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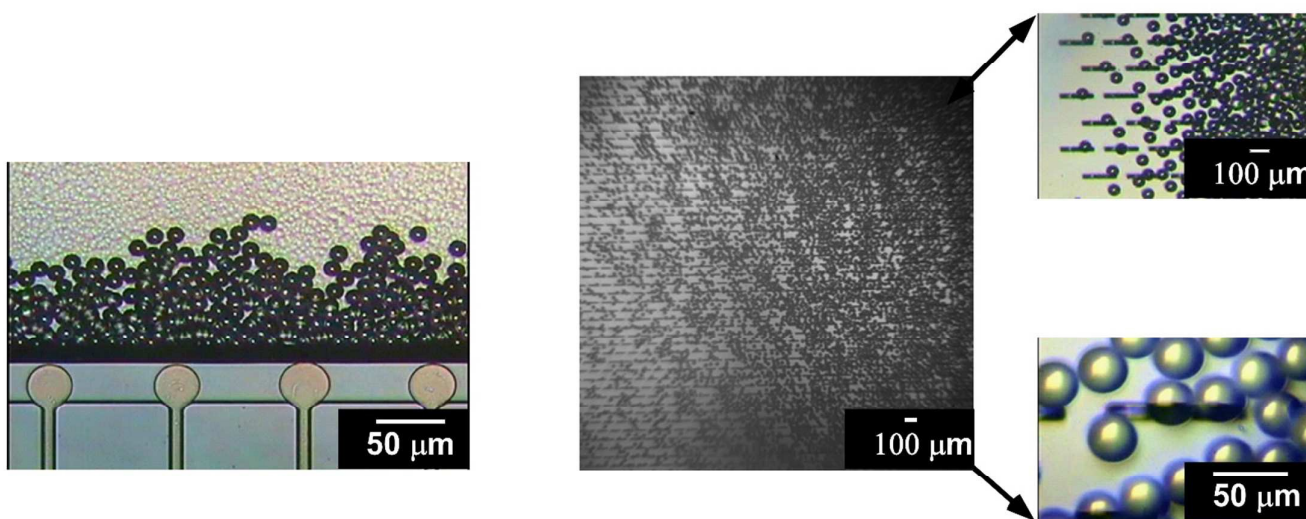
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## Graphical abstract

Food grade monodisperse O/W emulsions encapsulating ergocalciferol have been formulated using microchannel emulsification. The O/W emulsion droplets have encapsulation efficiency of over 85% within the evaluated storage period.



**Typical droplet generation encapsulating ergocalciferol in grooved microchannel emulsification**

**O/W emulsion encapsulating ergocalciferol in straight through microchannel emulsification**

1 **Formulation characteristics of triacylglycerol oil-in-water emulsions loaded with ergocalciferol**  
2 **using microchannel emulsification**

3 Nauman Khalid<sup>a, b, c</sup>, Isao Kobayashi<sup>a, \*</sup>, Zheng Wang<sup>a, c</sup>, Marcos A. Neves<sup>a, c</sup>, Kunihiko Uemura<sup>a</sup>,  
4 Mitsutoshi Nakajima<sup>a, c</sup> and Hiroshi Nabetani<sup>a, b</sup>

5  
6 <sup>a</sup> Food Engineering Division, National Food Research Institute, NARO, 2-1-12 Kannondai, Tsukuba,  
7 Ibaraki 305-8642, Japan

8

9 <sup>b</sup> Graduate School of Agricultural and Life Sciences, The University of Tokyo, 1-1-1 Yayoi, Bunkyo-  
10 ku, Tokyo 113-8657, Japan

11

12 <sup>c</sup> Faculty of Life and Environmental Sciences, University of Tsukuba, 1-1-1 Tennoudai, Tsukuba,  
13 Ibaraki 305-8572, Japan

14

15 \* Corresponding Author. Tel.: 81 29 838 8025; fax: +81-29-838-8122.

16 E-mail address: isaok@affrc.go.jp (I. Kobayashi)

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22 Ergocalciferol is one the important form of vitamin D that is needed for proper functioning of human  
23 metabolic system. The study formulates monodisperse food grade ergocalciferol loaded oil-in-water  
24 (O/W) emulsions by microchannel emulsification (MCE). The primary characterization was  
25 performed with grooved MCE, while storage stability and encapsulating efficiency (EE) was  
26 investigated with straight-through MCE. The grooved microchannel (MC) array plate has  $5 \times 18\text{-}\mu\text{m}$   
27 MCs, while asymmetric straight-through MC array plate consists of numerous  $10 \times 80\text{-}\mu\text{m}$  microslots  
28 each connected to a  $10\text{-}\mu\text{m}$ -diameter circular MC. Ergocalciferol at a concentration of 0.2-1.0%  
29 (w/w) was added to various oils and served as the dispersed phase, while the continuous phase  
30 constituted either of 1% (w/w) Tween 20, decaglycerol monolaurate (Sunsoft A-12) or  $\beta$ -  
31 lactoglobulin. The primary characterization indicated successful emulsification in the presence of 1%  
32 (w/w) Tween 20 or Sunsoft A-12. The average droplet diameter increased slowly with increasing  
33 concentration of ergocalciferol and ranged from 28.3 to  $30.0\text{-}\mu\text{m}$  with coefficient of variation below  
34 6.0%. Straight-through MCE was conducted with 0.5% (w/w) ergocalciferol in soybean oil together  
35 with 1% (w/w) Tween 20 in Milli-Q water as optimum dispersed and continuous phases.  
36 Monodisperse O/W emulsions with Sauter mean diameter ( $d_{3,2}$ ) of  $34\text{-}\mu\text{m}$  with relative span factor of  
37 less than 0.2 were successfully obtained from straight-through MCE. The resultant oil droplets were  
38 physically stable for 15 d at  $4\text{-}\text{C}$  without any significant increase in  $d_{3,2}$ . The monodisperse O/W  
39 emulsions exhibited ergocalciferol EE of more than 75% during the storage period.

40 **Keywords:** Microchannel emulsification, Asymmetric microchannel, Grooved microchannel, Oil-in-  
41 water emulsions, Monodisperse droplets, Ergocalciferol, Emulsifier concentration, Droplet  
42 generation, Dispersed phase flux

43

## 44 Introduction

45 Vitamin D plays a vital role in maintaining and developing healthy human skeletal system, since it  
46 maintains calcium level in the body. Deficiency of vitamin D results in increased risk of diabetes,  
47 hypertension, cancer and autoimmune diseases.<sup>1-4</sup> Broad spectrum deficiencies of vitamin D include  
48 rickets in children, osteomalacia in adults and osteoporosis in women, all of these lead to softening  
49 and weakening of bones.<sup>5-7</sup> Nutritional and cultural factors leading to vitamin D deficiency include  
50 insufficient fortified food consumption, sun-block usage, limited body exposure to sun and fear for  
51 excessive intake of vitamin D.<sup>7,8</sup> Vitamin D is synthesized in the skin and involves the  
52 phytochemical conversion of pro-vitamin D by the action of ultraviolet (UV-B) rays. This process  
53 takes place if the UV-B rays fall between 290-315 nm of spectrum. These rays are only emitted in  
54 the regions that lie below 35° latitude.<sup>9,10</sup>

