e-fuels are discussed along with recommendations.

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1 Introduction

For reaching net-zero by 2050, global H₂ production needs to grow 80–95% per annum from the current H₂ production of ~120 MM tonnes per annum (tpa) according to the “Mission Possible” report.¹ As per the global carbon-neutral goal by 2050 and sustainable development scenario (SDS), carbon capture, utilization, and storage (CCUS) capacity worldwide must increase from 40 MM tpa in 2020 to 800 MM tpa by 2030.² According to the IEA^{2,3} the net-zero emission goal is virtually impossible to achieve without CCUS. The countries in Asia

Pacific, the world's most populous and fastest-growing region economically, emit about half of the global greenhouse gas (GHG) emissions. The energy demand in Asia Pacific over the next two decades is expected to be almost two-thirds of the global energy demand growth, and a large part of that demand will be likely met by hydrocarbons. Demand for some key fossil fuel-based hydrocarbons can be met by carbon-neutral liquid e-fuels produced using H₂ and captured CO₂ to a reasonable degree in the medium-term, whereas e-fuels will completely substitute fossil fuels in some key industries (e.g., aviation) by 2050.

There is wide interest in H₂ as a fuel in the mobility (FCEVs, HICE), power generation (gas turbines or fuel cell power plants),

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and other industries (steel, chemical, heat, etc.) according to the routes listed in Fig. 1. Among these different options where H₂



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Fig. 1 A list of available routes to integrate hydrogen in various sectors of the economy, including power, gas, mobility, and industry.

can be integrated within the economy, the primary demand growth drivers of H₂ are expected to be transportation and industrial uses. In contrast, the use of hydrogen as a fuel for power generation (electric and gas utilities) is unlikely to be its growth driver because of high production costs and efficiency losses which make H₂ too expensive in power generation,⁴ however, despite the cost disadvantage, the motivation for using H₂ in power generation at present is primarily to meet decarbonization



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Fig. 2 Utilization of CO₂ as a valuable commodity in various sectors of the economy, including new pathways, such as fuels and chemicals.

goals, increasing interest in renewable energy and energy storage. The growing potential of hydrogen in the power sector will require lower costs, refurbishing existing coal and gas power plants that enable burning H₂-rich fuels, and creation of markets and hubs. Similarly, global consumption of CO₂ in 2019 was estimated to be 230 MM tpa⁵ (with ~57% in urea and 34% in EOR) for applications shown in Fig. 2, and it is expected to grow to 272 MM tpa by 2025. Unlike H₂, the price of CO₂ varies significantly based on the region and the industry, such that the price of CO₂ can range from \$3 to >\$400 per ton and its supply is closely related to ammonia and fertilizer manufacturing.⁵

Although H₂ can be integrated into various sectors of the economy through power, gas, mobility, and industry based on the routes listed in Fig. 1, it needs H₂-compatible midstream and downstream infrastructure that remains uncertain to predict in terms of its development and timeline. The diverse applications of H₂ would require the deployment of large-scale infrastructure, but despite the potential economic and environmental prospects from these applications, securing investment for midstream and downstream infrastructure that typically involves a wide number of stakeholders is challenging due to the lack of a clear business model.

With the challenge mentioned above in securing investment for H₂-compatible infrastructure, the most realistic application for large-scale utilization of H₂ in the near- to mid-term is to produce liquid electro-fuels (e-fuels) derived from H₂ and captured CO₂ (e.g., carbon-neutral synthetic methanol and kerosene) because of the following unique advantages of liquid e-fuels:

- Compatible with existing infrastructure for storage and transportation of liquid fossil fuels.
- Compatible with existing internal combustion engines (ICE) in aviation, shipping, freight, *etc.*, without requiring any modification to the engine or other equipment.
- Synthetic kerosene is low in sulfur and can also be mixed with conventional kerosene produced using fossil fuel.

- Having an existing market with huge demand and carbon-neutral liquid e-fuels are the only realistic options in the near- to mid-term in reducing carbon emissions at scale from road, maritime, and aviation transport.

Carbon-neutral e-methanol and e-kerosene are the two most important fuels that can be produced using captured CO₂ and H₂. More than 95 billion liters of methanol (~98 MM tpa) is manufactured every year, making it the world's most commonly shipped chemical commodity.⁶ Methanol is a highly versatile chemical that is widely used in various applications, for instance, as a transportation fuel and as a feedstock to produce various chemicals/products. Further, the need for a high-energy-density liquid fuel in aviation is provided by kerosene, and its combustion is responsible for ~98% of emission in the aviation sector. The aviation sector is difficult to decarbonize because of its need for high energy-density liquid fuels like kerosene, which cannot be easily replaced in the coming decades. Currently, long-haul operational aircraft engines cannot operate on electricity or H₂; therefore, the concept of sustainable aviation fuel (SAF) is the only option to decarbonize aviation, which is enabled by a low-carbon kerosene (e-kerosene) produced using H₂ and captured CO₂. It is estimated⁷ that 65% of carbon mitigation to achieve net-zero in the aviation sector by 2050 will be contributed by SAF. For this reason, SAF annual production is expected to increase⁷ from the current 125 million liters to 5 billion by 2025 and potentially 30 billion liters by 2030. In the U.S., SAF production is expected to reach at least 3 billion gallons per year by 2030 which will reduce the emissions in aviation by 20%. For net-zero in aviation by 2050, the share of SAFs in jet fuel demand is expected to grow from 0% in 2019 to ~15% by 2030, 60–65% by 2040, and 100% by 2050.

The rest of the paper is organized as follows: Section 2.1 discusses the pathway to produce liquid e-fuels using H₂ and captured CO₂, including the status of H₂ production and CO₂ capture technologies. Sections 2.2 and 2.3 review the technologies to produce H₂ and capture CO₂, including their performance data and costs. Section 2.4 reviews the technologies required to produce e-methanol and SAF, including the processes, reactions, catalysts, and costs. Sections 3.1 and 3.2 review the current and future projects for commercial production of e-methanol and SAF. The final section discusses the outlook and challenges in producing liquid e-fuels along with recommendations.

2 Method and technologies

2.1 Pathways and summary of technology readiness

Although H₂ can be used as a fuel directly, the infrastructure required to support large-scale application of H₂ does not yet exist. Therefore, liquid electro-fuels (e-fuels) derived from H₂ and captured CO₂ are attractive for multiple reasons, which include (i) being easier to store than gaseous or liquid H₂, (ii) being able to be transported using existing petroleum infrastructure, and (iv) being compatible in aviation, shipping, freight, *etc.*, without any modification to engines or equipment.





Fig. 3 A schematic illustrating the use of oil and gas resources to produce carbon-neutral liquid e-fuels. Hydrogen can be processed with captured CO₂ to produce carbon-neutral liquid e-fuels (e.g., e-methanol, e-kerosene) which (i) are compatible with existing engines, (ii) are easier to store, and (iii) can be transported using existing petroleum infrastructure.

Fig. 3 shows a summarized overview of strategies to integrate H₂ production and low-carbon e-fuels derived from H₂ through existing oil and gas resources and infrastructure. Specifically, H₂ can be produced either from fossil fuels directly or through electrolysis that runs on electricity provided by geothermal reservoirs. Hydrogen can either be used directly for its various applications listed in Fig. 1, or further processed with captured CO₂ and converted to e-methanol and/or e-kerosene.

A summary of all major and novel state-of-the-art H₂ production and CO₂ capture technologies in terms of the technology readiness level (TRL) (minimum of 1 indicating the basic principles observed and maximum of 9 indicating the actual system proven in the operational environment) is presented in Table 1. The technologies listed in Table 1 for H₂ production and CO₂ capture are discussed in detail in the following sections, including their performance data and costs.

2.2 Hydrogen production

2.2.1 Comparison of technologies. Hydrogen production technologies that are expected to play an important role in producing large-scale H₂ in short- to long-term, along with their advantages, disadvantages, TRL, and range of cost, are presented in Table 2. The production of H₂ is categorized into 4 categories, which are H₂ produced from fossil fuel, from biomass and waste-stream, from electrolysis of water, and from natural free-state occurrence. Hydrogen can be produced from fossil fuels using seven methods,^{8–16,18,19} which are coal gasification, steam reforming (or popularly known as steam methane reforming when methane is used as a feedstock), plasma reforming, partial oxidation (POX), auto-thermal reforming (ATR), pyrolysis of methane, and *in situ* combustion of underground reservoirs. Hydrogen can also be produced from biomass and waste-stream^{20,21} using the three technologies discussed here, which are dark fermentation, photofermentation,

and gasification. The third category of H₂ production is by electrolysis of water,^{8–13,30,31} which refers to splitting water into H₂ and oxygen molecules using electricity, and within this category three technologies are discussed, which are alkaline electrolyzers, solid oxide electrolyzers, and polymer electrolyte membranes (PEM), respectively. Finally, the last category of H₂ production through its natural occurrence in geological media^{22–29} is considered to be the least known, but it offers the potential to produce large-scale H₂ most economically among all methods.

2.2.2.1 SMR with membrane reactors. Although H₂ production through SMR is mostly through conventional reactors, membrane reactors have the potential to improve energy efficiency and conversion efficiency, and reduce costs (relaxed operating conditions) through process intensification measures like (i) membrane reactors that combine multiple processes into a single unit (e.g., reaction and purification) and (ii) low-carbon sources of heat and energy (e.g., microwave heating, plasma, etc.). The SMR performance data with different membrane reactors and their operating conditions is presented in Table 3.

2.2.2.2 Electrolysis

2.2.2.2.1 Electricity consumption. Solid oxide electrolyzers are technically less mature, but they offer the highest efficiency among all types by combining heat and electricity to produce H₂. The comparison of three main technologies for electrolysis of water in terms of their performance as a function of current-voltage (electricity consumption) data is presented in Fig. 4, which shows that solid oxide electrolyzers consume the least amount of electricity, while alkaline electrolyzers consume the most electricity.

2.2.2.2.2 Startup time. Of these three different types of electrolyzers, alkaline electrolyzers are technically the most



Table 1 Status of H₂ production and CO₂ capture technologies^{8–39} in terms of their technology readiness level (TRL)

| TRL (# and description) | H ₂ production technologies | CO ₂ capture technologies |
|---|---|---|
| 1 Basic principles observed | <ul style="list-style-type: none"> • Natural free-state geological occurrence | |
| 2 Technology concept formulated | | |
| 3 Experimental proof-of-concept | <ul style="list-style-type: none"> • Photoelectrochemical water-splitting | <ul style="list-style-type: none"> • Post-combustion ionic liquids • BECCS power • Pre-combustion low-T separation • Dense inorganic membranes • Hydrate-based capture |
| 4 Technology validated in lab | <ul style="list-style-type: none"> • Thermochemical water-splitting | |
| 5 Technology validated in the industrial environment | <ul style="list-style-type: none"> • Pyrolysis of methane • <i>In situ</i> combustion of hydrocarbon reservoirs • Dark fermentation of biomass • Photofermentation of biomass • Solid-oxide electrolysis water-splitting • Plasma reforming | <ul style="list-style-type: none"> • Dense inorganic membranes (H₂ separation for reformer) |
| 6 Technology demonstrated in the industrial environment | <ul style="list-style-type: none"> • Gasification of biomass | <ul style="list-style-type: none"> • Polymeric membranes (power plants and NG processing) • Post-combustion biphasic solvents • CLC • CaL • Polymeric membranes (NG industry) • Pre-combustion IGCC + CCS • Oxy-combustion coal power plant • Post-combustion adsorption • BECCS industry • DAC (adsorbents and absorbents) • Cryogenic (solid CO₂) • Fuel cell capture • Oxy-combustion gas turbine • Pre-combustion PSA with cryogenic (liquid CO₂) |
| 7 System prototype demonstrated in the operational environment | | <ul style="list-style-type: none"> • Post-combustion amines (power plants) • Pre-combustion NG processing (gas sweetening) |
| 8 System complete and qualified | <ul style="list-style-type: none"> • Proton exchange membrane electrolysis water-splitting | |
| 9 Actual system proven in the operational environment | <ul style="list-style-type: none"> • Coal gasification • Steam reforming • Partial oxidation • Auto-thermal reforming • Alkaline electrolysis water-splitting | |

BECCS: bioenergy with carbon capture and storage. NG: natural gas. CLC: chemical looping capture. CaL: calcium carbonate looping. IGCC: integrated coal gasification combined cycle. PSA: pressure swing adsorption. DAC: direct air capture.

mature, but they have several limitations when working with intermittent renewable energy sources. PEM electrolyzers overcome some of the limitations of alkaline electrolyzers, including (i) integration with fluctuating renewable energy power systems and (ii) a faster response time, as shown in Fig. 5.⁵⁰ Most commercially-available PEM electrolyzers have input power limits of 5 MW and 10 MW as single units (also called stacks; a module is a combination of several stacks; a system is a combination of multiple modules), but these stacks can be grouped to form a bigger unit with a higher power limit.

2.2.2.2.3 Efficiency versus system size. According to the survey of commercially-available alkaline (from Pure Energy, McPhy, Hydrogenics, and IHT) and PEM (from Nel, ITM, Hydrogenics, and Areva) electrolyzers for a range of system sizes (0.1 kW to 100 MW),⁵¹ it was found that gains in efficiency with the increase in system size reaches a plateau around 100–300 kW size for both types (alkaline and PEM) of electrolyzers, as shown in Fig. 6; the reason for the plateau in efficiency is likely due to modular stacks above a certain scale.⁵¹ The highest efficiency (or lowest power consumption) for alkaline and PEM electrolyzers is ~ 50 kW h kg⁻¹ and ~ 55 kW h kg⁻¹, respectively.

2.3 CO₂ capture

2.3.1 Comparison of technologies. There are 7 major carbon capture technologies, which are listed in Table 4. The two most popular capture technologies are post-combustion and gas sweetening, primarily due to a large number of industrial applications in which CO₂ is separated using these two technologies; power plants use post-combustion to capture CO₂ from the flue gas through regenerative solvents, while natural gas processing facilities capture CO₂ through the gas sweetening process.

2.3.2 Technology performance data. Table 5 shows the empirical data^{66,67} reported by the EDGAR (Energy Delta Gas Research) CO₂ purity project, which present the levels of impurities in captured CO₂ stream from different capture technologies. Table 5 demonstrates that post-combustion (amine solvent-based CO₂ absorption) provides the highest level of purity in captured CO₂, but with a large variation in the levels of impurities.

