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Predicting the electrical conductivity in polymer carbon nanotube nanocomposites based on the volume fractions and resistances of the nanoparticle, interphase, and tunneling regions in conductive networks

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Some limited models have been suggested to determine the conductivity of polymer carbon nanotube (CNT) nanocomposites (PCNTs). However, earlier models (*e.g.*, the Kovacs model) cannot properly consider the roles of the interphase regions or tunneling properties on the percolation threshold and subsequent conductivity of PCNTs. In this paper, the Kovacs model is further developed by assuming that the CNT, interphase, and tunneling regions are separate phases. Also, some simple equations are provided to calculate the percolation threshold as well as the volume fractions and resistances of the CNT, interphase, and tunneling regions in conductive networks. The experimental conductivity results for several samples are compared with the predictions of the developed model. In addition, the calculations of the developed model at different parameter levels are explained and justified. The conductivity calculations show good agreement with the experimental data. Moreover, the developed model reasonably explains the roles of the different parameters on the conductivity. For example, long, thin, and straight CNTs efficiently improve the conductivity because they form large networks in the nanocomposites. Additionally, a thick interphase enlarges the conductive networks, resulting in a desirable conductivity. The conductivity of PCNTs only depends on the tunneling resistance; this is the case because the poor resistance/significant conductivity of the CNT and interphase regions do not influence the conductivity. The developed equations can replace conventional approaches for predicting the conductivity of nanocomposites.

1 Introduction

Polymer carbon nanotube (CNT) nanocomposites (PCNTs) are interesting because they show excellent conductivity. The electrical conductivity of CNTs reaches 10^6 S m^{-1}, but polymer matrices usually show poorer conductivity values between 10^{-16} and 10^{-12} S m^{-1}. However, adding very low concentrations of CNTs into polymer matrices can significantly increase their conductivity.[1–8] Conductive polymer nanocomposites have the potential to be used in electronics, sensors, and actuators, as well as many other applications in the electronics industry.[9,10] Conductivity in nanocomposites commonly occurs at a critical

filler concentration, known as the percolation threshold, where nanoparticles form conductive networks within nanocomposites.[11,12] The percolation level is experimentally determined by measuring the electrical conductivity at different filler concentrations. Earlier reports commonly related the percolation threshold to the size of the nanofiller material;[13,14] however, the structure and dispersion quality of CNTs, in addition to the interphase properties, can also influence the percolation level.[15,16]

The high surface area of nanoparticles per unit weight, as well as the strong interfacial interaction between the polymer matrix and nanofiller, create interphase regions in the polymer nanocomposites.[17,18] These interphase regions are actually modified zones of the matrix, caused by the large surface area of nanoparticles and the strong interfacial interactions. Fig. 1 depicts a schematic illustrating the interphase regions that form around CNTs. The interphase thickness is defined as the thickness of the interphase zone formed between the nanoparticles and the polymer matrix. The extent of the interphase regions directly governs the mechanical properties of a nanocomposite.[18–24] In addition, some authors have suggested that the interphase areas

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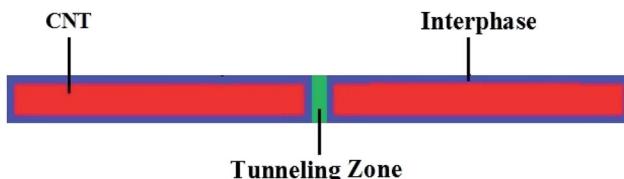
Fig. 1 Schematic illustration of CNT, interphase and tunneling regions in nanocomposites.

around nanoparticles can cause percolation networks to form before the nanoparticles actually join together.[17,25–27] This means that the percolation networks initially form based on the interphase areas because the interphase regions surrounding CNTs can produce network structures before the nanoparticles are physically connected. Therefore, these interphase regions can reduce the percolation threshold of nanoparticles in nanocomposites. Interphase regions can help create large conductive networks in PCNTs, thereby influencing the electrical conductivity; however, earlier works have not investigated this topic.

It has been suggested that the main mechanism for the electrical conductivity in PCNTs is electron hopping, in which electrons in CNTs are conveyed by the tunneling effect.[28–30] In this approach, neighboring CNTs produce conductivity *via* electron jumping and the tunneling effect depends on the tunneling properties between CNTs rather than their network (Fig. 1). Some micromechanics models were developed to account for the tunneling effect, agglomeration, and waviness of CNTs;[31,32] however, the intricate and indistinct equations of these models are not useful in practice. There is not a simple model that can show the conductivity of polymer nanocomposites based on the properties of the conductive nanoparticles, interphase regions, and networks.

Kovacs *et al.*[33] proposed a model to determine the conductivity of PCNTs by assuming the weight percentage, dimensions, and resistance of CNTs, as well as the tunneling effect. However, they did not consider the interphase regions in nanocomposites. In addition, they did not appropriately express the tunneling resistance or the fractions of the interphase and tunneling regions in the conductive networks. The Kovacs model correlates the conductivity to the volume fraction of all nanoparticles; however, only networked CNTs improve the conductivity of nanocomposites. In our study, the Kovacs model is further developed by assuming that the interphase and tunneling regions are separate phase in PCNTs. Simple equations express the volume fractions and the intrinsic resistances of the CNT, interphase, and tunneling regions in the conductive networks. Therefore, the developed model can predict the conductivity of nanocomposites by accounting for the interphase and tunneling spaces. The experimental conductivity results from several samples and parametric analysis were used to assess the developed model. The good agreement between experimental results and predictions, in addition to the accurate calculations of the developed model at different parameter levels, validate the developed model.