55 The terminology and classification related to vitamin D is confusing and can be classified  
56 into 5 different forms and metabolites. Among these vitamin D<sub>2</sub> (ergocalciferol) and D<sub>3</sub>  
57 (cholecalciferol) are important (Fig. 1).<sup>11,12</sup> Vitamin D<sub>2</sub> is naturally present in some plants and is  
58 produced commercially by UV irradiation of yeast, while vitamin D<sub>3</sub> is naturally produced in human  
59 and animal bodies. Vitamin D<sub>2</sub> is substantially used for fortification and supplementation in food and  
60 pharmaceutical industries.<sup>12</sup> Several researchers pointed out rapid metabolism of vitamin D<sub>2</sub> in  
61 comparison to vitamin D<sub>3</sub>, while the action become bioequivalent if taken daily.<sup>13,14</sup> Both forms of  
62 vitamin D are converted to 25-hydroxy vitamin D [25-(OH)D] in the liver. The quantification of 25-  
63 (OH)D in blood gives the quantitation of vitamin D status. A cutoff value of 30 ng mL<sup>-1</sup> is  
64 sometimes used for optimal vitamin D status.<sup>12</sup> Ergocalciferol was produced in 1920s through UV-B  
65 exposure of foods, leading to the formation of first medicinal preparation called Viosterol.<sup>15</sup>  
66 Ergocalciferol has limited natural sources and the most significant source is wild mushrooms.<sup>16</sup>  
67 Ergocalciferol is prone to oxidation and is also isomerized to isotachysterol in the presence of

68 sunlight and mostly under acidic conditions.<sup>16,17</sup> Ergocalciferol is mostly supplemented and fortified  
69 in fat based products due to its hydrophobic nature.

70 Emulsification technologies play an important role in the production of encapsulated foods,  
71 pharmaceuticals, cosmetics and chemicals.<sup>18,19</sup> The emulsions are usually either single (O/W and  
72 W/O) emulsions or double emulsions (W/O/W and O/W/O).<sup>19</sup> These different emulsion systems are  
73 produced by either conventional devices including colloid mills, high pressure homogenizers and  
74 rotor-stator homogenizers or modern devices such as microfluidic devices (lab-on-a-chip),  
75 membrane emulsification and microchannel emulsification (MCE) devices.<sup>19,20</sup> Conventional devices  
76 produce polydisperse emulsions with broader size distributions, which in turn reduce the emulsion  
77 stability and functionality. Microfabricated emulsification devices have potential to produce  
78 monodisperse emulsions with the smallest coefficient of variation (CV) less than 10% for membrane  
79 emulsification and around 5% for microfluidic devices and MCE.<sup>20</sup>

80 MCE is a progressive technique that enables production of monodisperse emulsions by  
81 spontaneous transformation of oil-water interface specifically driven by interfacial tension dominant  
82 on a micron scale.<sup>21</sup> MCE studies were comprehensively reviewed by Vladislavljević *et al.*<sup>20,22</sup>  
83 Similarly, this emulsification technique allows integration of hundreds of thousands of droplet  
84 generation units on a single plate.<sup>23,24</sup> MCE has been used for producing O/W, W/O and W/O/W  
85 emulsions with diameters ranged from 1  $\mu\text{m}$  to 550  $\mu\text{m}$ .<sup>22</sup> Based on microfabrication design, the  
86 MCE devices can either be categorized into grooved microchannel (MC) arrays each consisting of  
87 uniform microgrooves and a slit-like terrace and straight-through MC arrays each having uniform  
88 asymmetric microholes together with microslots.<sup>22</sup> Grooved MC array plates are further classified  
89 into dead-end and cross-flow types. Grooved MCE plates of cross-flow type are particularly useful to  
90 observe the entire droplet generation process together with droplet collection at low dispersed phase  
91 flow rates.<sup>25,26</sup> On the other hand, straight-through MC arrays are designed to improve the throughput

92 capacity of MCE. Straight-through MC arrays have ability to increase the production capacity of  
93 monodisperse emulsion droplets over  $2000 \text{ L m}^{-2} \text{ h}^{-1}$ .<sup>22</sup>

94 MCE has also been used to produce monodisperse microdispersions (e.g. solid lipid  
95 microspheres<sup>26</sup>, gel microbeads<sup>27</sup>, and giant vesicles<sup>28</sup>). MCE has promising potential for producing  
96 uniformly sized oil droplets containing functional lipids such as  $\beta$ -carotene<sup>29</sup>,  $\gamma$ -oryzanol<sup>30</sup>, L-  
97 ascorbic acid<sup>31</sup>, ascorbic acid derivatives<sup>32</sup>, oleuropein<sup>33</sup>, and vitamin D.<sup>34</sup> Different food grade  
98 materials (e.g. refined vegetable oils, a medium-chain triglyceride oil, hydrophobic and hydrophilic  
99 emulsifiers, proteins, and hydrocolloids) were utilized to produce monodisperse O/W, W/O, W/O/W  
100 emulsions and microparticles by MCE.<sup>35,36</sup>

101 We previously encapsulated vitamin D (both vitamin D<sub>2</sub> and D<sub>3</sub>) in O/W emulsions using  
102 MCE and reported long-term stability studies and encapsulation efficiencies of O/W emulsions  
103 encapsulating vitamin D<sub>2</sub> and D<sub>3</sub>.<sup>34</sup> Ergocalciferol is a plant-based vitamin D type, and previous  
104 studies seldom report its encapsulation in different formulations. Keeping its rapid metabolism rate  
105 and importance in human diet, the present study was conducted to encapsulate only ergocalciferol in  
106 triacylglycerol oil-in-water emulsions using MCE. The basic characterization and optimization of  
107 these emulsions were performed using a grooved MC array plate. Straight-through MCE was carried  
108 out to investigate the effect of dispersed phase flux on the production characteristics and as well as  
109 physical and chemical stability of ergocalciferol-loaded O/W emulsions. The effects of different  
110 triacylglycerol oils and emulsifiers on preparation characteristics of O/W emulsions by MCE were  
111 also evaluated. The results of this research are expected to formulate new aqueous based functional  
112 foods.

## 113 **Experimental**

### 114 **Chemicals**

115 Ergocalciferol, polyoxyethylene (20) sorbitan monolaurate (Tween 20), olive oil, and soybean oil  
116 were purchased from Wako Pure Chemical Industries Ltd. (Osaka, Japan). Medium chain  
117 triacylglycerol (MCT, sunsoft MCT-7) with a fatty acid residue composition of 75% caprylic acid  
118 and 25% capric acid and decaglycerol monolaurate (Sunsoft A-12) were procured from Taiyo  
119 Kagaku Co. Ltd. (Yokkaichi, Japan). Safflower oil was purchased from MP biomedical (Illkirch,  
120 France).  $\beta$ -Lactoglobulin ( $\beta$ -lg) from bovine milk (>90% purity) was purchased from Sigma-Aldrich  
121 Co. LLC. (St. Louis, USA). All other chemicals used in this study were of analytical grade and used  
122 as received.