The minimum energy required (as estimated from the combined first and second laws of thermodynamics) to capture CO₂ (with a known starting CO₂ concentration) increases sharply with a slope of ~ -11 kJ mol_{CO₂}⁻¹ for CO₂ concentration lying between 0.4 and 0.05, and with a slope of ~ -220 kJ mol_{CO₂}⁻¹ for CO₂ concentration below 0.05 in the



gas mixture.⁶⁸ Specifically, capturing CO₂ from the most concentrated source, such as fuel gas from coal gasification, flue gas from coal and natural gas oxidation, *etc.*, requires relatively less energy between 1 and 4 kJ mol_{CO₂}⁻¹, compared to capturing CO₂ from air using DAC (with ~0.04% or 409 ppm CO₂ concentration), which requires between 19 and 21 kJ mol_{CO₂}⁻¹.

Table 2 Summary of technologies for production of hydrogen^{8–38} at a medium to large scale. Each technology is color-coded to depict the greenhouse gas emissions associated with the produced H₂, where grayish blue represents the technology with the largest amount of emissions and dark green represents the technologies with the least amount of emissions. 2.2.2 Technology performance data

| Class | Technology | Description | Advantages | Disadvantages | TRL (max. 9) | Cost [\$ per kg H ₂] |
|-------------------------------|---|--|--|--|--------------------|------------------------------------|
| From fossil fuels | Coal gasification | Steam and oxygen are used for combustion and reacted with coal | Simpler emission control over conventional combustion | Produces CO ₂ and other pollutants | 9 (6–7 with CCS) | 1.34 (without CCS)–1.63 (with CCS) |
| | Steam reforming (SR) | The steam created by combustion with air is reacted with the feedstock and catalyst. Endothermic | Mature technology and easier to scale up | Produces CO ₂ | 9 (7–8 with CCS) | 2.08 (without CCS)–2.27 (with CCS) |
| | Plasma reforming | Similar to SR, but uses high temperature electric heat from plasma devices instead of steam | Does not require a catalyst. Reduced reactor size and weight | High electricity requirements. Produces CO ₂ | 5–6 | <2.08 |
| | Partial oxidation (POX) | Steam created by combustion with partial use of oxygen. No catalyst used. Exothermic | Faster start-up times and relative compactness. No catalyst required | Produces CO ₂ | 9 | 1.48 (with CCS) |
| | Auto-thermal reforming (ATR) | Combination of steam reforming and partial oxidation | Faster response times. Simpler and cheaper than SR. Compact design relative to other fossil fuel-based methods | Produces CO ₂ . Requires pure oxygen or air separation unit. Limited commercial experience | 9 (7–8 with CCS) | 1.48 (with CCS) |
| | Pyrolysis of methane | Uses a catalyst to crack methane at high temperature in the absence of oxygen | No CO ₂ emission. Produces solid carbon | Co-produces tar that can plug the reactor | 3–5 | 1.59–1.70 |
| | <i>In situ</i> combustion of hydrocarbon reservoirs | Steam/air/oxygen injection in fossil fuel-bearing reservoirs | Unwanted gases are not produced via downhole purification. Low-cost production | Complex <i>in situ</i> combustion that is difficult to control and predict | 3–5 | <2 |
| From biomass and waste-stream | Dark fermentation | Wet biomass. Uses anaerobic bacteria under dark conditions | Relatively simple technology. Waste recycling. CO ₂ -neutral process. | Low yield of H ₂ relative to reactor volume. | 4–5 (3–5 with CCS) | 2.57 |
| | Photo fermentation | Wet biomass. Uses anaerobic bacteria and light | Relatively simple technology. Waste recycling. CO ₂ -neutral process | Low yield of H ₂ relative to reactor volume | 4–5 (3–5 with CCS) | 2.83 |
| | Gasification | Dry biomass. Uses a controlled amount of oxygen and/or steam. No bacteria required. | Relatively simple technology. Waste recycling. CO ₂ -neutral process. | Pre-treatment cost. Fluctuating H ₂ yields because of feedstock impurities. Co-produces tar | 5–6 (3–5 with CCS) | 1.77–2.05 |



| Class | Technology | Description | Advantages | Disadvantages | TRL (max. 9) | Cost [\$ per kg H ₂] | |
|-------------------------------|------------------------------------|---|--|--|---|----------------------------------|---|
| From water-splitting | Thermochemical process | Produces H ₂ by splitting water through a series of high-temperature (800–900 °C) chemical reactions by using heat as the input energy. A single step conversion of water to H ₂ through direct thermolysis is possible, but not practical as it requires extremely high temperature (>2500 °C) | Suitable for large-scale production capacity that is larger than the scale of H ₂ refueling station. Can utilize sunlight and/or heat from nuclear waste | Requires additional H ₂ distribution network due to its large-scale production capacity. Commercial viability is currently challenging | 2–4 | 3.70 | |
| | Photoelectrochemical (PEC) process | Produces H ₂ by splitting water through semiconductor immersed in a water-based electrolyte that uses visible light as the input energy | Low operating temperatures and cost-effective materials (thin-film, particle semiconductor). Can utilize an unlimited source of solar light | Very low solar-to-H ₂ conversion efficiency (< 3%). Low current density due to reduced area of electrolysis in solar cell | 2–3 | 5.70 | |
| | Electrolysis | Alkaline | Electrolysis process converts water directly into H ₂ and oxygen (without any partial reactions with other chemicals/compounds) by using electricity as an input energy. Primary electrolysis components consist of an anode and a cathode separated by an electrolyte. | Mature technology. The first water splitting technology to be developed. Relatively low cost | Corrosive liquid electrolyte. Perform poorly with fluctuating power sources, because of a slow response (startup) time. | 9 | 2.30 (with \$0.037 per kWh as the electricity cost) |
| | | Solid-oxide | | Can leverage both heat and electrical energy | Require high temperature (>700–800 °C). Slower start-up time | 5 | 2.30 (with \$0.037 per kWh as electricity cost) |
| | | Polymer electrolyte [or proton exchange] membrane (PEM) | | Can operate at high current densities. Perform better with fluctuating input currents. Integrate better with variable power generation, such as wind and solar. Faster response time | Expensive materials that add to the cost. Scale-up to the MW scale is a challenge. | 6–8 | 2.30 (with \$0.037 per kWh as electricity cost) |
| Natural free-state occurrence | | Naturally occurring free-state H ₂ found in geological media. | Can be extracted using existing oil and gas drilling technology. | Its geology of occurrence is not well-understood. | 1 | Most economical | |

2.3.3 Cost of capture. The CCUS technology is about ~15 years old. However, the costs related to capture technology, which can be up to 40% of the entire project, can vary significantly due to the nature of the capture technology that is still evolving. The cost of capture varies by industry, from \$15 per ton to \$342 per ton, depending on the concentration of the emitted CO₂ in the flue stream⁶⁹ as shown in Fig. 7, which indicates that a higher concentration of CO₂ (red colored legend) leads to a lower capture cost. Most of the CO₂ emissions in the oil and gas industry are highly concentrated, such as in

natural gas processing, chemicals, and H₂ production by steam methane reforming.

The capture costs are the largest in the CCUS value chain, followed by the costs for compression and dehydration of CO₂, and then the cost of transporting CO₂, typically by pipelines.⁷⁰ The lowest costs in the CCUS are for the injection and MMV of stored CO₂, which is typically less than 10% of the total cost.

2.3.4 Capture technologies adopted by the oil and gas companies. Few oil and gas companies have chosen the capture technologies either for their own operations or as a service,



Table 3 SMR performance data with membrane reactors

| Membrane ↓ | Thickness (μm) | Area (cm ²) | T (K) | ΔP (kPa) | H ₂ permeance (mol m ² S ⁻¹ Pa ^{-0.5}) | H ₂ /N ₂ selectivity | Catalyst | GHSV (h ⁻¹) | S/C ratio | Sweep (mol h ⁻¹) | CH ₄ conversion (%) | Source |
|-----------------------------------|----------------|-------------------------|-------|----------|---|--|----------|-------------------------|-----------|------------------------------|--------------------------------|--------|
| Pd–Ru/PSS | 100 | 1.2 | 773 | 100 | 1.10 × 10 ⁻⁴ | ND | Ni | 30 | 3 | 0.4 | 80 | 40 |
| Pd/PSS | 11 | 20 | 800 | 100 | 1.10 × 10 ⁻³ | ND | Ni | 1120 | 3 | 1.3 | 82 | 41 |
| Pd/A ₁₂ O ₃ | 3.8 | 155 | 823 | 2500 | 3.70 × 10 ⁻³ | 97 | Ni | 150 | 3 | 0.13 | 91 | 42 |
| Pd-Alloy/PCS ^a | 7.3 | 93.3 | 823 | 800 | 2.20 × 10 ⁻³ | ND | Ni | 3000 | 3 | None | 68 | 43 |
| Pd | 11 | 35.8 | 873 | 1600 | 1.70 × 10 ⁻³ | 3000 | Ni | 600 | 3 | None | 37 | 44 |
| Pd–Ru/PSS ^b | 5 | 13.3 | 853 | 2900 | 2.70 × 10 ⁻³ | 200 | Ni | 150 | 3 | None | 85 | 45 |
| Pd–Au/PSS | 5 | 16.1 | 784 | 2800 | 2.40 × 10 ⁻³ | 6400 | Ru | 147 | 3 | None | 94 | 46 |
| Pd-Based | 13 | 44 | 673 | 300 | 3.80 × 10 ⁻³ | 9000 | Ni | 2600 | 3.5 | 1.36 | 84 | 47 |
| Pd–Ru/PSS | 6 | 100 | 773 | 253 | 3.50 × 10 ⁻³ | 59 | Ni | 837 | 3 | None | 77.5 | 48 |
| Pd-Based/PSS | 4–5 | 175 | 823 | 1013 | 2.40 × 10 ⁻³ | 618 | Ru | 2000 | 3 | None | 82 | 49 |

ND: no data. GHSV: gas hourly space velocity. S/C: steam-to-carbon. ^a Porous ceramic support. ^b Porous stainless-steel support.



Fig. 4 Comparison of alkaline, PEM, and solid oxide electrolyzer cell (SOEC) technologies for electrolysis of water as a function of electricity consumption (current and voltage).⁵¹ The indicative temperatures and pressures for each technology are a general representative of their operating conditions.

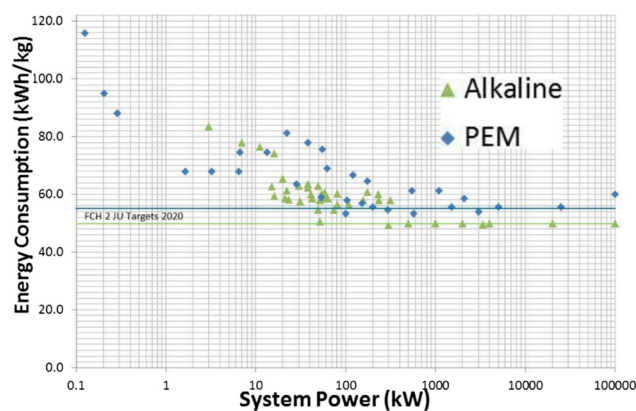


Fig. 6 Electrolysis energy consumption (indicator of efficiency) versus system size of the alkaline (from Pure Energy, McPhy, Hydrogenics, and IHT) and PEM (from Nel, ITM, Hydrogenics, and Areva) electrolyzers for a range of commercially available electrolyzers.⁵¹

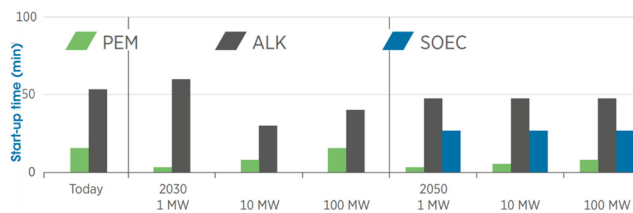


Fig. 5 Comparison of start-up times for PEM, alkaline (ALK), and solid oxide electrolyzer cell (SOEC) technologies.⁵⁰

where some of the notable companies are Oxy, Shell, Baker Hughes, and ExxonMobil.

Oxy is deploying the world's largest direct air capture (DAC) facility in the Permian Basin (referred to as DAC-1) to use captured CO₂ for enhanced oil recovery (EOR), which is currently in the front-end engineering and design phase and expected to be online by early 2024.⁷¹ The DAC-1 facility will extract up to 1 MM tpa of CO₂ (at a cost of ~\$500 MM) with >99% purity from air, which is equivalent to the annual emissions of about 215 000 cars. Additionally, Oxy is planning to build 70 DAC facilities by 2035, each with up to 1 MM tpa

capture capacity, where the oil produced using this captured CO₂ through EOR will be marketed as net-zero oil. Oxy signed its first contract to supply 200 000 bbl per year of net-zero oil (produced using CO₂ captured from DAC facilities) for 5 years to SK Trading International, based in Seoul, South Korea.⁷²

Shell has been testing various capture technologies in collaboration with other partners in Europe, and it has now decided to use solid sorbents in place of liquid solvents while moving from demonstration-scale to large-scale operations. Shell plans to scale solid adsorbent technology from current 1 tpd to 150 tpd by 2024 with an eventual target of 1000–2000 tpd commercial plants.⁷³ Shell's solid adsorbent technology can separate over 90% of the CO₂ from post-combustion flue gases with 95% purity, and it is reported to be 40% cheaper than liquid amine technology.

