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# Photonic flash-annealing of lead halide perovskite solar cells in 1 ms<sup> $\dagger$ </sup>

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An extremely fast annealing technique for mixed-halide perovskite solar cells is presented. Using photonic flash sintering, we have demonstrated that a spin-coated perovskite precursor may be fully annealed in as little as 1 ms. Devices annealed in 1.15 ms yielded power conversion efficiencies (PCEs) of upto 11.3% compared to 15.2% for samples annealed for 90 minutes on a hotplate.

#### **Introduction** 1

Since their inception in  $2009$ ,<sup>1</sup> followed by breakthrough de- $\overline{2}$ velopments in 2012;<sup>22</sup> solar cells based on organic-inorganic  $\overline{3}$ metal halide perovskite have experienced a meteoric rise in inter- $\overline{4}$ est within the photovoltaic community and beyond. Power con- $\overline{5}$ version efficiencies (PCEs) for perovskite solar cells (PSCs) have 6 risen from  $9.7\%$ <sup>2</sup> to certified 20.1%, a rate that has eclipsed other  $\overline{z}$ photovoltaic technologies. The deposition and heat treatment of  $\overline{8}$ the perovskite layer is a key step in producing efficient devices and several processing methods exist which yield perovskite films  $10$ with varying properties: one-step coating of both inorganic and  $11$ organic precursors,  $2^{2}$  -5 sequential deposition of precursors,  $6-8$  $12$ vacuum evaporation of precursors, <sup>9</sup> vapor-assisted deposition of  $13$ precursors  $^{10}$  and solvent-assisted crystallisation.  $^{11}$  A common  $14$ step required for the majority of these deposition processes is a  $15$ thermal anneal of the perovskite layer in order to drive off any 16 residual solvent from the precursor and/or to change the mor- $17$ phology of the perovskite microstructure to a more favourable 18 configuration.<sup>12</sup> Depending on the perovskite preparation tech- $19$ nique used, the annealing process may take between 5 and 120  $\overline{20}$ minutes.  $2,3,12$ ? -16 This time frame required to anneal the per- $21$ ovskite layer may pose a potential bottleneck in the eventual  $22$ commercial production, aspirational high volume and continu- $23$ ous manufacture of such devices. We have previously demon- $24$ strated that comparable PCEs to devices annealed in 45 minutes  $25$ in a conventional oven could be achieved in as little as 2.85 s  $\overline{26}$ by using an intense burst of near-infrared (NIR) radiation from  $27$ commercially available tungsten-halogen lamps.<sup>17</sup> NIR emitters 28 have a peak output at around 1,000 nm whereas "photonic" cur- $29$ 

and is employed in this study to anneal efficient perovskite films in as little as 1 ms. This curing method has been demonstrated to be effective at rapidly sintering nanoparticle inks,  $18-20$  metal oxide scaffolds, $^{21}$  as well as improving performance when used to selenise CuInSe<sub>2</sub> films in copper indium gallium selenide (CIGS) solar cells.<sup>22</sup> In this system, a xenon strobe lamp, with a spectral output close to that of a blackbody, can be adjusted by varying the voltage across the bulb, as well as changing the duration of the flash pulse in order to carefully control the amount of energy irradiated, optimising these processes minimises the total energy and time needed to complete annealing. We demonstrate that mesoporous  $Al_2O_3$ -infiltrated  $CH_3NH_3PbI_{3-x}Cl_x$  perovskite films can be fully annealed in atmospheric conditions in as little as 1 ms. In this study we achieved a maximum of 11.3% PCE device annealed in 1.15 ms compared to 15.2% PCE for an otherwise identical cell annealed for 90 min on a hotplate under a nitrogen atmosphere. These "ultra-fast" annealing times were obtained using a commercially available photonic curing system designed to thermally reduce metallic inks for printed electronics applications. We explore the implications of altering the annealing process window in order to obtain highly crystalline films and compare these to typical devices annealed on a hotplate. In addition, we characterise photonic annealed perovskite films using xray diffraction spectroscopy (XRD) and local photoluminescence spectroscopy (PL) to determine the impact of fast annealing on film formation, morphology and crystal growth. Transient Photovoltage (TPV) and Transient Photocurrent (TPC) decays were also measured to gain information on how the differing film morphologies and thicknesses obtained from conventional and photonically annealed perovskite films affects recombination in these devices.

ing boasts broadband spectral output between 200 and 1,000 nm



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**Fig. 1** Composed photograph of photonic annealed perovskite samples (28 mm  $\times$  28 mm) with increasing flash durations at 500 V lamp voltage, as well as a film annealed conventionally using a hotplate.