2 Theoretical expressions

Kovacs *et al.*[33] suggested a simple model to determine the conductivity of PCNTs by assuming the tunneling mechanism as:

$$\sigma = \frac{l w_f^{2x+1}}{2\pi R^2 (R_f + R_t)}. \tag{1}$$

here, "l", "R", "w_f", and "R_f" are the length, radius, weight fraction, and intrinsic resistance of CNTs, respectively. Similarly, "R_t" is the intrinsic resistance of tunneling regions and "x" is an exponent ($2x + 1$ was reported to be between 2.7 and 5.3 in ref. 33). Many models for the conductivity of polymer nanocomposites frequently account for the filler volume fraction.[34,35] This model can be further developed by assuming the volume fractions of the effective components. The CNT, interphase, and tunneling space fractions in the networks can improve the conductivity of nanocomposites, while the dispersed nanoparticles and the interphase regions surrounding them outside of the networks cannot increase the conductivity.

The percolation threshold of randomly dispersed CNTs in PCNTs is given by:[36]

$$\phi_p = \frac{V}{V_{ex}}. \tag{2}$$

here, "V" and "V_{ex}" denote the volume and excluded volume of nanoparticles, respectively. The excluded volume is the volume around a particle that is inaccessible to other particles.

The values of "V" and "V_{ex}" in PCNTs containing random CNTs were suggested to be:[36]

$$V = \pi R^2 l \tag{3}$$

$$V_{ex} = \frac{32}{3}\pi R^3 \left[1 + \frac{3}{4}\left(\frac{l}{R}\right) + \frac{3}{32}\left(\frac{l}{R}\right)^2 \right]. \tag{4}$$

The interphase layer around CNTs can accelerate the development of conductive networks in PCNTs. The interphase areas change the excluded volume as:

$$V_{ex} = \frac{32}{3}\pi(R+t)^3 \left[1 + \frac{3}{4}\left(\frac{l}{R+t}\right) + \frac{3}{32}\left(\frac{l}{R+t}\right)^2 \right]. \tag{5}$$

here, "t" is the interphase thickness.

Also, the large aspect ratio (length to diameter) of CNTs causes waviness in PCNTs, thereby reducing their effectiveness. An equivalent length (l_{eq}) is considered as the minimum distance between two ends of each nanotube, and the waviness parameter is defined as:

$$u = \frac{l}{l_{eq}}. \tag{6}$$

here, $u = 1$ implies a straight CNT with no waviness, while a higher "u" displays more waviness.

If we assume that "l_{eq}" is the effective length of wavy CNTs ($l_{eq} = l/u$) in "V_{ex}", then:

$$V_{ex} = \frac{32}{3}\pi(R+t)^3\left[1 + \frac{3}{4}\left(\frac{l/u}{R+t}\right) + \frac{3}{32}\left(\frac{l/u}{R+t}\right)^2\right]. \quad (7)$$

Now, the percolation threshold of CNTs when the roles of the interphase region and waviness are accounted for is suggested as:

$$\phi_p = \frac{\pi R^2 l}{\frac{32}{3}\pi(R+t)^3\left[1 + \frac{3}{4}\left(\frac{l/u}{R+t}\right) + \frac{3}{32}\left(\frac{l/u}{R+t}\right)^2\right]}. \quad (8)$$

This equation can predict the percolation threshold in PCNTs. Both the CNTs and the surrounding interphase can affect the size of networks, increasing the conductivity in nanocomposites.

The total volume fraction of the interphase region in PCNTs[37] is calculated by:

$$\phi_i = \phi_f\left(1 + \frac{t}{R}\right)^2 - \phi_f. \quad (9)$$

here, "ϕ_f" is the filler volume fraction. In addition, the effective volume fraction of the nanofiller in nanocomposites includes CNTs and the surrounding interphase as:

$$\phi_{eff} = \phi_f + \phi_i = \phi_f\left(1 + \frac{t}{R}\right)^2. \quad (10)$$

Moreover, only a fraction of the nanotubes form the conductive networks after reaching the percolation threshold, while other CNTs are dispersed throughout the PCNT.

The fraction of percolated CNTs[35] is calculated by:

$$f = \frac{\phi_f^{1/3} - \phi_p^{1/3}}{1 - \phi_p^{1/3}}. \quad (11)$$

This is further developed by including the effective filler fraction:

$$f = \frac{\phi_{eff}^{1/3} - \phi_p^{1/3}}{1 - \phi_p^{1/3}}. \quad (12)$$

Using "f", the volume fractions of CNT and interphase regions in the networks are expressed by:

$$\phi_N = f\phi_f \quad (13)$$

$$\phi_{iN} = f(\phi_{eff} - \phi_f). \quad (14)$$

Furthermore, tunneling regions are formed around the interphase areas surrounding CNTs. Consequently, the volume fraction of tunneling spaces in the networks is presented by:

$$\phi_{tN} = (\phi_N + \phi_{iN})\left(1 + \frac{d}{R+t}\right)^2 - \phi_N - \phi_{iN}. \quad (15)$$

here, "d" is the tunneling distance between adjacent CNTs. The latter equations can be applied to calculate the volume fractions of components in the networks.