Baker Hughes has three carbon capture technologies,⁷⁴ which are (i) chilled ammonia process (CAP), (ii) mixed salt process (MSP), and (iii) compact carbon capture (CCC). Of these three technologies, CAP is a post-combustion technology (with a TRL of 7) based on a non-proprietary solvent formulation that uses readily available ammonia to capture CO₂ from low-pressure flue gases generated by point-sources of emissions, such as fossil-fuel-based power plants, waste-to-energy



Table 4 Carbon capture technologies, the output, major industrial applications, and the CO₂ capturing medium^{39,52–65}

| Characteristics ↓ | Post-combustion | | | | | | |
|------------------------------------|---|---|---|--|---|--|--|
| | Pre-combustion | Traditional method | Specialized methods | | | Fuel cells | DAC |
| | | | Cryogenic | Oxyfuel combustion | Chemical looping | | |
| Source of CO ₂ emission | Syngas coming from gasification units prior to combustion | Flue gas due to combustion with air and fuel | Flue gas due to combustion with air and fuel | Flue gas due to combustion with oxygen and fuel. O ₂ is supplied externally from an air separation unit | Flue gas due to combustion with oxygen and fuel. O ₂ is extracted internally from the solid-state oxygen carrier through reduction–oxidation reactions | Flue gas due to combustion with air (and/or oxygen) and fuel | Air. No combustion |
| Capture mechanism | Sorption with pressure and/or temperature swing | Sorption with pressure and/or temperature swing | Direct phase change from gas to liquid/solid | Sorption with pressure and/or temperature swing | Sorption with pressure and/or temperature swing | FCs pump CO ₂ through the electrolyte to separate CO ₂ via selective ionic transport | Membrane separation and/or sorption |
| CO ₂ capturing agents | Solvents and membranes | Solvents, membranes, and adsorbents | Cryogenic cooling with liquid solvents | Solvents and membranes | Solvents and membranes | Electrochemical system | Adsorbents and membranes |
| Outputs | CO ₂ and H ₂ | CO ₂ and N ₂ | CO ₂ , N ₂ , SO _x , NO _x , and Hg | CO ₂ and steam | CO ₂ and O ₂ | CO ₂ , water, and some H ₂ | CO ₂ and air |
| Advantages | High capture efficiency | Most mature technology | A high concentration of CO ₂ is captured | Leads to a high concentration of CO ₂ in flue stream, which is easier to capture | Cost-effective option to oxy-combustion, but with similar benefits | Very high capture efficiency. Cheaper. Can also utilize CO ₂ as the working fluid | Can capture CO ₂ anywhere on the earth without the need for point-source emission |
| Disadvantages | Less mature technology | Lower capture efficiency | Relatively high CAPEX | Relatively high CAPEX | Less mature technology | Less mature technology | Relatively high CAPEX |
| Major industrial sectors | Power and industrial gases | Power and cement | Power and cement | Power and steel | Power and steel | Power and industrial gases | Greenhouse and carbonated beverages |



Table 5 Carbon capture technologies and the corresponding level of impurities in the captured CO₂ stream. Adapted and expanded after ref. 66 and 67

| Capture technologies | Pre-combustion | | | | Post-combustion | | | DAC | | Oxyfuel combustion | |
|----------------------|---------------------------------|----------------|--|--|---|------------|------------|----------|-----------------------------|--------------------|--|
| | Selexol IGCC | Reactisol IGCC | Amine scrubbing | Sour SEWGS | Amine scrubbing | Adsorption | Absorption | Membrane | Oxyfuel and double flashing | | |
| CO ₂ | 98.1–99.7% | 95–98.5% | >97.2% | >99% | 99.8–99.9% | 30–90% | 90–99% | 2.5–20% | 97% | | |
| H ₂ | 1.50% | 20 ppm | <1% | <1% | — | — | — | — | — | | |
| O ₂ | — | <1% | <1% | — | 150–300 ppm | — | — | — | 1.20% | | |
| N ₂ | 195 ppm | <1% | <1% | <1% | 450–900 ppm (inc. Ar) | — | — | — | 1.60% | | |
| Ar | 178 ppm | 150 ppm | <1% | <1% | 450–900 ppm (inc. N ₂) | — | — | — | 0.40% | | |
| Sulfur compounds | 2 < H ₂ S < 1700 ppm | 0.2–20 ppm | H ₂ S < 200 ppm for the 2-stage plant | <5000 ppm to ppm level with H ₂ S stage | 10–20 ppm (SO ₂ predominantly) | — | — | — | 35 ppm SO ₂ | | |
| NOx | — | — | <1% | — | 20–40 ppm | — | — | — | 150 ppm | | |
| CO | 100–1300 ppm | 400 ppm | <1% | <1% | 10–20 ppm | — | — | — | — | | |
| CH ₄ | 112 ppm | 100 ppm | <1% | <1% | — | — | — | — | — | | |
| MeOH | — | 20–200 ppm | — | — | — | — | — | — | — | | |
| H ₂ O | 376 ppm | 0.1–10 ppm | 1.80% | 500 ppm (drying step) | 100–600 ppm | — | — | — | — | | |

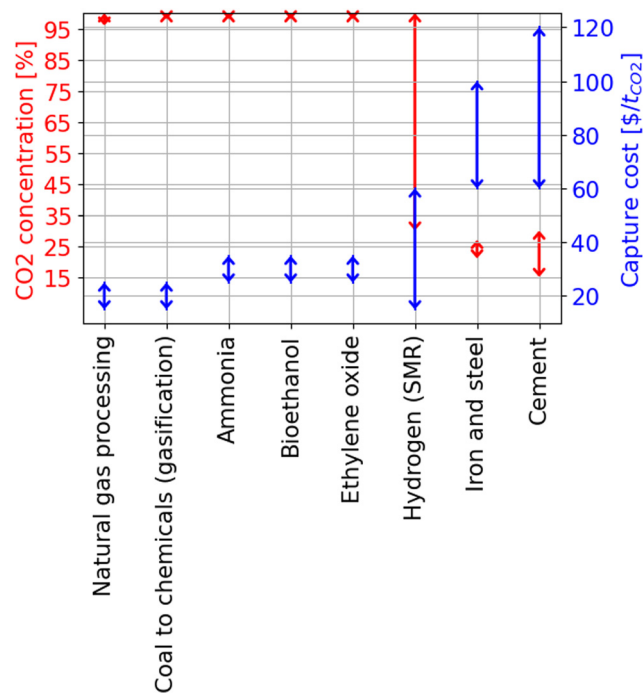


Fig. 7 Range of CO₂ concentration in % (red colored legend) and the corresponding carbon capture costs in \$ per ton of CO₂ captured (blue colored legend) for specific industrial applications. The figure was created using the data from ref. 5.

power plants, biomass power plants, cement plants, refineries, and petrochemical complexes. The MSP capture technology (acquired from SRI International) is a post-combustion technology that uses a non-amine solvent (widely available and environmentally friendly) formulation based on commodity chemicals with reduced energy consumption and greater efficiency in the form of negligible solvent-degradation and reduced water use. Baker Hughes' CCC technology (acquired from 3C) uses solvent-based rotating packed beds. Solved-based rotating packed beds are compact (75% smaller and 50% cheaper than conventional amine capture), modular (easy installation and retrofittable), and solvent-agnostic. The capture capacity of Baker Hughes' CCC technology is 250–500 tpd of CO₂ with >99% purity.

ExxonMobil has invested in Global Thermostat (a U.S.-based DAC company founded in 2010) and using its technology to deploy DAC at Haru Oni Project (Punta Arenas, Chile), which is an e-methanol (renewable methanol) plant anticipated to be completed by mid-2022.⁷⁵

2.4 Liquid e-fuel production

Catalytic CO₂ reduction to produce high-value fuels is a major pursuit towards sustainable production of carbon-neutral fuels to reduce atmospheric carbon emissions. The low-carbon fuels possible to be produced by reacting CO₂ with H₂ can range from as simple as methane, ethane (precursor to ethylene, which is used to make plastics), and propane (for heating and cooking), to other commercially high-value liquid e-fuels that include methanol and SAF (synthetic jet fuel).

Conversion of CO₂ to liquid e-fuels can be through either a one-step or a two-step process, depending on the efficacy of the catalyst, which is a key ingredient in the process that seeks to activate chemical reactions without being consumed itself in the process. A one-step process converts CO₂ directly to liquid fuels, whereas the two-step process converts CO₂/H₂ to CO/H₂O in the first reaction (called reverse water gas shift), followed by the second reaction that combines CO with H₂ to form the liquid fuel. The majority of catalysts that enable conversion of CO₂ to liquid fuels have limitations in terms of either the efficiency of conversion to liquids (selectivity) and/or the rate of formation of liquids. Besides the reactor design that can facilitate optimum operating conditions for the reactions, appropriate catalyst selection is key to the performance of the process to convert CO₂/H₂ to high-value liquid e-fuels. The technologies involved in producing e-methanol and SAF, including the process, reactions, and catalysts, are discussed in the following sections.

2.4.1 e-Methanol production

2.4.1.1 Process. Although almost all the methanol is conventionally produced *via* syngas where the CO and H₂ in the syngas react in an exothermic reaction to form methanol, methanol can also be produced renewably by direct hydrogenation of the captured CO₂ (Fig. 8) according to eqn (1) (direct hydrogenation) and (2) (reverse water gas shift).⁷⁶ The two reactants (H₂ and CO₂) are pressurized/compressed (~25 bar) before feeding them into the first reactor which operates at high temperature and high pressure⁷⁷ in case the initial pressures of the supplied CO₂ and H₂ are lower than the operating pressure of the synthesis reactor. The unused reactants following the methanol production, which are separated at the exit stream through condensation, can be recycled *via* a compressor and fed back into the reactor in addition to the fresh reactants. The formation of methanol is an exothermic process that generates heat, which is supplied for the endothermic reaction in the first reactor (Fig. 9).

One key operational difference between the traditional and sustainable methanol production is the significant production of water in the exit stream in the case of sustainable methanol production (approximately 30–40% water by mass in crude

methanol), which reduces the activity and lifetime of the catalyst.⁷⁷

Some of the key factors that influence the methanol synthesis are as follows:

- The composition of the syngas feed (when the produced H₂ is not pure).
- The converter designs to remove the heat of the exothermic reaction, which includes gas-cooled and steam-raising variants (axial, radial, and axial–radial configurations).

The three commercially used designs of the methanol synthesis reactor in the market are based on different heat transfer mechanisms, which include⁷⁹ (i) quench converter (direct cool *via* feed gas injection), (ii) tube-cooled converter (counter-current gas exchange), and (iii) steam-raising converter (isothermal bed temperatures). Of these three reactor designs, the tube-cooled converter (TCC) design enables the largest methanol production and carbon efficiency (moles of methanol in crude methanol to moles of CO and CO₂ in syngas) per unit volume of the reactor, whereas the quench-type reactor system typically contains the largest catalyst volume.⁷⁹

2.4.1.1.1 H₂ and CO₂ utilization. Producing a kg of methanol requires 0.189 kg H₂ and 1.373 kg CO₂^{80,81} under a limited conversion rate, or more specifically, according to the process flow diagram in Fig. 9, producing a kg of methanol requires an estimated 0.20 kg H₂ and 1.66 kg CO₂⁷⁸ with BaCe_{0.2}Zr_{0.6}Y_{0.16}Zn_{0.04}O₃ and Cu/Zn/Al as the catalysts for the RWGS reaction and the methanol synthesis, respectively. Few other studies^{82–84} mention the net CO₂ utilization for e-methanol synthesis as 1.4t CO₂ per 1t of e-methanol (or equivalently, a kg of methanol requires 1.4 kg of CO₂), which is close to the other two numbers (1.373 kg CO₂^{80,81} and 1.66 kg CO₂⁷⁸).

2.4.1.2 Reactions. The synthesis of methanol through direct hydrogenation of CO₂ (eqn (1)) is an exothermic reaction, but it competes with the reverse water gas shift (RWGS) reaction, which is an endothermic reaction.⁸⁵ The synthesis of methanol requires retaining an equilibrium, such that at high temperatures the yield of methanol begins to decrease⁷⁷ as shown in Fig. 10, which means that an increase in temperature facilitates CO₂ activation to undesirable CO and H₂O, and reduces its equilibrium conversion rate.

Conversion of CO₂ to e-methanol can be either a one-step or a two-step process, where a one-step process converts CO₂ directly to liquid fuels, whereas the two-step process converts CO₂/H₂ to CO/H₂O in the first reaction (*via* RWGS), followed by the second reaction that combines CO with H₂ to form e-methanol.

One-step process (direct CO₂ hydrogenation):

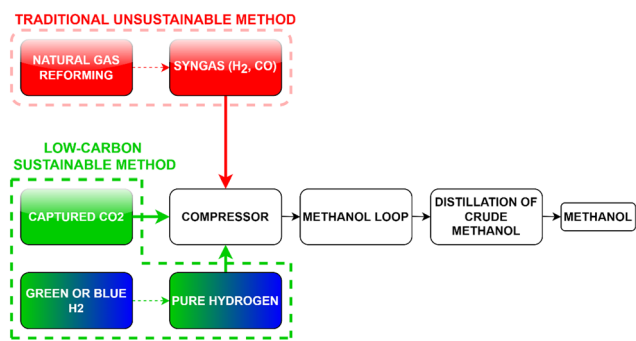


Fig. 8 Block diagram illustrating the traditional and renewable (pure H₂ with captured CO₂) methods of methanol production. Modified after ref. 76.





Fig. 9 Process flow diagram to produce e-methanol. From ref. 78.

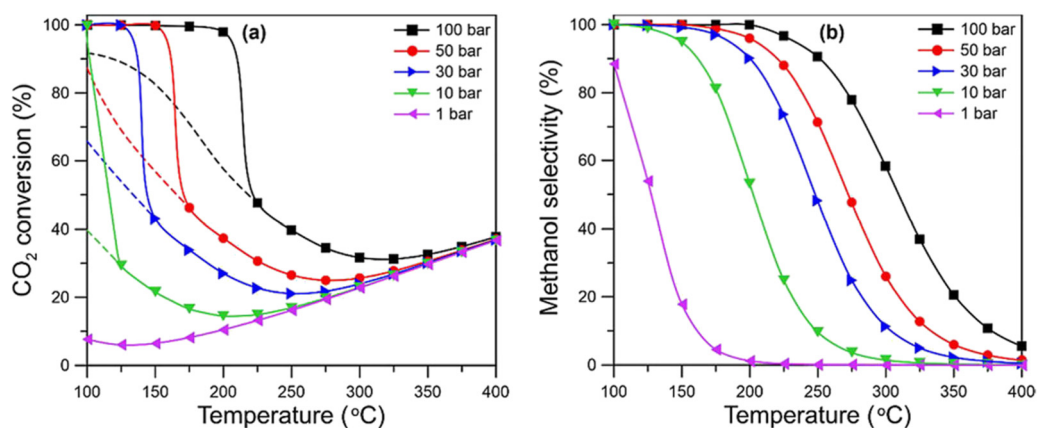
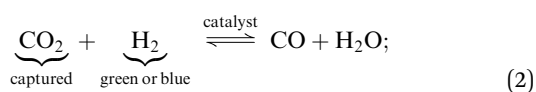


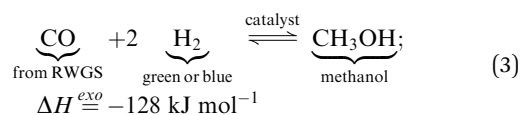
Fig. 10 Sensitivity of methanol synthesis (from CO_2 and H_2) as a function of pressure and temperature.^{77,86}

Two-step process:

RWGS (600 °C, 24.5 bar⁷⁸):



$$\Delta H \stackrel{\text{endo}}{=} 41.22 \text{ kJ mol}^{-1} [\sim 600 - 900 \text{ °C}]$$