## <sup>62</sup> **2 Results & Discussion**

 Initial visual observations were made of photonically annealed perovskite films in order to determine flash times with an ideal <sup>65</sup> film being assumed to have a uniform, dark brown appearance similar to that of conventionally annealed films. Figure 1 shows 67 4 such films processed with increasing flash durations at a fixed lamp voltage as well as a sample annealed for 90 minutes on a <sup>69</sup> hotplate at 100°C under nitrogen. It is interesting to note the difference in transparency along opposite edges in the photonic annealed samples: these regions are masked from the light source by metal strips used to secure the glass sample to the instrument platform, consequently, these covered areas do not crystallise to form the perovskite structure. This effect demonstrates that an- nealing is driven only by direct exposure of the precursor film to a photonic pulse, thus excluding the possibility of indirect heating of the precursor via the substrate.

 $\frac{78}{17}$  Similar to other rapid annealing techniques, <sup>17</sup> Figure 1 demon-<sup>79</sup> strates how careful tuning of the annealing time is required for 80 optimal device appearance. The  $750 \mu s$  annealed film shows <sup>81</sup> spherulitic formations arising from un-annealed precursor solu-82 tion reacting with moisture within the air, demonstrating that the film has not been fully annealed into the desired  $\mathrm{CH_{3}NH_{3}PbI_{3}}$ 83 84 perovskite material. Conversely, the  $1,500 \mu s$  annealed film ex-85 hibits yellow discolouration which is indicative of thermal decom- $_{86}$  position to  $PbI_2$ .<sup>15,23</sup> We also note a flame-like pattern progress-87 ing from left to right across photonic annealed films with increas-88 ing exposure. This is a result of the forced directional airflow 89 across the sample intended to protect the flash bulb from evolved 90 solvents during annealing. This airflow blows CH<sub>3</sub>NH<sub>3</sub>Cl evolved 91 from the precursor during annealing across the sample surface, <sup>92</sup> causing the light to be occluded behind the so-called "forced-air <sup>93</sup> front". This light attenuation results in regions below the evolved 94 CH<sub>3</sub>NH<sub>3</sub>Cl being annealed to a lesser degree than more exposed <sup>95</sup> areas. A schematic diagram further illustrating this phenomena is 96 shown in Figure S1 in the ESI†.

97 The option of drying the deposited precursor prior to flash an- nealing would likely improve film reproducibility. The effects of solvent evaporation causing discontinuous annealing would be greatly reduced in this case. In addition, using perovskite

precursor solutions eschewing  $PbCl<sub>2</sub>$ , such as those containing  $\frac{101}{2}$ only  $CH_3NH_3I$  and  $PbI_2$ , may improve film reproducibility as no  $102$  $CH<sub>3</sub>NH<sub>3</sub>Cl$  would be evolved, occluding the film during crystalli- 103 sation. The contract of the co

As well as colour differences across the surface of photonic an-<br>105 nealed samples, there also appeared to be variations in surface 106 roughness within the same film. In some regions, the perovskite 107 films appear extremely smooth and reflective whereas other regions show a more "hazy" surface. Surface roughness measure-<br>ments were performed using a profilometer and found tvoical Ra ments were performed using a profilometer and found typical Ra values of 5 nm and 100 nm for respective smooth and reflective 11. regions, with the 230 nm thick bare  $\text{Al}_2\text{O}_3$  scaffold measuring at  $^{112}$ 3 nm Ra. Corresponding surface profile plots are seen in Figure S2 113 in the ESI†. Figure 2 shows SEM micrographs of different regions 114 of a photonic annealed film, as well as cross-section schemat- <sup>115</sup> ics suggesting the distribution of perovskite mate-rial through- $_{11}$ out the film: Section "a" represents a characteristic hazy region,  $\frac{1}{11}$ whereas "b" represents a typical smooth and reflective region. 118 The micrographs demonstrate that, in the case of the smooth sec-<br>119 tions, the entire bulk of perovskite material is confined within <sup>120</sup> the mesoporous  $Al_2O_3$  film. In the more hazy section, outcrops  $121$ of perovskite material are seen above the  $\text{Al}_2\text{O}_3$  film in a struc-  $\frac{122}{2}$ ture more similar to that observed in devices which have a perovskite capping layer that extends beyond that of the mesoporous 124 structure.<sup>24</sup> We suggest that the lack of a discrete and continuous capping layer across the film's surface is due to the near- <sup>126</sup> instantaneous phase transformation undergone during annealing 127 which may have lead to precursor being ejected from the glass  $\frac{128}{129}$ <br>surface.  $\frac{1}{2}$ surface.

