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Highly dense $Cu_{2-x}S$ bulks, fabricated by a meltsolidification technique, show high thermoelectric performance with zT of ~ 1.9 at 970 K. The $Cu_{2-x}S$ bulks show good thermal heat flow and diffusivity stability, and they exhibit excellent mechanical properties, with hardness of ~ 1 GPa. Density functional theory calculations indicate that $Cu_{2-x}S$ is an intrinsic p-type conductor.

1 Introduction

High temperature thermoelectric materials have received great attention due to their crucial roles in direct energy conversion between heat and electricity, based on the Seebeck effect¹ and Peltier effect². It is well known that the energy conversion efficiency for thermoelectric devices at a temperature T can be estimated by the dimensionless figure-of-merit (*zT*), defined as $zT = S^2T\sigma/\kappa$, where S, T, σ , and κ are the Seebeck coefficient, absolute temperature, electrical conductivity, and total thermal conductivity, respectively.³⁻ ⁷Apparently, high *zT* values can be achieved with concurrent high S and σ values, and low κ values.

Recently, it has been reported that hot-pressed Cu_{2-x}S polycrystalline bulks show high thermoelectric performance with the highest *zT* values on record, ~ 1.7 at 1000 K.^{8, 9} Furthermore, Cu_{2-x}S consists of copper and sulfur, both of

which are naturally abundant and non-toxic. Therefore, Cu_{2-r}S should be one promising high temperature thermoelectric materials. It should be noted that the polycrystalline bulks were generally fabricated by the hot pressing method using spark plasma sintering (SPS) systems under high temperature and high pressure. This approach requires costly instruments and high electrical current for SPS, and may lead to Cu migration¹⁰, which is disadvantageous for the large-scale fabrication of homogeneous thermoelectric materials. Therefore, it is favourable to find one time and energy efficient method to fabricate highly dense $Cu_{2-x}S$ samples. Furthermore, good stability for the thermoelectric properties such as electrical conductivity, Seebeck coefficient, and thermal conductivity are crucial for the practical applications of thermoelectric materials. Hence, it is essential to do repeated heating and cooling measurements to test the thermoelectric stability of the $Cu_{2-x}S$ compound.

In addition, mechanical stress caused by the good contact between the thermoelectric modules and the heat source, and thermal stress, induced by the temperature gradient between the hot and cold sides, coexist in the interior of thermoelectric devices, which can reduce the reliability of thermoelectric modules.¹¹⁻¹³Therefore, besides the high *zT* values, thermoelectric materials should also have good mechanical properties, and it is important to investigate the mechanical properties of the fabricated $Cu_{2,x}S$ samples.

It should be noted that the high-temperature α -phase Cu_{2-x}S has the same cubic crystal structure (space group: Fm3m)¹⁴⁻¹⁶ and superionic transport¹⁷ as Cu_{2-x}Se^{18, 19}, which makes this family of compounds distinct from other high temperature thermoelectric materials and leads to additional considerations for their use²⁰. It has been reported that hot-pressed Cu_{2-x}Se bulks show lower electrical conductivity than hot-pressed Cu_{2-x}Se bulks^{9, 19}, indicating that there may be some differences in doping or in their electronic band structures due to the differences in the lattice parameter and ionic radius of Se²⁻ and S²⁻. Therefore, it is desirable to investigate the electronic band structure for the Cu_{2-x}S system.

Herein, we report the successful fabrication of highly dense Cu₂S and Cu_{1.97}S bulks through a melt-solidification technique. The fabricated Cu_{1.97}S bulks show *zT* values as high as ~ 1.9 at 973 K, which confirms the reported high *zT* result and is somewhat higher than for the hot-pressed polycrystalline Cu_{1.97}S bulks. Moreover, the fabricated Cu₂S and Cu_{1.97}S samples show good thermal stability during repeated heating and cooling processes, and they exhibit excellent mechanical performance with the Cu_{1.97}S having a much higher Vickers hardness of ~ 1.0 GPa compared to PbTe²¹, Bi₂Te₃²², and PbSe²³ polycrystalline bulks. Density functional theory (DFT) calculations of the high temperature α -phase Cu_{2-x}S reveal that copper deficient Cu_{2-x}S compounds are intrinsic p-type conductors with similar band structure but shifted Fermi level compared to the stoichiometric Cu₂S.