Now, the intrinsic resistances of all components are expressed. The intrinsic resistance of CNTs is suggested as:

$$R_f = \frac{l}{\pi R^2 \sigma_f}. \quad (16)$$

here, "σ_f" is the CNT conductivity. However, the waviness weakens the conductivity of CNTs.[38] Therefore, the conductivity of wavy CNTs is suggested to be:

$$\sigma_{CNT} = \frac{\sigma_f}{u}. \quad (17)$$

Based on this, the intrinsic resistance of wavy CNTs can be expressed as:

$$R_f = \frac{l}{\pi R^2 \sigma_{CNT}} = \frac{lu}{\pi R^2 \sigma_f}. \quad (18)$$

In addition, previous articles have not suggested an equation for estimating the interphase conductivity in nanocomposites. It can be stated that the interfacial interactions between the polymer matrix and CNTs control the interphase conductivity. The interphase thickness in nanocomposites commonly indicates the extent of interfacial adhesion/interactions.[39,40] Thus, the interphase conductivity can be expressed by the interphase thickness as:

$$\sigma_i = \frac{t\sigma_{CNT}}{t_m}. \quad (19)$$

here, "t_m" is the maximum interphase thickness in the PCNT. The interphase thickness in polymer nanocomposites should be smaller than the gyration radius of polymer chains. Thus, the maximum level of the interphase thickness in our system is considered to be 50 nm. Therefore, the interphase conductivity can be expressed as a function of the interphase thickness and filler conductivity:

$$\sigma_i = \frac{t\sigma_{CNT}}{50}. \quad (20)$$

Using this equation, the intrinsic resistance of interphase regions is expressed as:

$$R_i = \frac{l}{\pi t^2 \sigma_i} = \frac{50lu}{\pi t^3 \sigma_f}. \quad (21)$$

This shows that the interphase resistance inversely depends on the interphase thickness.

In addition, the tunneling resistance (R_t) is related to the resistances due to the CNTs and polymer matrix in the tunneling spaces. The tunneling resistance includes the resistances of the CNT fraction (R_1) and polymer layer (R_2) in the tunneling regions:

$$R_t = R_1 + R_2. \quad (22)$$

It has been suggested that "R_1" can be described as:[41]

$$R_1 = \frac{1}{2R\sigma_{\text{CNT}}}. \tag{23}$$

"R_2" can be defined as a function of the tunneling resistivity, tunneling distance, and contact area:

$$R_2 = \frac{\rho d}{S} = \frac{\rho d}{3R^2}. \tag{24}$$

here, "ρ" is the tunneling resistivity (ohm m) and "S" is the contact area between two adjacent CNTs. "S" is considered to be $3R^2$ due to the end-to-end and end-to-body contacts between nearby CNTs.[31]

Assuming the latter equations, the intrinsic tunneling resistance is:

$$R_t = \frac{1}{2R\sigma_{\text{CNT}}} + \frac{\rho d}{3R^2}. \tag{25}$$

Finally, eqn (1) can be further developed by including the volume fractions and intrinsic resistances of the CNT, interphase, and tunneling areas in the conductive networks:

$$\sigma = \frac{l(\phi_N + \phi_{iN} + \phi_{tN})^{2x+1}}{2\pi(R + t + d)^2 (R_f + R_i + R_t)}. \tag{26}$$

When proper equations are inserted into eqn (26), the developed model can estimate the conductivity of PCNTs by assuming the effective interphase and tunneling properties.

3 Results and discussion

The developed model can predict the conductivity in PCNTs by assuming the CNT dimensions as well as the interphase, waviness, and tunneling effects.

