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## Recent advances of bifunctional electrocatalysts and electrolyzers for overall seawater splitting

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As a promising method for hydrogen (H<sub>2</sub>) production, seawater electrolysis has gained increasing attention as seawater is the most abundant water resource on Earth. The development of high-performance bifunctional electrocatalysts that facilitate both hydrogen evolution reaction and the oxygen evolution reaction and efficient electrolyzers are the key factors for H<sub>2</sub> production from seawater. This review endeavors to provide a comprehensive analysis of the progress and challenges associated with bifunctional electrocatalysts for seawater splitting, along with efficient electrolyzers. We start with a brief overview of the fundamental aspects, including the involved reaction mechanisms and the evaluation parameters relevant to bifunctional electrocatalysts for seawater splitting. Subsequently, recent advancements in bifunctional electrocatalysts and electrolyzers designed for overall seawater splitting are summarized and discussed. Finally, we propose perspectives for the future development of highly efficient bifunctional electrocatalysts and electrolyzers for seawater splitting.

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### 1. Introduction

As the global demand for clean energy continues to rise, hydrogen (H<sub>2</sub>) is increasingly recognized as the optimal energy option in the low-carbon era due to its high energy density of approximately 284 kJ mol<sup>-1</sup> and environmentally friendly

characteristic.<sup>1,2</sup> At present, the dominant industrial approaches to H<sub>2</sub> production, including natural gas reforming, methanol reforming, and coal gasification, pose substantial environmental challenges due to their substantial carbon dioxide (CO<sub>2</sub>) emissions and the generation of other detrimental byproducts.<sup>3–6</sup> Water electrolysis offers a promising

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alternative for green H<sub>2</sub> production. Currently, the commercial water splitting technology includes proton exchange membrane (PEM) water electrolysis and alkaline (ALK) water electrolysis, which both rely on fresh water as the electrolyte.<sup>7,8</sup> Considering the lack of fresh water, the study of seawater (about 96.5% of the world's water resource)<sup>9</sup> electrolysis is receiving increasing attention. By utilizing the abundant seawater resources and integrating with renewable energy sources, such as solar and wind power, seawater electrolysis holds significant potential in facilitating the transition to a sustainable and environmentally friendly energy landscape.<sup>10</sup> Nevertheless, the complex composition of natural seawater presents some formidable challenges when it comes to realizing large-scale industrial applications of its electrolysis process.

Seawater electrolysis faces challenges similar to electrolysis using fresh water in facilitating both hydrogen evolution reaction (HER) and oxygen evolution reaction (OER) simultaneously. HER in seawater can be hindered by impurities like dissolved cations (*e.g.*, Mg<sup>2+</sup> and Ca<sup>2+</sup>), bacteria, microorganisms, and particles that may clog or damage electrodes, reducing durability. OER faces challenges from electrochemically active anions (Cl<sup>-</sup>), which can interfere with the reaction. Interestingly, Qiao's team recently reported a positive effect of Cl<sup>-</sup> in alkaline seawater electrolysis, rather than the commonly perceived negative effect.<sup>11,12</sup> They found that the adsorption sites for Cl<sup>-</sup> on the surface of NiFe layered double hydroxide (LDH) catalysts are Fe sites rather than Ni sites. This means that Cl<sup>-</sup> can inhibit the leaching of Fe while creating more active Ni sites, thereby increasing the activity and stability of the catalyst. This is a novel and interesting point of view that provides a new perspective and idea to understand and optimize processes and catalysts for alkaline seawater electrolysis. Nevertheless, the limitation is that it only explores one specific catalyst, NiFe LDH, which may not be applicable to other types of catalysts or other ions in seawater. In general, both HER and OER reactions often suffer from limited rates and voltage requirements.<sup>13</sup> In particular, a higher voltage range of 1.8–2.0 V is required, exceeding the theoretical voltage of 1.23 V.<sup>14</sup>

In order to realize the large-scale H<sub>2</sub> production from seawater electrolysis, electrocatalysts and electrolyzers are two key factors. Most reported catalysts are used for HER<sup>15–19</sup> or OER,<sup>20–24</sup> so two different electrocatalysts must be applied in the seawater electrolysis process. If there are efficient bifunctional electrocatalysts, which have the ability to promote the reaction of HER and OER simultaneously, the overall seawater splitting process will be easier to carry out. Bifunctional catalysts not only enhance reaction rates and reduce the required voltage, but also contribute to achieving higher electrolysis efficiency, potentially reducing the cost of H<sub>2</sub> production. Meanwhile, the study of bifunctional catalysts is conducive to the exploration of novel catalytic mechanisms and principles, and provides guidance for the design and synthesis of more efficient catalysts. Therefore, the development of bifunctional catalysts with high activity and low cost is key to achieve efficient H<sub>2</sub> production from seawater.

Efficient seawater splitting also relies on the design of efficient, high-performance, and cost-effective seawater

electrolyzers. In addition to PEM and ALK electrolyzers that are more mature in the commercial market, there are anion exchange membrane electrolyzers<sup>25,26</sup> and solid oxide electrolytic cells (SOEC).<sup>27</sup> They are relatively new and costly compared to the above two technologies. However, when these electrolyzers are used directly for the seawater electrolysis, the complex natural composition of seawater significantly impacts the process, such as the physical or chemical clogging of the ion exchange membranes and corrosion of the metal components. Effectively addressing these issues is critical for the widespread adoption of seawater electrolysis technology. Research and development efforts are primarily dedicated to improving the durability of ion exchange membranes to prevent clogging and exploring alternative corrosion-resistant materials for the metal components. Moreover, exploring new materials and engineering approaches to withstand the harsh conditions inherent in seawater will facilitate improving the overall performance and durability of seawater electrolyzers. In conclusion, the selection and design of catalyst materials can influence the structure and performance of the electrolyzer. A well-planned electrolyzer design can maximize the utilization of the catalyst activity and enhance the electrolysis efficiency.

Several recent reviews have discussed the electrocatalysts for seawater splitting from different perspectives, mainly single-function OER catalysts<sup>28,29</sup> and design strategies of electrocatalysts.<sup>30,31</sup> Recently, our team completed a review covering both lab-scale fundamental research and pilot-scale reactor levels, as well as future trends in the field of seawater electrolysis.<sup>32</sup> However, there are few reviews that are particularly focused on bifunctional electrocatalysts and electrolyzers for overall seawater splitting. In this review, we begin by introducing the fundamentals of seawater electrolysis, including the principles of the reactions involved and the parameters used to evaluate the performance of bifunctional catalysts. Subsequently, we present a comprehensive overview of recently reported bifunctional catalysts for seawater splitting, focusing on their activity and stability. Common bifunctional catalysis materials for seawater electrolysis encompass noble metal-based catalysts and transition metal-based catalysts such as transition metal phosphides, borides, chalcogenides, nitrides, oxides, and hydroxides. Furthermore, we delve into recent advancements in electrolyzers, encompassing both membrane and membrane-free systems, and provide a detailed analysis of these developments. Finally, we discuss future research directions and highlight opportunities to promote the practical application of seawater electrolysis systems and technologies.

## 2. Principles of electrolytic seawater

### 2.1 Reaction mechanisms

**2.1.1 Oxygen evolution reaction.** OER occurs at the anode and is the rate-limiting step in the H<sub>2</sub> production process by water electrolysis. Specifically, OER is a four-electron transfer process with a very complex mechanism (*e.g.*, AEM or LOM),<sup>33,34</sup> and a slow kinetic reaction, resulting in a high overpotential. The reaction equations at different situations are shown in (1) and (2). Furthermore, the reaction process is depicted in Fig. 1a,

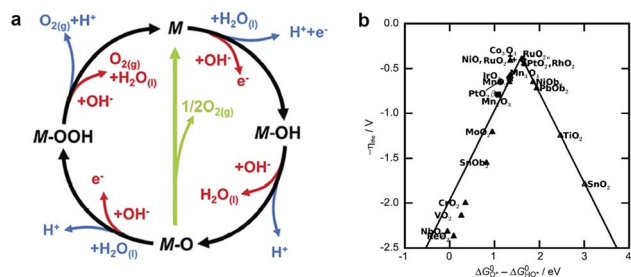
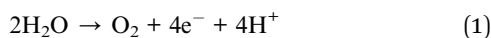


Fig. 1 (a) The mechanism of OER on an electrode surface. Reprinted with permission.<sup>35</sup> Copyright 2017, The Royal Society of Chemistry. (b) Activity trends for OER as a function of  $\Delta G_{O^*} - \Delta G_{OH^*}$  for rutile and anatase oxides. The activity is expressed by the value of the overpotential to achieve a certain value of current density. Reprinted with permission.<sup>36</sup> Copyright 2011, Wiley-VCH.

where the red and blue curves represent reactions under alkaline and acidic conditions, respectively.<sup>35</sup> Here, 'M' symbolizes the active site, while 'MOH', 'MO', and 'MOOH' represent the three active intermediates.

Acidic:



Alkaline:

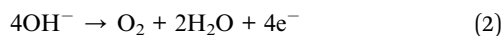


Fig. 1b compares the effectiveness of the first row of transition metal oxides as oxygen generation catalysts under acidic or alkaline conditions based on their redox properties.<sup>36</sup> The figure shows that RuO<sub>2</sub> and IrO<sub>2</sub> are the best catalysts for oxygen generation due to their low redox potentials and high electrical conductivity. However, they are costly and do not perform well in hydrogen generation reactions. Therefore, some more economical and sustainable bifunctional catalysts, such as Co

phosphates/phosphides and Ni-S composites, have been developed, which are highly active in both oxygen generation and hydrogen generation reactions and have good electrochemical stability.

**2.1.2 Hydrogen evolution reaction.** The HER occurs at the cathode, and the reaction paths are shown in Fig. 2a. Depending on the type of adsorption, HER has two reaction mechanisms, called Volmer–Heyrovsky mechanism and Volmer–Tafel mechanism.<sup>37</sup> Under different pH situations, the reaction equations are shown in (3) and (4):

Acidic:



Alkaline:



Fig. 2b shows the curve relating the logarithm of the HER exchange current density ( $\log j_0$ ) for different metals to the strength of the metal–hydrogen (M–H) bond in an acidic environment.<sup>38</sup> This volcano curve allows a quick comparison of the activity of different metals. However, this volcano curve only considers the effect of the M–H bond energy (or the properties of the metal) on the HER kinetics, and does not take into account other factors, such as the pH of the solution. Perhaps, it seems more convincing that this plot becomes a 3D volcano plot obtained with pH as the third axis.

**2.1.3 Chlorine evolution reaction (CER).** The composition of seawater is extremely complex, encompassing a high concentration of NaCl, along with other ions present in lower quantities, such as SO<sub>4</sub><sup>2-</sup> (2SO<sub>4</sub><sup>2-</sup> → S<sub>2</sub>O<sub>8</sub><sup>2-</sup> + 2e<sup>-</sup> ( $E^0 = 2.01$  V vs. SHE, pH = 0), 2SO<sub>4</sub><sup>2-</sup> → S<sub>2</sub>O<sub>8</sub><sup>2-</sup> + 2e<sup>-</sup> ( $E^0 = 2.01$  V vs. SHE, pH = 14)), Br<sup>-</sup> (2Br<sup>-</sup> → Br<sub>2</sub> + 2e<sup>-</sup> ( $E^0 = 1.09$  V vs. SHE, pH = 0)), 2Br<sup>-</sup> + 6OH<sup>-</sup> → BrO<sub>3</sub><sup>-</sup> + 3H<sub>2</sub>O + 6e<sup>-</sup> ( $E^0 = 0.61$  V vs. SHE, pH = 14)),<sup>32</sup> and more. When seawater is utilized as a raw material for

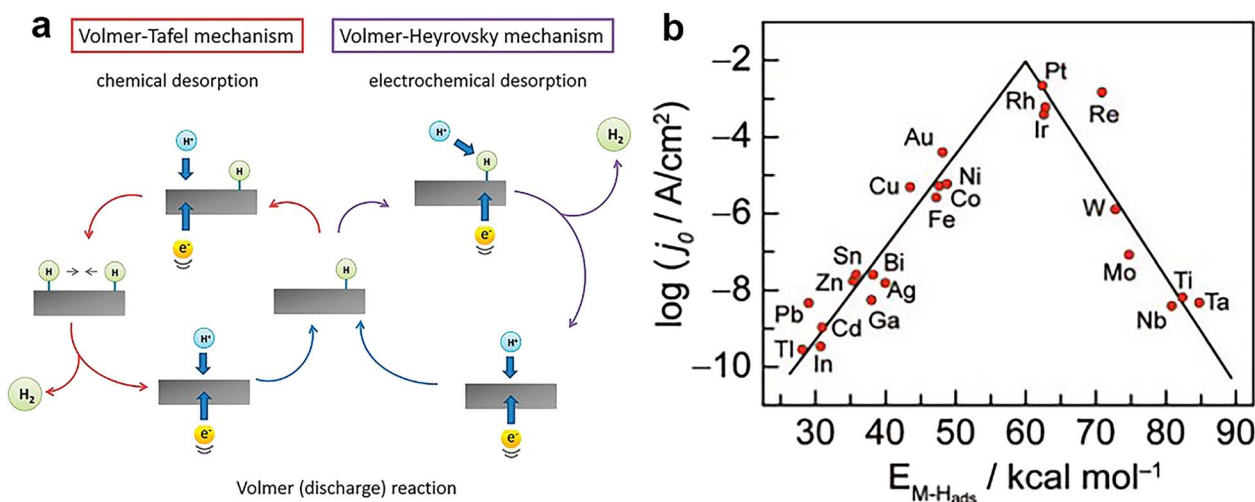


Fig. 2 (a) The mechanism of HER on the surface of an electrode in acidic solutions. Reprinted with permission.<sup>37</sup> Copyright 2014, The Royal Society of Chemistry. (b) Volcano plot for the HER on metal electrodes in acidic media. The log of the exchange current density  $j_0$  is plotted versus the M–H bond energy for each metal surface. Reprinted with permission.<sup>38</sup> Copyright 1972, Elsevier.