2.4.1.3 Catalysts. CO_2 is an inert gas due to its low reactivity (a stable molecule with a large bond dissociation energy of 1072 kJ mol^{-1}), and therefore it requires an active metal

catalyst to promote its reaction with the H_2 to form methanol. An appropriate catalyst is important not only from the point of view of reaction performance, but also from an economic standpoint.⁸⁷ Traditionally, the catalysts that have been used for the synthesis of methanol are known to be found in abundance (*e.g.*, Cu, Zn, Al), but their tolerance to water is not robust, so significant water production in the synthesis of the e-methanol process reduces the activity (*e.g.*, through water adsorption, morphology changes, oxidation of the metal, *etc.*) and lifetime of the traditional catalysts.⁷⁷

For e-methanol synthesis, catalysts exhibiting higher stability and activity in the presence of water are required for CO_2 hydrogenation. Various catalysts have been studied for the synthesis of e-methanol *via* heterogeneous catalysis, which range from transition metals/metal oxides to main group metals/metal oxides, particularly Cu-based, precious-metal-based, and metal oxides from main group elements.⁸⁸ Fig. 11 compares



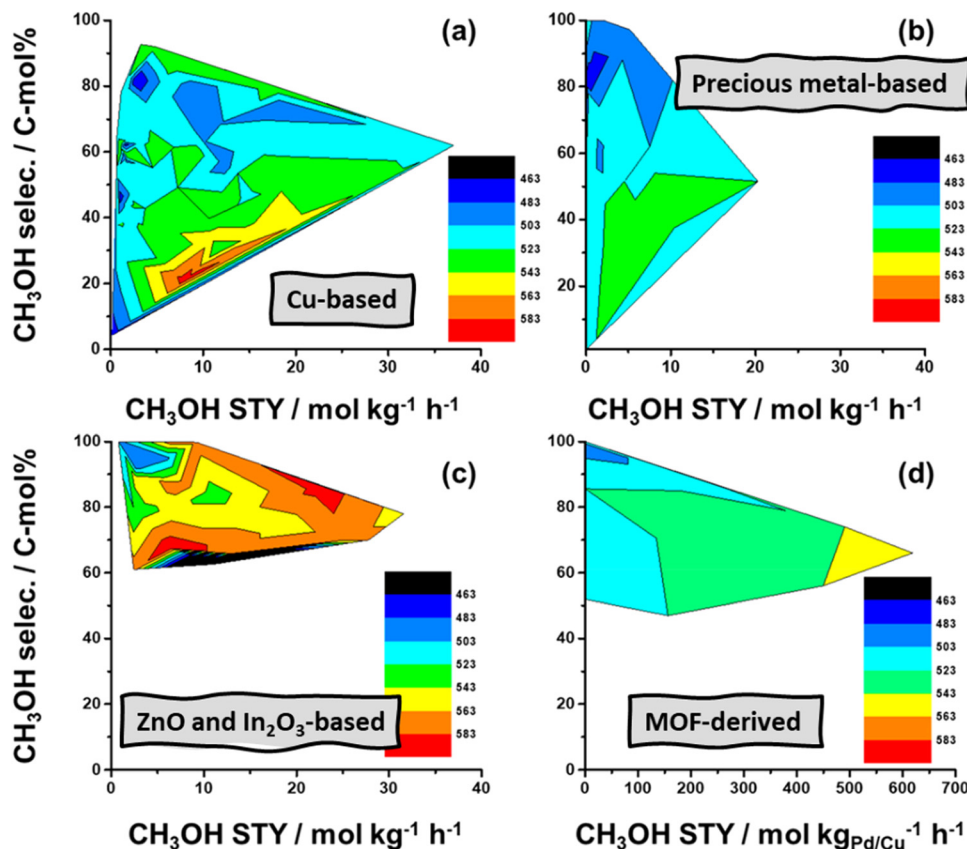


Fig. 11 Contour plots depicting catalytic performance in selectivity (conversion rate; in C-mol%) and space-time yield (STY; production rate; in $\text{mol kg}^{-1} \text{h}^{-1}$) domain versus the reaction temperature (in K; color legend). The e-methanol production rate with MOF/ZIF-derived catalysts is normalized on active metals. Adapted from ref. 88.

four types of catalysts *via* contour plots showing catalytic performance in selectivity (conversion rate; in C-mol%) and space-time yield (STY; production rate; in $\text{mol kg}^{-1} \text{h}^{-1}$) domain versus the reaction temperature (in K; color legend). Fig. 11 shows that Cu-based catalysts provide the largest production rate of e-methanol among all the catalysts (the rate with MOF/ZIF-derived catalysts is normalized on active metals). However, the selectivity of methanol decreases as the methanol production rate increases (*e.g.*, ~ 90 C-mol% to ~ 60 C-mol% for Cu-based catalysts). Although lower temperatures generally provide higher selectivity of methanol, it usually comes with a trade-off of lower production rates. Catalysts emerging recently, such as In_2O_3 - and ZnO -based and MOF/ZIF-derived, have generally provided relatively high selectivity to methanol than Cu-based catalysts even with similar production rates, but they require relatively high operational temperature which translates to more energy input.⁸⁸ The performance of some of the catalysts presented in Fig. 11 have also been tested at a recent demonstration-scale e-methanol plant (FRESMé), which show similar observations as shown in Fig. 12.

Ruthenium (Ru)-based catalysts have been used to convert CO_2 to CH_4 (*e.g.*, *via* the Sabatier methanation process) with a selectivity between 99 and 100% over a range of operating temperatures, from a low of 60°C to a high of $\sim 450^\circ\text{C}$.⁹⁰ Ru-based catalysts have been recently explored for their



Fig. 12 Performance of selected catalysts in terms of the rate of production versus the input energy in the FRESMé project.⁸⁹

potential in the synthesis of e-methanol from H_2/CO_2 and incorporating Ru with indium (In) has been shown to prevent methanation and instead produce methanol with $>85\%$ selectivity.⁹⁰ Other laboratory-scale advancements in preventing methanation include coating ruthenium with a thin layer of a porous plastic/polymer.^{91,92}

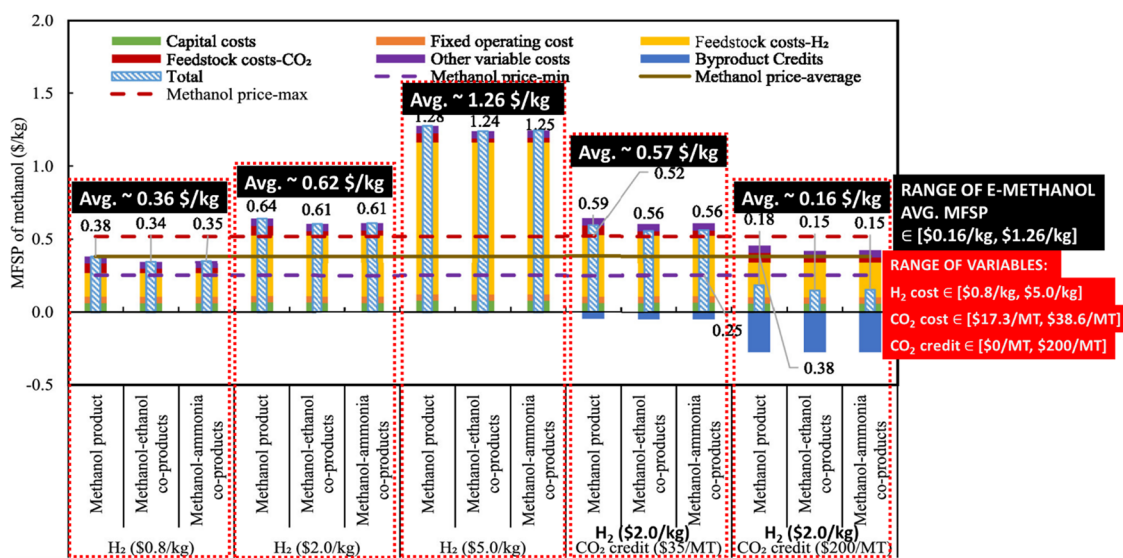
In the case of a two-step process for e-methanol production that also includes a high-temperature RWGS reactor (usually the case, as shown in Fig. 9), barium zirconate-based perovskite-type catalysts doped with Y, Zn, and Ce show stable performance;⁹³



particularly, $\text{BaCe}_{0.2}\text{Zr}_{0.6}\text{Y}_{0.16}\text{Zn}_{0.04}\text{O}_3$ has been used as a favorable candidate for the RWGS reaction according to recent studies.⁷⁸

2.4.1.4 Costs. The minimum fuel selling price (MFSP; a price at which the net present value is zero) of methanol varies based on the cost of H_2 production, the cost of CO_2 as a feedstock, and the credit of saved CO_2 as shown in Fig. 13a. Fig. 13a shows that the average MFSP of e-methanol, compared to an average of \$0.38 per kg as the market price over the 2015–2020 period, varies between \sim \$0.16 per kg and \sim \$1.26 per kg depending on the cost of H_2 production (\in [\$0.8 per kg, \$5.0 per kg] with the base price as \$2 per kg), the cost of CO_2 as a feedstock

(\in [\$17.3 per MT, \$38.6 per MT]), and the cost of saved carbon that can be traded (\in [\$0 per MT, \$200 per MT]) as a credit.⁷⁸ The feedstock costs of CO_2 assumed in Fig. 13a are \$17.3 per MT, \$20.6 per MT, and \$38.6 per MT for the methanol–ethanol coproduction, methanol–ammonia coproduction, and stand-alone methanol production systems, respectively.⁷⁸ For the MFSP of e-methanol to equal the market average over 2015–2020 (\$0.38 per kg), the breakeven costs of H_2 production with CO_2 credit (of \$200 per metric ton (MT)) and without CO_2 credit are estimated to be within \$2.09–2.24 per kg and \$0.77–0.95 per kg, respectively. By some estimates,^{94–96} 65% of the total methanol production cost is the cost of producing renewable H_2 . The estimated results in Fig. 13a are for a



(a)



(b)

Fig. 13 (a) MFSP of e-methanol as a function of the H_2 production cost, CO_2 cost, and the credit for saved carbon, for a production capacity of 1190 MT per day. Adapted from ref. 78. (b) Cost of e-methanol production versus production plant capacity. From ref. 97.



production capacity of 1190 MT per day,⁷⁸ whereas based on the results of several studies,⁹⁷ as shown in Fig. 13b, the cost of e-methanol production decreases with increasing capacity until and beyond 4400 t per day.

2.4.2 e-Kerosene/sustainable aviation fuel (SAF) production.

Carbon emissions from aviation account for ~2–3% of global carbon emissions, and the emissions from air travel continue to grow rapidly. One possible solution to reduce emissions from the aviation sector is through the use of sustainable aviation fuel (SAF), which is the name given to the synthetic aviation fuels produced using clean H₂ and captured CO₂. Besides being a carbon-neutral fuel, a major practical advantage of SAF is that it can be blended with the conventional fossil fuel-based aviation fuel with no infrastructure or equipment changes. The first commercial use of SAF was in a Boeing 737 passenger service flight on February 8, 2021, from Amsterdam to Madrid, which carried 500 liters of e-kerosene mixed with a fossil fuel-based regular aviation fuel.

2.4.2.1 Process. SAF can be produced using the Fischer-Tropsch (FT) process, which is a heterogeneously catalyzed process to convert CO₂/H₂ and syngas (CO/H₂) to liquid hydrocarbons (e.g., e-diesel/e-kerosene) with the desired composition (carbon chain and length) based on the process/operating conditions. The composition of the SAF consists of *n*-alkanes, iso-alkanes, and cycloalkanes, with a typical carbon chain length distribution ranging from C8 to C18.⁹⁸ The SAF production *via* FT synthesis includes six process areas, which are (i) H₂ and CO₂ compression, (ii) RWGS reactor, (iii) FT synthesis reactor, (iv) hydro-processing, (v) power generation, and (vi) utility.⁹⁹ The FT synthesis takes place in a second reactor as it requires CO as the feedstock that is generated using CO₂/H₂ in the first reverse water gas shift reaction (RWGS) reactor.

Just like the synthesis of e-methanol, H₂ and CO₂ are pressurized/compressed (~25 bar) before feeding them into the first reactor that operates at high temperature and high pressure in case the initial pressures of the supplied CO₂ and

H₂ are lower than the operating pressure of the reactor. The FT reaction is highly exothermic generating heat, which is supplied for the endothermic reaction in the RWGS reactor (Fig. 14).

A key factor that influences the FT synthesis is the efficient removal of heat from the reactor as FT reactions are highly exothermic which generate heat. The four commercially used designs of the FT synthesis reactor are based on different heat transfer mechanisms, which include¹⁰⁰ (i) the circulating fluidized bed reactor, (ii) the fluidized bed reactor, (iii) the tubular fixed bed reactor, and (iv) the slurry phase reactor.

2.4.2.1.1 H₂ and CO₂ utilization. Based on the FT process flow diagram shown in Fig. 14, producing a kg of SAF requires an estimated ~1.36 kg H₂ and 14.55 kg CO₂,⁹⁹ with Co- and Fe-based catalysts for the FT synthesis and BaCe_{0.2}Zr_{0.6}Y_{0.16}Zn_{0.04}O₃ as the catalyst for the RWGS reaction. Few other studies^{82,83,101} mention the net CO₂ utilization in the FT process as 2.6 t CO₂ per 1t of liquid FT fuel (or equivalently, a kg of FT fuel requires 2.6 kg of CO₂), but these estimates are for the traditional FT fuel (*versus* the synthetic FT fuel) that is produced using CO₂ and methane reforming.¹⁰¹

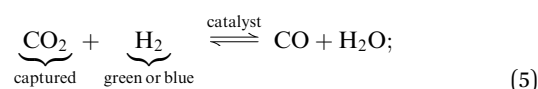
2.4.2.2 Reactions. The main FT reaction (eqn (4)) requires CO as the feedstock, which is generated from the captured CO₂ *via* the RWGS reaction of H₂ and CO₂ (eqn (5)).