Fig. 2 illustrates the experimental and theoretical results for epoxy/multi-walled CNT (MWCNT) ($R = 8$ nm, $l \approx 30$ μm, $u = 1.2$, and $\phi_p = 0.0002$),[42] poly(vinyl chloride) (PVC)/MWCNT ($R = 8$ nm, $l \approx 16$ μm, $u = 1.2$, and $\phi_p = 0.0005$),[43] epoxy/single-walled CNT (SWCNT) ($R = 1$ nm, $l \approx 2$ μm, $u = 1.6$, and $\phi_p = 0.0003$)[44] and polycarbonate (PC)/acrylonitrile butadiene styrene (ABS)/MWCNT ($R = 5$ nm, $l \approx 1.5$ μm, $u = 1.2$, and $\phi_p = 0.002$)[45] samples. When the dimensions and percolation thresholds of
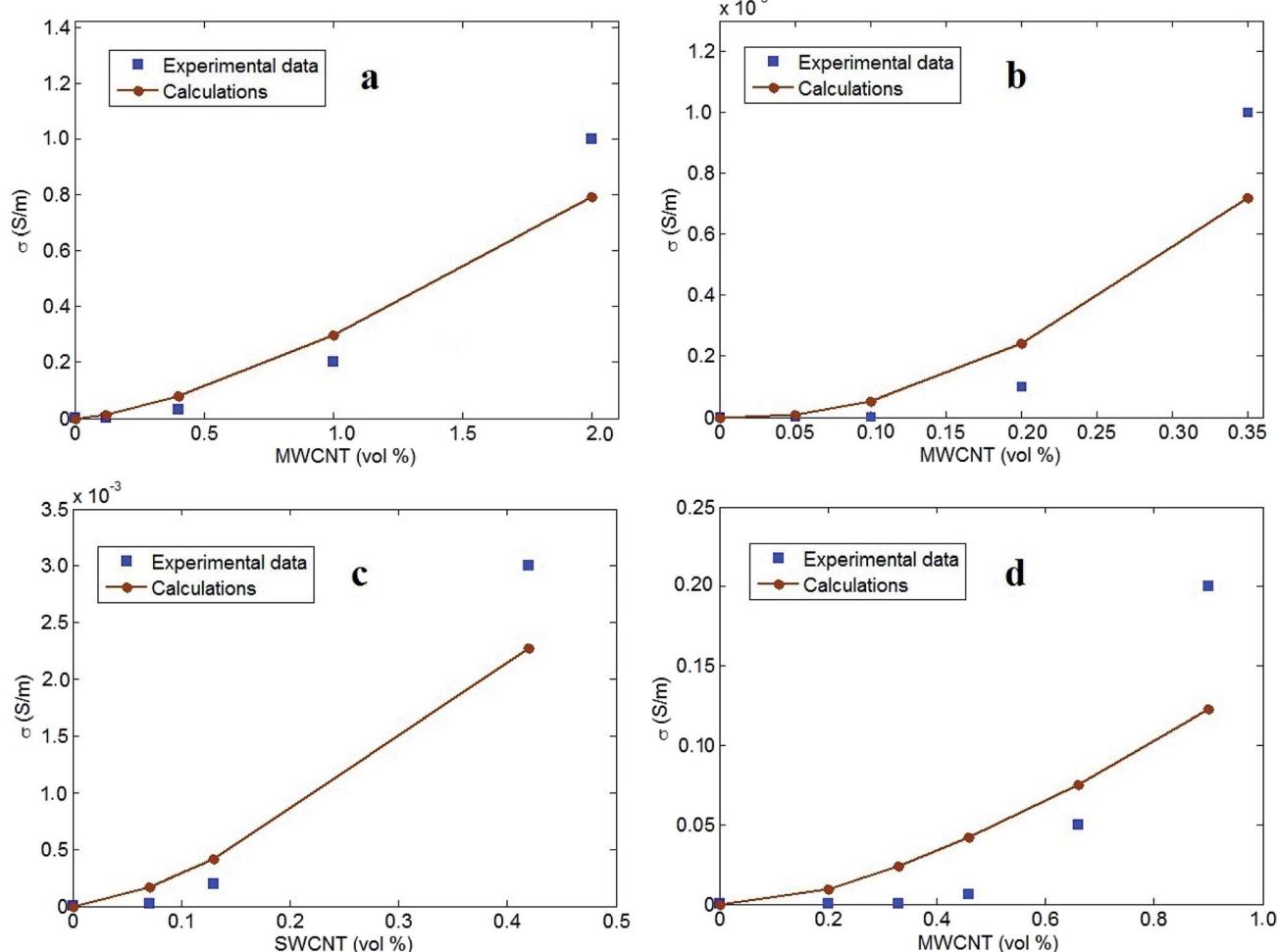
Fig. 2 Experimental results and calculations by the developed model for (a) epoxy/MWCNT,[42] (b) PVC/MWCNT,[43] (c) epoxy/SWCNT[44] and (d) PC/ABS/MWCNT[45] samples.

CNTs are applied to eqn (8), the interphase thickness (t) values are calculated to be 5, 3, 3, and 5 nm for the epoxy/MWCNT, PVC/MWCNT, epoxy/SWCNT, and PC/ABS/MWCNT samples, respectively. These results show the formation of different interphase regions in the nanocomposites, which reduce the percolation level. Accordingly, the interphase regions act as percolation regions in PCNTs, significantly influencing the conductivity. The conductivity predictions made by the developed model show good agreement with the experimental data of reported samples, although some deviations are observed at high filler concentrations; this is due to poor dispersion and aggregation/agglomeration of the nanoparticles.[46,47] Accordingly, the developed model is validated by the experimental measurements.

The values of (d, ρ) are also determined to be (2, 50), (5, 200), (4, 100), and (1, 10) (nm, ohm m) for the epoxy/MWCNT, PVC/MWCNT, epoxy/SWCNT, and PC/ABS/MWCNT samples, respectively. The tunneling distance changes from 2 to 5 nm for the reported samples, while the tunneling resistivity varies from 10 to 200 ohm m. These results reveal the different tunneling properties in the reported samples. The PC/ABS/MWCNT sample demonstrates the shortest tunneling distance and the lowest tunneling resistance, whereas the largest tunneling distance and the highest tunneling resistance are observed in the PVC/MWCNT nanocomposite. In addition, "x" has values of 10^{-4}, 0.1, 0.01, and 10^{-6} for the epoxy/MWCNT, PVC/MWCNT, epoxy/SWCNT and PC/ABS/MWCNT samples, respectively. The smallest and highest values of "x" are exhibited in the PC/ABS/MWCNT and PVC/MWCNT samples, respectively.