Photoluminescence intensity measurements for the photonic 130 and hotplate annealed films are shown in Figure 3a. There is a  $131$ blue-shift in emission from hotplate to photonic annealing which 132 is attributed to the smaller crystal sizes obtained when using such  $\frac{1}{133}$ a rapid heating method. XRD measurements for hotplate and photonic annealed films, seen in Figure 3b confirm these hypothe-<br>ses.  $\text{ses.}$  126

While the films shown in Figure 1 exhibit yellowed regions in-<br>1350 dicating the presence of  $PbI_2$ , the XRD and photoluminescence  $\frac{138}{13}$ measurements shown in Figure 3 were performed on samples 130 further optimised between 1.0 ms and 1.2 ms which showed no visual evidence of PbI<sub>2</sub>. The spectra for photonic annealed perovskite films shows reduced preferential orientation compared to 142 hotplate annealed counterparts as a result of this scaffold confine-<br>143 ment. In slow hotplate annealing, grains have more time to grow 144 into large, oriented crystals as seen in Figure 2. By comparison,<br>photonic annealed films are crystallised in timeframes 4.5 million photonic annealed films are crystallised in timeframes 4.5 million <sup>146</sup> times faster using entirely different crystallisation kinetics, thus 147 leading to smaller grain sizes.  $148$ 

An analysis of J-V statistics is presented in Figure 4. While over- 149 all PCEs in photonic annealed cells are lower than hotplate an- $150^\circ$ nealed devices the V<sub>OC</sub> remains high in the optimised group. This  $151$ would indicate that the drop in performance is not due to pinhole  $_{152}$ formation or poor perovskite film coverage as this has been found 153 to reduce voltages in perovskite devices due to recombination at 154 the interface between the c-TiO<sub>2</sub> and Spiro-OMeTAD that arises  $155$ inside pinholes. <sup>25</sup> The high V<sub>OC</sub> indicates good coverage and in-  $156$ 



**Fig. 2** Top: SEM micrographs showing different surface regions of a photonic annealed perovskite film. a) Represents a reflective region whereby the perovskite material appears to be confined within the mesoporous scaffold. b) Represents a "hazy" region where perovskite "islands" protrude through the scaffold surface. Also included is a micrograph of a hotplate-annealed perovskite film which shows a more continuous perovskite capping layer. Bottom: Schematic cross-section representations of the corresponding films, whereby a) indicates total perovskite confinement within the scaffold, b) shows some capping layer outcrops above the Al $_2$ O $_3$ , and c) shows a near continuous perovskite capping layer.

 $_{157}$  timate contact between the electron selective TiO<sub>2</sub> compact layer and perovskite film. This suggests that, while annealing is driven by direct exposure of the perovskite precursor to light instead of a traditional substrate-driven thermal reaction, there is sufficient photon penetration to anneal perovskite at the c-TiO<sub>2</sub> interface. Short-circuit current density and fill factor are markedly lower in the fast processed devices. The drop in  $J_{SC}$  is attributed to the <sup>164</sup> lack of perovskite capping layer above the  $\text{Al}_2\text{O}_3$  scaffold, which limits the thickness. The lower fill factors arise in part due to an apparent increase in series resistance, which can be attributed to poor contact between the Spiro-OMeTAD and the perovskite layer. The lack of capping layer in the photonically annealed de- vices means that instead of forming a conformal heterojunction (as would be expected in the presence of a capping layer), the <sup>171</sup> Spiro-OMeTAD makes contact with outcrops of  $\text{Al}_2\text{O}_3$ , as well as 172 the perovskite, reducing the effective contact area and thereby