### 123 **Preparation of solutions**

124 The continuous phase was prepared by dissolving either 1% (w/w) Tween 20, 1% (w/w) Sunsoft A-  
125 12 or 1% (w/w)  $\beta$ -lg in Milli-Q water with a resistivity of 18M $\Omega$  cm. The dispersed phase was  
126 prepared by dissolving 0.2-1.0% (w/w) ergocalciferol in MCT, soybean, olive or safflower oil at 85  
127  $^{\circ}\text{C} \pm 3^{\circ}\text{C}$  for 20 min and afterwards cooling at room temperature for 2 h before storage at  $4 \pm 1^{\circ}\text{C}$ .  
128 During storage, dissolved ergocalciferol molecules could form nuclei whose growth eventually  
129 makes crystals large enough to sediment. Before initiating experiments, the samples were therefore  
130 shaken slightly to avoid formation of any ergocalciferol crystals.

### 131 **Silicon plates for MCE**

132 The experiments have been carried out by using silicon MC array plates (model CMS 6-2 and  
133 WMS11-1, EP. Tech Co., Ltd., Hitachi, Japan). Fig. 2a is a schematic representation of a CMS 6-2  
134 plate with 540 parallel channels on 10 consecutive MC arrays. Each MC array contains 54 parallel  
135 MCs with a depth of 5  $\mu\text{m}$ , a width of 18  $\mu\text{m}$  and a length of 140  $\mu\text{m}$  and a terrace with a depth of 5  
136  $\mu\text{m}$  and a length of 60  $\mu\text{m}$ . Each continuous-phase channel outside the terrace outlet has a depth of  
137 100  $\mu\text{m}$ . Fig. 2b is a schematic representation of a WMS 11-1 plate with 27,400 MCs compactly  
138 arranged within a  $10 \times 10$  mm square region in the plate center. Each MC consists of a cylindrical 10



139  $\mu\text{m}$  diameter straight microhole with a depth of  $200\ \mu\text{m}$  and a  $10 \times 80\ \mu\text{m}$  microslot with a depth of  
140  $40\ \mu\text{m}$ . The slot aspect ratio of 8 was above the threshold value of 3 for successfully generating  
141 monodisperse emulsion droplets.<sup>37</sup> The distance between the two adjacent MCs in the vertical was  
142  $105\ \mu\text{m}$ , and the distance between the centers of MCs in the adjacent rows was  $70\ \mu\text{m}$ . The MC array  
143 plates were subjected to plasma oxidation in plasma reactor (PR41, Yamato Science Co. Ltd., Tokyo,  
144 Japan) to activate a silicon dioxide layer on their surfaces. The activated silicon dioxide layer is  
145 capable of maintaining their hydrophilicity during MCE.

#### 146 **Experimental procedure for MCE**

147 For grooved MCE, the setup consists of an MC module, a 10 mL liquid chamber that contains the  
148 disperse phase and a syringe pump (Model 11, Harvard Apparatus Inc., Holliston, USA) that feeds  
149 the continuous phase with a 50 mL glass syringe (Fig. 3a). MCE was carried out for approximately 3  
150 h and monitored through an inverted metallographic microscope equipped with an objective lens of  
151 2.5x to 20x and a CCD camera (MS-511B, Seiwa Kougaku Sesakusho Ltd., Tokyo, Japan). The  
152 whole process was recorded with a video recorder (RDR-HX67; Sony Co., Tokyo, Japan). Droplet-  
153 generation experiments were performed with the grooved MCE setup depicted in Fig. 3b. The  
154 module was initially filled with the continuous phase before mounting the CMS 6-2 plate. The  
155 pressurized dispersed phase was introduced into the module. The pressure applied to the dispersed  
156 phase ( $\Delta P_d$ ) was gradually increased.  $\Delta P_d$  can be given by

$$157 \quad \Delta P_d = \rho_d \Delta h_d g \quad (1)$$

158 where  $\rho_d$  is the dispersed-phase density,  $\Delta h_d$  is the difference in the hydraulic heads between the  
159 chamber containing the dispersed phase and the channels of the module, and  $g$  is the acceleration due  
160 to gravity. To generate droplets, the dispersed phase was forced through the MCs onto the terrace  
161 and into the continuous phase channel.

162 For straight-through MCE, the MC array plate was degassed in a continuous aqueous phase  
163 by ultrasonic bath for 20 min and the setup consists of an MC module (comprising of six steel parts  
164 and two glass plates of different dimensions and rubber seals) and syringe pumps (Model 11,  
165 Harvard Apparatus Inc.) that feed the continuous and dispersed phases (Fig. 4a). MCE was carried  
166 out for approximately 1 h and monitored through FASTCAM-1024 PCI high speed video system at  
167 250 to 500 fps (Photron Ltd., Tokyo, Japan) attached to the inverted metallographic microscope. The  
168 droplet generation process was depicted in Fig. 4b. Droplet generation started with injecting the  
169 disperse phase through the syringe pump at the dispersed phase flow rate ( $Q_d$ ) ranging from 0.5 to  
170 2.0 mL h<sup>-1</sup> (5 to 20 L m<sup>-2</sup> h<sup>-1</sup> in dispersed phase flux ( $J_d$ )). The generated droplets were removed by  
171 varying the continuous phase flow rate ( $Q_c$ ) from 100 to 500 mL h<sup>-1</sup> through the gap between the MC  
172 array plate and the glass plate. The shear stress ( $\tau$ ) in the module surrounding the WMS 11-1 plate is  
173 given by

$$174 \quad \tau = \frac{3Q_c \eta_c}{2h^2 W} \quad (2)$$

175 where  $h = 1$  mm is the gap height and  $W = 12$  mm is the gap width, and  $\eta_c$  is the continuous phase  
176 viscosity.  $\tau$  had a negligible value of 0.002 to 0.02 Pa at the  $Q_c$  range applied in this study. After  
177 each experiment the MC array plates were cleaned in three steps. In the first step the MC array plates  
178 were washed with neutral detergent together with Milli-Q water in an ultrasonic bath (VS-100 III, As  
179 One Co., Osaka, Japan) for 20 min, afterwards treatment with 50% Milli-Q water and 50% ethanol in  
180 an ultrasonic bath, lastly cleaned in an ultrasonic bath with Milli-Q water and stored in 50 mL of  
181 Milli-Q water prior to reuse for MCE.

### 182 **Determination of droplet size and droplet size distribution**

183 The size and size distribution of the resultant O/W emulsion droplets from grooved MCE were  
184 determined as follows. The average droplet diameter ( $d_{av}$ ) was defined by

185 
$$d_{av} = \sum_{i=1}^n d_i / n \quad (3)$$

186 where  $d_i$  is the diameter of the  $i^{\text{th}}$  droplet measured using WinRoof software (Mitani Co., Ltd., Fukui,  
187 Japan) and  $n$  is the number of the droplets measured ( $n= 250$ ). The droplet size distribution was  
188 expressed as CV, and is defined as

189 
$$CV = \frac{\sigma}{d_{av}} \times 100 \quad (4)$$

190 where  $\sigma$  is the standard deviation and  $d_{av}$  is the average droplet diameter.