electrolysis, aside from the HER and OER that can occur, other ions in the seawater can also participate in the reaction. This can influence the progression of the two necessary reactions, HER and OER, within the electrolysis system. Dresp *et al.*<sup>39</sup> have conducted a comprehensive review summarizing some of the potential redox reactions that occur in seawater electrolysis. Among these reactions, CER is a strong opponent to OER. As depicted in Fig. 3a,  $\text{Cl}^-$  reacts differently at different pH conditions, and the primary reactions that occur during seawater electrolysis are the  $2\text{Cl}^- \rightarrow \text{Cl}_2 + 2\text{e}^-$  ( $E^0 = 1.36 \text{ V vs. SHE}$ ,  $\text{pH} < 3.5$ ) and  $\text{Cl}^- + 2\text{OH}^- \rightarrow \text{ClO}^- + \text{H}_2\text{O} + 2\text{e}^-$  ( $E^0 = 0.89 \text{ V vs. SHE}$ ,  $\text{pH} > 7.5$ ).<sup>40</sup> The OER is a complex process involving the transfer of four electrons, which presents kinetic challenges. Conversely, the CER only requires the participation of two electrons, providing a kinetic advantage. In other words, from

a kinetic perspective, CER is more likely to occur than OER.<sup>41</sup> In addition, the potential difference between the CER and the OER at pH values greater than 7.5 is a maximum of 480 mV. However, from the thermodynamic perspective, the anode favors the OER over the CER due to the higher overpotential required for the latter process (Fig. 3b). This distinction in electron transfer pathways highlights the diverse nature of redox reactions that can occur during the electrolysis of seawater. Understanding and characterizing these reactions will be crucial for optimizing the efficiency and overall performance of seawater electrolysis systems. In addition, the pH values near the electrode surface can fluctuate dramatically (Fig. 3c), and buffers or additives are typically employed to control pH.<sup>42</sup> Buffer solutions like 1 M KOH ( $\text{pH} = 14$ ), 0.1 M borate ( $\text{pH} = 9.2$ ), carbonate ( $\text{pH} = 8.6$ ), and 0.1 M phosphate ( $\text{pH} = 7$ ) have been attempted by various

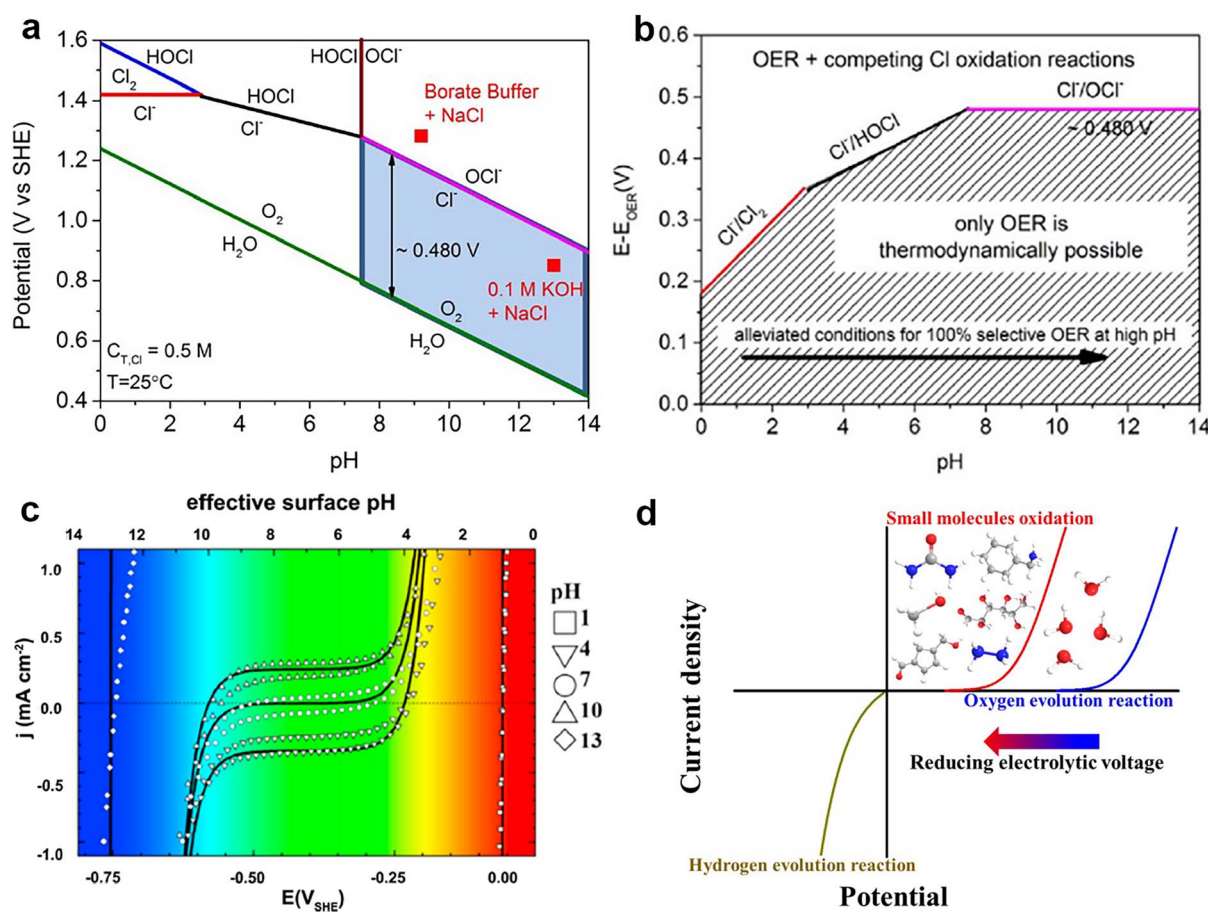


Fig. 3 (a) Pourbaix diagram for the artificial seawater model. A chlorine system, in the case of dissolved 0.5 M NaCl aqueous solution and no other chlorine sources, with a total chlorine species ( $C_{\text{T,Cl}}$ ) of 0.5 M. The electrode potential for OER is also included (assuming oxygen partial pressure of 0.21 atm = 0.021 MPa). Two red square points show the operating potentials (vs. SHE) after 1 h constant current electrolysis (10 mA  $\text{cm}^{-2}$ ) with the NiFe layered double hydroxide (NiFe LDH) catalyst in 0.1 M KOH + 0.5 M NaCl (pH 13) and 0.3 M borate buffer + 0.5 M NaCl (pH 9.2) electrolyte. The light blue box highlights our proposed design criterion. (b) The maximum allowed overpotential of the OER electrolyzer catalysts to ensure 100% selective water splitting. Values are obtained as the difference between the standard electrode potentials of the 3 relevant chloride oxidation reactions (chlorine, hypochlorous acid, and hypochlorite formation) and the OER versus pH. The dashed area corresponds to oxygen-selective overpotential–pH conditions where the thermodynamics point to 100% selective oxygen evolution. Above the limiting lines, chlorine-based reaction products are thermodynamically feasible, yet may be limited by kinetic overpotentials. Reprinted with permission.<sup>49</sup> Copyright 2016, Wiley-VCH. (c) The current density–surface pH relation obtained by cyclic voltammetry in  $\text{H}_2$ -saturated, unbuffered solutions of bulk pH 1–13. Reprinted with permission.<sup>50</sup> Copyright 2011, Elsevier. (d) Comparison of water electrolysis with the OER and with small-molecule oxidation reactions. Reprinted with permission.<sup>48</sup> Copyright 2022, Wiley-VCH.



researchers.<sup>43–47</sup> Considering the challenges of OER, some researchers hope to decouple the OER reaction and replace it with another easier anode reaction, thereby boosting H<sub>2</sub> production. Fig. 3d is a schematic diagram of the bipolar system built for electrochemical water splitting.<sup>48</sup> Obviously, HER couples a small molecule oxidation reaction that can substitute for the OER, which provides an option for reducing the working potential.

## 2.2 Evaluation parameters for catalysts

**2.2.1 Overpotential.** In the ideal state, the operating potential required for an electrochemical reaction is the equilibrium potential. However, the actual working potential in a reaction often needs to overcome the hindrance of kinetic processes and exhibits a value higher than the equivalent equilibrium potential, and the difference between them is the overpotential, which directly reflects the catalytic activity of the electrolytic reaction.<sup>51</sup> According to the Nernst equation,<sup>52</sup> the actual working potential can be expressed by eqn (5), where  $E$ ,  $E_0$ ,  $T$ ,  $R$ ,  $F$ ,  $N$ ,  $C_0$ , and  $C_R$  represent the working potential of the actual reaction, the standard potential of the reaction, absolute zero ( $-273.15$  °C), ideal gas constant ( $8.314$  J mol<sup>-1</sup> K<sup>-1</sup>), Faraday's constant ( $96\,485$  C mol<sup>-1</sup>), the number of electrons transferred in the reaction, the concentration of oxidation products, and the concentration of reduction products, respectively. Then, the overpotential can be expressed by eqn (6).

Nernst equation:

$$E = E_0 + \frac{RT}{nF} \ln \frac{C_0}{C_R} \quad (5)$$

Overpotential formula:

$$\eta = E_i - E_t \quad (6)$$

The presence of an overpotential means that more energy than thermodynamics is required to drive the related reaction. With a lower overpotential of the catalyst at the specified current density, a better catalytic ability of the catalyst for the target reaction can be achieved. For overall water splitting, the overpotential is the part of the cell voltage that is over 1.23 V vs. RHE.

**2.2.2 Tafel slope.** The Tafel slope can provide an invaluable reference for exploring reaction mechanisms, especially in elucidating the rate-determining steps and reaction pathways. For HER in alkaline situation, the theoretical Tafel slopes of 120 mV dec<sup>-1</sup>, 40 mV dec<sup>-1</sup>, and 30 mV dec<sup>-1</sup> correspond to the Volmer–Heyrovsky step, the Heyrovsky step, and the Tafel step as the rate-determining step, respectively.<sup>53</sup> To explain this parameter clearly, it is first necessary to introduce the Butler–Volmer formula<sup>54</sup> that represents the kinetic relationship in electrochemical experiments, as shown in eqn (7), where,  $i$ ,  $i_0$ ,  $n$ ,  $E$ ,  $\alpha_a$ , and  $\alpha_c$  denote the current density, exchange current density, number of electrons transferred in the reaction, the applied voltage, anode electron transfer coefficient, and cathode electron transfer coefficient, respectively. At high anode

potential situation, the current mainly comes from the anode, then eqn (7) can be simplified to eqn (8), where  $\eta$  indicates the overpotential; this is the Tafel formula. Then, the logarithm of both sides of the Tafel formula is taken, which can be changed to eqn (9), where  $b$  indicates the Tafel slope. Also,  $b$  can be expressed as eqn (10), where it can be seen that smaller Tafel slope values indicate faster kinetics and better catalytic activity of the catalyst. Basically, the smaller the value of the Tafel slope, the faster the current density increases, indicating faster kinetics and better catalytic activity of the catalyst.

Butler–Volmer formula:

$$i = \left[ \exp\left(\frac{\alpha_a n F E}{RT}\right) + \exp\left(\frac{\alpha_c n F E}{RT}\right) \right] \quad (7)$$

Tafel formula:

$$i = i_0 \exp\left(\frac{\alpha_a n F \eta}{RT}\right) \quad (8)$$

Logarithm of both sides of the Tafel formula:

$$\log(i) = \log(i_0) + \frac{\eta}{b} \quad (9)$$

Tafel slope formula:

$$b = \frac{\partial \eta}{\partial \log(i)} = \frac{2.303 RT}{\alpha F} \quad (10)$$

**2.2.3 Faraday efficiency.** The Faraday efficiency (FE) can be understood as the percentage of actual production to theoretical production. Its magnitude is influenced by temperature, electrolyte concentration, applied voltage, solution acidity and even the purity of the electrode material. The specific calculation can be seen in eqn (11), where  $m$  is the actual number of moles of product,  $n$  is the number of electrons in the reaction,  $F$  is the Faraday constant (the amount of electricity contained in one mole of electrons),  $I$  is the current, and  $t$  is the time. A good catalyst should have a high FE, and the ideal catalyst should have 100% Faraday efficiency.

$$FE = \frac{m \times n \times F}{I \times t} \quad (11)$$

**2.2.4 Stability.** The stability of a catalyst is the duration time that maintains a stable activity during the catalytic process, which means the working current density without attenuation. The longer the reaction lasts, the better the catalytic stability of the catalyst. In addition, the stability of the catalysts includes various aspects, such as chemical stability, thermal stability, anti-toxic stability, and mechanical stability. Usually, this evaluation index can be reflected by measuring the chronoamperometry (CA) and chronopotentiometry (CP) curves of different catalysts. The degree of overlap between the linear scanning voltammetry (LSV) curves before and after the stability test can also serve as an indicator of the stability quality.

**2.2.5 Turnover frequency.** Turnover frequency (TOF) is the number of catalytic reactions per unit time per active site at a given temperature, pressure, reactant ratio, and degree of reaction, and its numerical magnitude can reflect the intrinsic activity of the catalyst. Usually, it can be calculated according to eqn (12), where  $\alpha$  is the number of electrons transferred corresponding to the half-reaction that produces one molecule of the target product or consumes one molecule of the target reactant,  $N$  is the number of catalytically active sites,  $j$  is the current density at a certain state potential, and  $A$  is the working electrode area.

$$\text{TOF} = \frac{jA}{\alpha NF} \quad (12)$$

However, it is difficult to determine the number of active sites, resulting in subtle differences in the calculation of TOF for different catalytic materials. The active sites (those parts of the catalyst that really play the catalytic role, often also called active centre) differs for each catalyst. It can be an atom, a cluster of surface atoms, a coordination complex, an unsaturated atom on a solid surface or others, which makes it difficult to obtain TOF accurately. For the OER reaction, the ring current collected in the rotating ring-disk electrode (RRDE) can be used to calculate the TOF.<sup>55</sup> Also, for some single transition metal materials (Ni, Co, Fe, *etc.*) undergoing electrocatalysis and having a known number of redox-transferred electrons, the number of active sites can be determined by calculating the redox charge  $Q$  (peak area).<sup>56,57</sup> In any case, the characteristics of different materials are distinct, and the calculation of TOF should be combined with specific analysis of each work.

### 3. Seawater treatment

Seawater treatment is an important step in realizing H<sub>2</sub> production from seawater electrolysis, which can effectively remove harmful substances in seawater and improve the efficiency and selectivity of electrolysis. There are various methods for seawater treatment, which mainly include the following:

#### 3.1 Filtration

Separate solid impurities, microorganisms, organics, *etc.* from seawater by physical or chemical means, so as to reduce the contamination of electrodes and membranes. The advantages of the filtration method are simplicity and low cost, but the disadvantages are that it cannot remove calcium and magnesium ions in seawater, and it may cause clogging or depletion of filter materials. Guo *et al.*<sup>58</sup> filtered out solid impurities and removed microbes in natural seawater (pH = 7.9) before electrolysis.

#### 3.2 Alkali addition method

By adding alkaline substances such as sodium hydroxide (NaOH) and potassium hydroxide (KOH) to seawater, the pH of the seawater is raised, thus inhibiting the oxidation reaction of Cl<sup>-</sup> and increasing the generation of oxygen.<sup>59</sup> The advantages of the alkali addition method are that it can improve the

selectivity of electrolysis and has a low electrolytic voltage, but the disadvantages are that it requires high corrosion resistance of the materials used in electrolytic device and will increase the conductivity of seawater, resulting in an increase in the energy consumption of electrolysis, and may cause the waste of alkaline substances or the problem of seawater discharge.

#### 3.3 Acid addition method

By adding acidic substances, such as sulfuric acid and hydrochloric acid, to seawater, the pH value of seawater is lowered, thus inhibiting the precipitation reaction of calcium ions (Ca<sup>2+</sup>) and magnesium ions (Mg<sup>2+</sup>), and reducing the scaling of electrodes and membranes. The advantages of the acid addition method are that it can improve the efficiency of electrolysis and avoid possible CER side reactions in alkaline electrolytes, but the disadvantages are that it also requires high corrosion resistance of the materials used in electrolytic device and will increase the corrosiveness of seawater, leading to the damage of electrodes and membranes, and may cause the waste of acid or the problem of seawater discharge. However, under acidic conditions, the difference in overpotential between HER and OER is not significant.