FT reaction for e-diesel:



$$n \in [17, 32]; \quad \Delta H^{\text{exo}} \approx -x \text{ kJ mol}^{-1}$$

RWGS (600 °C, 24.5 bar⁹⁹):



$$\Delta H^{\text{endo}} = 41.22 \text{ kJ mol}^{-1} [\sim 600 - 900 \text{ }^\circ\text{C}]$$

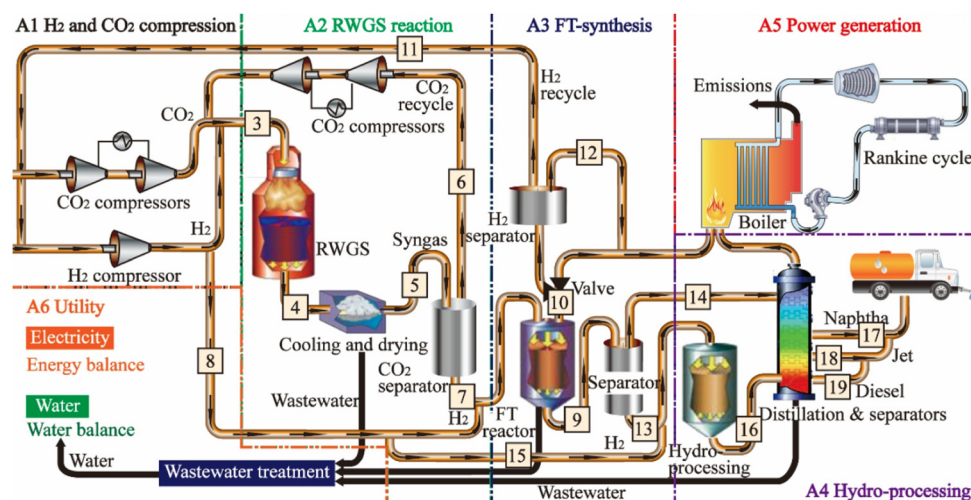


Fig. 14 Process flow diagram to produce a high-density liquid e-fuel (e.g., SAF) *via* the Fischer-Tropsch (FT) process. From ref. 99.





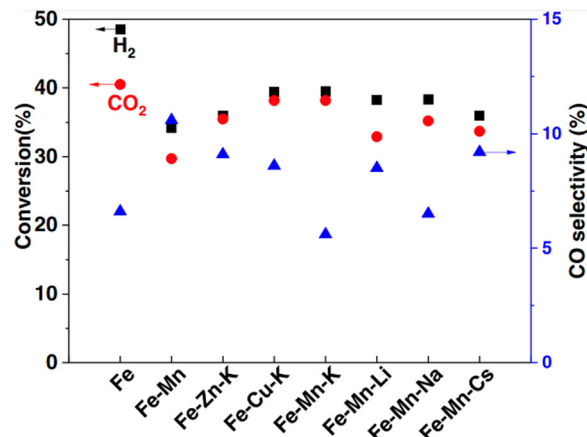
Fig. 15 Probabilistic distribution of the hydrocarbon products with different carbon chain lengths in the Fischer–Tropsch (FT) process.⁹⁷

The probabilistic distribution of the carbon chain length in the FT synthesis is described by the Anderson–Schulz–Flory distribution, which is mathematically expressed in eqn (6) and graphically illustrated in Fig. 15. The parameters W_n , n , and α in eqn (6) represent the weight fraction of the hydrocarbon product, the carbon chain length of the hydrocarbon product, and the growth probability of the carbon chain, respectively. The probability of the carbon chain (α) with length n is a function of the catalysts used in the FT process, plus the composition of the syngas and the operating conditions.⁹⁷ The SAF produced using the FT process is typically liquid products with 17–32 carbon atoms per chain. As shown in Fig. 15, there are various lengths of carbon chains produced in the FT process whose relative weights are a function of the chain growth probability. Other non-diesel products produced *via* FT are converted to diesel *via* upgrading, which primarily involves hydrocracking of waxes according to eqn (7).

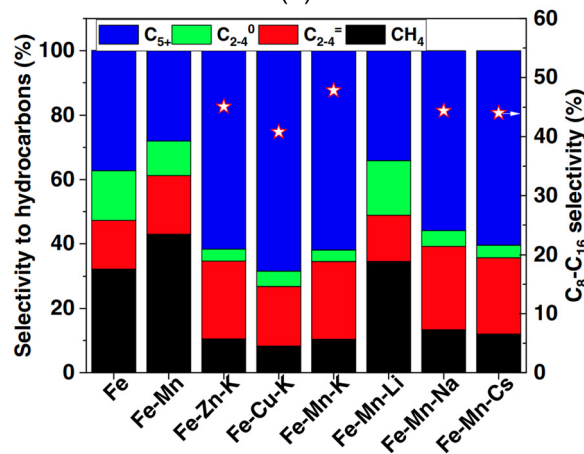
$$W_n = n(1 - \alpha)^2 \alpha^{n-1} \quad (6)$$



2.4.2.3 Catalysts. Traditionally, Co- and Fe-based catalysts have been used for commercial-scale FT processes, whereas precious metal-based catalysts (*e.g.*, nickel- and ruthenium-based) that are catalytically more active do not yet find a practical role in industrial applications.⁹⁷ Other relevant catalysts like porous metal oxides (*e.g.*, zeolite and aluminum oxide) with large specific surfaces are used as carriers for the catalyst. The use of Co-based catalysts is limited to operating conditions with relatively low temperatures (200–240 °C), but the Fe-based catalyst can be used over a wider range of operating temperatures ranging from low (200–240 °C) to high (300–360 °C).⁹⁹ Recent laboratory-scale advancements in catalysts for FT synthesis include combining Fe-based catalysts with transition metal promoters (*e.g.*, Fe–Mn–K) for high conversion rates and high selectivity to SAF;¹⁰² the catalytic performance using the three transition metal promoters (Na-, K-, and Cs-based) was found to



(a)



(b)

Fig. 16 Catalyst performance for the FT synthesis in terms of (a) the CO₂/H₂ conversion rate and (b) selectivity to hydrocarbons, especially longer-chain carbons (SAF). From ref. 102.

be similar, but the K-based metal promoter (Fe–Mn–K catalyst) showed high CO₂/H₂ conversion rates (Fig. 16a) and higher selectivity in longer-chain hydrocarbons (47.8% for C₈–C₁₆) than the selectivity from Na- and Cs-based metal promoters (44.4% and 44.0%, respectively) as shown in Fig. 16b.

2.4.2.4 Costs. The variation in the MFSP of FT fuel (SAF) with the cost of H₂ production, the cost of CO₂ as a feedstock, and the credit of saved CO₂ capture is shown in Fig. 17. Fig. 17 shows that the average MFSP of SAF varies between ~\$4.30 per gal and ~\$6.78 per gal depending on the cost of H₂ production (€[\$0.8 per kg, \$5.0 per kg] with the base price as \$2 per kg), the cost of CO₂ as a feedstock (€[\$0 per MT, \$76.2 per MT] with the base price as \$17.3 per MT), and the cost of saved carbon that can be traded (€[\$0 per MT, \$300 per MT] with the base price as \$0 per MT) as a credit.⁹⁹ The lowest MFSP (low-cost production) of FT fuel is potentially possible when the CO₂ is sourced from the ethanol, ethylene oxide, and ammonia plants, whereas the highest MFSP is potentially when the CO₂ is sourced from the hydrogen industry.⁹⁹ Besides the cost of H₂, CO₂, and CO₂ credit, the dominant parameters that have a major impact on



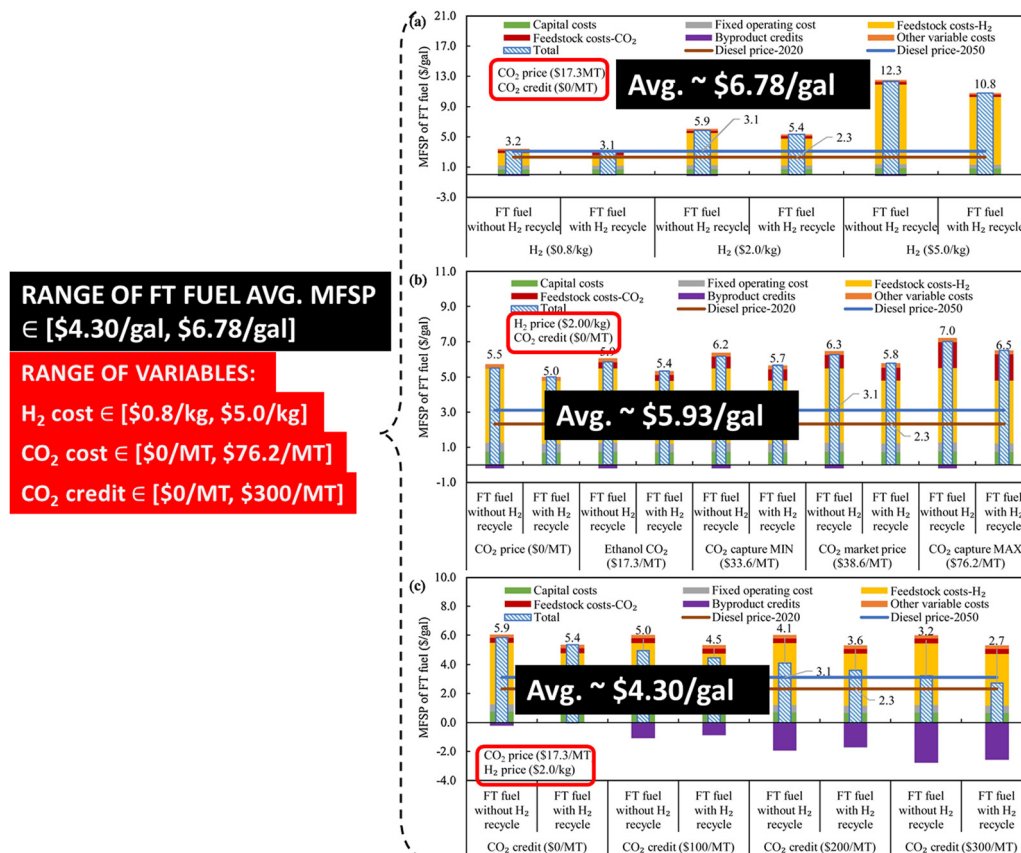


Fig. 17 MFSP of SAF (FT fuel) as a function of the H₂ production cost, CO₂ cost, and the credit for saved carbon for a production capacity of 351 MT per day (divided among 90 MT per day of naphtha, 164 MT per day of jet fuel, and 97 MT per day of diesel). Adapted from ref. 99.

the MFSP of FT fuel are the H₂ recycle ratio, CO conversion ratio of the FT reaction, and the CO₂ recycle ratio.⁹⁹ The estimated results in Fig. 17 are for a FT fuel production capacity of 351 MT per day (351 MT per day divided among 90 MT per day of naphtha, 164 MT per day of jet fuel, and 97 MT per day of diesel).⁹⁹

3 Projects

The number of currently operational e-methanol and SAF production plants around the world is very few, where almost all these plants are at the pilot- or demonstration-scale, but many new commercial-scale plants are currently under development and many new plants are being announced. Table 6 summarizes the projects for commercial production of e-methanol and SAF projects that are described ahead in detail.

3.1 e-Methanol production

Four renewable methanol plants discussed below are the Harun Oni project in Chile, e-CO₂Met project in Germany, MefCO₂ in Germany, and George Olah plant (also called CRI) in Iceland.

3.1.1 George Olah Plant, Svartsengi, Iceland (2012). George Olah (GO) plant, operated by Carbon Recycling International (CRI), is an industrial-scale e-methanol facility, shown in

Fig. 18, with a production capacity of 4000 tpa,⁷⁶ which uses the 5600 tpa of CO₂¹⁰³ captured from a nearby geothermal power plant and 800 tpa (1200 N m³ h⁻¹) of H₂¹⁰³ produced through an alkaline electrolyzer run on renewable grid electricity.

3.1.2 MefCO₂, Niederaussem, Germany (2019). This pilot-scale MefCO₂ (methanol fuel from CO₂) plant, shown in Fig. 19, is one of the largest e-methanol synthesis plants in the European Union and uses 1.5 tpd of captured CO₂ from a coal (lignite)-fired power plant along with 1.5 tpd of H₂ from a 600 kW PEM electrolyzer (from Hydrogenics/Cummins) to produce 1 tpd (500 tpa capacity) of methanol.

3.1.3 e-CO₂Met Project, Leuna, Germany (2021). TotalEnergies is the largest producer of conventional methanol in Europe, producing ~700 000 tpa of conventional methanol using fossil fuels at its refinery in Leuna, Germany. In 2019, TotalEnergies invested €150 MM in its refinery at Leuna with an aim to reduce the production of heavy products due to its decreasing demand, and increase the production of methanol which is one of the key raw materials in the chemical industry. TotalEnergies is partnering with Sunfire (Germany-based electrolyzer manufacturer) and Fraunhofer CBP (Germany-based biotech and sustainable chemistry research institute) to produce 1.5 tpd¹⁰⁵ of e-methanol *via* green H₂ produced from a 1 MW electrolyzer (high-temperature SOEC technology with



Table 6 Summary of projects for commercial production of liquid e-methanol and SAF

| e-Fuel ↓ | Project name | Companies | Location | Date started | Material consumption info | | Production capacity |
|------------------|------------------------|---|---------------------------|--------------|--|---|--|
| | | | | | H ₂ | CO ₂ | |
| e-Methanol | George Olah Plant | Carbon Recycling International (CRI) | Svartsengi, Iceland | 2012 | 800 tpa (1200 N m ³ h ⁻¹) produced using an alkaline electrolyzer powered by renewable energy | 5600 tpa captured from a nearby geothermal power plant | 4000 tpa |
| | MefCO ₂ | Consortium of 9 partners funded by the EU | Niederaussem, Germany | 2021 | 1.5 tpd from a 600 kW PEM electrolyzer from Cummins | 1.5 tpd of captured CO ₂ from a coal (lignite)-fired power plant | 1 tpd (500 tpa capacity) |
| | e-CO ₂ Met | TotalEnergies | Leuna, Germany | 2021 | 1 MW electrolyzer (high-temperature SOEC with 80% efficiency, from Sunfire) | Captured from TotalEnergies' refinery in Leuna | 1.5 tpd |
| | FReSMe | Consortium of 13 partners funded by the EU | Luleå, Sweden | 2021 | 100 N m ³ h ⁻¹ recovered from the blast furnace in addition to production by electrolysis | 14 tpd captured from an industrial steel blast furnace | 1 tpd (2.5 tpd capacity) |
| | Haru Oni | Siemens Energy, Porsche, HIF, Enel, Exxon-Mobil, Gasco and ENAP | Punta Arenas, Chile | 2022 | 1.2 MW PEM electrolyzer (from Siemens Energy) powered by wind energy (3.4 MW Siemens Gamesa turbine) | DAC (from Global Thermostat) | ~ 750 000 liters in 2022 and 1 000 000 tons by 2026 |
| e-Kerosene (SAF) | Synthetic diesel plant | Velocys | Oklahoma City, USA | 2017 | — | — | 250 bpd |
| | atmosfair FairFuel | Solarbelt Fair-Fuel gGmbH | Werlte, Germany | 2021 | 160 tpa or 20.7 kg h ⁻¹ using a 1.25 MW PEM electrolyzer powered by wind energy | DAC module and from waste valorization (biogas) | 350 tpa of synthetic crude oil |
| | Haru Oni | Siemens Energy, Porsche, HIF, Enel, Exxon-Mobil, Gasco and ENAP | Punta Arenas, Chile | 2022 | 1.2 MW PEM electrolyzer (from Siemens Energy) powered by wind energy (3.4 MW Siemens Gamesa turbine) | DAC (from Global Thermostat) | ~ 130 000, ~ 55 million, and ~ 550 million liters per year of e-gasoline ^a by the end of 2022, 2024, and 2026, respectively |
| | Bayou Fuels Plant | Velocys/OLCV | Natchez, Mississippi, USA | 2023 | — | — | 25 million gallons per year (35 million as capacity) |

^a Haru Oni project uses the terms e-methanol and e-gasoline as two products, but it does not provide a separate number for e-kerosene, which is assumed to be part of e-gasoline.