191 The droplet size distribution of the O/W emulsions obtained from straight-through MCE was  
192 measured by using a laser scattering instrument that works on the principle of Polarization Intensity  
193 Differential Scattering Technology (LS 13 320, Beckman Coulter, Inc., Brea, USA). This instrument  
194 have ability to measure the size ranging from 0.04 to 2000  $\mu\text{m}$  with a resolution of 116 particle size  
195 channels. The mean droplet size was expressed as Sauter mean diameter ( $d_{3,2}$ ), defined as the  
196 diameter of a droplet having the same area per unit volume as that of the total collection of droplets  
197 in emulsions. The width of droplet size distribution was expressed as relative span factor (RSF),  
198 defined as

199 
$$RSF = \frac{d_{v0.9} - d_{v0.1}}{d_{v0.5}} \quad (4)$$

200 where  $d_{v0.9}$  and  $d_{v0.1}$  are the representative diameters where 90% and 10% of the total volume of the  
201 liquid is made up of droplets with diameters smaller than or equal to the stated value, and  $d_{v0.5}$  is the  
202 representative diameter where 50% of the total volume of the liquid is made up of droplets with  
203 diameters larger than the stated value and 50% is made up of droplets with diameters smaller than  
204 the stated value.

## 205 **Measurement of fluid properties**

206 The densities of dispersed and continuous phases were measured using a density meter (DA-130 N,  
207 Kyoto Electronics Manufacturing Co., Ltd., Kyoto, Japan) at  $25 \pm 2^\circ\text{C}$ . Their viscosities were  
208 measured with a vibro viscometer (SV-10, A&D Co., Ltd., Tokyo, Japan) at  $25 \pm 2^\circ\text{C}$  by taking  
209 either 10 or 35 mL of samples in a measuring vessel followed by immersion of sensor plates in that  
210 vessel. Viscosity was measured by detecting the electric current needed to resonate the sensor plates.  
211 The static interfacial tension between the preceding two phases was measured with a fully automatic  
212 interfacial tensiometer (PD-W, Kyowa Interface Sciences Co., Ltd., Saitama, Japan) using a pendant  
213 drop method. The key physical properties of the dispersed and continuous phases used in this study  
214 are presented in Table 1.

#### 215 **Physical and chemical stability of O/W emulsions**

216 The physical stability of the O/W emulsion droplets loaded with ergocalciferol was evaluated  
217 according to the method described in an earlier section. The  $d_{3,2}$ , RSF, consistency and coalescence  
218 during 15 d of storage at  $4 \pm 1^\circ\text{C}$  under dark conditions were observed.

219 The amount of ergocalciferol encapsulated in the O/W emulsions was determined  
220 spectrophotometrically. All spectral measurements of the ethanolic extracts of these O/W emulsions  
221 were carried out using a UV/VIS/NIR spectrophotometer (UV-1700, Shimadzu Co., Kyoto, Japan).  
222 First, 1 mL of the emulsion was mixed with 9 mL of ethanol, followed by ultrasonication for 20 min.  
223 The ethanolic extracts were then centrifuged (Avanti HP-25, Beckman Coulter, Inc.) at 20,000 g for  
224 15 min. A 1 mL aliquot of the supernatants was diluted ten times with ethanol and then injected into a  
225 quartz cell with a 10 mm path length. The absorbance of ergocalciferol in emulsion extract was  
226 measured at 310 nm using an appropriate blank. A representative standard curve of absorbance  
227 versus concentration gave linear least-squares regression with a coefficient of determination ( $r^2$ ) of  
228 0.9996. All experiments were repeated in triplicate and mean values were calculated. The Beer's law  
229 was obeyed in the concentration range of 0.1-0.5 mg mL<sup>-1</sup> and the sensitivity of measurement has

230 relative standard deviation of 0.85% (n=15). The Molar absorptivity ( $\epsilon$ ) for ergocalciferol during this  
231 study was  $2.52 \text{ mM}^{-1} \text{ cm}^{-1}$ . The encapsulation efficiency (EE) of ergocalciferol in samples were  
232 calculated with the equation

$$233 \quad EE = \frac{W_t}{W_0} \times 100 \quad (5)$$

234 where  $W_t$  is the total amount of ergocalciferol in the O/W emulsions at a specific time (t) and  $W_0$  is  
235 the total amount of ergocalciferol initially quantified at day 1.

## 236 **Results and discussion**

### 237 **Basic droplet generation characteristics through grooved MCE**

#### 238 *Effect of disperse phase composition*

239 Fig. 5a illustrates the effect of different oils on the  $d_{av}$  and CV of the O/W emulsions prepared using  
240 CMS6-2 plate. MCE was carried out using 0.5% (w/w) ergocalciferol in MCT, soybean, olive or  
241 safflower oil as the dispersed phase and 1% (w/w) Tween 20 in Milli-Q water as the continuous  
242 phase. A gradual increase in  $\Delta P_d$  caused the dispersed phase to enter the terrace in front of the MC  
243 inlets. When  $\Delta P_d$  reached the break-through pressure of about 3.0 kPa, the dispersed phase started to  
244 pass through the MCs, leading to the periodic generation of oil droplets. The MCE was performed at  
245 a  $\Delta P_d$  of 3.2 kPa slightly higher than the break-through pressure.  $Q_c$  was fixed at  $2 \text{ mL h}^{-1}$  throughout  
246 the experiment. Successful generation of monodisperse O/W emulsion droplets took place,  
247 regardless of the oil types used. The  $d_{av}$  of the resultant O/W emulsions loaded with ergocalciferol  
248 ranged from 28.3 to 30.0  $\mu\text{m}$  with CV between 3.6 and 6.1%. Fig. 5b(i-iv) shows the droplet  
249 detachment process with different dispersed phases. The different dispersed phase solutions  
250 exhibited successful emulsification with smooth detachment of droplets from the terrace outlets, and  
251 narrower droplet size distributions were seen in the emulsions prepared with olive oil, safflower oil  
252 and soybean oil in comparison to MCT (Fig. 5c). The O/W emulsions prepared with MCT had a

253 somewhat greater CV of about 6%. Uniformly sized droplets are stably generated in MCE, if the  
254 inflow of the continuous phase toward the terrace is sufficiently fast compared to the outflow of the  
255 dispersed phase from the MC outlets.<sup>38</sup> The viscosity ratio ( $\zeta = \eta_d/\eta_c$ ) is also a key factor  
256 determining the monodispersity of emulsions.<sup>38</sup> The viscosity ratio of all the oils used in this study  
257 was sufficiently high (Table 1), leading to successful preparation of monodisperse O/W emulsions  
258 encapsulating ergocalciferol. The less monodispersity with MCT might be attributed to some  
259 attractive interaction of MCT with MC and terrace surfaces. Such interaction causes slight increase  
260 in CV of O/W emulsion droplets in comparison to other viscous oils. Tan *et al.*<sup>39</sup> pointed out that  
261 hydrophobicity of the dispersed phase is the critical parameter affecting the generation of oil droplets  
262 in MCE.