#### 3.4 Salt addition method

Wu *et al.* used 0.68 g Na<sub>2</sub>CO<sub>3</sub> to remove Mg and Ca salts before application.<sup>46</sup> This treatment reduces deposition and corrosion problems during electrolysis and improves the efficiency of electrolysis; this also changes the pH of the seawater and increases the cost of the electrolyte, which needs to be replaced or treated regularly.

The method of seawater treatment should be selected on the basis of different electrolyzers and electrolysis conditions, while the cost and effectiveness of seawater treatment, as well as seawater monitoring and discharge issues, should also be considered. The aim of seawater treatment is to improve the feasibility and sustainability of seawater electrolysis for hydrogen production, contributing to energy and environmental development.

## 4. Bifunctional electrocatalysts for seawater splitting

So far, various kinds of catalysts have been reported to catalyze both HER and OER efficiently in alkaline electrolyte, including noble-metal-based catalysts and transition-metal-based catalysts. Some bifunctional transition-metal-based electrocatalysts have been demonstrated to be highly efficient toward HER-OER, with some even surpassing the performance of benchmark noble metal catalysts. The following sections will give a detailed discussion on their synthesis, performance, and the real active sites.

#### 4.1 Noble metal-based compounds

Platinum (Pt) is widely recognized as the benchmark catalyst for the HER, while iridium (Ir) and ruthenium (Ru) oxides are

respectively acknowledged as benchmark catalysts for the OER.<sup>60,61</sup> This implies that Pt exhibits exceptional catalytic activity in HER, whereas Ir and Ru oxides demonstrate outstanding catalytic performance in OER. Given the scarcity and high cost of precious metals, some researchers have adopted strategies to reduce the usage of these precious metals, while preserving their excellent catalytic performance. Mu *et al.*<sup>62</sup> introduced an electrocatalyst for water electrolysis known as ultralow Ru-incorporated amorphous cobalt-based oxides (Ru-CoO<sub>x</sub>/NF), which exhibited exceptional bifunctional electrocatalytic capabilities in both alkaline water and seawater environments. As a bifunctional catalyst for overall seawater splitting, it exhibited a lower overpotential of 1390 mV to achieve a current density of 1 A cm<sup>-2</sup> compared to Pt/C/NF||RuO<sub>2</sub>/NF (1530 mV) under the same conditions (Fig. 4a),

and the FE was almost 100% (Fig. 4b). According to the content of the article, the authors asserted that this catalyst's high activity can be attributed to several factors. The amorphous structure provides additional active sites and the incorporation of Ru modulates the electronic structure of cobalt-based oxides, facilitating charge transfer. Additionally, surface electronic restructuring of cobalt-based oxides and the formation of β-CoO(OH) occur during the OER process. Recently, Wu and colleagues<sup>63</sup> employed an electroless deposition technique to synthesize Ru-incorporated amorphous-crystalline Ni(Fe)P<sub>2</sub> nanosheets directly on a nickel foam substrate (Ru-Ni(Fe)P<sub>2</sub>/NF), as shown in Fig. 4c. These nanosheets were utilized as a bifunctional electrocatalyst for alkaline seawater electrolysis. In alkaline seawater, this catalyst exhibited overpotentials of 295 mV for the HER and 375 mV for the OER to attain the large

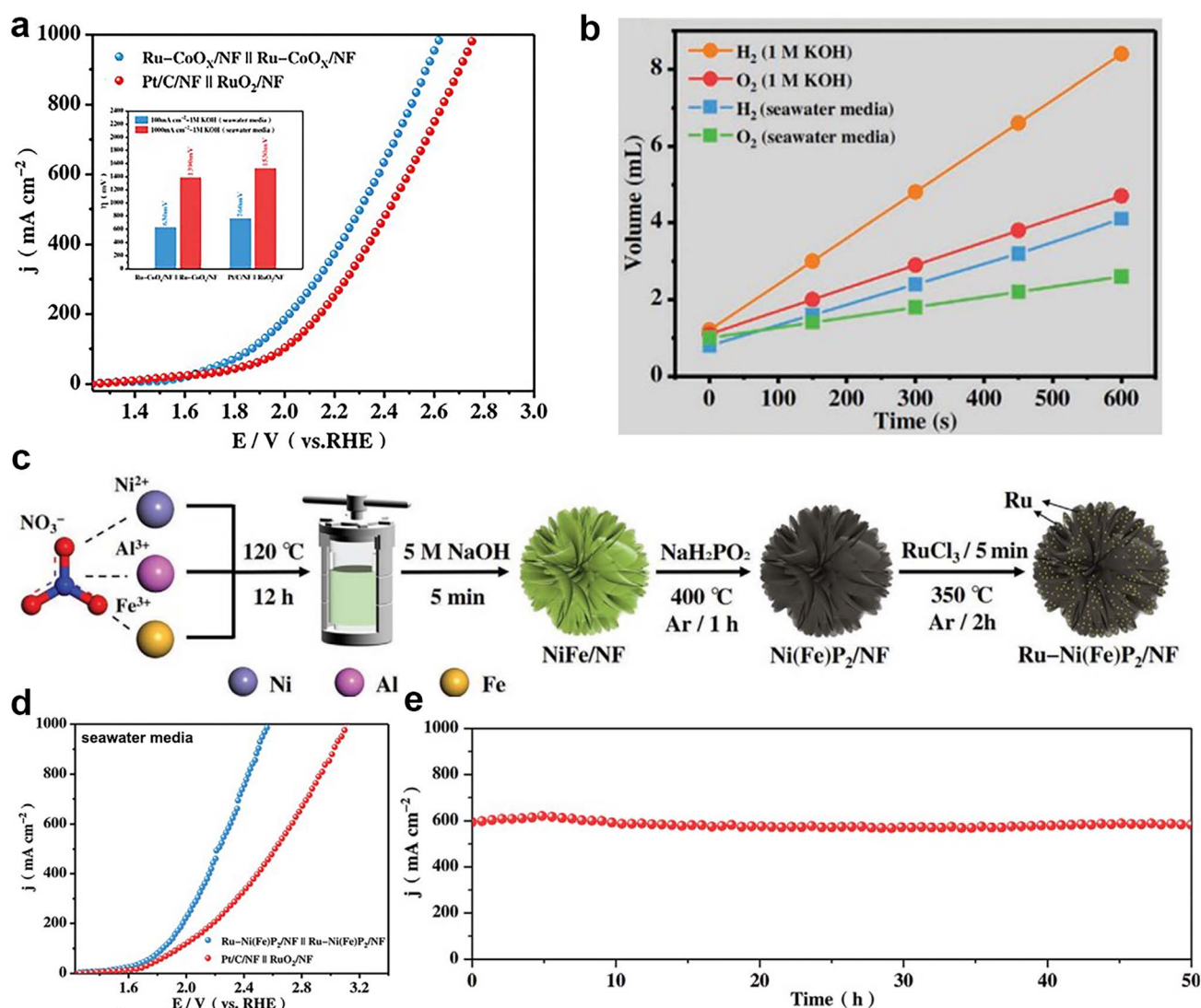


Fig. 4 (a) Polarization curves of Ru-CoO<sub>x</sub>/NF||Ru-CoO<sub>x</sub>/NF and Pt/C/NF||RuO<sub>2</sub>/NF toward overall water splitting in seawater media. Inset: the value of  $\Delta E$ . (b) Diagram of the amount of H<sub>2</sub> and O<sub>2</sub> released over time in 1 M KOH and seawater media. Reprinted with permission.<sup>62</sup> Copyright 2021, Wiley-VCH. (c) Construction route of Ru-Ni(Fe)P<sub>2</sub>/NF. (d) Polarization curves of Ru-Ni(Fe)P<sub>2</sub>/NF||Ru-Ni(Fe)P<sub>2</sub>/NF and Pt/C/NF||RuO<sub>2</sub>/NF toward water splitting in seawater media. (e) 50 h constant current stability test plot of Ru-Ni(Fe)P<sub>2</sub>/NF in seawater media. Reprinted with permission.<sup>63</sup> Copyright 2023, Wiley-VCH.

current density of  $1 \text{ A cm}^{-2}$ , surpassing the performance of commercial Pt/C and  $\text{RuO}_2$  catalysts. The assembled electrolyzer achieved the same current density at a low voltage of 1.63 V (Fig. 4d) and demonstrated remarkable stability, sustaining continuous operation at  $1 \text{ A cm}^{-2}$  for 50 hours with less than 10% reduction in performance (Fig. 4e). The unique amorphous-crystalline structure of the catalyst provided additional active sites, expanded the electrochemical active surface area, and reduced the adsorption free energy of the hydrogen-containing intermediates, resulting in enhanced HER catalytic efficiency. Additionally, the incorporation of Ru into the catalyst adjusted the electronic structure of  $\text{Ni}(\text{Fe})\text{P}_2$ , facilitating charge transfer and reducing the adsorption free energy of the oxygen-containing intermediates, thus improving the OER catalytic efficiency.

The incorporation of small amounts of noble metals to enhance the catalyst performance is regarded as an effective and practical strategy. By doping trace amounts of noble metals into cost-effective non-noble metal catalysts, catalyst performance can be effectively improved while reducing costs. This approach not only enhances the catalytic activity but also improves stability and selectivity, making it more suitable for practical applications. However, this strategy also presents several challenges. Firstly, achieving the effective and uniform dispersion of noble metals within non-noble metal catalysts for efficient utilization remains a technical challenge. Secondly, optimizing the doping concentration of noble metals for optimal performance requires further investigation. Moreover, for applications involving water electrolysis in complex media such as seawater, the impact of side reactions like chlorine evolution needs to be considered. In summary, this is a promising field worthy of further research. Through continuous refinement and improvement, an efficient, stable, and cost-effective seawater electrolysis technology is anticipated.

#### 4.2 Transition metal phosphides

Generally, transition metal phosphides have good HER properties because they can provide the appropriate electron transfer capacity, active sites, adjustable structure, and reduce energy barriers to facilitate the reduction of  $\text{H}^+$  to  $\text{H}_2$ .<sup>64</sup> At present, there are mainly monometallic phosphides and bimetallic phosphides for seawater electrolysis, of which the latter has been reported relatively more. Recently, Hao's group<sup>65</sup> deposited cobalt phosphorus-based species on a robust nickel net ( $\text{Co-P@NN}$ ) by the one-step mild electroless plating method (Fig. 5a). With different active sites including P for HER and  $\text{Co}^{2+}$  for OER, as a bifunctional catalyst,  $\text{Co-P@NN}$  required overpotentials of 298 and 235 mV to attain current densities of 500 and  $10 \text{ mA cm}^{-2}$  for HER and OER in 1 M KOH with 0.5 M NaCl solution, respectively. Moreover, the Tafel slopes of 61.5 and  $70 \text{ mV dec}^{-1}$  for HER and OER were lower than that for the Pt foil electrode ( $76.4 \text{ mV dec}^{-1}$ ) and  $\text{IrO}_2@\text{NN}$  ( $78.2 \text{ mV dec}^{-1}$ ), exhibiting faster kinetics. During the overall seawater splitting process, the two-electrode system with  $\text{Co-P@NN}$  as the anode and cathode showed better performance than Pt foil|| $\text{IrO}_2@\text{NN}$  in 1 M KOH and 0.5 M NaCl electrolyte, accompanied with ultra-

stability of 2880 h at  $500 \text{ mA cm}^{-2}$  without obvious decay (6.95%) (Fig. 5b and c). Feng *et al.*<sup>66</sup> constructed a cobalt-based catalyst rich in phosphorus vacancies (denoted as  $\text{Co}_x\text{P}_y@\text{NC}$ ). According to the paper, this bifunctional catalyst had two different active sites, including  $\text{Co}(\text{OH})_2$  coated on  $\text{Co}_x\text{P}_y$  for HER and the new formed active species of  $\text{CoO}(\text{OH})$  for OER. The introduction of the P vacancy could optimize the adsorption energy of active intermediates for HER and accelerate the reconstruction of active species for OER (Fig. 5d and e). A two-electrode system used  $\text{Co}_x\text{P}_y@\text{NC}$  as the anode and the cathode with 1.0 M KOH seawater as the electrolyte, requiring a low voltage of 1.88 V to afford  $1.0 \text{ A cm}^{-2}$  and exhibiting no significant decrease over the 100 h test. Fu *et al.*<sup>67</sup> synthesized a class of catalysts by growing robust Ni-P nanospheres on flexible corrosion-resistant hydrophobic asbestos (HA) (Fig. 5f). The Ni-P and  $\text{NiO}_x\text{H}_y$  compounds are the real catalytically-active species during the HER and OER process (Fig. 5g). During the overall seawater splitting process, the ratio of  $\text{H}_2$  to  $\text{O}_2$  produced is close to 2 : 1, meaning that the FE of this system is close to 100% (Fig. 5h). Moreover, the overall electrolysis system composed of this catalyst as the cathode and anode can work stably for 40 days at a current density of  $500 \text{ mA cm}^{-2}$  (Fig. 5i).

In addition, bimetal phosphides can improve the catalyst activity and stability through a synergistic effect of the bimetal. Ren *et al.*<sup>68</sup> reported a bifunctional catalyst  $\text{Ni}_2\text{P-Fe}_2\text{P/NF}$  with bi-active neutral P atoms for HER and Ni/Fe-oxides or -hydroxides for OER. Moreover, the self-support effect and from the alloying Ni and Fe with P atoms enhanced the stability and corrosion resistance of the catalyst. In the two-electrode system with 1 M KOH seawater electrolyte,  $\text{Ni}_2\text{P-Fe}_2\text{P/NF}$  required voltages of 1.811 V to attain a current density of  $100 \text{ mA cm}^{-2}$  for the overall seawater splitting that was superior to the benchmark of  $\text{IrO}_2||\text{Pt/C}$ , and can operate continuously for 48 h. In a recent study, Luo *et al.*<sup>69</sup> designed a high-performance bifunctional catalyst doping of Mn atoms in bimetallic compounds ( $\text{Ni}_2\text{P/Fe}_2\text{P}$ ) by a facile hydrothermal-phosphorylation method. Owing to the increased number of active sites, this catalyst exhibited excellent catalytic performance. It only needed an overpotential of 358 mV and 470 mV to drive a large current density of  $1000 \text{ mA cm}^{-2}$  for HER and OER in alkaline seawater, respectively. Moreover, the two-electrode system with it as cathode and anode required a tank voltage of 2.02 V to achieve the current density of  $500 \text{ mA cm}^{-2}$  and could operate steadily for 120 h.

Transition metal phosphides have received much attention in the study of bifunctional catalysts for the electrolysis of seawater due to their unique structures and properties. They represent an important research direction in the field of catalysts, and may play an important role in energy conversion and other related applications in the future.