2 Experimental

Highly dense $Cu_{2,x}$ Spolycrystalline bulks were fabricated by a melt-solidification technique. A mixture of Cu and S powders in the molar ratio 2-*x* : 1 (*x* = 0 and 0.03) was pressed into pellets and sealed in evacuated quartz tubes, before being heated to 400 °C for 1-5 hours with a heating rate of 5 °C/min, and then heated to ~ 1150 °C for 1-2 hours with a heating rate of 5 °C/min, followed by a furnace cooling to room temperature. The obtained bulks were shaped into disks with dimensions of $\Phi 10 \text{ mm} \times 1 \text{ mm}$ for the thermal diffusivity measurements. After the measurements, the same sample disks were cut into rectangular bars for measurements of the electrical conductivity and Seebeck coefficient.

X-ray diffraction (XRD) patterns and field emission scanning electron microscope (FE-SEM) images were collected on GBC MMA and JEOL JSM-7500FA systems, respectively. The electrical conductivity and Seebeck coefficient were measured simultaneously in a helium atmosphere in the temperature range from 400 to 973 K using a RZ2001i system. The thermal diffusivity (D) was measured by the laser flash method (LINSEIS LFA 1000), and the specific heat (C_p) was determined by differential scanning calorimetry (Mettler Toledo TGA/DSC 1). The sample density (*dd*) was determined by the Archimedes method. The thermal conductivity (κ) was calculated by $\kappa = D \times C_p \times dd$. Vickers hardness of the as-prepared samples was measured at different locations employing the Duramin 70 Vickers hardness tester applying a load of 0.1 N.

First principles calculations were performed using

density functional theory (DFT) implemented by the Cambridge Serial Total Energy Package (CASTEP) package²⁴. The generalized gradient approximation (GGA)²⁵ was used in this calculation, with parameterization by the Perdew-Burke-Ernzerhof (PBE)²⁶ and ultra-soft pseudopotentials. The plane wave cut-off energy was set at 400 eV. A 4×4×4 Monkhorst-Pack k-point mesh, with a Brillouin zone path of Γ XWL Γ K of the primitive cell, was employed for the band structure calculations. The total and partial density of states of Cu₂S and copper deficient Cu_{1.875}S were calculated on a 2×2×2 super-cell of the primitive cell.

3 Results and discussion

Fig. 1 shows the X-ray diffraction patterns and typical field emission scanning electron microscope cross-sectional image for the the Cu₂S and Cu_{1.97}S bulks fabricated by a melt-solidification technique. The results indicate that all the fabricated bulks are single phase and crystallized in the orthorhombic structure (PDF No. 23-961). Furthermore, the bulks are composed of highly dense and micro-scale grains without any visible voids or porosity.



Fig. 1 (a) X-ray diffraction patterns for the Cu₂S and Cu_{1.97}S bulks fabricated by a melt-solidification technique, and for standard low temperature β -phase Cu₂S (PDF No. 23-961), and (b) Typicalfield emission scanning electron microscope cross-sectional image of the melted-solidified bulks.

Fig. 2 shows the temperature dependence of the electrical conductivity, Seebeck coefficient, thermal conductivity, and dimensionless figure-of-merit for the fabricated Cu₂S and Cu_{1.97}S bulks in the temperature range from 400 K to 1000 K. The electrical conductivity for the high temperature α -phase Cu_{1.97}S bulks decreases as the temperature increases, showing the typical electrical

conductivity behavior of metallic or heavily doped semiconducting materials, with values between 185 and 120 $S \cdot cm^{-1}$ over a wide temperature range from 700 to 1000 K. On the other hand, the Cu₂S bulks have much smaller electrical conductivity over the whole measured temperature range compared to the Cu_{1.97}S bulks, with the highest value ~ 30 $S \cdot cm^{-1}$ at 973 K. The Cu₂S bulks have a much higher Seebeck coefficient than Cu_{1.97}S from 400 to 1000 K, with the highest values being $\sim 240~\mu V \cdot K^{\text{-1}}$ for $Cu_{1.97}S$ and $\sim 370~\mu V \cdot K^{\text{-1}}$ for Cu₂S, respectively. The above data reveals that the Cu_{1.97}S should have a higher power factor than the Cu₂S, and the temperature dependence of the power factor is shown in Fig. S1[†]. The temperature dependence of the specific heat displayed in Fig. S2[†] indicates that both samples have two phase transitions at around 350 - 400 K and 600 - 750 K. The thermal conductivity displayed in Fig. 2c indicates that both