### 263 *Effect of different emulsifiers*

264 The effect of the emulsifier type on oil droplet generation by grooved MCE was also investigated.  
265 Food-grade hydrophilic emulsifiers (Tween 20, Sunsoft A-12 and  $\beta$ -lg) with a noticeable ability to  
266 prepare O/W emulsions were used at a concentration of 1% (w/w) in the Milli-Q water. These  
267 aqueous emulsifier solutions were used as the continuous phase. 0.5% (w/w) ergocalciferol in  
268 soybean oil was used as the dispersed phase. The important physical properties of different  
269 emulsifiers were presented in Table 1. There was not a prominent difference in the viscosity and  
270 density values of emulsifier solutions, while  $\beta$ -lg had higher interfacial tension (12.6 mN m<sup>-1</sup>) in  
271 comparison to Tween 20 and Sunsoft A-12. All of these emulsifier solutions exhibited successful  
272 emulsification with smooth detachment of droplets from the terrace outlets (Fig. 6a). Uniformly-  
273 sized emulsion droplets were stably generated from the MCs especially in the presence of Tween 20  
274 and Sunsoft A-12. There was neither the generation of bigger droplets nor a continuous outflow of  
275 dispersed phase. Fig. 6b illustrates the effect of the emulsifier type on the  $d_{av}$  and CV of O/W  
276 emulsions. The  $d_{av}$  and CV of the resultant O/W emulsions were 28.5  $\mu$ m and 5.9% for Tween 20  
277 and 28.1  $\mu$ m and 6.6% for Sunsoft A-12. Uniformly-sized droplets stabilized by Tween 20 or

278 Sunsoft A-12 were successfully generated due to high interfacial activity, as these emulsifiers have  
279 low interfacial tension values of about  $5.0 \text{ mN m}^{-1}$ . Droplet generation and detachment processes for  
280  $\beta$ -lg at pH 7.3 were initially stable with the smallest  $d_{av}$  of  $26.6 \mu\text{m}$ . However, after 5 min few  
281 droplets started sticking in the well (Fig. 6a(iii) and Fig. 6c) and coalesced with passage of time,  
282 resulting in the increase of CV value to 7.2%. The result suggests that  $\beta$ -lg did not adsorb strongly at  
283 the newly created interface, presumably because the weak electrostatic interactions between  
284 ergocalciferol and  $\beta$ -lg clearly observed from high interfacial tension value.

285 Kobayashi and Nakajima<sup>40</sup> investigated the effect of the emulsifier type on droplet generation  
286 characteristics by using a straight-through extrusion filter. They reported Tween 20 and decaglycerol  
287 monolaurate as suitable, hydrophilic food-grade emulsifiers in MCE without ergocalciferol. Patel  
288 and San Martin-Gonzalez<sup>17</sup> also demonstrated successful preparation of solid lipid nanoparticles  
289 loaded with ergocalciferol stabilized by Tween 20. The preceding results demonstrate that Tween 20  
290 and Sunsoft A-12 as potential emulsifiers for generating ergocalciferol-loaded O/W emulsions, either  
291 with conventional homogenization techniques (data not shown) or MCE.

#### 292 *Effect of ergocalciferol concentration*

293 Fig. 7 illustrates the effect of concentration of ergocalciferol on the  $d_{av}$  and CV of the O/W  
294 emulsions prepared using two different emulsifiers and CMS6-2 plate. The concentration of  
295 ergocalciferol varied from 0.2% to 1.0% (w/w) in soybean oil. According to US Pharmacopeia,  
296 ergocalciferol is sparingly soluble in different oils but have good solubility in organic solvents,  
297 except hexane. In our study, we noticed a maximum solubility of 1% (w/w) ergocalciferol in  
298 different oils at  $85 \pm 2^\circ\text{C}$  with no solubility at room temperature. Successful MCE was conducted  
299 with different concentrations of ergocalciferol by keeping  $\Delta P_d$  at 3.2 kPa and  $Q_c$  around  $2 \text{ mL h}^{-1}$ .  
300 The  $d_{av}$  of the ergocalciferol-loaded O/W emulsions increased slowly with increasing concentration  
301 of ergocalciferol when emulsified with 1% (w/w) Tween 20. Their  $d_{av}$  ranged between 23.8 and 28.5

302  $\mu\text{m}$  with CV between 5.9 and 6.2%. Comparatively similar results were obtained with Sunsoft A-12  
303 (Fig. 7). The ergocalciferol-loaded O/W emulsions stabilized with 1% (w/w) Sunsoft A-12 had  $d_{\text{av}}$  of  
304 24.5 to 27.5  $\mu\text{m}$  and have CV of 6.5 to 8.4%. A better droplet size distribution expressed as a smaller  
305 CV was seen in the emulsions stabilized with Tween 20 in comparison to those stabilized with  
306 Sunsoft A-12 (Fig. 7). A reason behind the increased  $d_{\text{av}}$  with increasing ergocalciferol concentration  
307 could be attributed to weak attractive interaction between oil encapsulating ergocalciferol and MC  
308 and terrace surfaces during MCE. These types of interactions with terrace surfaces in MCE during L-  
309 ascorbic acid encapsulation were previously reported by Khalid *et al.*<sup>41</sup> To remain in optimum range  
310 and easiness of the process we conducted stability and encapsulating efficiency experiments by using  
311 0.5% (w/w) ergocalciferol in soybean oil as an optimum dispersed phase. Moreover, this  
312 concentration has no effect on different parameters, since we evaluated low and high concentration  
313 effect also. The other reason for choosing this concentration is to make process more practical at  
314 industrial scale; i.e., 0.5% (w/w) ergocalciferol in the dispersed phase is mostly desired in different  
315 industries.

#### 316 *Effect of dispersed phase flow rate*

317 Dispersed phase flow rate ( $Q_d$ ) is an important parameter in MCE that correlates with droplet  
318 productivity at the stable droplet generation regime. Fig. 8a depicts the effect of  $Q_d$  on the  $d_{\text{av}}$  and  
319 CV of the droplets generated using CMS6-2 plate. The dispersed phase constitutes 0.5% (w/w)  
320 ergocalciferol in soybean oil, while the continuous phase includes 1% (w/w) Tween 20 in Milli-Q  
321 water.