#### 4.3 Transition metal oxides and hydroxides

Transition metal oxides and hydroxides have been extensively studied as catalysts for seawater splitting because of their unique advantages, including rich electronic structure,



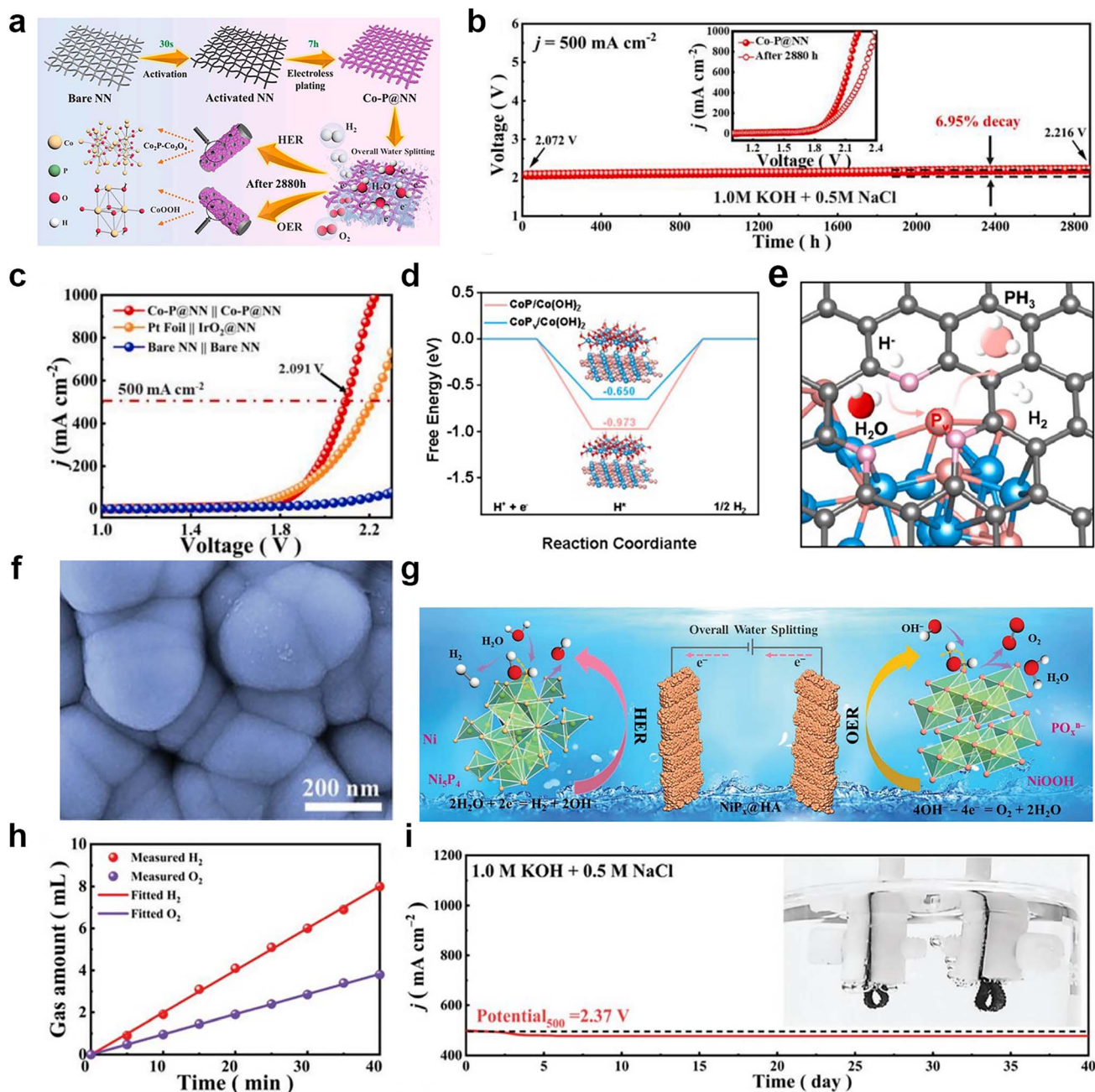


Fig. 5 (a) Illustration of the synthesis process of the Co-P@NN electrode for the overall water splitting. (b) CP response curves for the overall seawater splitting device at  $500 \text{ mA cm}^{-2}$  (inset: LSV curves of Co-P@NN||Co-P@NN before and after 2880 h overall seawater splitting). (c) LSV curves of Co-P@NN||Co-P@NN, Pt foil||IrO<sub>2</sub>@NN and bare NN||bare NN for overall seawater splitting. Reprinted with permission.<sup>65</sup> Copyright 2023, Elsevier. (d) Hydrogen evolution of CoP<sub>x</sub>/Co(OH)<sub>2</sub> and CoP/Co(OH)<sub>2</sub>. (e) Schematic illustration of P vacancies in Co<sub>x</sub>P<sub>y</sub>@NC. Reprinted with permission.<sup>66</sup> Copyright 2023, Elsevier. (f) SEM image of NiP<sub>x</sub>@HA. (g) Schematic illustration showing the HER and OER mechanisms of the NiP<sub>x</sub>@HA bifunctional electrode in alkaline simulated seawater. (h) FE curve for the NiP<sub>x</sub>@HA bifunctional electrode. (i) CP measurement of NiP<sub>x</sub>@HA||NiP<sub>x</sub>@HA at  $500 \text{ mA cm}^{-2}$  for 960 h. Reprinted with permission.<sup>67</sup> Copyright 2023, Wiley-VCH.

electrochemical activity, and low cost. Especially for OER, they can lower the energy barrier and promote the desorption of O<sub>2</sub>.<sup>70</sup> Iron oxides, nickel oxides, and cobalt oxides are the three most common of the transition metal oxide catalyst family. NiFe LDH has excellent electrocatalytic activity, especially OER. However, its stability is often unsatisfactory. In order to make it suitable for seawater splitting, Enkhtuvshin and colleagues<sup>71</sup> reported

a surface reconstructed NiFe LDH (Fig. 6a and b) by RF-plasma treatment under reducing conditions, which transformed it into a nanostructure consisting of a crystalline Ni<sub>3</sub>Fe alloy and a low-crystalline NiFe (oxy)hydroxide phase. The Ni<sub>3</sub>Fe alloy phase as a Cl<sup>-</sup> blocking layer was able to effectively inhibit the adsorption and corrosion of Cl<sup>-</sup> on the surface of NiFe LDH, thus improving the selectivity and stability of seawater

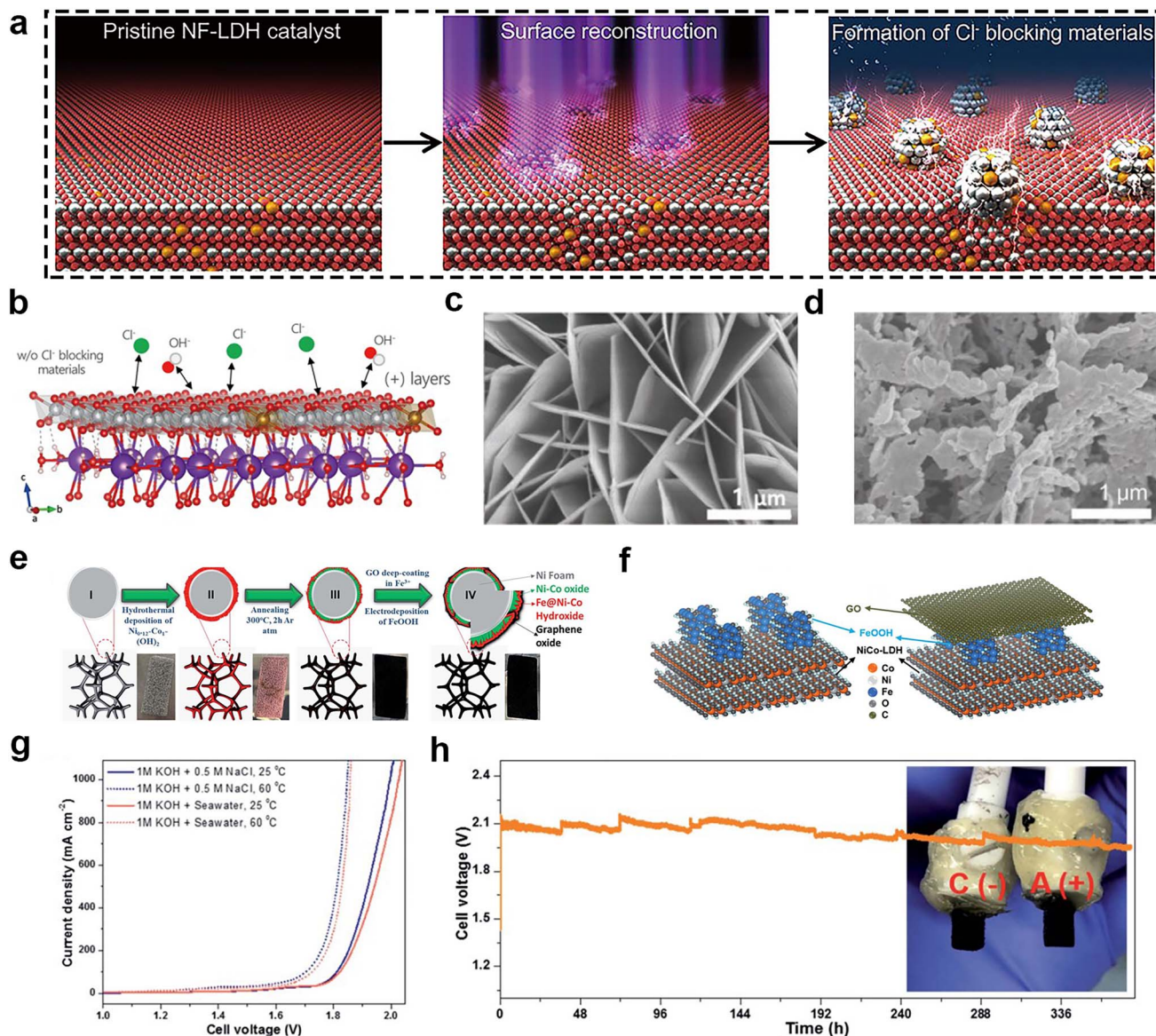


Fig. 6 (a) Schematic illustration of the surface reconstruction process of pristine NiFe LDH catalyst transforming to a mixture of NiFe (oxy)hydroxide and metallic alloy phases *via* the RF-plasma process. (b) Positively charged surface layer of  $\text{Ni}_{0.9}\text{Fe}_{0.1}(\text{OH})_2$  with intercalated potassium and water molecules. Gray, brown, red, white, purple, and green balls indicate Ni, Fe, O, H, K, and Cl atoms, respectively. SEM images of (c) pristine NF-LDH and (d) c-NF//a-NF-LDH NS. Reprinted with permission.<sup>71</sup> Copyright 2023, Wiley-VCH. (e) Schematic illustration of the synthesis procedure for a free-standing  $\text{GO@Fe@Ni-Co@NF}$  electrode with corresponding digital images of the electrode in intermediate steps [II: Ni-Co hydroxide@NF, III: Ni-Co@NF, IV:  $\text{GO@Fe@Ni-Co@NF}$ ]. (f) Model of the outermost layer structure of the  $\text{Fe@Ni-Co@NF}$  catalyst (left) and the  $\text{GO@Fe@Ni-Co@NF}$  catalyst with a GO overlayer (right). (g) Overall alkaline seawater splitting performance of the  $\text{GO@Fe@Ni-Co@NF}||\text{GO@Fe@NiCo@NF}(-)$  electrolyzer in different electrolytes and temperature. (h) Durability tests (378 h) recorded at a constant current density of  $1000 \text{ mA cm}^{-2}$  of the seawater splitting electrolyzer under  $1 \text{ M KOH} + 0.5 \text{ M NaCl}$  (inset images; a digital photograph of anode and cathode after 378 h of seawater splitting testing under  $1 \text{ M KOH} + 0.5 \text{ M NaCl}$ ). Reprinted with permission.<sup>73</sup> Copyright 2023, The Royal Society of Chemistry.

electrolysis. Meanwhile, the NiFe alloy had efficient reduction reaction (HER) activity, while the NiFe (oxy)hydroxide phase was responsible for the oxidation reaction (OER) activity, realizing the bifunctional catalysis. This material has the structure of nanosheets that is beneficial for catalytic activity (Fig. 6c and d). According to the data, this bifunctional catalyst could steadily work for 100 h at current density of  $100 \text{ mA cm}^{-2}$  in concentrated alkaline solution (30 wt% KOH and 0.5 M NaCl) during

overall water splitting. Our group also had found that benzoate anions-intercalated NiFe LDH nanosheet on carbon cloth could enhance the stability during the process of alkaline seawater electrolysis.<sup>72</sup>

Moreover, it is also possible to design a catalyst with different components in which an oxide can act as a resistance barrier to chloride ions. For instance, in order to deal with the challenge caused by  $\text{Cl}^-$ , Lee's group<sup>73</sup> proposed a method of



using an interfacial  $\text{Cl}^-$  blocking layer on the catalyst surface. They reported an active material in which FeOOH deposited  $\beta$ -Ni-Co hydroxide with an outer graphene oxide (GO) layer. This catalyst had a multilayer structure (Fig. 6e and f). The GO layer formed nanochannels (0.3–0.7 nm), acting as a sieve to block the ions movement of  $\text{Cl}^-$  and  $\text{Na}^+$  and allow  $\text{HO}^-$  and  $\text{H}_2$  gas penetration. The *o*-tolidine test suggested that there was no chloride oxidation product after 378 h during the stability test (Fig. 6h), which means this catalyst had great selectivity. Moreover, the metal oxide layer underneath helped to lower the charge transfer resistance of the catalyst. Using it as the anode and the cathode to form the alkaline seawater electrolyzer, a large current density of  $1000 \text{ mA cm}^{-2}$  was driven at a low voltage of 2.02 during the overall seawater splitting (Fig. 6g).

Both anion electrostatic repulsion and catalyst surface reconstruction to form a chloride ion barrier are effective response strategies to the OER challenge (CER). The efficiency

and stability of seawater electrolysis can be significantly improved by changing the surface structure and composition of the catalyst. These provide the possibility of developing new and more efficient technologies for seawater electrolysis.