Fig. 18 CRI's GO plant in Svartsengi, Iceland, which uses CO₂ captured from the nearby geothermal power plant (in background) and H₂ produced through electrolysis to form renewable methanol. From ref. 103.

80% efficiency, from Sunfire) and CO₂ produced at TotalEnergies' refinery (in Leuna),¹⁰⁶ as shown in Fig. 20.

3.1.4 FReSMe Project, Luleå, Sweden (2021). FReSMe (From Residual Steel gases to Methanol) is a demonstration-scale

project to produce e-methanol for ship transportation using CO₂ captured from an industrial steel blast furnace, and H₂ recovered from the blast furnace in addition to its production by electrolysis. The FReSMe project, shown in Fig. 21, used 14 tpd of CO₂ with 100 N m³ h⁻¹ of H₂ from electrolysis to produce 1 tpd of e-methanol,⁸⁹ although the e-methanol production capacity of the plant is 2.5 tpd.¹⁰⁷

3.1.5 Haru Oni Project, Punta Arenas, Chile (expected by the end of 2022). A group of companies (Siemens Energy, Porsche, HIF, Enel, ExxonMobil, Gasco and ENAP) led by HIF is building a plant to produce e-methanol in Chilean Patagonia using green H₂ and CO₂ captured from a DAC facility, which will produce ~ 750 000 litres (~ 350 tpa) of e-methanol in 2022 and later expanded to 1 000 000 tons by 2026.^{75,108} This integrated plant (Fig. 22) will produce H₂ using a 1.2 MW PEM electrolyzer (from Siemens Energy) powered by 3.4 MW of wind energy (Siemens Gamesa turbine), which will be processed in a methanol synthesis reactor (Johnson Matthey's design) with



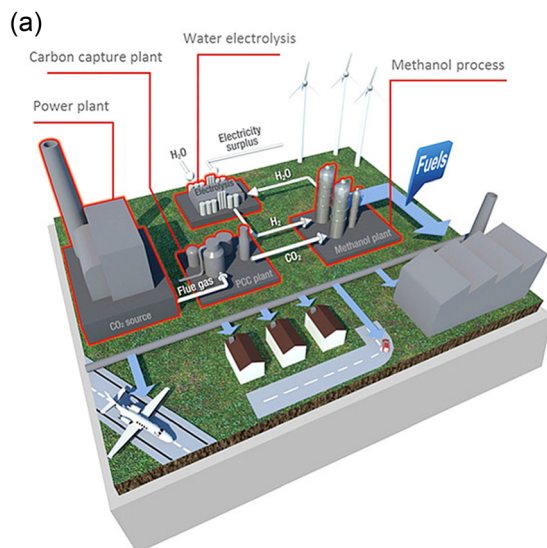


Fig. 19 (a) Schematic of the MefCO₂ plant⁷⁷ and (b) the actual pilot-scale MefCO₂ plant (right) at RWE's lignite-fired coal power plant in Niederaussem, Germany.¹⁰⁴



Fig. 20 Schematic of the e-CO₂Met Project, Leuna, which is scheduled to be fully operational after phase 2 which starts in 2022.

CO₂ captured from the air (from Global Thermostats) to produce e-methanol, and ~40% of the e-methanol will be converted to synthetic gasoline compatible with existing engines through a methanol to gasoline (MTG) plant located at the site

Pilot Layout

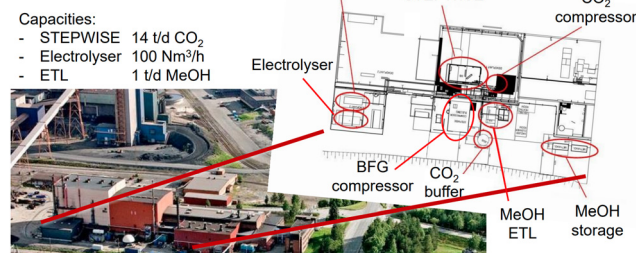


Fig. 21 Layout of the FReSMe project.⁸⁹

(ExxonMobil's Technology). The carbon-neutral synthetic gasoline will be transported to Europe *via* a container ship, each having a loading capacity of 25 000–30 000 liters, to be used by Porsche and others for modern and classic sports cars.

3.1.6 Other proposed projects. Other projects that are under planning and/or development include¹¹⁰ the following:

- Hy2Gen project in Germany with 61 000 tpa e-methanol production capacity. The CO₂ will be captured from a biogas plant and H₂ will be produced by electrolysis.
- A project in Norway by Swiss Liquid Future/Thyssenkrupp with 80 000 tpa e-methanol production capacity. The CO₂ will be captured from a ferrosilicon plant and H₂ will be produced by electrolysis powered by hydropower.
- A project in China by CRI and Jiangsu Sailboat Petrochemicals with 100 000 tpa e-methanol production capacity. The CO₂ and H₂ will be produced by electrolysis of water.
- A project in France by Vicat and Hynamics with 200 000 tpa e-methanol production capacity. The CO₂ will be captured from a cement plant and H₂ will be produced by electrolysis.

3.2 SAF production

Four renewable methanol plants discussed below are the Harun Oni project in Chile, e-CO₂Met project in Germany, MefCO₂ in Germany, and George Olah plant (also called CRI) in Iceland, respectively.

3.2.1 Synthetic diesel plant, Oklahoma city, USA (2017). The synthetic diesel plant at Oklahoma City¹¹¹ (Fig. 23a) demonstrated Velocys' Fischer-Tropsch technology through full commercial operation with 250 bpd of operational capacity.¹¹² This plant sold over 10 000 barrels of products (waxes, diesel and naphtha) to commercial off-takers and generated RIN credits under the Renewable Fuel Standard (RFS). This plant provided 1500+ hours data in enabling Velocys to scale its FT synthesis technology to other projects (*e.g.*, Mississippi Biorefinery and UK waste to jet projects). The H₂ was produced as syngas (an optimized mixture of carbon monoxide and hydrogen) by reforming natural gas, landfill gas, or by gasification of biomass or waste;¹¹² therefore, from the nomenclature perspective, SAF produced in this case could be referred to as bio-kerosene instead of e-kerosene.

Following a 20 month period of operation, a leak was identified at the ancillary coolant system of this plant which led to a reduction in its production capacity (a single reactor),





Fig. 22 (a) Schematic of the Haru Oni project, southern Chile, which will produce industrial-scale e-methanol starting from the end of 2022. Adapted from ref. 75. (b) Actual site of the Haru Oni project. From ref. 109.

and this subsequently resulted in closure of the plant due to accumulating effects, such as operating losses, not maintaining the specific requirements to generate RINs under the RFS pathway, *etc.*

3.2.2 atmosfair FairFuel, Werlte, Germany (2021). World's first commercial-scale plant to produce synthetic kerosene using H₂ and captured CO₂ started operations in October 2021 at Werlte, Germany, as shown in Fig. 24.^{114,115} The plant (owned and operated by Solarbelt FairFuel gGmbH; Lufthansa Group is a pilot customer) produces 350 tpa of synthetic crude oil through Fischer-Tropsch synthesis from carbon monoxide (recovered from CO₂) and H₂, where synthetic crude oil is used to manufacture climate-neutral kerosene meant for aviation. The H₂ is produced using a 1.25 MW PEM electrolyzer (160 tpa

or 20.7 kg h⁻¹ of H₂) powered by wind energy, while the CO₂ is captured using a DAC module and from waste valorization (biogas).

3.2.3 Bayou Fuels Plant, Natchez, Mississippi, USA (expected by the end of 2023). Velocys is using the experience gained through its Oklahoma City plant (U.S.) in developing a similar larger-scale (Fig. 25) FT gas-to-liquid plant (Bayou Fuels plant) at Natchez, Mississippi, US, in partnership with Oxy Low Carbon Ventures (OLCV).¹¹⁶ This plant will use 3000 tons of woody biomass as the feedstock to produce 25 million gallons of SAF (with 35 million gallons per year of capacity) plus renewable naphtha. The SAF production capacity of this plant will be the largest capacity in the U.S. by the time it comes online in 2023, and it is also cited by the U.S. Federal Government as one



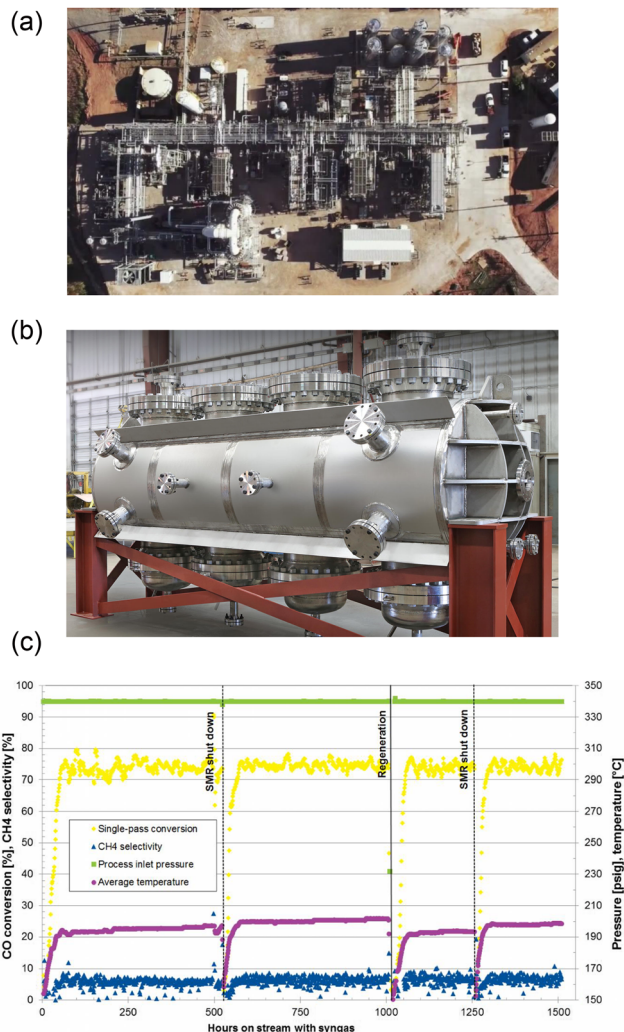


Fig. 23 (a) Velocys' first FT gas-to-liquid technology plant at Oklahoma City, US. From ref. 113. (b) Image of Velocys' FT reactor for the synthesis of hydrocarbons, particularly the SAF. (c) ~1500 hours of operational data from Velocys' synthetic diesel plant. From ref. 113.



Fig. 24 Actual site of the 350 tpa of SAF production plant at Werlte in Germany, including the electrolysis system that forms the core of the plant.^{114,115}

of the projects that will help achieve the 2030 goal of producing at least 3 billion gallons per year of SAF in the U.S.

3.2.4 Haru Oni Project, Punta Arenas, Chile (expected by the end of 2022). This plant will also produce SAF in addition to



(a)



(b)

Fig. 25 (a) Schematic of the site of Velocys' proposed FT gas-to-liquid plant (Bayou Fuels plant) at Natchez, Mississippi, US. From ref. 116. (b) Schematic showing the layout of the Bayou Fuels Plant. From ref. 116.

e-methanol (as discussed earlier). The plant's capacity will be incrementally increased to produce ~130 000, ~55 million, and ~550 million litres per year of e-gasoline by the end of 2022, 2024, and 2026, respectively. The project does not provide a separate number for e-kerosene, which is assumed to be part of e-gasoline.

3.2.5 Other proposed projects. Other projects that are under planning and/or development include the following:

- A project development start-up called Synkero is developing a commercial-scale (50 000 tpa) plant at the Port of Amsterdam for the production of SAF using green H₂ and CO₂ which is scheduled to be completed in 2027. The Port of Amsterdam has an existing pipeline that supplies kerosene to Schiphol Airport.^{117,118} The e-kerosene production plant will be powered by a 200 MW electrolysis system driven by wind energy (30 off-shore turbines) which will produce 25 000 tpa of H₂, which will be processed with 200 000 tpa of captured CO₂ to produce 50 000 tpa of e-kerosene.¹¹⁸

- A consortium called Zenid,¹¹⁹ comprising the Rotterdam airports (RTHA, RHIA), a sustainable air fuel (SAF) company (SkyNRG), and a DAC manufacturing company (Climeworks), is investigating the construction of an industrial-scale demonstration plant in Rotterdam, the Netherlands, to produce SAF with H₂ produced using the co-electrolysis unit and CO₂ captured from the air through a modular Fischer-Tropsch reactor.

- Infinium (a low-carbon liquid fuel producer in the U.S.) and Denbury (an oil and gas operator in the U.S.) announced a



partnership to build an e-fuel facility in Brazoria County, Texas, which will convert green H₂ (from renewable power) and industrial-sourced CO₂ into SAF and diesel using Infinium's proprietary technology.¹²⁰ This facility is anticipated to use 1.5 MM tpa of CO₂ captured from industrial sources and transported by Denbury using its CO₂ pipeline infrastructure.

- ExxonMobil and Neste will supply 1.25 million liters of SAF blended with refined jet fuel to Changi Airport for Singapore Airlines and Scoot flights by the third quarter of 2022.¹²¹

- Oxy initiated a front-end engineering and design (pre-FEED) for a 100 million liter (26.4 million gallons) annual capacity plant in British Columbia, Canada, to produce ultra-low carbon fuel for air, marine, rail, and truck transportation in Canada. The plant will use Carbon Engineering's DAC technology to capture CO₂.¹²²

- Norsk e-Fuel will build a SAF plant in Mosjøen, Norway, on a 24 000 m² large plot, which will use 100% renewable electricity to produce H₂ through electrolysis (from Sunfire) and capture CO₂ from air using Climeworks' DAC technology.¹²³ The plant's production capacity will be 12.5 million liters of SAF by 2024 and 25 million liters of SAF by 2026.