322 At the lowest  $Q_d$  of  $2 \times 10^{-3} \text{ mL h}^{-1}$ , the resultant droplets with a monomodal and very narrow  
323 size distribution had a  $d_{\text{av}}$  of 23.5  $\mu\text{m}$  and a CV of 5.4%. When  $Q_d$  was increased stepwise,  
324 monodisperse emulsions with CV of 4 to 10% were produced at  $Q_d$  of  $8 \times 10^{-2} \text{ mL h}^{-1}$  or less. In this  
325  $Q_d$  range,  $d_{\text{av}}$  of the resultant droplets ranged from 23.7  $\mu\text{m}$  to 26.7  $\mu\text{m}$ . The microscopic



326 observations during MCE confirmed that the resultant droplet size hardly changed at  $Q_c$  between 0  
 327 mL h<sup>-1</sup> and 5.0 mL h<sup>-1</sup>. The generation of droplets even without external flow of the continuous  
 328 phase depicts the unique spontaneous transformation of interface in MCE. In contrast, at  $Q_d$  of 8  
 329  $\times 10^{-2}$  mL h<sup>-1</sup> or more, the  $d_{av}$  and CV of O/W emulsions dramatically increased to > 30  $\mu\text{m}$  with CV  
 330 values more than 10% (Fig. 8a). Moreover the droplet size distribution became wider and shifted  
 331 towards large droplet size area. The CMS 6-2 plate used here enabled the production of O/W  
 332 emulsions with uniformly sized droplets at a critical  $Q_d$  of  $8 \times 10^{-2}$  mL h<sup>-1</sup>, which was higher than a  
 333 maximum  $Q_d$  ( $5 \times 10^{-3}$  mL h<sup>-1</sup>) for the previously reported studies from grooved MCE.<sup>42</sup>

334 After reaching the critical  $Q_d$ , some of the dispersed phase that passed through the MCs  
 335 expanded instead of generating droplets, suggesting that the flow state of the dispersed phase was  
 336 affected by the dispersed-phase velocity inside the MC. Sugiura *et al.*<sup>21</sup> reported that the droplet  
 337 generation behavior inside MCs are related to the capillary number of the dispersed phase that flows  
 338 inside MCs. The capillary number ( $Ca$ ), which indicates the balance between viscous force and  
 339 interfacial force, can be determined by:

$$340 \quad Ca = \eta_d U_d / \gamma \quad (6)$$

341 where  $\eta_d$  is the dynamic viscosity (Pa.s) of the dispersed phase,  $U_d$  is the dispersed phase velocity  
 342 inside an MC ( $\text{m s}^{-1}$ ) and  $\gamma$  is the interfacial tension between the two phases ( $\text{N m}^{-1}$ ).  $Ca$  at the critical  
 343  $Q_d$  of  $8 \times 10^{-2}$  mL h<sup>-1</sup> was 0.017. This critical  $Ca$  value was similar to the previous findings with  
 344 grooved MCE.<sup>21, 43</sup>

345 The influence of  $Q_d$  on the droplet generation frequency per MC array plate ( $f$ ) (Fig. 8b) can  
 346 be estimated by:

$$347 \quad f = \frac{Q_d}{V_{av}} = \frac{6Q_d}{\pi d_{av}^3} \quad (7)$$

348 where  $V_{av}$  is the average droplet volume. The  $f$  increased with increasing  $Q_d$  in the range of  $8 \times 10^{-2}$   
 349 mL h<sup>-1</sup> or less. Further increase in  $Q_d$  lowered the  $f$ , and uniform fine droplets were generated at a  
 350 maximum  $f$  of  $8.0 \times 10^6$  h<sup>-1</sup> (Fig. 8b).

### 351 **Stability evaluation of ergocalciferol-loaded O/W emulsions prepared by MCE**

352 Stability and EE of the emulsion system is directly depended on the droplet size and droplet size  
 353 distribution. The more monodisperse is the system, the better the efficiency of process parameters.  
 354 Grooved MCE provides useful information regarding basic characterization of droplet generation,  
 355 whereas its drawback lies in low droplet productivity (e.g. a maximum of  $1.5 \times 10^{-3}$  L h<sup>-1</sup>).<sup>25</sup> In  
 356 comparison, straight-through MCE can increase the throughput capacity of droplets and work even at  
 357  $Q_d$  of 0.27 L h<sup>-1</sup> with uniform droplet productivity.<sup>44</sup> Straight-through MC arrays comprised of  
 358 narrow microholes and microslots that can accommodate  $>10^4$  asymmetric MCs per 1 cm<sup>2</sup>.<sup>45</sup> Here  
 359 we focus on the stability and encapsulation efficiency of soybean oil loaded-ergocalciferol O/W  
 360 emulsions prepared by straight-through MCE.

### 361 *Effect of dispersed phase flux on droplet size stability during storage*

362 Fig. 9a shows the effect of  $J_d$  on the  $d_{3,2}$  and RSF of the oil droplets containing ergocalciferol  
 363 prepared using WMS 11-1 plate. Dispersed phase flux ( $J_d$ ) is a useful indicator of droplet  
 364 productivity via MCs as well as other microfabricated devices.  $J_d$  is defined as:

$$365 \quad J_d = \frac{Q_d}{A_{MCA}} \quad (8)$$

366 where  $A_{MCA}$  is the total active area of the MC array ( $10 \times 10$  mm<sup>2</sup>). The maximum  $Q_d$  used here was  
 367 2 mL h<sup>-1</sup> which corresponds to  $J_d$  of 20 L m<sup>-2</sup> h<sup>-1</sup>, as it was the critical value in this study. After  
 368 crossing this critical  $J_d$  there was continuous outflow of dispersed phase via some MCs, resulting in  
 369 unstable droplet production. There was little increase in the  $d_{3,2}$  of the resultant O/W emulsions with  
 370 increasing  $J_d$  of 20 L m<sup>-2</sup> h<sup>-1</sup> or less (Fig. 9a). Their  $d_{3,2}$  ranged between 33.9 and 35.4 μm. Their RSF

371 was less than 0.4 and slowly increased with increasing  $J_d$ , demonstrating monodispersity of the  
372 ergocalciferol-loaded O/W emulsions prepared here. The droplet production behavior with varying  $J_d$   
373 was presented in Fig. 9b. There was smooth detachment of oil droplets before reaching the critical  $J_d$ .

374 The results presented in Fig. 9 deviate with previous findings of Vladislavljevic *et al.*<sup>44</sup> They  
375 reported the size stable zone of soybean oil-in-water emulsions which ranged between 0 and 50 L m<sup>-2</sup>  
376 h<sup>-1</sup>. Moreover, they reported critical  $J_d$  of 260 L m<sup>-2</sup> h<sup>-1</sup> for soybean oil loaded emulsions without  
377 loading any bioactive computed from CFD simulations. Our results are somewhat similar to the  
378 findings of Neves *et al.*<sup>30</sup> They formulated soybean oil-in-water emulsions loaded with  
379 polyunsaturated fatty acid at a critical  $J_d$  of 80 L m<sup>-2</sup> h<sup>-1</sup>. It should be noted that the flow rate of the  
380 continuous phase hardly affected the  $d_{3,2}$  and RSF of the O/W emulsions encapsulating ergocalciferol  
381 (Fig. 9c), which is another advantage for stable preparation of emulsion droplets.