#### 4.4 Transition metal chalcogenides

As mentioned before, the CER competes with the OER, so the design of catalysts applied to seawater electrolysis must take this into account. Recently, based on CoFe LDH with good performance for OER, Zhang's group<sup>74</sup> designed a bifunctional catalyst by partial selenization (Se-CoFe-LDH), as shown in Fig. 7a. This article argued that the introduction of Se during electrolysis can create an ionic aggregation state around the electrodes (selenate), thus achieving resistance to  $\text{Cl}^-$ . The introduction of selenium atoms does not usually act as active sites for the catalyst. Rather, it is used to modify the internal structure of the precursor, thereby increasing the active surface

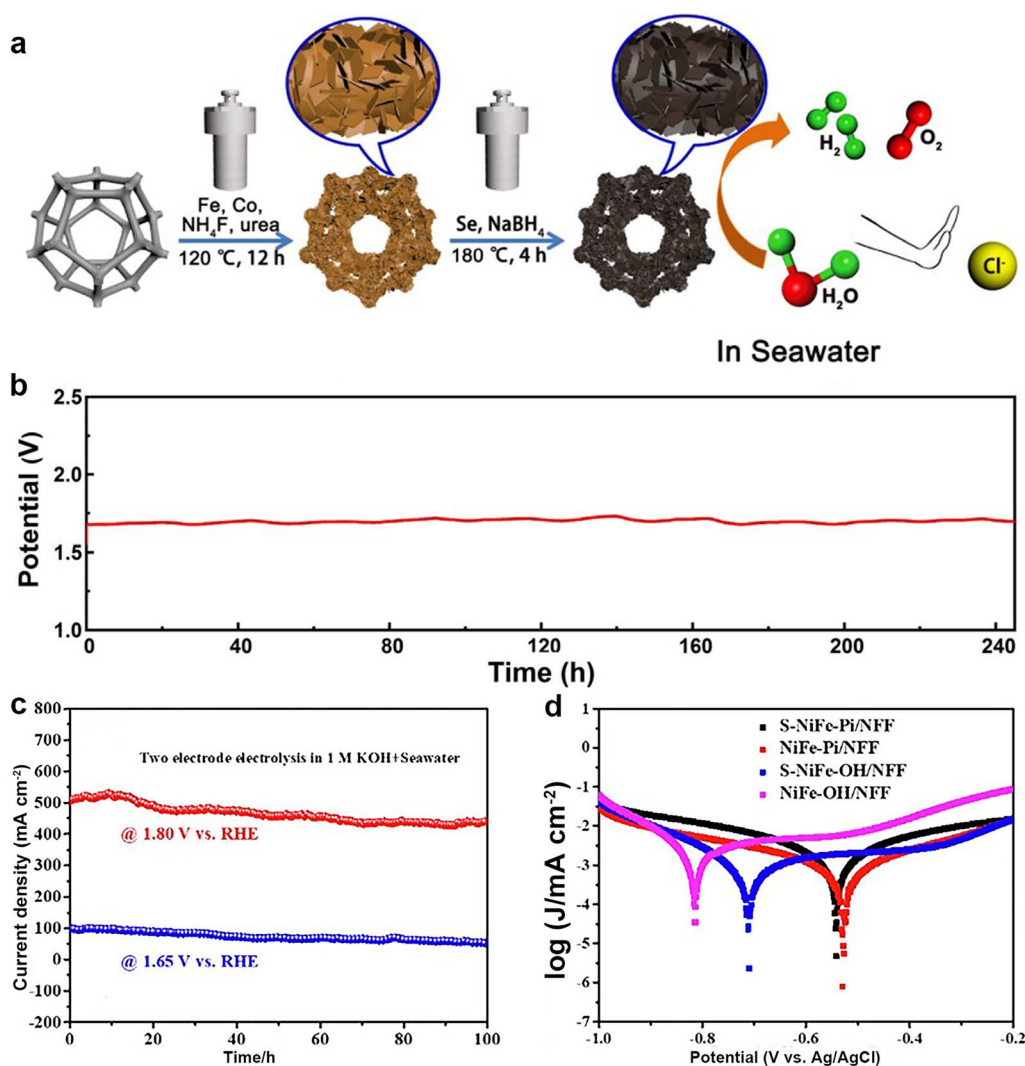


Fig. 7 (a) Schematic illustration of the synthetic process and seawater electrolysis of Se-FeCo-LDH. (b) The stability test (at  $10 \text{ mA cm}^{-2}$ ) of alkaline seawater splitting for 245 h. Reprinted with permission.<sup>74</sup> Copyright 2023, Elsevier. (c)  $I-t$  curves of the S-NiFe-Pi/NFF electrolyzer at a constant voltage of 1.68 and 1.80 V for overall seawater electrolysis, respectively. (d) Corrosion polarization curve in pure natural seawater. Reprinted with permission.<sup>76</sup> Copyright 2023, Elsevier.

area, and ultimately enhancing the activity of the catalyst. According to the data, this catalyst both as the anode and the cathode for overall seawater splitting could work for 245 h steadily (Fig. 7b). However, its true active sites were the oxides/(oxy)hydroxides of Fe and Co.

As a homologous element, sulfur also has the same properties as selenium. Tanveer ul Haq and Yousef Haik<sup>75</sup> found that the introduced S enhanced the hydrophilicity aerophobicity and ECSA of the free-standing electrode material. Song and coworkers<sup>76</sup> reported a bifunctional catalyst denoted as S–NiFe–Pi/NFF for overall seawater splitting. They found that the doping of the S atom distorted the lattice of NiFe–phosphate and regulated the local electronic environment around the Ni/Fe active metal, which enhanced the electrocatalytic activity. As a result, S–NiFe–Pi/NFF||S–NiFe–Pi/NFF required voltage of 1.8 V to attain a large current density of 500 mA cm<sup>−2</sup> and could continuously work for 100 h (Fig. 7d) because the phosphate groups repelled Cl<sup>−</sup>. The values of the corrosion potential and corrosion current also reflect the reason for good stability. As shown in Fig. 7d, S–NiFe–Pi/NFF had higher corrosion potential and lower corrosion current, meaning that it has better resistance to seawater corrosion. Furthermore, a nickel–iron sulfide nanosheet array on nickel foam (NiFeS/NF)<sup>77</sup> was a superb bifunctional catalyst for seawater splitting that had been proven by our group. Thus, NiFeS/NF can drive the industrially demanded current density of 500 mA cm<sup>−2</sup> at overpotentials of 300 and 347 mV cm<sup>−2</sup> for HER and OER in alkaline seawater. Additionally, our group reported a bifunctional catalyst Fe–NiS/NF,<sup>78</sup> which could attain a current density of 1000 mA cm<sup>−2</sup> at 1.88 V during the overall seawater splitting.

According to these reported literature studies, the role of S is not as a true active site. However, it is worth noting that as the electrolysis process proceeds, sulfur or selenium being an anion is electronegative with Cl<sup>−</sup> and appears to be more suitable for real seawater in terms of chlorine corrosion resistance. Also, S could combine with Mg<sup>2+</sup> and Ca<sup>2+</sup> to solve the problem of HER caused by the complexity of seawater.<sup>79</sup>

#### 4.5 Transition metal borides

Transition metal borides can be used as electrocatalysts for the OER and HER to produce high-purity H<sub>2</sub> and O<sub>2</sub>. There are more than 100 different crystalline phases of transition metal borides, in which the boron atoms can exhibit a rich variety of covalent bonding modes, affecting the electronic structure and catalytic activity.<sup>80</sup> There have also been a lot of reports written about it. For instance, Mandavkar and coworkers<sup>81</sup> reported on a ternary nickel–molybdenum–boron (NiMoB) electrocatalyst with multi-sphere morphology (Fig. 8a), which was fabricated by the incorporation of B atoms into the NiMo system. The B atoms boosted the catalytic property by modifying the electronic structure to lower the kinetic barriers with the electron enriched metallic sites and improving the stability of electrodes. As a bifunctional catalyst, the two-electrode system using NiMoB as the anode and the cathode could be applied to a variety of environments, *i.e.*, 1 M KOH (pH ~ 14), 0.5 M H<sub>2</sub>SO<sub>4</sub> (pH ~ 1), 1 M phosphate-buffered saline (pH ~ 7), 1 M KOH + seawater,

1 M KOH + river water, and 6 M KOH at 60 °C, as shown in Fig. 8b. However, the stability of the two-electrode system used in those different solutions was not desirable, which hindered its practical application. In contrast, Fan *et al.*<sup>82</sup> reported that amorphous CoB was successfully “interspersed” on MOF-based CC *via* mild one-step and electroless plating. The stability performance was better than that of NiMoB, and the catalyst has a nanosheet structure (Fig. 8c). This bifunctional catalyst has different active sites for HER and OER. The XPS results showed that the boron oxides (BO<sub>x</sub>) with the “chimney effect” were beneficial to the HER, and the Co atoms on the surface oxidized to CoO(OH) were beneficial for OER. Moreover, the electrochemical tests suggested that it required low overpotentials of 266 and 423 mV for HER and OER to attain the large current density of 500 mA cm<sup>−2</sup> in simulated seawater (1 M KOH + 0.5 M NaCl), and could steadily run for about 2500 h during the overall seawater splitting process (Fig. 8d). Transition metal borides have other morphologies, such as those shown in Fig. 8e,<sup>83</sup> Fig. 8f,<sup>84</sup> and Fig. 8g.<sup>85</sup>

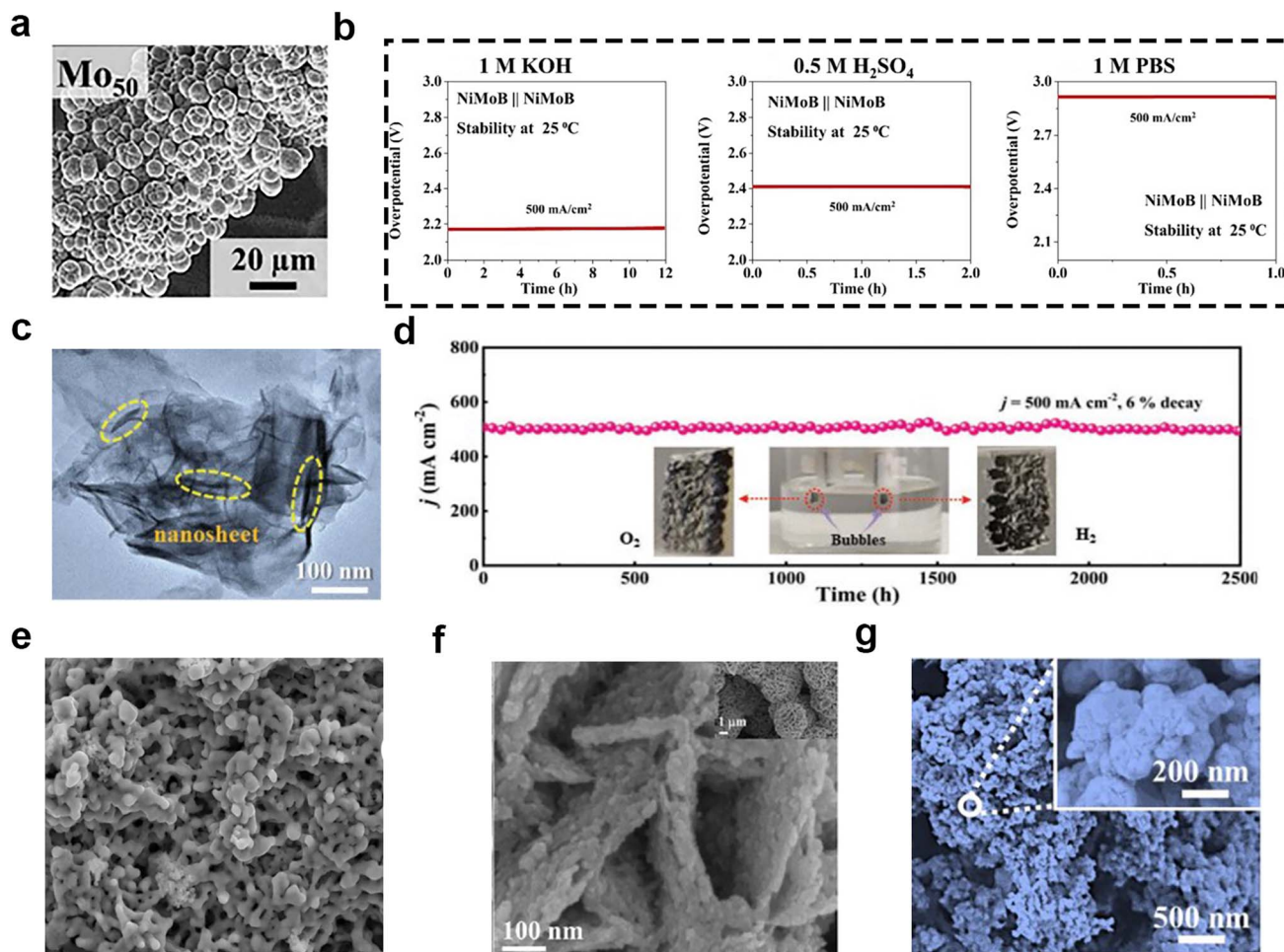
Transition metal borides show excellent HER and OER activities. However, in practical applications, higher energy inputs may be required, which may increase the overall energy costs and efficiency issues. Although some transition metal borides show good stability, our understanding of these catalysts may be incomplete; for example, how it responds to HER and OER challenges. Seawater is a very complex electrolyte, so more research may be needed to fully understand and optimize the performance of these catalysts.

#### 4.6 Transition metal nitrides

Transition metal nitrides (TMNs) are a class of two-dimensional materials that exhibit high conductivity, high catalytic activity, and high catalytic stability.<sup>86</sup> These characteristics endow them with a wide range of applications in electrocatalytic energy conversion. The formation of TMNs results in a narrower d-band filled state and a wider unfilled state of the metal, which results in the electronic structure of the TMNs being similar to that of the noble metal and improves the rate of the electrocatalytic reaction. For the HER, the change of the electronic states on the surface of the TMNs brings the Gibbs free energy of adsorbed hydrogen closer to zero, which improves the catalytic activity. For the OER, the metal bonding in the TMNs improves the electrical conductivity and accelerates the electron transport, thus increasing the catalytic activity.<sup>87</sup> Although TMNs show good activity in HER or OER, the activity remains limited when used as bifunctional catalysts. In order to construct efficient bifunctional catalysts, an effective strategy is to selectively couple materials with HER activity and OER activity into a heterogeneous structure, which results in the formation of new active sites to achieve the simultaneous promotion of HER and OER to realize total hydrolysis.