The significance of the different parameters on the electrical conductivity of PCNTs is explained using the developed model. The average values of the parameters are $\phi_f = 0.01$, $R = 10$ nm, $l = 10$ μm, $t = 10$ nm, $\sigma_f = 10^5$ S m^{-1}, $u = 1.2$, $d = 5$ nm, $\rho = 200$ ohm m, and $x = 0.01$. Fig. 3 shows the roles of "ϕ_f" and "l" on the conductivity of nanocomposites, while maintaining the other factors at their average values. The highest conductivity (0.05 S m^{-1}) is obtained with $\phi_f = 0.02$ and $l = 18$ μm, but the conductivity decreases to about 0 at $\phi_f < 0.009$ and $l < 6$ μm.

Accordingly, both "ϕ_f" and "l" directly govern the conductivity of nanocomposites. In other words, a better conductivity is obtained with higher concentrations of long CNTs, whereas a low content of short CNTs does not improve the conductivity of nanocomposites.

The developed model demonstrates logical effects of "ϕ_f" and "l" on the conductivity. A high concentration of conductive fillers, above the percolation threshold, clearly creates large networks in the nanocomposite, thereby promoting conductivity. Alternatively, a low filler concentration cannot reach the percolation threshold and/or produces small networks that do not influence the conductivity. Moreover, larger CNTs lead to a smaller percolation threshold and produce larger networks in nanocomposites. Therefore, it is sensible to achieve a higher conductivity by using large CNTs. Similar impacts of "ϕ_f" and "l" on the conductivity of nanocomposites have been reported previously.[16,48] As a result, the developed model reasonably predicts the roles of these parameters on the conductivity of PCNTs.

Fig. 4 demonstrates the effects of "R" and "u" on the conductivity of nanocomposites, while using average values of the other parameters. The highest conductivity (0.018 S m^{-1}) is observed at $R = 5$ nm and $u = 1$, while the lowest conductivity (0.002 S m^{-1}) is found at $R = 45$ nm and $u = 1.5$. These results indicate that both the CNT radius and waviness inversely influence the conductivity of nanocomposites. Therefore, a desirable conductivity can be obtained by using thin CNTs with small waviness, whereas thick and wavy CNTs reduce the conductivity of PCNTs.

Thin and straight CNTs (no waviness) produce low percolation thresholds (eqn (8)) and high effective filler concentrations (eqn (10)). As a result, thin and straight CNTs produce larger networks in nanocomposites. Alternatively, CNTs with a larger thickness and higher waviness do not influence the conductivity as effectively; this is the case because they increase the percolation threshold and condense the interphase regions (eqn (9)). Thin and straight CNTs efficiently decrease the percolation level while the interphase zones enhance the conductivity of nanocomposites. Moreover, based on these explanations, the
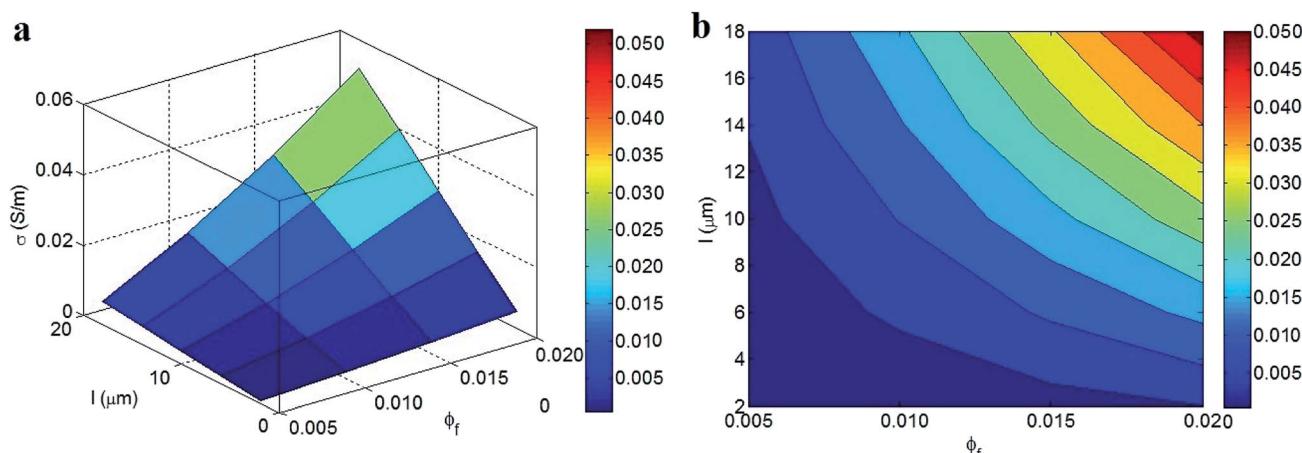
Fig. 3 (a) 3D and (b) contour patterns for the influences of "ϕ_f" and "l" parameters on the conductivity of nanocomposites at average levels of other variables.
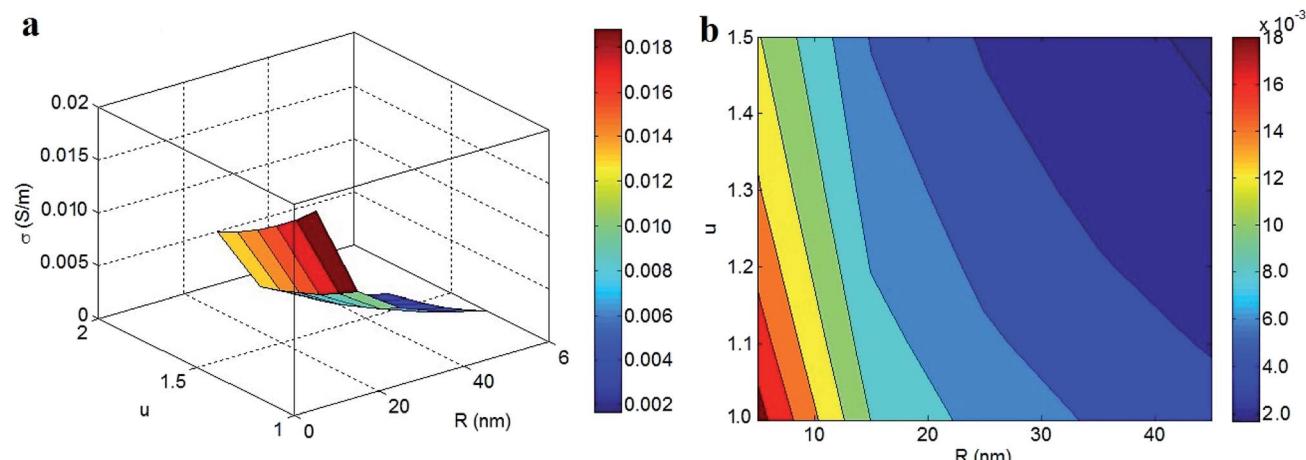
Fig. 4 Roles of "*R*" and "*u*" parameters in the conductivity of nanocomposites at average levels of other parameters: (a) 3D and (b) contour plots.