382 The monodisperse O/W emulsions loaded with ergocalciferol prepared using WMS11-1 plate  
383 were stored at  $4 \pm 1^\circ\text{C}$  for 15 d. MCE was performed by keeping  $J_d$  at 5 L m<sup>-2</sup> h<sup>-1</sup> and  $Q_c$  of 150 mL  
384 h<sup>-1</sup>. Immediately after collection, the O/W emulsion samples had a colorless turbid appearance with  
385 good flowability. Their appearance did not change with storage time. Fig. 10 depicts time changes in  
386 the  $d_{3,2}$  and RSF values of the resultant O/W emulsions loaded with ergocalciferol. There was hardly  
387 any increase in their  $d_{3,2}$  and RSF values during evaluated storage time, indicating high physical  
388 stability of the monodisperse O/W emulsions loaded with ergocalciferol.

### 389 *Encapsulation efficiency of ergocalciferol in O/W emulsions*

390 The freshly prepared O/W emulsions had an initial ergocalciferol retention of 0.06 mg mL<sup>-1</sup> and  
391 regarded as 100% encapsulated efficiency (EE), since in MCE it was difficult to maintain the volume  
392 fraction with passage of time in comparison to conventional emulsification processes. Fig. 11 shows  
393 the EE and retention of ergocalciferol in the O/W emulsions prepared by MCE. The EE of  
394 ergocalciferol slightly decreased with storage time, reaching 76% after 15 d of storage at 4 °C. This

395 result is comparable with EE of previously encapsulated bioactives in MCE. For example, the EE of  
396 L-ascorbic acid in the W/O/W emulsions prepared through MCE was >80% after 10 d of storage.<sup>31</sup>  
397 These high EE values can be ascribed to very mild droplet-generation process as well as narrow  
398 droplet size distribution. It should be noted that droplet generation in MCE is based upon  
399 spontaneous transformation of the oil-water interface over the MC outlets rather than high-energy  
400 homogenization processes<sup>46</sup>. The EE with conventional devices like high pressure homogenizer and  
401 rotor-stator homogenizer were significantly lower (about <50%, data not shown) than MCE (>75%).  
402 The energy efficiency in MCE was around 27%, while that in conventional devices like high  
403 pressure homogenizers was very low around 0.1%.<sup>47,48</sup> However, scale up of MCE is still an ongoing  
404 process.

405 The potential reason for such decrease is the conversion of ergocalciferol to its isomeric  
406 form, isotachysterol. This conversion is accelerated in the presence of light and under slight acidic  
407 condition. In conventional emulsification system this process is highly accelerated due to heat and  
408 other stress conditions, and the EE are always lower around 60% even within one week of storage. In  
409 comparison MCE system improves the stability as well as encapsulation efficiency up to two weeks  
410 of storage. In our research these emulsions were stored at 4°C and most of the emulsion samples  
411 encapsulating ergocalciferol were subjected to this optimum temperature for storage. In our previous  
412 study we found no prominent different in EE of O/W emulsions encapsulating both ergocalciferol  
413 and cholecalciferol and at 4 and 25°C.<sup>34</sup>

414 Semo *et al.*<sup>49</sup> encapsulated ergocalciferol in casein micelles, having initial EE of over 85%.  
415 Moreover, the concentration of ergocalciferol in casein micelles was about 5.5 times than the  
416 concentration in serum surrounding around micelles. Ron *et al.*<sup>50</sup> encapsulated ergocalciferol in  $\beta$ -Ig  
417 stabilized nanoparticles. The concentration of ergocalciferol in nanoparticles was 55 times higher in  
418 comparison to unbounded ergocalciferol. Ergocalciferol encapsulated in the above-mentioned studies

419 performed better against oxygen diffusion, interaction with oxidizing agents and harmful effects of  
420 UV radiations. The evaluation of these mechanisms is beyond the scope of the present study.

## 421 **Conclusions**

422 Monodisperse food-grade O/W emulsions loaded with ergocalciferol were successfully  
423 formulated through grooved MCE and straight-through MCE. The key point of our findings is stable  
424 generation of uniformly sized O/W droplets that encapsulate ergocalciferol via MC arrays of  
425 asymmetric microstructure, without any coalescence or wetting of dispersed phase during MCE.  
426 Successful grooved MCE is achieved with different food grade ingredients as dispersed and  
427 continuous phases. The high throughput studies with straight-through MCE indicates successful  
428 operating conditions under a critical dispersed phase flux as well as under 1% (w/w) Tween 20 as an  
429 optimum emulsifier in the continuous phase. There was hardly any increase in droplet size during 15  
430 days of storage period. The resultant O/W emulsions containing ergocalciferol have encapsulating  
431 efficiency of more than 75% after 15 days of storage time. The improved physical and chemical  
432 stability correlate well with the monodispersity of the emulsion system. Our results indicate that  
433 MCE is a promising technique for encapsulating bioactive compounds, with superior control of  
434 processing parameters and various other physical conditions. The forthcoming scaling up of MCE  
435 devices is expected to further improve the production capacity of emulsions, so that making it  
436 practical on industrial scales through much more throughput production capacities.

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442 **Figures and Table captions**

443 **Figure 1:** Chemical structures of important forms of vitamin D. (a) Ergocalciferol. (b)  
444 Cholecalciferol.

445 **Figure 2:** (a) Schematic drawings of the grooved MC array plate (CMS 6-2) and part of an MC array  
446 together with different dimensions. (b) Schematic drawings of the straight-through MC array plate  
447 (WMS 11-1) and MCs dimensions.

448 **Figure 3:** (a) Schematic drawing of a grooved MCE setup. (b) Schematic drawing of droplet  
449 generation via part of an MC array having 5  $\mu\text{m}$  depth.

450 **Figure 4:** (a) Schematic representation of a straight-through MCE setup. (b) Droplet generation  
451 representation through asymmetric MCs.

452 **Figure 5:** (a) Effect of different dispersed phase composition on  $d_{\text{av}}$  and CV of O/W emulsions. ( $\square$ )  
453 denotes  $d_{\text{av}}$  of different dispersed phases, while ( $\bullet$ ) denotes CV of different dispersed phases. (b)  
454 Typical generation behaviors of O/W emulsions droplets encapsulating ergocalciferol by using  
455 different dispersed phase oils. (c) Micrographic images of droplets encapsulating ergocalciferol using  
456 different dispersed phases.

457 **Figure 6:** Effect of different emulsifiers on droplet generation behavior in grooved MCE. (a) Droplet  
458 generation with (i) Tween 20, (ii) Sunsoft A-12 and (iii)  $\beta$ -lg. (b) Effect of different emulsifiers on  
459  $d_{\text{av}}$  and CV of O/W emulsions, ( $\square$ ) denotes  $d_{\text{av}}$  of different emulsifiers, while ( $\bullet$ ) denotes CV of  
460 different emulsifiers. (c) Typical droplet generation characteristics with  $\beta$ -lg as emulsifier.

461 **Figure 7:** Effect of ergocalciferol concentration in soybean oil on  $d_{\text{av}}$  and CV of O/W emulsions  
462 either stabilized by 1% (w/w) Tween 20 or Sunsoft A-12.