Wang *et al.*<sup>88</sup> synthesized a cobalt molybdenum nitride supported on nitrogen-doped carbon nanosheets catalyst (MoN–Co<sub>2</sub>N) using a metal–organic framework (ZIF-67) template (Fig. 9a), which consisted of cobalt molybdenum nitride with HER activity and nitrogen-doped carbon





**Fig. 8** (a) SEM image of the NiMoB electrode, where Mo<sub>50</sub> indicates 50% of Mo and 50% Ni. (b) Two-electrode stability in 1 M KOH, 0.5 M H<sub>2</sub>SO<sub>4</sub> and 1 M PBS at 500 mA cm<sup>-2</sup>. Reprinted with permission.<sup>81</sup> Copyright 2022, Elsevier. (c) High-resolution TEM image of the CoB@MOF@CC electrode. (d) Chronopotentiometry curve (*V*-*t*) of CoB@MOF@CC for overall water splitting at 500 mA cm<sup>-2</sup> (inset: photograph of CoB@MOF@CC for overall water splitting). Reprinted with permission.<sup>82</sup> Copyright 2022, Wiley-VCH. (e) SEM image of the crystalline Co<sub>2</sub>B\* catalyst. Reprinted with permission.<sup>83</sup> Copyright 2023, Wiley-VCH. (f) SEM images of Co-Mo-B/CoMoO<sub>4-x</sub>/CF; the insets show the morphology at low magnifications. Reprinted with permission.<sup>84</sup> Copyright 2021, The Royal Society of Chemistry. (g) SEM image of Fe-B-O@FeB<sub>x</sub>/HC. Reprinted with permission.<sup>85</sup> Copyright 2023, Elsevier.

nanosheets with OER activity, creating new active sites and enhancing the catalytic efficiency of alkaline seawater electrolysis. During its use as the anode and cathode to assemble the two-electrode system for overall seawater splitting, it required 1.70 V to attain the current density of 100 mA cm<sup>-2</sup> (Fig. 9b) and could steadily operate over 62 h. They found the introduction of molybdenum facilitates the performance of HER and OER (Fig. 9c and d). Ojha's team<sup>89</sup> reported a bifunctional catalyst: Ni<sub>3</sub>N and Fe<sub>3</sub>N nanoparticles encapsulated in a nitrogen-doped carbon (NC) layer were prepared by a one-pot method under ambient conditions using polyacryloylhydrazine (PAHz) as a reductant and encapsulant, followed by high-temperature treatment under nitrogen ambient to obtain Ni<sub>3</sub>N and Fe<sub>3</sub>N nanoparticles. The NC-Ni<sub>3</sub>N and NC-Fe<sub>3</sub>N nanocomplexes were coated on the surface of nickel foam (NF), on which a FeOOH layer was grown to form a FeOOH-NC-Ni<sub>3</sub>N/Fe<sub>3</sub>N heterostructure electrode (Fig. 9e). The results showed that the

presence of metal nitrides improved the conductivity and charge transfer ability of the electrodes, which reduced the overpotentials for the OER and HER (Fig. 9f). In particular, the efficiency of the OER and HER increased when the content of Ni<sub>3</sub>N is increased.

These works make use of heterogeneous structures to improve the performance of the catalysts, whereby the kinetic and thermodynamic properties of the reaction can be optimized by forming interfaces between different materials. This is an effective strategy for designing bifunctional catalysts by combining components that can act on HER and OER separately.

#### 4.7 Other compounds

Increasing the number of active sites and improving the intrinsic activity of the catalyst are two effective methods to enhance the electrocatalytic performance of catalytic materials.

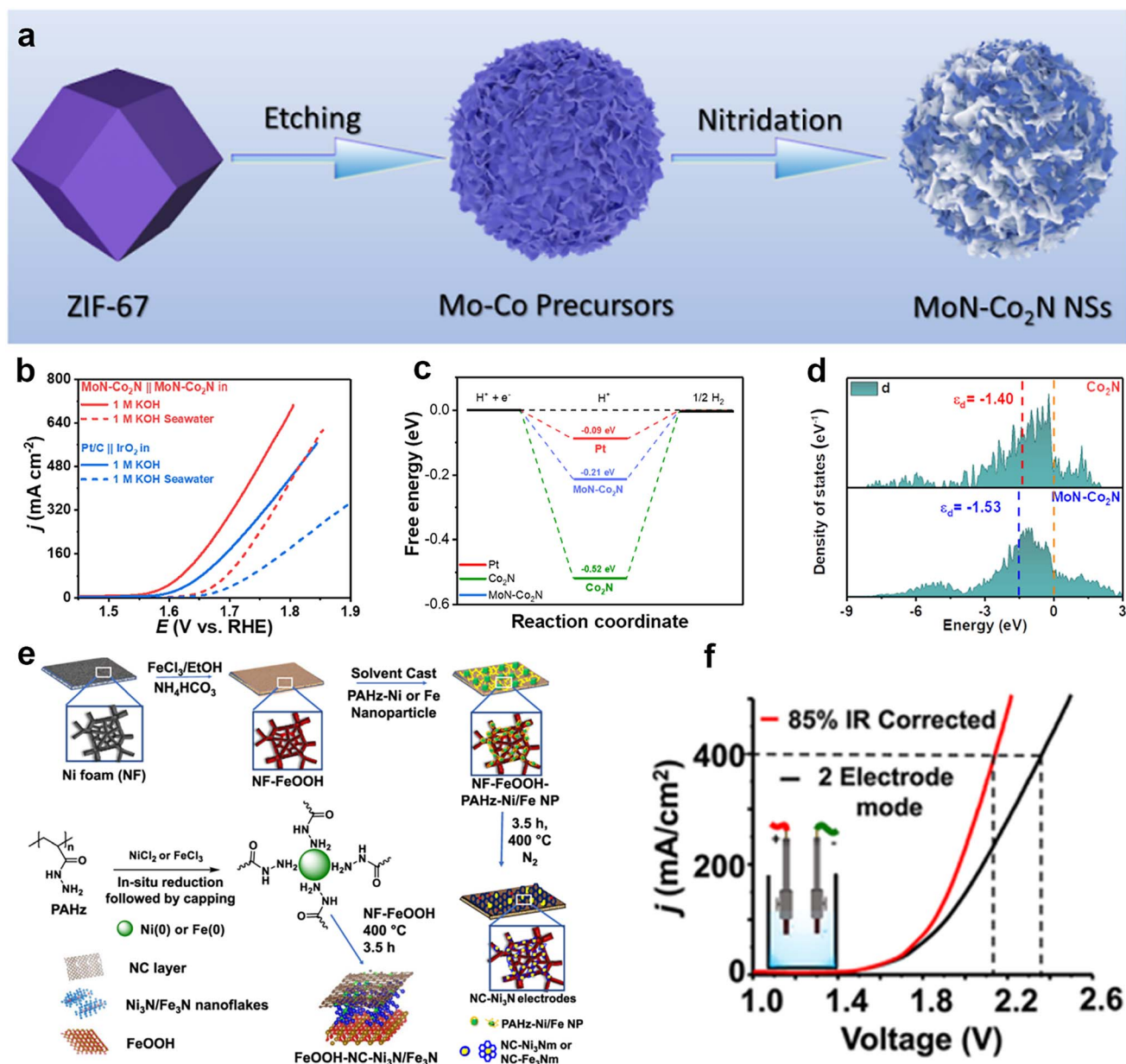


Fig. 9 (a) Schematic illustration of the synthesis of MoN-Co<sub>2</sub>N nanosheets. (b) Overall water/seawater splitting performance of MoN-Co<sub>2</sub>N/NF||MoN-Co<sub>2</sub>N/NF and Pt/C||IrO<sub>2</sub> pair in 1 M KOH and 1 M KOH seawater. (c) Calculated free energy diagram of H\* adsorption on the surface of Pt, Co<sub>2</sub>N, and MoN-Co<sub>2</sub>N. (d) The d-band centers of Co 3d partial DOS for Co<sub>2</sub>N and MoN-Co<sub>2</sub>N. Reprinted with permission.<sup>88</sup> Copyright 2022, American Chemical Society. (e) Schematics showing the FeOOH coating of the NF, followed by the *in situ* growth of the NC-Ni<sub>3</sub>N or NC-Fe<sub>3</sub>N nanocomposite layer and synthesis of PAHz-Ni/Fe nanoparticles, followed by NC-Ni<sub>3</sub>N/Fe<sub>3</sub>N nanocomposite. (f) IR-uncorrected and corrected LSV traces of NC-Ni<sub>3</sub>N<sub>21</sub> recorded under two-electrode mode in seawater possessing 2 M KOH. Reprinted with permission.<sup>89</sup> Copyright 2023, American Chemical Society.

As the size of the nanoparticles decreases, the number of atoms exposed on the surface usually increases, resulting in changes in the atomic structure of the surface, the electronic structure and the surface defects. The number of ligand-unsaturated atoms can increase as the size of the particle decreases, thus improving the catalytic activity. Single-atom catalysts (SACs) have been promising candidates for bifunctional catalysts for seawater splitting. Recently, Feng *et al.*<sup>90</sup> reported a bifunctional catalyst for efficient water/seawater splitting, which consisted of

Ru single atoms stabilized by flower-like amorphous MoO<sub>3-x</sub> nanoflakes (Fig. 10a-d). The catalyst exhibited excellent activity and stability for both HER and OER in alkaline media (Fig. 10e and f), and achieved low voltage and high yield for overall water/seawater splitting. The high performance was attributed to the large surface area and abundant active sites of the amorphous structure, as well as the efficient utilization and synergistic effect of Ru single atoms. They successfully stabilized single-atom Ru on an amorphous MoO<sub>3-x</sub> substrate, harnessing the

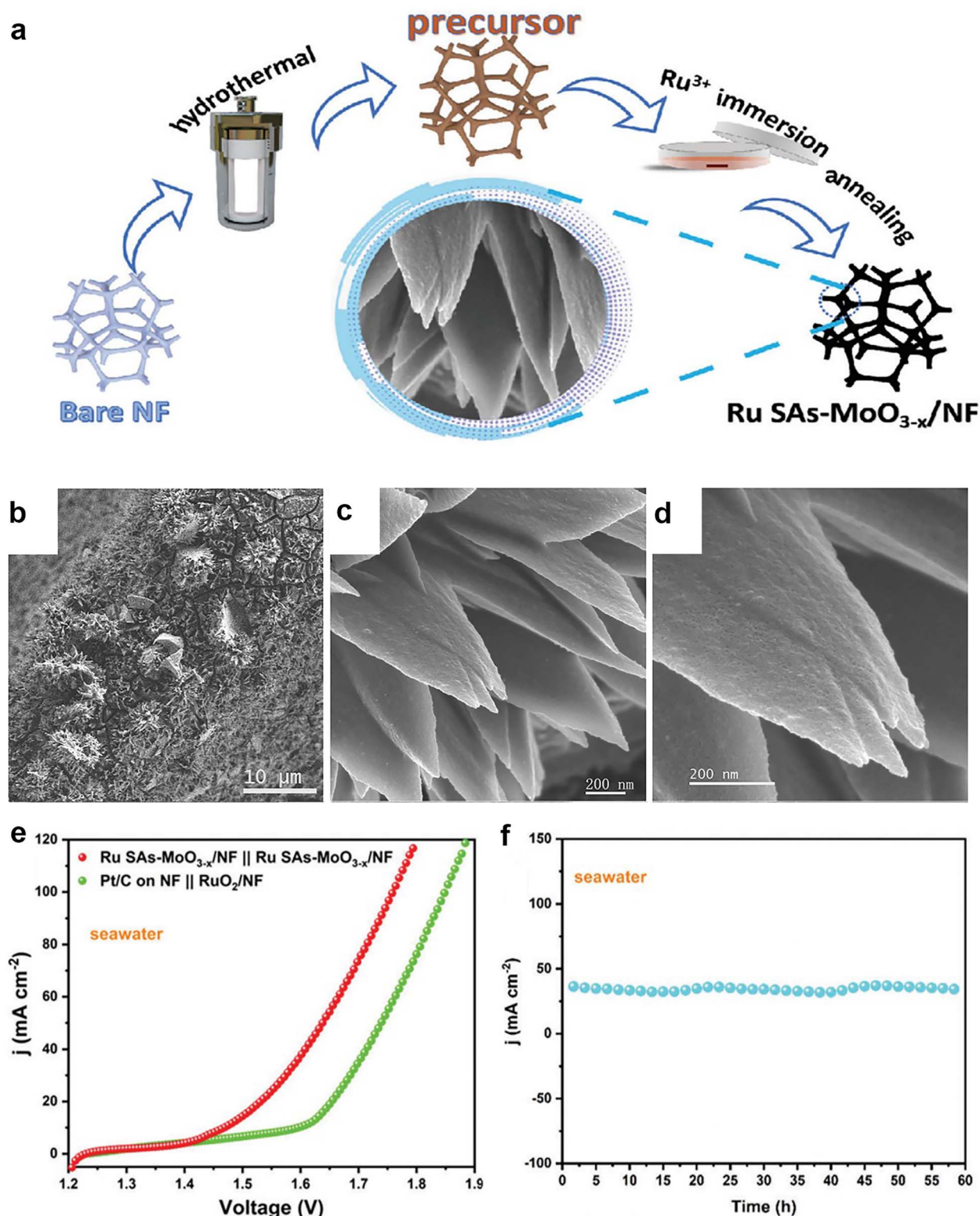


Fig. 10 (a) Schematic illustration for the fabrication of Ru SAs-MoO<sub>3-x</sub>/NF. (b-d) FESEM images of Ru SAs-MoO<sub>3-x</sub>/NF. (e) Polarization curves of the Ru SAs-MoO<sub>3-x</sub>/NF||Ru SAs-MoO<sub>3-x</sub>/NF couple and commercial catalyst couple toward overall water splitting in alkaline seawater media. (f) Stability test of the Ru SAs-MoO<sub>3-x</sub>/NF||Ru SAs-MoO<sub>3-x</sub>/NF couple in alkaline seawater media. Reprinted with permission.<sup>90</sup> Copyright 2023, Wiley-VCH.



advantages of the amorphous matrix to enhance both the performance and stability of the catalyst.

Single-atom catalysts offer the highest degree of atomic efficiency, leveraging unique quantum size effects and tailor-made active sites to significantly enhance the catalytic activity and selectivity. This presents a novel avenue for the development of cost-effective catalysts. Furthermore, the amorphous matrix, characterized by its distinct structure and properties, offers the advantage of additional active sites and oxygen vacancies. This feature proves advantageous in enhancing the catalyst's conductivity and reaction kinetics. It introduces a novel avenue for designing highly efficient catalysts.

## 5. Electrolyzers design

In addition to the development of bifunctional catalysts, the design of the efficient electrolyzer also served as a pivotal factor in increasing the seawater electrolysis efficiency, and achieving the sustainable, cost-effective production of H<sub>2</sub> from seawater. At present, there are two ways to achieve H<sub>2</sub> production from seawater, including direct and indirect seawater electrolysis. They differ in that indirect seawater electrolysis adds an extra step of desalination. After desalination, seawater splitting is equivalent to freshwater electrolysis, which is already in used industry. As mentioned for ALK and PEM, they are relatively mature in freshwater electrolysis applications, while SOCE is still in the laboratory stage. A comprehensive comparison of these three electrolysis techniques is shown in Table 1. However, it is relatively difficult to use these electrolyzers directly for seawater electrolysis, so it is necessary to make corresponding improvements on their basis. Park and his group<sup>91</sup> proposed a different

type electrolyser coupled with anion exchange membranes, cation exchange membranes (CEM) and bipolar membranes (BPMs), as shown in Fig. 11a. Anion exchange membranes and CEM could achieve unidirectional transport of Cl<sup>-</sup> and Na<sup>+</sup> to attain the purpose of desalination of brine. And the BPMs could continual supply OH<sup>-</sup> and H<sup>+</sup> to maintain the pH of anolyte (pH ~ 14) and catholyte (pH ~ 0.5), which was beneficial for reducing the overpotential of OER. Coupling NiFe LDH as the anode and NiMo as the cathode, this electrolysis system could achieve the FE above 95% for O<sub>2</sub> and H<sub>2</sub> production at a current density of 100 mA cm<sup>-2</sup> over 20 h. Meanwhile, the direct seawater splitting has two types of electrolyzers, including membrane electrolyzers and membrane-free electrolyzers. In the following presentation, we collect the most recent developments in electrolyzer design for direct seawater splitting.