4 Outlook and recommendations

Although the current market for CO₂ utilization is relatively small and will not likely rise much in the short- to medium-term without a significant policy change that puts a competitive price on CO₂ emissions in major CO₂ emitting countries, one of the major sectors with a potential to drive the CO₂ utilization demand in the absence of a policy is the blending of e-methanol and SAF with fossil fuel-produced methanol and jet fuel/diesel, respectively. Unlike hydrogen as a fuel, these e-fuels are readily-compatible with existing internal combustion engines in aviation, shipping, freight, *etc.*, and do not require any changes to the handling and logistics infrastructure. The production of liquid e-fuels is energy intensive and requires significant quantities of both H₂ and CO₂, and arranging such a large supply of both H₂ and CO₂ to produce e-fuels at scale can be complex and challenging. The production costs for liquid e-fuels are also significantly higher than their fossil fuel-produced counterparts, primarily due to the costs involved in producing hydrogen. However, these holistic challenges must consider the following two incentives:

(1) Reaching net-zero by 2050 requires a relatively huge reduction in CO₂ compared to the current capture capacity, such that the 2030 target (800 MM tpa), and possibly the 2050 target, does not appear to be practically achievable. This implies that, due to the current under-capacity of CCUS and the large jump required to reach 800 MM tpa in less than a decade, the social and political pressure will ramp up as an alternative to not meeting the climate goals, which can suddenly lead to cost-prohibitive measures from various societal instruments, including government, law, *etc.* In this direction, a small but initial step has been taken by the recent U.S. Securities and Exchange Commission rule which enhanced

the monitoring requirements for reporting Scope 1, Scope 2, and Scope 3 emissions, enforcing which did not require any new or exclusive law. The oil and gas companies that are already taking steps to decarbonize their value chain will be in a much better position to face these challenges.

(2) CO₂ utilization is not an alternative to the large-scale CO₂ storage required for reductions in CO₂ emissions, but it can still support the goal of reducing the emissions. Cultivating an early opportunity in CO₂ utilization through the production of liquid e-fuels will not only help create partnerships required to secure CO₂ supply chains, it can also lead to new markets for carbon-neutral liquid e-fuels that can be simply blended with their fossil fuel-based counterparts.

Author contributions

Harpreet Singh: conceptualization, investigation, project administration, writing – original draft preparation, writing – review and editing. Chengxi Li: project administration, writing – review and editing. Peng Cheng: funding acquisition, resources, supervision. Xunjie Wang: funding acquisition, resources, supervision. Qing Liu: writing – review and editing.

Conflicts of interest

There are no conflicts to declare.

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References

- 1 Auguste and others, Mission Possible: Reaching net-zero carbon emissions from harder-to-abate sectors, 2018, <https://www.energy-transitions.org/publications/mission-possible/>.
- 2 IEA, Energy Technology Perspectives 2020, 2020, p. 174. https://iea.blob.core.windows.net/assets/181b48b4-323f-454d-96fb-0bb1889d96a9/CCUS_in_clean_energy_transitions.pdf, DOI: [10.1787/d07136f0-en](https://doi.org/10.1787/d07136f0-en).
- 3 N. Adomaitis and J. Harvey, *Global climate goals 'virtually impossible' without carbon capture* – IEA, Reuters, 2020.
- 4 G. Hering and B. Montgomery, *First major US hydrogen-burning power plant nears completion in Ohio*, S&P Global Platts Media, 2021.
- 5 IEA, *Putting CO₂ to Use: Creating value from emissions*, 2019, <https://www.iea.org/reports/putting-co2-to-use>, DOI: [10.1787/dfcabbf4-en](https://doi.org/10.1787/dfcabbf4-en).
- 6 C. Hobson and C. Márquez, Renewable methanol report, 2018, pp. 1–26.



- 7 CAPA, Aviation Sustainability and the Environment, CAPA 23-Jun-2022|CAPA, CAPA – Centre for Aviation, 2022.
- 8 M. Kayfeci, A. Keçebaş and M. Bayat, Hydrogen production, in *Solar Hydrogen Production*, ed. F. Calise, M. D.D'Accadia, M. Santarelli, A. Lanzini and D. Ferrero, Academic Press, 2019, ch. 3, pp. 45–83, DOI: [10.1016/B978-0-12-814853-2.00003-5](https://doi.org/10.1016/B978-0-12-814853-2.00003-5).
- 9 N. Sazali, Emerging technologies by hydrogen: A review, *Int. J. Hydrogen Energy*, 2020, **45**, 18753–18771.
- 10 M.-K. Kazi, F. Eljack, M. M. El-Halwagi and M. Haouari, Green hydrogen for industrial sector decarbonization: Costs and impacts on hydrogen economy in qatar, *Comput. Chem. Eng.*, 2021, **145**, 107144.
- 11 U.S. DOE, *Hydrogen Program Plan*, 2020, https://www.hydrogen.energy.gov/pdfs/program_plan2011.pdf.
- 12 H. Nazir, *et al.*, Is the H₂ economy realizable in the foreseeable future? Part I: H₂ production methods, *Int. J. Hydrogen Energy*, 2020, **45**, 13777–13788.
- 13 F. Elmanakhly, *et al.*, Hydrogen economy transition plan: A case study on Ontario, *AIMSE*, 2021, **9**, 775–811.
- 14 C. M. Kalamaras and A. M. Efstathiou, Hydrogen Production Technologies: Current State and Future Developments, *Conf. Pap. Energy*, 2013, e690627.
- 15 R. Pinsky, P. Sabharwall, J. Hartvigsen and J. O'Brien, Comparative review of hydrogen production technologies for nuclear hybrid energy systems, *Prog. Nucl. Energy*, 2020, **123**, 103317.
- 16 H. Thomas, *et al.*, *Options for producing low-carbon hydrogen at scale*, The Royal Society, 2018.
- 17 N. Sánchez-Bastardo, R. Schlögl and H. Ruland, Methane Pyrolysis for Zero-Emission Hydrogen Production: A Potential Bridge Technology from Fossil Fuels to a Renewable and Sustainable Hydrogen Economy, *Ind. Eng. Chem. Res.*, 2021, **60**, 11855–11881.
- 18 P. R. Kapadia, M. Kallos, L. Chris and I. D. Gates, Potential for Hydrogen Generation during In Situ Combustion of Bitumen, OnePetro, 2009, DOI: [10.2118/122028-MS](https://doi.org/10.2118/122028-MS).
- 19 T. Jacobs, *Canadian Operator Works To Transform an Oil Field Into a Hydrogen Factory*, SPE JPT, 2021.
- 20 A. Akhtar, V. Krepl and T. Ivanova, A Combined Overview of Combustion, Pyrolysis, and Gasification of Biomass, *Energy Fuels*, 2018, **32**, 7294–7318.
- 21 V. Singh and D. Das, Chapter 3 – Potential of Hydrogen Production From Biomass, in *Science and Engineering of Hydrogen-Based Energy Technologies*, ed. P. E. V. de Miranda, Academic Press, 2019, pp. 123–164, DOI: [10.1016/B978-0-12-814251-6.00003-4](https://doi.org/10.1016/B978-0-12-814251-6.00003-4).
- 22 V. Zgonnik, The occurrence and geoscience of natural hydrogen: A comprehensive review, *Earth-Sci. Rev.*, 2020, **203**, 103140.
- 23 V. Zgonnik, *et al.*, Evidence for natural molecular hydrogen seepage associated with Carolina bays (surficial, ovoid depressions on the Atlantic Coastal Plain, Province of the USA), *Prog. Earth Planetary Sci.*, 2015, **2**, 1–15.
- 24 S. P. Gregory, M. J. Barnett, L. P. Field and A. E. Milodowski, Subsurface Microbial Hydrogen Cycling: Natural Occurrence and Implications for Industry, *Microorganisms*, 2019, **7**, 53.
- 25 J. Guélard, *et al.*, Natural H₂ in Kansas: Deep or shallow origin?, *Geochem., Geophys., Geosyst.*, 2017, **18**, 1841–1865.
- 26 A. Prinzhofer, C. S. Tahara Cissé and A. B. Diallo, Discovery of a large accumulation of natural hydrogen in Bourakebougou (Mali), *Int. J. Hydrogen Energy*, 2018, **43**, 19315–19326.
- 27 S. L. Worman, L. F. Pratson, J. A. Karson and W. H. Schlesinger, Abiotic hydrogen (H₂) sources and sinks near the Mid-Ocean Ridge (MOR) with implications for the subseafloor biosphere, *Proc. Natl. Acad. Sci. U. S. A.*, 2020, **117**, 13283–13293.
- 28 R. M. Coveney, Jr., E. D. Goebel, E. J. Zeller, G. A. M. Dreschhoff and E. E. Angino, Serpentinization and the Origin of Hydrogen Gas in Kansas, *AAPG Bull.*, 1987, **71**, 39–48.
- 29 E. D. Goebel, R. M. Coveney, Jr, E. E. Angino and E. Zeller, Naturally Occurring Hydrogen Gas from a Borehole on the Western Flank of Nemaha Anticline in Kansas, *AAPG Bull.*, 1983, **67**, 1324.
- 30 A. Kovač, M. Paranos and D. Marciuš, Hydrogen in energy transition: A review, *Int. J. Hydrogen Energy*, 2021, **46**, 10016–10035.
- 31 S. A. Grigoriev, V. N. Fateev, D. G. Bessarabov and P. Millet, Current status, research trends, and challenges in water electrolysis science and technology, *Int. J. Hydrogen Energy*, 2020, **45**, 26036–26058.
- 32 A. Morozov, Comparative Analysis of Hydrogen Production Methods with Nuclear Reactors, 2008.
- 33 R. Perret, Solar Thermochemical Hydrogen Production Research (STCH) Thermochemical Cycle Selection and Investment Priority, 2011, <https://www.osti.gov/biblio/1671699-solar-thermochemical-hydrogen-production-research-stch-thermochemical-cycle-selection-investment-priority>.
- 34 A. Boretti, Technology Readiness Level of Solar Thermochemical Splitting Cycles, *ACS Energy Lett.*, 2021, **6**, 1170–1174.
- 35 F. Safari and I. Dincer, A review and comparative evaluation of thermochemical water splitting cycles for hydrogen production, *Energy Convers. Manage.*, 2020, **205**, 112182.
- 36 U.S. DOE, DOE Technical Targets for Hydrogen Production from Thermochemical Water Splitting, 2021, <https://www.energy.gov/eere/fuelcells/doe-technical-targets-hydrogen-production-thermochemical-water-splitting>.
- 37 U.S. DOE, DOE Technical Targets for Hydrogen Production from Photoelectrochemical Water Splitting, 2021, <https://www.energy.gov/eere/fuelcells/doe-technical-targets-hydrogen-production-photoelectrochemical-water-splitting>.
- 38 U.S. DOE, DOE Technical Targets for Hydrogen Production from Electrolysis, 2021, <https://www.energy.gov/eere/fuelcells/doe-technical-targets-hydrogen-production-electrolysis>.
- 39 M. Bui, *et al.*, Carbon capture and storage (CCS): the way forward, *Energy Environ. Sci.*, 2018, **11**, 1062–1176.
- 40 S. W. Nam, S. P. Yoon, H. Y. Ha, S.-A. Hong and A. P. Maganyuk, Methane steam reforming in a Pd-Ru membrane reactor, *Korean J. Chem. Eng.*, 2000, **17**, 288–291.