**Fig. 3** a) Photoluminescent intensity for hotplate and photonic annealed perovskite films. b) X-ray diffraction spectra for mp- $Al_2O_3$  coated FTO, photonic annealed and hotplate annealed films.

introducing series resistance losses. Despite remarkably low an- $173$ nealing times, a clear optimum flash length may be ob-served in 174 Figure 4. between  $1,125 \mu s$  and  $1,175 \mu s$  pulse exposure which  $175$ may at first seem problematic as the processing window seems  $176$ rather limited, but looking closer at the statistical JV data it can  $17.7$ be seen that there are significant improvements in performance at  $178$ an exposure time of  $1150 \mu s$  compared to exposure times of just  $179$  $\pm$ 50  $\mu$ s. This indicates the degree of precision and accuracy of the 180 instruments control system that would be essential to make this a 181 commercially viable technique for perovskite solar cell manufac $true.$ 



**Fig. 4** Statistical analysis of J-V parameters for photonic annealed cells processed at different exposure times, as well as hotplate annealed counterparts.

(TPC) decay experiments were carried out on a selection of devices. Data from these experiments are presented in Figure 5. <sup>186</sup> Figure 5a shows the TPV lifetime of a hotplate annealed device  $\frac{187}{18}$ and that of a photonically annealed device. The TPV decay curves in this case were multi-exponential as observed elsewhere.<sup>25</sup> In line with the reasoning of O'Regan and coworkers,  $^{26}$  to extrapolate the decay lifetimes we fit a double exponential function to the decay and take the faster of the two time constants as the  $102$ effective recombination lifetime. Looking at Figure 5a one can 193 see why V<sub>OC</sub> remains high in photonically annealed devices. It 194 appears that recombination is slower (for a given  $V_{OC}$ ) in the 195 photonically annealed device. This is further evidence of a good 196 conformal contact between c-TiO $_2$  and perovskite layer. For an  $_{\, \, \rm 197}$ 



**Fig. 5** Comparisons between hotplate and photonically annealed perovskite solar cells: a) Recombination lifetimes of devices for a given  $V_{\text{OC}}$ . b) Charge density for a given  $V_{\text{OC}}$ . c) Recombination lifetime for a given charge density.

198 explanation of the drop in  $J_{SC}$ , the charge density of the devices can be obtained from their respective TPV and TPC data via cal- culation of the differential capacitance.<sup>26</sup> This data is shown in  $F_{201}$  Figure 5b and it is clear that the charge density (C cm<sup>-2</sup>) in pho- tonically annealed devices is significantly lower, supporting the hypothesis that the poorer performance is due to a thinner per- ovskite film thickness or lack of a capping layer. Having identified the effective recombination lifetime and charge density, we can 206 look at recombination lifetime for a given charge density  $(C \, \text{cm}^{-2})$ , this is shown in Figure 5c. Conversely to Figure 5a, Figure 5c shows that recombination (for a given charge density) is faster in the photonically annealed device. This primarily results from the thinner perovskite layer and so emphasises the need for further optimisation of the technique or process conditions so that per- ovskite film thickness and capping layers remain favourable for increased device performance.

Despite the aforementioned drop in photonically annealed de- <sup>214</sup> vice current and fill factor compared to hotplate processed cells, a 215 maximum PCE of 11.3% is produced compared to 15.2% for the 216 conventionally produced cell as seen in Table 1. Figure 6a shows 217 J-V curves for the best performing photonic and hotplate pro- <sup>218</sup> cessed devices, whereas Figure 6b shows time-dependent lamp <sup>219</sup> power density measurement extracted from the photonic sintering tool corresponding to a pulse profile yielding the highest per-<br>
<sub>22</sub>1 forming cell. 222



**Fig. 6** a) J-V curves for highest performing photonic and hotplate annealed perovskite solar cells. b) A time-dependent power density plot of the flash used to anneal the highest performing device.