developed model properly predicts the impacts of "*R*" and "*u*" on the conductivity of nanocomposites.

The influences of "*t*" and "σ_f" on the conductivity of nanocomposites, as determined by the developed model, are shown in Fig. 5. The conductivity increases to 0.02 S m^{-1} at *t* > 32 nm, whereas the poorest conductivity (0.008 S m^{-1}) is observed at *t* < 6 nm. Thus, the interphase thickness directly changes the conductivity of nanocomposites, even with different CNT conductivity values, indicating that the CNT conductivity does not affect the overall conductivity. These results show the important role of the interphase thickness on the conductivity of nanocomposites containing CNTs with varying conductivity.

A thicker interphase around CNTs produces a lower percolation threshold in nanocomposites (eqn (8)); this is due to the fact that the interphase areas contribute to the conductive networks. Also, a thicker interphase produces a better interphase conductivity and a smaller interphase resistance in nanocomposites (eqn (19–21)). In other words, a thick interphase enlarges the conductive regions in nanocomposites, creating a low percolation threshold and large conductive networks. According to these observations, obtaining a higher

conductivity by creating a thicker interphase is reasonable. Previous studies reported a similar trend between the conductivity of nanocomposites and the interphase thickness.[16,48] However, a high filler conductivity significantly reduces the intrinsic resistances of the CNT and interphase regions (eqn (18) and (21)). In fact, a very high CNT conductivity (about 10^6 S m^{-1}) produces very low resistances in the CNT and interphase regions, as compared to the tunneling resistance (eqn (25)). As a result, a high CNT conductivity overrides the influence of the CNT and interphase resistances on the conductivity of nanocomposites; thus, the conductivity of nanocomposites does not depend on the CNT conductivity. These results indicate that the developed model can successfully predict the conductivity of PCNTs. Therefore, it can be concluded that the conductivity suggested by the developed model only depends on the tunneling resistance; the low resistance values of the CNT and interphase regions do not have an effect.

Fig. 6 depicts the conductivities of nanocomposites calculated by the developed model at different levels of "*d*" and "ρ" while maintaining average values for the other parameters. The highest conductivity (0.05 S m^{-1}) is produced at *d* = 2 nm and ρ
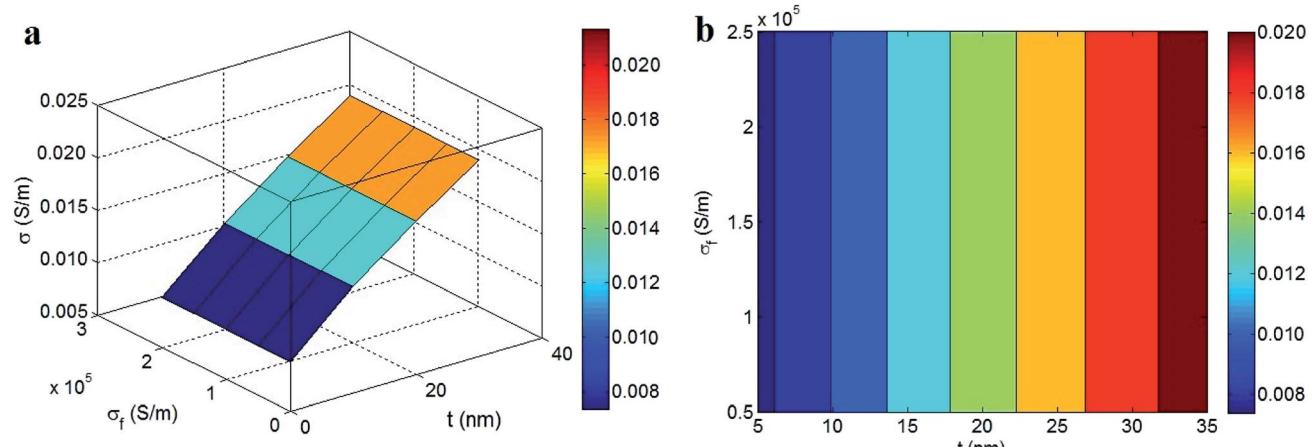