- 41 J. Tong and Y. Matsumura, Effect of catalytic activity on methane steam reforming in hydrogen-permeable membrane reactor, *Appl. Catal., A*, 2005, **286**, 226–231.
- 42 M. Sarić, Y. C. van Delft, R. Sumbharaju, D. F. Meyer and A. de Groot, Steam reforming of methane in a bench-scale membrane reactor at realistic working conditions, *Catal. Today*, 2012, **193**, 74–80.
- 43 T. Kume, *et al.*, Performance evaluation of membrane on catalyst module for hydrogen production from natural gas, *Int. J. Hydrogen Energy*, 2013, **38**, 6079–6084.
- 44 B. Dittmar, *et al.*, Methane steam reforming operation and thermal stability of new porous metal supported tubular palladium composite membranes, *Int. J. Hydrogen Energy*, 2013, **38**, 8759–8771.
- 45 H. W. Abu El Hawa, S. N. Paglieri, C. C. Morris, A. Harale and J. Douglas Way, Application of a Pd–Ru composite membrane to hydrogen production in a high temperature membrane reactor, *Sep. Purif. Technol.*, 2015, **147**, 388–397.
- 46 H. W. Abu El Hawa, S.-T. B. Lundin, N. S. Patki and J. Douglas Way, Steam methane reforming in a PdAu membrane reactor: Long-term assessment, *Int. J. Hydrogen Energy*, 2016, **41**, 10193–10201.
- 47 B. Anzelmo, J. Wilcox and S. Liguori, Natural gas steam reforming reaction at low temperature and pressure conditions for hydrogen production *via* Pd/PSS membrane reactor, *J. Membr. Sci.*, 2017, **522**, 343–350.
- 48 C.-H. Kim, J.-Y. Han, H. Lim, D.-W. Kim and S.-K. Ryi, Methane steam reforming in a membrane reactor using high-permeable and low-selective Pd-Ru membrane, *Korean J. Chem. Eng.*, 2017, **34**, 1260–1265.
- 49 C.-H. Kim, *et al.*, Hydrogen production by steam methane reforming in a membrane reactor equipped with a Pd composite membrane deposited on a porous stainless steel, *Int. J. Hydrogen Energy*, 2018, **43**, 7684–7692.
- 50 IRENA, *Hydrogen: A renewable energy perspective*, 2019, <https://www.irena.org/publications/2019/Sep/Hydrogen-A-renewable-energy-perspective>.
- 51 J. Davies, F. Dolci, D. Klassek-Bajorek, R. Ortiz Cebolla and E. Weidner, Current status of Chemical Energy Storage Technologies, 2020, <https://publications.jrc.ec.europa.eu/repository/handle/JRC118776>.
- 52 R. Shaw and S. Mukherjee, The development of carbon capture and storage (CCS) in India: A critical review, *Carbon Capture Sci. Technol.*, 2022, 100036, DOI: [10.1016/j.cst.2022.100036](https://doi.org/10.1016/j.cst.2022.100036).
- 53 A. I. Osman, M. Hefny, M. I. A. Abdel Maksoud, A. M. Elgarahy and D. W. Rooney, Recent advances in carbon capture storage and utilisation technologies: a review, *Environ. Chem. Lett.*, 2021, **19**, 797–849.
- 54 M. Zaman and J. H. Lee, Carbon capture from stationary power generation sources: A review of the current status of the technologies, *Korean J. Chem. Eng.*, 2013, **30**, 1497–1526.
- 55 N. S. Sifat and Y. Haseli, A Critical Review of CO₂ Capture Technologies and Prospects for Clean Power Generation, *Energies*, 2019, **12**, 4143.
- 56 O. Linjala, Review on post-combustion carbon capture technologies and capture of biogenic CO₂ using pilot-scale equipment, in Katsaus polton jälkeiseen hiilidioksidin talteenottoon kehitettyihin teknologioihin sekä biopärisen hiilidioksidin talteenotto pilot-mittakaavan koe-laitteistolla, Master's thesis, LUT University, 2021.
- 57 T. Lockwood, A Compararitive Review of Next-generation Carbon Capture Technologies for Coal-fired Power Plant, *Energy Procedia*, 2017, **114**, 2658–2670.
- 58 Y. Yamauchi and K. Akiyama, Innovative zero-emission coal gasification power generation project, *Energy Procedia*, 2013, **37**, 6579–6586.
- 59 J. Li, *et al.*, CO₂ Capture with Chemical Looping Combustion of Gaseous Fuels: An Overview, *Energy Fuels*, 2017, **31**, 3475–3524.
- 60 L.-S. Fan, L. Zeng, W. Wang and S. Luo, Chemical looping processes for CO₂ capture and carbonaceous fuel conversion – prospect and opportunity, *Energy Environ. Sci.*, 2012, **5**, 7254–7280.
- 61 S. Ferguson and A. Tarrant, Molten Carbonate Fuel Cells for 90% Post Combustion CO₂ Capture From a New Build CCGT, *Front. Energy Res.*, 2021, **9**, 359.
- 62 X. Zhang, Current status of stationary fuel cells for coal power generation, *Clean Energy*, 2018, **2**, 126–139.
- 63 Osaki CoolGen Corp, The Progress of Osaki CoolGen Project ~ Oxygen-blown Integrated Coal Gasification Fuel Cell Combined Cycle Demonstration Project, 2017.
- 64 T. M. Gür, Carbon Dioxide Emissions, Capture, Storage and Utilization: Review of Materials, Processes and Technologies, *Prog. Energy Combust. Sci.*, 2022, **89**, 100965.
- 65 S. Consonni, L. Mastropasqua, M. Spinelli, T. A. Barckholtz and S. Campanari, Low-carbon hydrogen *via* integration of steam methane reforming with molten carbonate fuel cells at low fuel utilization, *Adv. Appl. Energy*, 2021, **2**, 100010.
- 66 R. Barker, Y. Hua and A. Neville, Internal corrosion of carbon steel pipelines for dense-phase CO₂ transport in carbon capture and storage (CCS) – a review, *Int. Mater. Rev.*, 2017, **62**, 1–31.
- 67 S. Walspurger and H. A. J. Van Dijk, *EDGAR CO₂ purity*. Type and quantities of impurities related to CO₂ point source and capture technology. A Literature study, 2012.
- 68 J. Wilcox, R. Haghpanah, E. C. Rupp, J. He and K. Lee, Advancing Adsorption and Membrane Separation Processes for the Gigaton Carbon Capture Challenge, *Annu. Rev. Chem. Biomol. Eng.*, 2014, **5**, 479–505.
- 69 Accenture, Industrial Clusters and the Path to Net Zero, <https://www.accenture.com/us-en/insights/utilities/industrial-clusters-net-zero-future>, 2021.
- 70 D. Kearns, H. Liu and C. Consoli, Technology readiness and costs of CCS, 2021.
- 71 C. Davis, *Oxy Looks to Ramp Permian Carbon Capture by Early 2024, Consider More JVs in Lower 48*, Natural Gas Intelligence, 2021.
- 72 B. Wright, Oxy To Sell Industry's First Net-Zero Oil, *J. Petrol. Technol.*, 2022, <https://www.oxy.com/news/news-releases/occidental-sk-trading-international-sign-first-agreement-for-net-zero-oil-created-from-captured-atmospheric-carbon-dioxide/>.
- 73 S. Van Paasen, *et al.*, *Int. J. Greenhouse Gas Control*, 2021, **109**, 103368.



- 74 BHI, Carbon Capture|Baker Hughes Carbon Capture, Baker Hughes, Inc., 2022.
- 75 Haru Oni, Tomorrow's fuel|Haru Oni, *e-Fuel*, 2021, <https://www.haruoni.com/#/en>.
- 76 D. S. Marlin, E. Sarron and Ó. Sigurbjörnsson, Process Advantages of Direct CO₂ to Methanol Synthesis, *Front. Chem.*, 2018, **6**, 446.
- 77 M. Bowker, Methanol Synthesis from CO₂ Hydrogenation, *ChemCatChem*, 2019, **11**, 4238–4246.
- 78 G. Zang, P. Sun, A. Elgowainy and M. Wang, Technoeconomic and Life Cycle Analysis of Synthetic Methanol Production from Hydrogen and Industrial Byproduct CO₂, *Environ. Sci. Technol.*, 2021, **55**, 5248–5257.
- 79 S. Stanbridge, *Teaching an old plant new tricks: The rise of the methanol plant revamp*, Hydrocarbon Processing, 2016.
- 80 S. Schemme, *et al.*, H₂-based synthetic fuels: A technoeconomic comparison of alcohol, ether and hydrocarbon production, *Int. J. Hydrogen Energy*, 2020, **45**, 5395–5414.
- 81 F. Schorn, *et al.*, Methanol as a renewable energy carrier: An assessment of production and transportation costs for selected global locations, *Adv. Appl. Energy*, 2021, **3**, 100050.
- 82 E. Ruiz Martínez and J. M. Sánchez Hervás, Chemical Valorization of CO₂, in *Carbon Dioxide Utilization to Sustainable Energy and Fuels*, ed. Inamuddin, R. Boddula, M. I. Ahamed and A. Khan, Springer International Publishing, 2022, pp. 1–30, DOI: [10.1007/978-3-030-72877-9_1](https://doi.org/10.1007/978-3-030-72877-9_1).
- 83 S. M. Jarvis and S. Samsatli, Technologies and infrastructures underpinning future CO₂ value chains: A comprehensive review and comparative analysis, *Renewable Sustainable Energy Rev.*, 2018, **85**, 46–68.
- 84 R. Chauvy, N. Meunier, D. Thomas and G. De Weireld, Selecting emerging CO₂ utilization products for short- to mid-term deployment, *Appl. Energy*, 2019, **236**, 662–680.
- 85 S. Dang, *et al.*, A review of research progress on heterogeneous catalysts for methanol synthesis from carbon dioxide hydrogenation, *Catal. Today*, 2019, **330**, 61–75.
- 86 K. Stangeland, H. Li and Z. Yu, Thermodynamic Analysis of Chemical and Phase Equilibria in CO₂ Hydrogenation to Methanol, Dimethyl Ether, and Higher Alcohols, *Ind. Eng. Chem. Res.*, 2018, **57**, 4081–4094.
- 87 R. Dębek, F. Azzolina-Jury, A. Travert and F. Maugé, A review on plasma-catalytic methanation of carbon dioxide – Looking for an efficient catalyst, *Renewable Sustainable Energy Rev.*, 2019, **116**, 109427.
- 88 X. Jiang, X. Nie, X. Guo, C. Song and J. G. Chen, Recent Advances in Carbon Dioxide Hydrogenation to Methanol via Heterogeneous Catalysis, *Chem. Rev.*, 2020, **120**, 7984–8034.
- 89 FreSMe, *FreSMe Pilot Plant Operation*, 2021.
- 90 F. Geng, X. Zhan and J. C. Hicks, Promoting Methanol Synthesis and Inhibiting CO₂ Methanation with Bimetallic In–Ru Catalysts, *ACS Sustainable Chem. Eng.*, 2021, **9**, 11891–11902.
- 91 C. Zhou, *et al.*, Steering CO₂ hydrogenation toward C–C coupling to hydrocarbons using porous organic polymer/metal interfaces, *Proc. Natl. Acad. Sci. U. S. A.*, 2022, **119**, e2114768119.
- 92 <https://phys.org/news/2022-02-catalyst-carbon-dioxide-gasoline-efficiently.html>.
- 93 D. H. Kim, J. L. Park, E. J. Park, Y. D. Kim and S. Uhm, Dopant Effect of Barium Zirconate-Based Perovskite-Type Catalysts for the Intermediate-Temperature Reverse Water Gas Shift Reaction, *ACS Catal.*, 2014, **4**, 3117–3122.
- 94 Y. A. Daza and J. N. Kuhn, CO₂ conversion by reverse water gas shift catalysis: comparison of catalysts, mechanisms and their consequences for CO₂ conversion to liquid fuels, *RSC Adv.*, 2016, **6**, 49675–49691.
- 95 J. Kim, *et al.*, Methanol production from CO₂ using solar-thermal energy: process development and technoeconomic analysis, *Energy Environ. Sci.*, 2011, **4**, 3122–3132.
- 96 J. Kim, T. A. Johnson, J. E. Miller, E. B. Stechel and C. T. Maravelias, Fuel production from CO₂ using solar-thermal energy: system level analysis, *Energy Environ. Sci.*, 2012, **5**, 8417–8429.
- 97 V. Dieterich, A. Buttler, A. Hanel, H. Spliethoff and S. Fendt, Power-to-liquid via synthesis of methanol, DME or Fischer–Tropsch-fuels: a review, *Energy Environ. Sci.*, 2020, **13**, 3207–3252.
- 98 P. Kallio, A. Pásztor, M. K. Akhtar and P. R. Jones, Renewable jet fuel, *Curr. Opin. Biotechnol.*, 2014, **26**, 50–55.
- 99 G. Zang, P. Sun, A. A. Elgowainy, A. Bafana and M. Wang, Performance and cost analysis of liquid fuel production from H₂ and CO₂ based on the Fischer–Tropsch process, *J. CO₂ Util.*, 2021, **46**, 101459.
- 100 A. P. Steynberg, M. E. Dry, B. H. Davis and B. B. Breman, Fischer–Tropsch Reactors, in *Studies in Surface Science and Catalysis*, ed. A. Steynberg, and M. Dry, Elsevier, 2004, ch. 2, vol. 152, pp. 64–195.
- 101 H. Er-rbib, C. Bouallou and F. Werkoff, Production of Synthetic Gasoline and Diesel Fuel from Dry Reforming of Methane, *Energy Procedia*, 2012, **29**, 156–165.
- 102 B. Yao, *et al.*, Transforming carbon dioxide into jet fuel using an organic combustion-synthesized Fe–Mn–K catalyst, *Nat. Commun.*, 2020, **11**, 6395.
- 103 B. Stefansson, *Power and CO₂ emissions to methanol|CRI*, 2015.
- 104 CORDIS, MefCO₂ (Synthesis of methanol from captured carbon dioxide using surplus electricity), 2020, <https://cordis.europa.eu/project/id/637016/reporting/it>.
- 105 IRENA, Innovation Outlook: Renewable Methanol, 2021, <https://www.irena.org/publications/2021/Jan/Innovation-Outlook-Renewable-Methanol>.
- 106 TotalEnergies, TotalEnergies, Sunfire and Fraunhofer give the go-ahead for green methanol in Leuna, *TotalEnergies*, 2021.
- 107 G. Leonzio, State-Of-The-Art Overview of CO₂ Conversions, in *Carbon Dioxide Utilization to Sustainable Energy and Fuels*, ed. Inamuddin, R. Boddula, M. I. Ahamed and A. Khan, Springer International Publishing, 2022, pp. 335–353, DOI: [10.1007/978-3-030-72877-9_18](https://doi.org/10.1007/978-3-030-72877-9_18).
- 108 A. Benzinger, *Construction begins on world's first integrated commercial plant*, Siemens Energy, 2021.
- 109 HIF Global, Haru Oni Demonstration Plant, *HIF Global*, 2022.
- 110 Methanol Institute, Renewable and Biomethanol Projects 2021|Methanol Institute, Methanol Institute, 2022.



- 111 J. Lane, *ENVIA suspends operations, Velocys renews focus on Mississippi, UK projects*, Biofuels Digest, 2018, <https://www.biofuelsdigest.com/bdigest/2018/09/11/envia-suspends-operations-velocys-renews-focus-on-mississippi-uk-projects/>.
- 112 Velocys, *Velocys: Oklahoma City plant on track to reach final capacity*, Velocys, 2017.
- 113 N. Hargreaves, *Roll out of smaller scale GTL technology at ENVIA Energy's plant in Oklahoma City, USA*|Velocys, 2017.
- 114 Siemens, *The global energy transition will be based on the hydrogen economy*, Siemens Energy, 2021.
- 115 Siemens, *Power-to-Kerosene*|Green hydrogen for climate-neutral aviation, 2021, <https://assets.siemens-energy.com/siemens/assets/api/uuid:34bec577-f25a-48cd-8618-6dd848b38515/FactsheetWerlteEN.pdf>.
- 116 Velocys, *Velocys launches Bayou Fuels*|Velocys, Velocys, 2021.
- 117 J. Brinkman and A. Schilderman, *Synkero builds facility in the port of Amsterdam, producing sustainable aviation fuel from CO₂*, SkyNRG, 2021.
- 118 Synkero, *Synkero: Futureproof Aviation*, Synkero, 2021.
- 119 R. van Roon, *Zenid[®] Jet fuel from air*, Zenid[®], 2021, <https://zenidfuel.com/>.
- 120 INFINIUM, *InfiniumTM Enters into Strategic Alliance with Denbury for Ultra-Low Carbon Fuels Projects in Texas, Continuing Development Momentum*, Infinium, 2022.
- 121 Biofuels International, *ExxonMobil to supply SAF as part of Singapore pilot*|Biofuels International Magazine, Biofuels International, 2022.
- 122 E. Moses, *Oxy Low Carbon Ventures Selects Worley for Services Contract on Canadian Direct Air Capture (DAC)-to-Fuels Facility*, Oxy Low Carbon Ventures 2021.
- 123 Norsk e-Fuel, *COMING SOON: GREEN JET-FUEL FROM MOSJØEN, NORWAY*, Norsk e-Fuel, 2022.