The decay of lamp power over time is a result of the instruments capacitors draining as the flash bulb is engaged as shown  $2+$ in Figure 6b. It was found that "square" energy profiles could 225 only be achieved using short exposure times and lower voltages 220 than those required to fully anneal perovskite films in a single flash. Such uniform profiles would reduce the complexity of ob- $_{22}$ taining optimal flash annealing parameters. Interestingly, the energy density required to anneal the highest performing perovskite film, 3.99 J cm<sup>-2</sup>, corresponds to between 10-130 times the minimal erythemal dose required to sunburn skin depending on skin 23 color.<sup>27</sup> Despite these seemingly high energies, the process is remarkably more efficient than hotplate annealing which was mea-<br>
<sub>234</sub> sured using an electricity usage monitor to be ca. 200 J cm<sup>-2</sup> in 23<sup>6</sup> order to maintain a laboratory hotplate at 100℃ for 90 minutes. 236 This figure rises significantly if the hotplate's initial heating is in-<br>237 cluded. This 50 times reduction in power requirement poses a 236 substantial cost saving in the case of commercial production compared to hotplate annealing.  $240$ 

**Table 1** Hero cell efficiency data for both conventional and photonic annealed perovskite solar cells.

Annealing method	$V_{OC}$ (V)	$J_{SC}$ $(mA cm-2)$	Fill Factor (%)	PCE $(\% )$
Hotplate	1.03	19.8	75	15.23
Photonic	1.05	16.0	67	11.27

# **3** Conclusions

In conclusion, we have demonstrated that the time and energy required to fully anneal  $\mathrm{CH_3NH_3Pbl_{3-x}Cl_x}$  perovskite films may be 243 drastically reduced using a novel flash annealing process. In as <sup>244</sup> little as 1.15 ms, a spin-coated precursor solution may be fully <sup>245</sup> annealed using an intense flash of white light and yield PCEs <sup>246</sup> in excess of 11% compared to 15% in a 90 minute, inert atmo- <sup>247</sup>

 sphere, hotplate annealed cell. Such a rapid annealing process in- troduces new crystallisation kinetics which yield notably smaller perovskite crystals compared to conventionally processed films, as proven using PL and XRD measurements. While overall PCEs in fast-processed devices falls short of the conventional processing method, the amount of energy and time required to achieve such films is dramatically reduced. This work presents some initial op- timisation of the photonic annealing process however with addi- tional control of the photonic pulsing which inhibits the removal of the capping layer, devices with performance equivalent to con- ventionally produced devices are possible. In summary this pro- cess represents a 4.5 million times reduction in processing time and a 50 times reduction in the power requirements, both criti- cal contributors towards the successful commercial production of perovskite photovoltaics.

#### <sup>263</sup> **4 Experimental**

#### <sup>264</sup> **4.1 Device fabrication**

 Working electrodes were prepared by depositing a compact  $_{\rm 266}$   $\rm TiO_2$  (c-TiO $_{\rm 2}$ ) layer upon a 3 mm thick FTO glass substrate (7Ω sq<sup>-1</sup>, Ra: 12 nm, NSG Pilkington) through spray pyrolysis at <sup>268</sup> 450 °C A mesoporous  $\text{Al}_2\text{O}_3$  (mp- $\text{Al}_2\text{O}_3$ ) film was next deposited  $_{269}$  by diluting a dispersion of  $\mathrm{Al}_2\mathrm{O}_3$  nanoparticles (Sigma-Aldrich PN:702129) in isopropanol (1:2 by volume), and spin coating for 60 s at 4,500 rpm. Upon drying at 150 $\degree$ C for 10 minutes on a hot- plate, a 230 nm scaffold was produced. A mixed-halide perovskite precursor was prepared in DMF by dissolving a 40wt%, 3:1 molar <sup>274</sup> ratio of  $CH_3NH_3I$  and  $PbCl_2$  before spin coating onto the mp- $_{275}$  Al $_{2}$ O<sub>3</sub> layer for 45 seconds at 2,000 rpm. In the case of photonic annealing, this process was performed in air (20 $\degree$ C, c.50% RH), 277 whereas hotplate-annealed reference devices were deposited and <sup>278</sup> annealed in a N<sub>2</sub>-filled glovebox (<0.5 ppm H<sub>2</sub>O, <0.5 ppm O<sub>2</sub>, MBraun). Hotplate annealed samples underwent 100 $\degree$ C for 90  $_{280}$  minutes, followed by 120 $^{\circ}$ C for 10 minutes as described else- where.<sup>12</sup> The typical term "photonic curing" was used to de- scribe subjection of a precursor-coated sample to xenon flash-bulb emission over very small time scales. Photonic cured samples were immediately transferred from spin-coater to photonic cur- ing tool (PulseForge 1300, Novacentrix) and flash annealed in milliseconds without prior or subsequent heating. Distance be- tween lamp and sample was fixed at a point recommended by the manufacturer, initial trials undertaken at points outside the recommended distance showed much greater variability due to irradiance irregularity and so are not shown here. Lamp volt- age was maintained at 500 V. Upon completion of the annealing step, samples were cooled to room temperature before a solution containing 2-7,7-tetrakis(N,N-di-p-methoxyphenylamine)-9,9 17- spirobifluorene (spiro-OMeTAD) in chlorobenzene and additives 295 (10  $\mu$ l/ml tBP, 32  $\mu$ l/ml Li-TFSI solution: 600 mM in acetonitrile) was spin-coated onto the perovskite film before 80 nm thick Au contacts were evaporated at  $10^{-4}$  torr.