### 5.1 Membrane electrolyzer

As mentioned before, seawater has many complex compositions, which caused difficulties for direct seawater electrolysis. At present, there are several main strategies to deal with this problem. Firstly, the use of asymmetric electrolyzers means that the anode and cathode chambers have different electrolytic media. In 2020, Strasser *et al.*<sup>95</sup> proposed the concept of asymmetric electrolyzers. They systematically studied six different feeding methods (Fig. 11b) to demonstrate the promise for direct seawater splitting. Recently, Li's<sup>96</sup> team designed a pH asymmetric electrolyzer containing a sodium ion exchange membrane for direct seawater electrolysis (Fig. 11c), which prevented both chloride corrosion and calcium/magnesium ion precipitation problems and captured the chemical potential between the different electrolytes, thus reducing the required

Table 1 Comparison of three technologies for water electrolysis<sup>32,92–94</sup>

| Type   | ALK  | PEM  | SOEC  |
|--|--|--|---|
| Electrolyte used   | 20–40 wt% KOH (aqueous)  | Perfluorinated sulfonic acid (PFSA)                  | Ytria-stabilized zirconia (YSZ)<br>Sc <sub>2</sub> O <sub>3</sub> -ZrO <sub>2</sub><br>MgO-ZrO <sub>2</sub><br>CaO-ZrO <sub>2</sub> |
| Current density (conventional, A cm <sup>-2</sup> )        | 0.2–0.6  | 0.0–3.0 (up to 20)                                   | 0.0–2.0   |
| Cell voltage (V)   | 1.8–2.4  | 1.8–2.2  | 0.95–1.3  |
| Operating temperature (°C)                                 | 60–90  | 70–80  | 600–1000  |
| Hydrogen production purity                                 | >99.8%   | >99.99%  | —   |
| Electrolyte quality requirements                           | Stabilized power supply  | Stabilized power supply                              | Stabilized power supply   |
| Dynamic responsiveness                                     | Relatively strong  | Stronger   | Weaker  |
| Lifetime (h)   | 60 000–90 000  | 30 000–90 000  | 10 000–30 000   |
| Maintainability  | Strong alkali corrosion, low cost  | Non-corrosive media; low cost                        | —   |
| Technology maturity level                                  | Commercialization stage  | Preliminary commercialization                        | Lab-stage   |
| Operating pressure (bar)                                   | 10–30  | 20–50  | 1–15  |
| System efficiency (%)                                      | 60–75  | 70–90  | 85–100  |
| Energy consumption (kW h N <sup>-1</sup> m <sup>-3</sup> ) | 4.5–5.5  | 3.8–5.0  | 2.6–3.6   |
| Advantages   | Mature technology, low cost  | Good renewable energy applicability                  | High conversion efficiency  |
| Disadvantage   | Low energy efficiency; weak applicability to intermittent energy sources; high operation and maintenance costs | Requires high purity water, precious metal catalysts | Requires high temperature; poor durability; easy to deteriorate   |



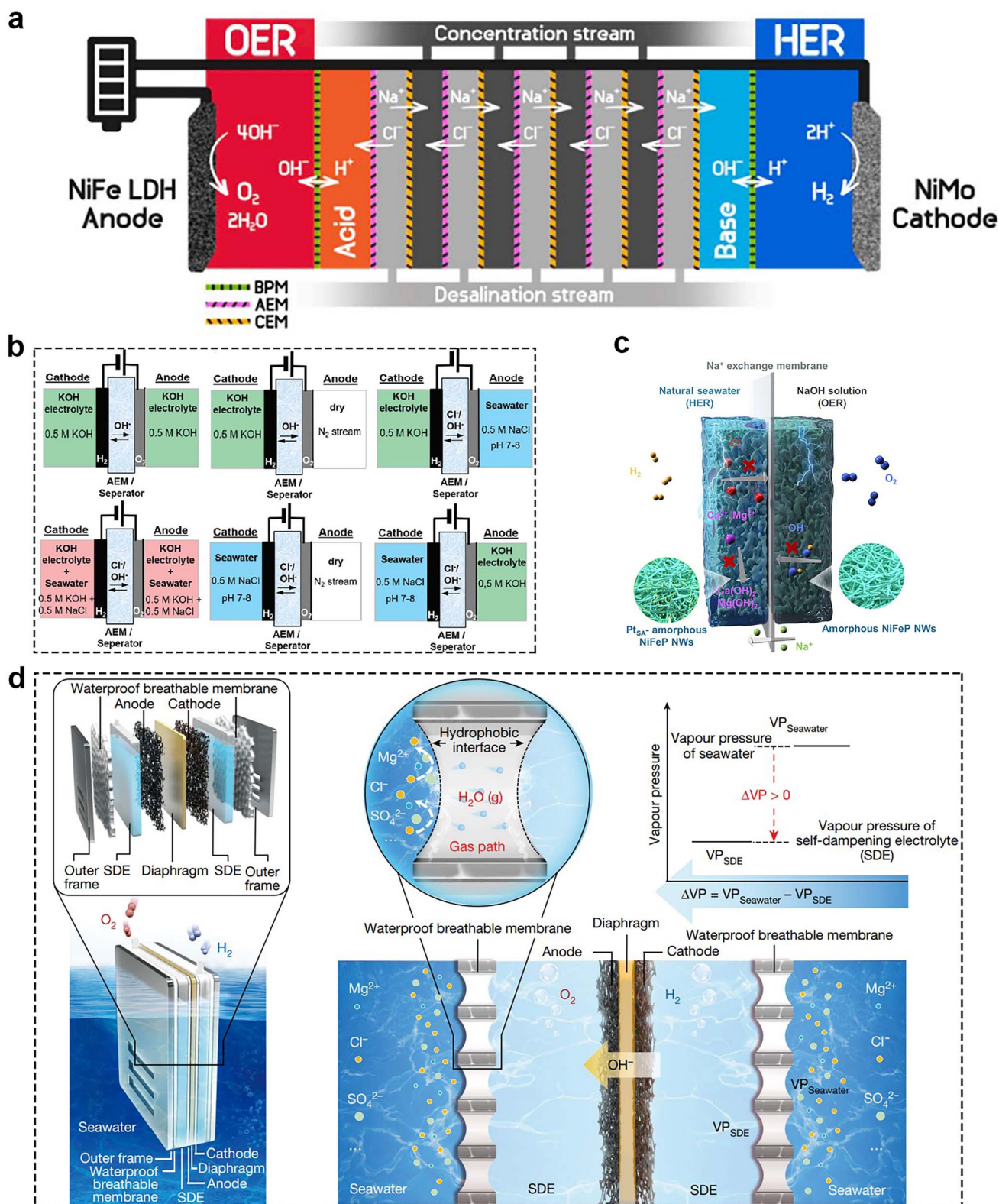


Fig. 11 (a) Desalination-coupled electrocatalytic stack device. The five desalination cells are stacked by alternately inserting anion exchange membranes and CEMs between acid and base cells. Sandwiched cells between adjacent two desalination cells are denoted as concentration cells. Reprinted with permission.<sup>91</sup> Copyright 2023, Elsevier. (b) Schemes for anion exchange membranes electrolyzers using independent electrolyte feeds with different electrolyte composition. Reprinted with permission.<sup>92</sup> Copyright 2020, The Royal Society of Chemistry. (c) Scheme for the asymmetric electrolyzer with sodium ions exchange membrane. Reprinted with permission.<sup>93</sup> Copyright 2023, Springer Nature. (d) Schematic diagram of a typical SES (left) and the liquid-gas-liquid phase transition-based migration mechanism of the water purification and migration process and the driving force. Reprinted with permission.<sup>94</sup> Copyright 2022, Springer Nature.

voltage.  $\text{Pt}_{\text{SA}}\text{-Ni}_{6.6}\text{-Fe}_{0.4}\text{P}_3$  was chosen as the cathode and  $\text{Ni}_3\text{Fe}_2\text{P}_3$  as the anode, while the electrolyte for the anode was 4 M NaOH and that for the cathode was 4 M NaCl to achieve overall seawater splitting. In this way, the asymmetric electrolyzer exhibits a large current density of  $400 \text{ mA cm}^{-2}$  at low voltage of 1.66 V at  $80^\circ\text{C}$ , corresponding to the electricity price of US\$1.36 per kg of  $\text{H}_2$ , which is lower than the Department of Energy (DOE) 2025 target of US\$1.4 per kg of  $\text{H}_2$ . Secondly, designing some special membranes. Xie *et al.*<sup>97</sup> developed a phase change migration-driven *in situ* direct electrolytic  $\text{H}_2$  production from seawater without desalination. They constructed a micron-scale gas phase isolation zone in seawater by using a waterproof breathable membrane and permeable layer (Fig. 11d). This design leveraged the inherent pressure difference caused by the self-humidifying electrolyte and seawater, facilitating the movement of water vapor. As a result, water vapor spontaneously transitioned from the seawater side, diffused through the membrane, and was absorbed and liquefied on the electrolyte side. According to their report, the designed electrolyzer could operate stably in natural seawater for more than 72 h. Moreover, using bipolar membrane-based devices is also a great method. For example, Marin *et al.*<sup>98</sup> introduced a novel bipolar membrane electrolyser for seawater electrolysis to produce  $\text{H}_2$  and  $\text{O}_2$ . It consists of a cation-

exchange layer and an anion-exchange layer, which can effectively control the ion transport and reaction environment. Compared with PEM, the bipolar membrane electrolyzer significantly inhibits the penetration and oxidation of chloride ions, thus avoiding the generation of harmful free chlorine species at the anode. Furthermore, the bipolar membrane electrolyzer has higher stability and selectivity for seawater electrolysis over a long period of time, whereas the PEM electrolyzer fails quickly.

## 5.2 Membrane-less electrolyzer

Because the membrane has the disadvantage of high cost and limited lifespan, the membrane-less electrolyzers offer an alternative approach. Membrane-less electrolyzers can be mainly classified into two types based on the type of electrodes employed, including membrane-less flow-by electrodes and flow-through electrodes (Fig. 12a).<sup>99</sup> Among them, the microfluidic electrolyzer caught the attention of some researchers. In 2013, the use of the microfluidic electrolyzer for energy conversion was first demonstrated,<sup>100</sup> and could attain the current density of  $100 \text{ mA cm}^{-2}$  at 2.5 V. Recently, some researchers applied it for seawater splitting. They proposed that a microfluidic alkaline membrane-less electrolyzer ( $\mu\text{AEM}$ )<sup>101</sup> (Fig. 12b) may resolve the

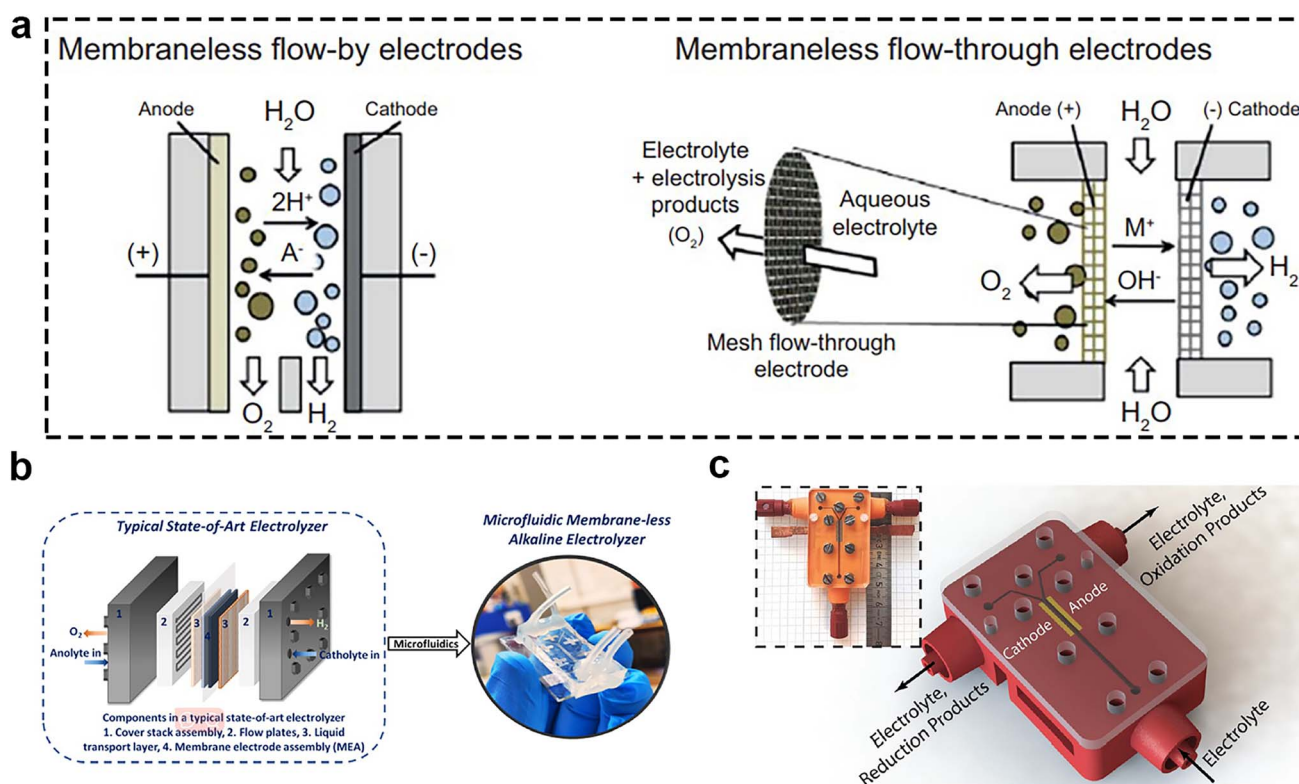


Fig. 12 (a) Emerging membrane-less electrolyzers based on flow-by electrodes (left) and flow-through electrodes (right). Reprinted with permission.<sup>103</sup> Copyright 2017, Elsevier. (b) Stacked, multilayer structure of a typical state-of-art electrolyzer can be implemented on a single chip using microfluidics. Reprinted with permission.<sup>98</sup> Copyright 2021, American Chemical Society. (c) Schematic illustration of the electrolysis cell: the main body (in red) is 3D printed with stereolithography technology. The electrodes (in yellow) are pressed into the devised slots and the assembly is covered by a transparent PMMA plate. A flexible sealing film is sandwiched in between this plate and the 3D printed part to prevent leaking. The inset shows the final assembled device with attached fluidic connectors. Reprinted with permission.<sup>102</sup> Copyright 2019, The Royal Society of Chemistry.