the Cu₂S and the Cu₁₉₇S bulks have low κ values between 0.5 and 0.3 W·m⁻¹·K⁻¹ in the temperature range from 400 to 1000 K. The low thermal conductivity may come from the liquidlike behavior of copper ions in the rigid face-centered cubic, fcc, sublattice constituted by the S atoms and the low average speed of sound⁹. The *zT* values for the Cu_2S and $Cu_{1.97}S$ bulks shown in Fig. 2d demonstrate that the total thermoelectric performance is very sensitive to the copper deficiency, with *zT* over 1.0 at T > 700 K and as high as 1.9 at 973 K for the $Cu_{1.97}S$, and zT of ~ 1.0 at 973 K for the Cu_2S . Furthermore, in the temperature range from 700 to 1000 K, the Cu₂S and Cu_{1.97}S bulks fabricated by the melt-solidification technique confirm the high thermoelectric performance of Cu_{2-x}S with perhaps even higher zT values compared to the SPS hotpressed samples⁹, which could be due to better optimization of the carrier concentration via the copper deficiency.



Fig.2 Temperature dependence of the thermoelectric properties for the fabricated Cu₂S and Cu_{1.97}S polycrystalline bulks: (a) electrical conductivity (σ), (b) Seebeck coefficient (*S*), (c) thermal conductivity (κ), and (d) dimensionless figure-of-merit (*zT*). The reproduced *zT* values for hot-pressed polycrystalline samples (labelled as hp-Cu₂S and hp-Cu_{1.97}S⁹) are also shown in Fig. 2d.

The electrical and thermal stability are quite essential for the practical applications of thermoelectric materials. Therefore, we repeated the electrical conductivity, Seebeck coefficient and thermal diffusivity measurements several times for the melt-solidified Cu_2S and $Cu_{1.97}S$ samples in the temperature range from 400 to 1000 K, to test whether they are stable or not.

Fig. 4 shows the the temperature dependence of the thermal diffusivity, electrical conductivity (σ), Seebeck coefficient (S), and power factor (PF) for the fabricated Cu₂S and Cu_{1.97}S polycrystalline samples. Additionally, the

differential scanning calorimeter (DSC) thermal response measurements plots for the fabricated $Cu_{1.97}S$ sample are also displayed in Fig. S3[†]. Both the temperature dependent thermal diffusivity and heat flow show good reproducibility, and these results indicate that the fabricated Cu_2S and $Cu_{1.97}S$ bulks are thermally stable during the repeated heating and cooling processes. The electrical conductivity and Seebeck coefficient for the Cu_2S and $Cu_{1.97}S$ samples, however, exhibit poor stability under the concurrent of high temperature and electrical field with repeated heating and cooling treatments. The electrical conductivity decreases with



Fig. 3 Temperature dependence of the thermoelectric properties for the fabricated Cu_2S and $Cu_{1.97}S$ polycrystalline bulks: (a) thermal diffusivity, (b) electrical conductivity (σ), (c) Seebeck coefficient (S), and (d) power factor (PF).



Fig. 4 Vickers hardness values of the fabricated Cu_2S and $Cu_{1.97}S$ bulks. The hardness values of polycrystalline Bi_2Te_3 , PbTe, PbSe, and Cu_2Se bulks are also provided for comparison.

the increasing times of heating and cooling processes, while the Seebeck coefficient shows the opposite trend with enhanced values. The calculated power factor for the fabricated Cu_2S and $Cu_{1.97}S$ bulks, especially for the $Cu_{1.97}S$, shows much better stability than that of the electrical conductivity and Seebeck coefficient, thanks to the interaction between them.

This poor reproducibility for the electrical conductivity, Sebbeck coefficient as well as the power factor for the Cu_2S and $Cu_{1.97}S$ samples can be ascribed to several factors. It might be related to the superionic conductivity of this compound, the copper ions could move from one side of the sample to the other side upon the application of an electrical field. Additionally, the evaporation of sulfur during the measurements can also lead to the poor reproducibility of electrical conductivity and Seebeck coefficient.²⁹ These problems might can be restained by decreasing the applied electrical field for measurements, doping approaches that can weaken the drift of copper ions, and increasing the pressure of inert gases in the measurement chamber to supress the evaporation. It should be noted that the stable thermal properties, such as heat flow and thermal diffusivity, and ehanced seebeck coefficient after repeated heating and cooling processess, could make this compound find potentail applications in other thermal related areas and sensor applications.