#### <sup>298</sup> **4.2 Characterisation**

<sup>299</sup> Scanning electron microscopy imaging of photonic and hotplate <sup>300</sup> annealed samples were collected using a JSM-7800F field emission gun electron microscope from Jeol (USA), with a 5 kV beam, 301  $10 \mu A$  at approximately 4.1 mm working distance. X-ray diffrac-  $302$ tion analyses of the crystalline properties of the annealed films 303 were carried out using a D8 Discover instrument from Bruker 304 (Germany) with a CuK $\alpha$  beam at 40 kV and 40 mA and scan pa-  $305$ rameters of 0.1 s/step at 0.01  $2\theta$  step size.  $306$ 

Transient photovoltage and photocurrent decays were mea- 397 sured as described previously.<sup>28</sup> The white bias light was pro- $308$ vided by a BRIDGELUX 9000 lumen LED array (Farnell) whilst 309 the pulse light was provided by a OSLON PowerCluster green 316 LED array (RS). Pulse intensity was chosen to ensure ΔV re- 31. mained within the small perturbation regime. A pulse length of  $312$  $10 \mu s$  was utilised and was generated via a fast MOSFET transis-<br>31. tor controlled by a National Instruments USB-6251 data acquisi- <sup>314</sup> tion board (DAQ) and WaveMetrics IGOR Pro software. Voltages 315 were measured directly using the DAQ. Currents were measured  $31\degree$ by the DAQ as a voltage drop across a 30  $\Omega$  resistor. The open- 31. circuit voltage was allowed to equilibrate for  $>60$  s before the  $\frac{318}{216}$ perturbation pulse was fired. The variance in photovoltage in the <sup>319</sup> preceding 10 s before the perturbation pulse was fired was found <sup>320</sup> to be, on average,  $\langle 1.2 \text{ mV}$ . A biphasic photovoltage decay was  $321$ observed and fit with a double exponential function. The faster 322 of the two resultant time constants was taken as the effective recombination lifetime. Differential capacitance and charge density 324 were calculated as described elsewhere.<sup>26</sup>  $325$ 

Emission spectra of perovskite thin films were observed using 326 a Olympus BX51 M microscope coupled with an Ocean Optics 32<sup>1</sup> USB2000+ spectrometer and optical fiber. The optical fiber was  $328$ placed down the eyepiece of the microscope to collect the emission spectrum of the whole imaged area. Samples were illumi- 330 nated with a UV-mercury lamp (100 W Ushio Olympus) through 331 a filter block consisting of an excitation filter (TXRED filter CWL  $=$  332 559 nm) a dichroic mirror (TXRED reflection band =  $533-580$  nm,  $333$ transmission band = 595-800 nm) and an emission filter (665 nm  $\frac{3}{3}$ 4 Longpass). Emission spectra were measured in-situ simultane-<br>
<sub>335</sub> ously to image collection through averaging 50 scans with an integration time of 0.1 s. All observations were carried out at  $22 °C$ . 33.77

Masked devices  $(0.09 \text{ cm}^2)$  were tested under a class AAA  $_{330}$ solar simulator (Newport Oriel Sol3A) at AM1.5 and 100 mW 33  $\text{cm}^{-2}$  illumination conditions calibrated against a KG5 filtered silicon reference cell (Newport Oriel 91150-KG5) using a Keithley 341 2400 source meter. Current-voltage sweeps were performed from 342 forward-to-reverse bias at a rate of  $0.1 \text{V s}^{-1}$ . **.** 343

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