Table 2 Summary of the recently reported bifunctional electrocatalysts for overall seawater splitting

| Electrocatalyst  | Electrolyte          | Cell voltage<br>(V @ mA cm <sup>-2</sup> ) | Pt/C  IrO <sub>2</sub> or RuO <sub>2</sub><br>(V @ mA cm <sup>-2</sup> ) | Stability<br>(h @ mA cm <sup>-2</sup> ) | Overpotentials of HER and<br>OER (mV @ cm <sup>-2</sup> ) | Tafel slopes of HER and<br>OER <sup>a</sup> (mV dec <sup>-1</sup> ) | Reference |
|--|----------------------|--|--|---|---|---|-----------|
| FCNP@CQDs  | 1 M KOH + seawater   | 1.61 @ 10                                  | —  | 50 @ 20                                 | 183 @ 50; 268 @ 20  | 87.0; 45.2  | 104       |
| Ni <sub>3</sub> Se <sub>2</sub> @MoO <sub>3</sub> /CF                                      | 1 M KOH + seawater   | 1.84 @ 100                                 | 2.05 @ 100   | 200 @ 100                               | 426 @ 500; 280 @ 100                                      | 39.6; 74.7  | 105       |
| Ni <sub>2</sub> P-Fe <sub>2</sub> P/NF   | 1 M KOH + seawater   | 2.004 @ 500                                | —  | 48 @ 100                                | 389 @ 1000; 431 @ 1000                                    | 86.0; 58.0  | 68        |
| Ru-CoFe <sub>2</sub> O <sub>4</sub> /NF  | 1 M KOH + seawater   | 1.778 @ 100                                | 1.85 @ 100   | 100 @ 30                                | —   | 44.49; 47.81  | 106       |
| S-NiMoO <sub>4</sub> @NiFe LDH   | 1 M KOH + seawater   | 1.73 @ 100                                 | 1.81 @ 100   | 20 @ 60                                 | 220 @ 100; 315 @ 100                                      | 69; 90  | 107       |
| Er-MoO <sub>2</sub>  | 1 M KOH + seawater   | 1.52 @ 10                                  | —  | 24 @ 10                                 | 94 @ 10; 173 @ 10   | —   | 108       |
| MnCo <sub>2</sub> O <sub>4</sub> @NiFe-LDH   | 1 M KOH + 0.5 M NaCl | 1.54 @ 10                                  | —  | 100 @ 100                               | 97 @ 10; 460 @ 500  | —; 45.4   | 109       |
| Fe-B-O@FeB <sub>x</sub> /HC  | 1 M KOH + 0.5 M NaCl | 2.06 @ 200                                 | 2.31 @ 200   | 168 @ 400                               | 135 @ 100; 358 @ 100                                      | 57.62; 65.44  | 85        |
| FMCO/NF  | 1 M KOH + seawater   | 1.58 @ 10                                  | 1.61 @ 10  | 180 @ 100                               | 250 @ 50; 365 @ 50  | 147.1; 52.1   | 110       |
| NRAHM-NiO  | 1 M KOH + 0.5 M NaCl | 2.01 @ 500                                 | 2.31 @ 500   | 168 @ 240 (60 °C)                       | 478 @ 500; 540 @ 500                                      | 116; 73   | 111       |
| NiFe/Fe-MoO <sub>2</sub>   | 1 M KOH + seawater   | 1.73 @ 100                                 | —  | 50 @ 50                                 | 38 @ 10; 219 @ 20   | 47; 65  | 112       |
| Mo-CoP <sub>x</sub> /NF  | 1 M KOH + seawater   | 2.16 @ 100                                 | —  | 100 @ 10                                | 158 @ 10; 260 @ 10  | 89; 35  | 113       |
| Co-Fe <sub>2</sub> P/NF  | 1 M KOH + 0.5 M NaCl | 1.69 @ 100                                 | 1.97 @ 100   | 22 @ 100                                | 221 @ 100; 266 @ 100                                      | 57; 45  | 114       |
| NiFe-P@NC  | 1 M KOH + seawater   | 1.93 @ 500                                 | —  | 12 @ 500                                | 149 @ 100; 280 @ 100                                      | 58; —   | 115       |
| F-FeCoP <sub>x</sub> @JF   | 1 M KOH + seawater   | 1.92 @ 1000                                | —  | 100 @ 1000                              | 210 @ 1000; 370 @ 1000                                    | 108; 118  | 116       |
| C@CoP-FeP/FF   | 1 M KOH + 0.5 M NaCl | 1.73 @ 100                                 | —  | 28 @ 100                                | 192 @ 100; 297 @ 100                                      | 67.23; 58.48  | 117       |
| NiPS/NF  | 1 M KOH + seawater   | 1.79 @ 200                                 | —  | 60 @ 200                                | 275 @ 500; 392 @ 500                                      | 89; 23  | 118       |
| S <sub>2</sub> P-(Ni <sub>1</sub> Mo <sub>1</sub> Fe <sub>1</sub> )OOH/NiMoP/wood aerogel  | 1 M KOH + seawater   | 1.861 @ 500                                | —  | 10 @ 100                                | 258 @ 500; 297 @ 500                                      | 91.7; 45.5  | 119       |
| MoN-Co <sub>2</sub> N  | 1 M KOH + seawater   | 1.7 @ 100                                  | —  | 62 @ 100                                | 351 @ 500; 432 @ 500                                      | 82.1; 35.6  | 88        |
| CoSe <sub>2</sub> -NCF   | 1 M KOH + seawater   | 1.842 @ 500                                | 1.929 @ 500  | 50 @ 500                                | 134 @ 10; 245 @ 10  | 67; 93  | 120       |
| CdFe-BDC   | Seawater             | 1.68 @ 10                                  | —  | 12 @ 9.5                                | 148 @ 10; 290 @ 100                                       | 108.71; 44.57   | 121       |
| NiFe-PBA-gel-cal   | 1 M KOH + 0.5 M NaCl | 1.66 @ 100                                 | —  | 60 @ 50                                 | /; 427 @ 500  | 82.4; 68.7  | 122       |
| NiCoHPi@Ni <sub>3</sub> N/NF   | 1 M KOH + 0.5 M NaCl | 1.86 @ 100                                 | —  | 40 @ 200                                | 174 @ 100; 365 @ 100                                      | 77.5; 79.8  | 123       |
| NiFe LDH/FeOOH   | 1 M KOH + 0.5 M NaCl | 1.55 @ 10                                  | —  | 105 @ 100                               | 181.8 @ 10; 286.2 @ 100                                   | —   | 124       |
| Ti@NiB 1.5 h   | 1 M KOH + 0.5 M NaCl | 1.75 @ 20                                  | —  | 40 @ 100                                | 149 @ 10; 397 @ 50  | 118; 34.2   | 125       |
| Ni@CNTs-Mo <sub>x</sub> C/Ni <sub>2</sub> P  | 1 M KOH + seawater   | 1.56 @ 10                                  | 1.59 @ 10  | 50 @ 50                                 | 65.9 @ 10; 230 @ 10                                       | 54; 43  | 126       |
| FeNiCoMnRu@CNT   | 1 M KOH + seawater   | 2.15 @ 100                                 | 2.2 @ 100  | 30 @ 10                                 | 286 @ 100; 490 @ 100                                      | 50; 107   | 127       |
| GDY/RhO <sub>2</sub> /GDY  | 1 M KOH + 0.5 M NaCl | 1.49 @ 100                                 | 1.71 @ 100   | 50 @ 500                                | 249 @ 1000; 261 @ 100                                     | 42; 68  | 128       |
| Pt-CoFe(η)LDHs (2.2 wt%)   | 1 M KOH + seawater   | 1.651 @ 100                                | 1.99 @ 100   | 20 @ 500                                | 224 @ 500; 375 @ 500                                      | 45.3; 43.6  | 129       |
| cRu-Ni <sub>3</sub> N/NF   | 1 M KOH + seawater   | 1.73 @ 100                                 | 1.84 @ 100   | —                                       | 36 @ 10; 280 @ 50   | 26.2; 40.4  | 130       |
| RuNi-Fe <sub>2</sub> O <sub>3</sub> /IF  | 1 M KOH + seawater   | 1.73 @ 100                                 | 2.03 @ 100   | 100 @ 100                               | 353 @ 1000; 497 @ 1000                                    | 85.08; 60.85  | 131       |
| Ir <sub>0.05</sub> -Co <sub>2</sub> P/Co <sub>2</sub> P <sub>2</sub> O <sub>7</sub> NWS/NF | Seawater             | 1.97 @ 30                                  | 2.32 @ 30  | —                                       | 205 @ 10; 280 @ 20  | 30; 138   | 132       |
| Ag <sub>2</sub> Se-Ag <sub>2</sub> S-CoCH/NF   | 1 M KOH + seawater   | 1.69 @ 100                                 | —  | 24 @ 100                                | 367 @ 200; 440 @ 100                                      | 185.59; 144.87  | 133       |
| Ru-CoV-LDH/NF  | 1 M KOH + seawater   | 1.809 @ 100                                | 1.973 @ 100  | —                                       | 147 @ 300; 440 @ 300                                      | 49.6; 53.5  | 134       |
| P-Fe <sub>2</sub> O <sub>3</sub> -CoP  | Seawater             | 1.65 @ 10                                  | —  | 12 @ 10                                 | 275 @ 50; 270 @ 10  | 95; 59  | 135       |
| MnCo/NiSe/NF   | 1 M KOH + seawater   | 2.11 @ 1000                                | —  | 200 @ 500                               | 270.1 @ 1000; 460.2 @ 1000                                | 45.05; 69.71  | 136       |
| Fe <sub>2</sub> P/Ni <sub>1.5</sub> Co <sub>1.5</sub> N/Ni <sub>2</sub> P                  | 1 M KOH + seawater   | 1.742 @ 500                                | —  | 40 @ 50                                 | 141 @ 500; 307 @ 500                                      | 43.4; 29.1  | 137       |
| Au-Gd-Co <sub>2</sub> B@TiO <sub>2</sub>   | 1 M KOH + seawater   | 1.68 @ 500                                 | —  | 200 @ 500                               | 194 @ 500   | 65; 43  | 138       |
| Cu <sub>2</sub> O-CoO/CF   | 1 M KOH + seawater   | 1.82 @ 100                                 | —  | 50 @ 100                                | 359 @ 500; 410 @ 500                                      | 83.0; —   | 139       |

<sup>a</sup> The Tafel slopes of these bifunctional catalysts were obtained using 1 M KOH as the electrolyte.



challenges of conventional membrane-based electrolyzers, and minimize the number of components and condense the membrane-based electrolyzers to a single chip, marking a new paradigm for water splitting. In order to make the micro-fabrication of the electrolyzer simple, the bifunctional catalyst is important for this type of electrolyzers. Psaltis *et al.*<sup>102</sup> reported a novel membrane-less electrochemical reactor (Fig. 12c) that could perform brine electrolysis at room temperature and atmospheric pressure without the use of ion-conducting membranes or separators. Using the 3D printing technology, they integrated flow plates and fluid ports into a single component and used the inertial fluid forces to separate the generated gases. The results unequivocally demonstrated the reactor's remarkable capacity to yield exceedingly high-purity (>99%) and impressive FE (>90%) in the production of hydrogen, oxygen, chlorine, and sodium hydroxide. These findings are commensurate with the performance of commercial brine electrolyzers, thus underscoring the reactor's potential as a groundbreaking technology in this scientific domain.

## 6. Conclusions and perspectives

Seawater electrolysis holds the chance to be a cost-effective and sustainable approach for the production of H<sub>2</sub> in the future owing to the demand of clean energy power and the advancement of related technologies. With growing academic research results, electrolysis of seawater has become a major topic for research within the field of H<sub>2</sub> production. Nevertheless, it is important to note that research in seawater electrolysis remains in its early stages and has encountered several significant challenges. In view of this, this review highlighted the current advances in bifunctional catalysts capable of converting both anodic and cathodic reactants, as well as the experimental findings in nicely designed electrolytic system, with the goal of helping scientists find feasible bifunctional catalysts for industrial-scale H<sub>2</sub> product in seawater. A wide range of bifunctional materials (noble metal-based material, transition metal phosphides, chalcogenides, borides, nitrides, oxides, and hydroxides) as efficient electrocatalysts toward overall seawater splitting is reviewed (Table 2).

These bifunctional transition metal compounds all exhibit high activity towards HER and OER. However, they also have some improvements: the electronic structure and valence states of oxides are difficult to regulate and have low conductivity; sulfides, nitrides, phosphides, and borides are relatively complex to synthesize and are easily oxidized, leading to a decrease in their catalytic activity and stability. Despite considerable progress made in recent years of seawater electrolysis, research in the following sub-areas should be prioritized in future work:

(1) For seawater electrolysis to become more productive and stable, the catalyst design is crucial. For example, the catalytic performance can be improved by investigating state-of-the-art materials, tailoring compositions, and optimizing active sites. Developing protective outer/inner-coatings, robust catalyst structures, and knowing degradation mechanisms are all key considerations for ensuring long-term operation.

(2) More powerful bifunctional nano-architectures with increased well-adjusted catalytic sites should be constructed in order to facilitate large-scale seawater to H<sub>2</sub> electrolysis.

(3) Efficiency, scalability, and durability of electrolyzers can all be improved by upgrading cell configurations, electrodes materials, and mass transport control.

(4) Only renewable energy sources (*e.g.*, wind power)-enabled electrolysis represents the carbon-neutral method to reduce the use of fossil fuels, which makes the H<sub>2</sub> production truly sustainable. Researchers should thus create integration strategies to improve energy management systems, allowing for the efficient exploitation of clean and plentiful renewable energy.

(5) Although different types of bifunctional catalysts exist in alkaline media, such as metal-sulfur compounds, borides, oxides, carbide, and phosphides, which can make the necessary changes in electronic properties and morphology, very few of them can be directly applied in natural seawater. Researchers should simulate or even use real seawater for use as an electrolyte.

(6) Substituting the conventional OER with alternative oxidation reaction, such as the Selective Methanol Oxidation Reaction (SMOR),<sup>140</sup> holds the promise of significantly enhancing both energy efficiency and sustainability. This forward-looking approach not only paves the way for reduced energy consumption, but also unlocks intriguing possibilities for simultaneous production of valuable chemicals. This dual benefit not only enhances the economic viability of the process, but also aligns with environmental sustainability goals. As we look ahead, the adoption of such innovative strategies is poised to play a pivotal role in shaping the landscape of clean energy production and resource utilization.

(7) At present, research on direct seawater electrolysis is still insufficient. In the future, we should pay more attention to and study the technology of *in situ* direct electrolysis of seawater without desalination for H<sub>2</sub> production. This will have significant implications for the commercialization of seawater electrolysis for H<sub>2</sub> production. Such a research direction can not only promote technological progress, but also help solve energy problems and achieve sustainable development.

(8) In the majority of research literature on bifunctional catalysts for seawater electrolysis, the chosen electrolyte (*e.g.*, 1 M KOH + seawater, 1 M KOH + 0.5 M NaCl) deviates significantly from the conditions of natural seawater. This does not contribute significantly to addressing the challenges of cathodic reactions, such as calcium and magnesium precipitation. Therefore, future research should focus more on conditions that closely resemble natural seawater, or even under actual seawater conditions. This will have significant implications for achieving the goal of large-scale seawater electrolysis for hydrogen production. Such a research direction can not only promote technological progress, but also help solve energy problems and achieve sustainable development.

## Conflicts of interest

There are no conflicts to declare.



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