Fig. 4 shows the Vickers hardness values of the Cu₂S and Cu_{1.97}S polycrystalline bulks. The Vickers hardness values of several other thermoelectric materials are also presented for comparison. It was reported that hot-pressed polycrystalline Bi₂Te₃²⁷, PbTe²⁸, and PbSe²³ bulks show hardness of around 0.62, 0.40, and 0.60 GPa, respectively. Compared to the Cu₂, se polycrystalline bulks having hardness of around 0.42 GPa, the Cu₂S and Cu_{1.97}S bulks exhibit much higher hardness, with values of ~ 0.97 GPa for the Cu₂S and ~ 1.0 GPa for the Cu_{1.97}S, respectively.



Fig.5 Calculated electronic band structures for the stoichiometric $\mathrm{Cu}_2\mathrm{S}.$

Band structure calculations enable us to gain insight into the electronic states near the Fermi level (E_F) as well as the charge carrier types in the system. Fig.5 shows the calculated electronic band structures for the high temperature cubic phase of the stoichiometric Cu₂S. The calculations predict that Cu₂S will be a small-band-gap semiconductor. The calculated band gap is essentially zero at the Γ point, but it is well known that the DFT method often underestimates the gap.

Fig.6 shows the calculated total and partial density of states (DOS) for the stoichiometric Cu_2S and copper deficient $Cu_{1.875}S$. It reveals that the valence bands consist of three regions: a lower region between 12 and 16 eV below the E_F , which is mainly constituted by S 3s states, a middle region between 4 and 8 eV below the E_F , which is a mixture of Cu 3p, 3d, and 4s states, and S 3p states, and an upper region between the E_F and -4 eV, which mostly consists of Cu 3d states, even though the S 3p states also contribute to this region.

For the stoichiometric Cu₂S, the calculated partial and total DOS is in good agreement with the electronic band structure calculation results, further evidence that the stoichiometric Cu₂S is a small-band-gap semiconductor. As to the copper deficient Cu_{1.875}S, the Cu 3d states and S 3p states of the middle region, belonging to the valence bands, penetrate into E_F . This explains well why the copper deficient Cu_{2-x}S is a p-type conductor and why its conductivity is higher than that of the stoichiometric Cu₂S from experimental observations.



Fig. 6 Calculated total and partial density-of-states (DOS) for the stoichiometric Cu_2S (left) and copper deficient $Cu_{1.875}S$ (right) using density functional theory.

4 Conclusions

In summary, our results indicate that the meltsolidification technique works well for the fabrication of highly dense Cu_2S and $Cu_{1.97}S$ polycrystalline bulks. The fabricated $Cu_{1.97}S$ bulks show excellent thermoelectric performance, with *zT* as high as ~1.9 at 973 K, and good mechanical properties with a Vickers hardness of ~ 1.0 GPa. Moreover, both the synthesized Cu₂S and Cu_{1.97}S show quite good repeatibility for the thermal diffusivity during the repeated heating and cooling processes, while they exhibit poor reproducibility for the electrical conductivity, Seebcek

coefficient and power factor under the concurrent of high temperature and electrical field. Density functional theory calculations reveal that stoichiometric Cu_2S is a small-band-gap semiconductor, and copper deficiency makes the copper deficient $Cu_{2-x}S$ to be an intrinsic *p*-type conductor.

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Notes and references

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†Electronic Supplementary Information (ESI) available: Temperature dependence of power factor (PF) for the fabricated Cu₂S and Cu_{1.97}S bulks (Fig. S1); temperature dependence of the specific heat for the fabricated Cu₂S and Cu_{1.97}S (Fig. S2); differential scanning calorimeter thermal response plots for the fabricated Cu_{1.97}S bulks (Fig. S3); ideal version of unit cell and primitive cell for the high temperature α -phase Cu₂S (Fig. S4); and X-ray diffraction patterns for the polycrystalline pellets used for the thermal diffusion measurements (Fig. S5).

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