Fig. 5 The roles of "*t*" and "σ_f" in the conductivity of nanocomposites by the developed model at average values of other parameters: (a) 3D and (b) contour designs.
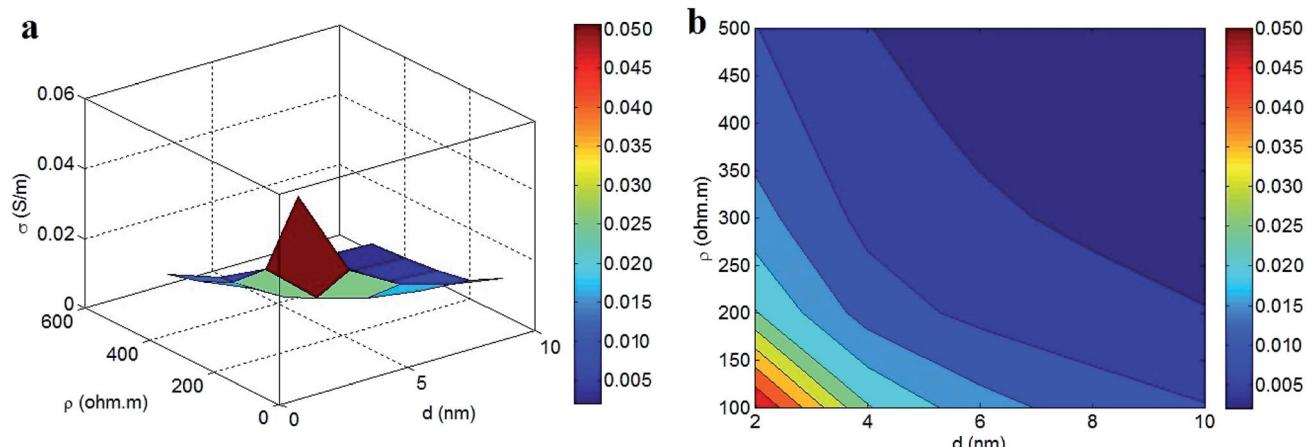
Fig. 6 Expression of conductivity by the developed model at different levels of "d" and "ρ" parameters: (a) 3D and (b) contour plots.

= 100 ohm m, but the conductivity decreases to 0.003 S m^{-1} at $d > 6$ nm and $\rho > 350$ ohm m. Accordingly, a high conductivity is obtained with small values of "d" and "ρ", signifying that the tunneling distance and tunneling resistivity adversely influence the conductivity of nanocomposites. A short tunneling distance and poor tunneling resistivity lead to a high conductivity in nanocomposites, and the conductivity is weakened by a larger tunneling distance and stronger tunneling resistivity. Thus, it is better to ensure short tunneling distances and poor tunneling resistivity to achieve a higher conductivity in PCNTs.

A large tunneling distance and the high tunneling resistivity due to the polymer matrix increase the intrinsic tunneling resistance (eqn (25)), which reduces the transportation of electrons through tunneling regions. Alternatively, a short tunneling distance and poor tunneling resistivity decrease the tunneling resistance, leading to more desirable conditions for electron transfer between adjacent CNTs. Therefore, the tunneling distance and resistivity directly affect the intrinsic tunneling resistance, as suggested by eqn (25). Since the conductivity of nanocomposites seriously depends on electron transfer through the tunneling regions, the tunneling distance

and resistivity inversely control the conductivity.[45,49,50] As a result, the developed model correctly reports the effects of the tunneling distance and resistivity on the conductivity of PCNTs.

Fig. 7 exhibits the predictions of the developed model at various values of "f" and "x". The highest conductivity of 0.03 S m^{-1} is obtained at $f = 0.7$ and $x < 0.017$, while the conductivity is reduced to 0.004 S m^{-1} at $f = 0.1$. Accordingly, a high "f" and a low "x" are necessary to obtain desirable conductivity in nanocomposites. The presence of higher percentages of CNT and interphase regions in the networks and a low "x" exponent can improve the conductivity of nanocomposites, whereas a lower fraction of percolated CNTs cannot increase the conductivity. These results implicitly reveal that the conductivity of nanocomposites largely depends on the dimensions of the conductive networks.

A high "f" obviously increases the fractions of the nanoparticle (eqn (13)), interphase (eqn (14)), and tunneling (eqn (15)) regions in the conductive networks. In other words, a higher "f" creates larger networks containing CNTs, interphase regions, and tunneling spaces. Since large networks within nanocomposites can successfully transfer electrons, it is
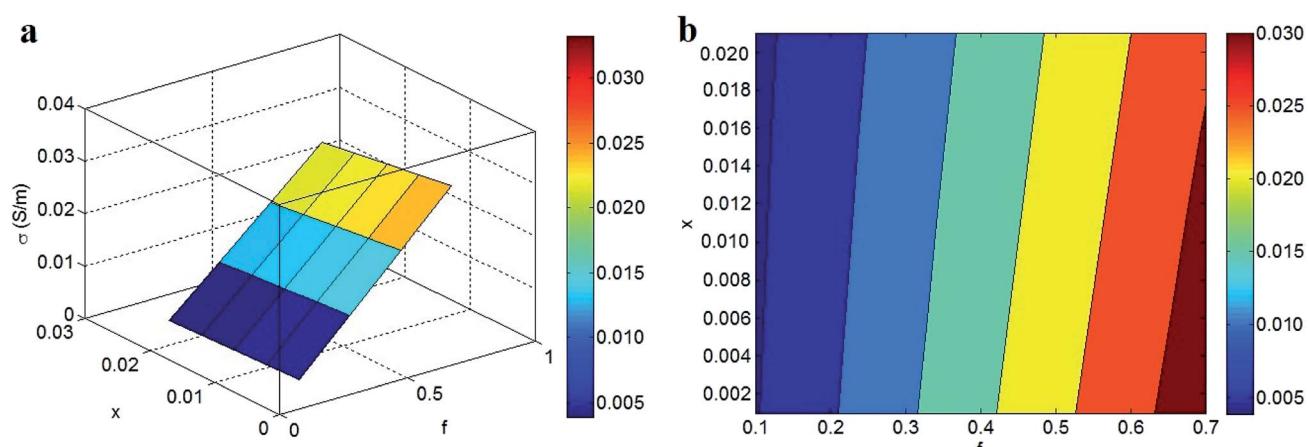

Fig. 7 Dependences of conductivity on "f" and "x" parameters at average values of other factors: (a) 3D and (b) contour plots.

reasonable that a higher "f" produces superior conductivity in nanocomposites.

According to eqn (12), high filler concentrations, large interphase regions, and low percolation thresholds lead to increased values of "f". Therefore, it is important to promote the interphase regions and decrease the percolation threshold at a constant filler fraction to produce a desired "f" value. However, the lower "f" caused by a thin interphase and high percolation threshold shortens the conductive networks and deteriorates the conductivity of nanocomposites. In addition, a high "x" exponent undesirably affects the conductivity of nanocomposites by suppressing the influences of the filler, interphase, and tunneling regions on the conductivity (eqn (26)). Accordingly, the developed model correctly reveals the effects of "f" and "x" on the conductivity of nanocomposites.

4 Conclusions

In this study, the Kovacs model was further developed by assuming that the CNT, interphase, and tunneling regions in PCNTs were separate phases. In addition, some equations were expressed to determine the volume fractions and resistances of these phases in the networks. The predictions of the developed model agreed well with the experimental data of several samples. Moreover, the developed model suggests reasonable impacts for all of the parameters on the conductivity. These results validate the ability of the developed model to predict the conductivity of PCNTs. A high conductivity is obtained with a high concentration of long, thin, straight CNTs; this is the case because the percolation threshold decreases and large networks are made under these conditions. A thicker interphase also produces a lower percolation threshold and a smaller interphase resistance in nanocomposites, thereby increasing the conductivity. However, using CNTs with high conductivity overrides the influences of the CNT and interphase resistances on the conductivity of PCNTs. Accordingly, the conductivity of PCNTs only depends on the tunneling resistance as a function of the tunneling properties. Thus, a better conductivity is obtained with shorter tunneling distances and poorer tunneling resistivity. In addition, a high value of "f" creates large networks in PCNTs that contain CNTs, interphase regions, and tunneling spaces, leading to an improvement in the conductivity.

Conflicts of interest

There are no conflicts to declare.

Nomenclature

σ	Conductivity of PCNT
σ_f	CNT conductivity
R_f	Intrinsic resistance of CNT
σ_{CNT}	The conductivity of waved CNT
σ_i	Interphase conductivity
R_t	Tunneling resistance
R_1	Resistance of CNT fraction in tunneling spaces
R_2	Resistance of polymer in tunneling zones
l	CNT length
R	CNT radius
w_f	Weight fraction of CNT in nanocomposite
x	An exponent
V	CNT volume
V_{ex}	Excluded volume of nanoparticles
l_{eq}	Equivalent length of waved CNT
u	Waviness parameter
t	Interphase thickness
t_m	Maximum interphase thickness
ϕ_p	Percolation threshold
ϕ_f	Filler volume fraction
f	The fraction of percolated CNT
ϕ_N	The volume fraction of CNT in the networks
ϕ_{iN}	The volume fraction of interphase regions in the networks
ϕ_{tN}	The volume fraction of tunneling spaces in the networks
d	Tunneling distance between adjacent CNT
ρ	Tunneling resistivity
S	Contact area between two CNT

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