463 **Figure 8:** (a) Effect of  $Q_d$  on  $d_{\text{av}}$  and CV of the O/W emulsions encapsulating soybean oil loaded-  
464 ergocalciferol produced using the CMS 6-2 plate. (b) Effect of  $Q_d$  on the droplet generation  
465 frequency per hour.

466 **Figure 9:** (a) Effect of dispersed phase flux ( $J_d$ ) on sauter mean diameter ( $d_{3,2}$ ) and relative span  
467 factor (RSF) of O/W emulsions encapsulating ergocalciferol. (b) Typical droplet generation behavior  
468 at (i) low flux of 5  $\text{L m}^{-2} \text{h}^{-1}$  and (ii) critical flux of 20  $\text{L m}^{-2} \text{h}^{-1}$ . (c) Effect of continuous phase flow  
469 rate ( $Q_c$ ) on  $d_{3,2}$  and RSF of O/W emulsions encapsulating ergocalciferol.

470 **Figure 10:** Storage stability of O/W emulsions encapsulating ergocalciferol stored at  $4 \pm 1^\circ\text{C}$ . The  
471 data was presented in term of  $d_{3,2}$  and RSF.

472 **Figure 11:** Encapsulating efficiency and retention profile of O/W emulsions with storage time. The  
473 emulsions were prepared at  $J_d$  of 5  $\text{L m}^{-2} \text{h}^{-1}$ , and the data was presented over 15 days of storage time.

474 **Table 1:** Fluid properties of the systems containing ergocalciferol together with different oils used  
475 for preparing O/W emulsions

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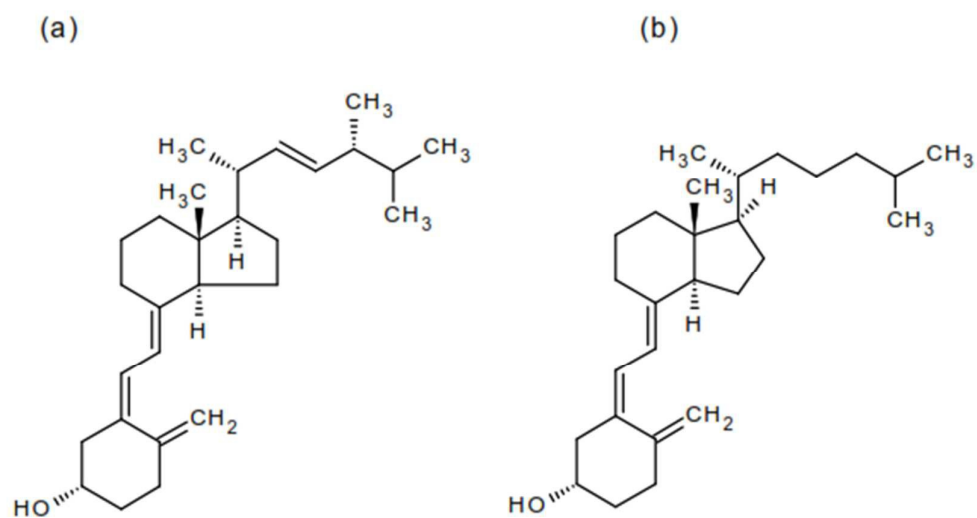


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11 **Figure 1**

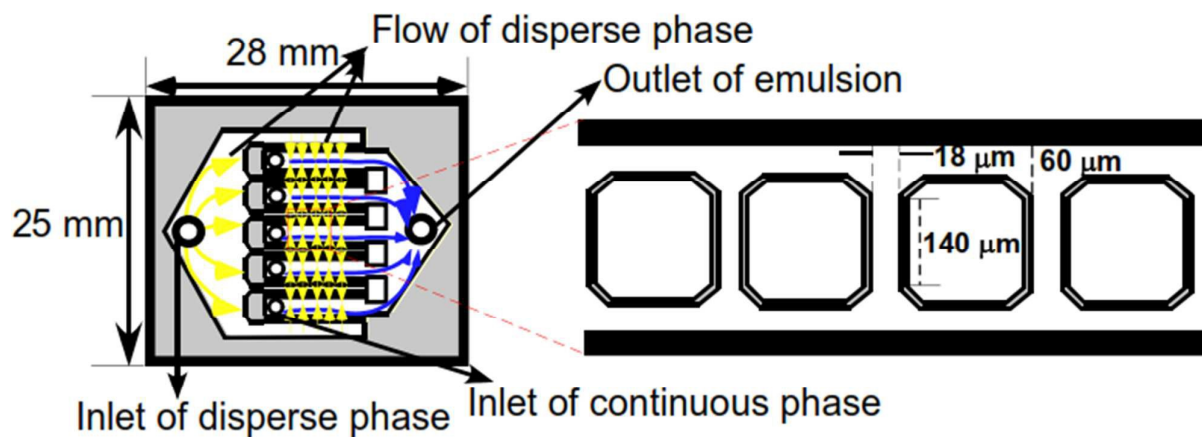
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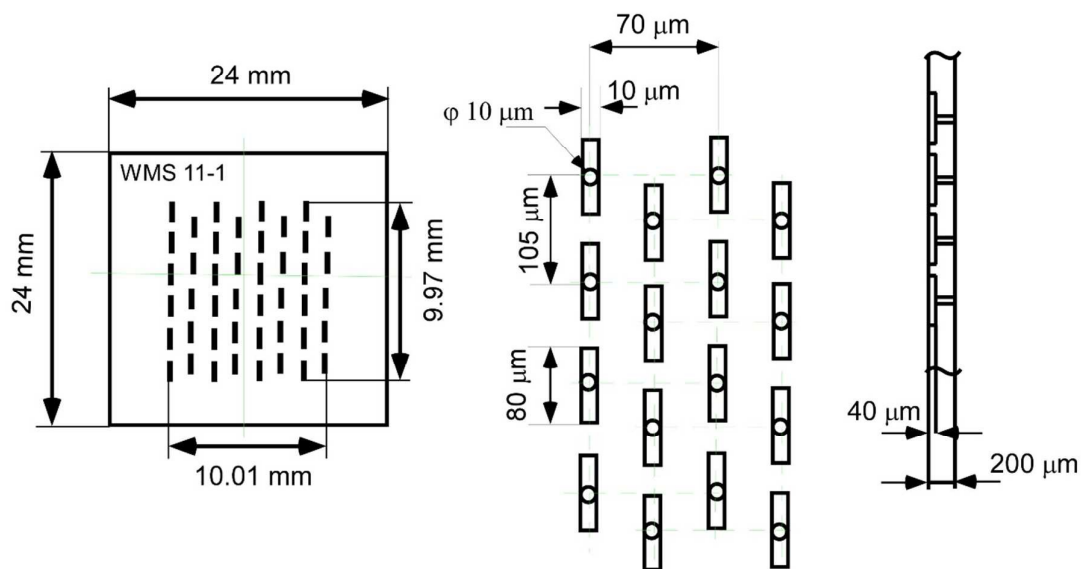
16 (a)



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19 (b)



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21 **Figure 2**

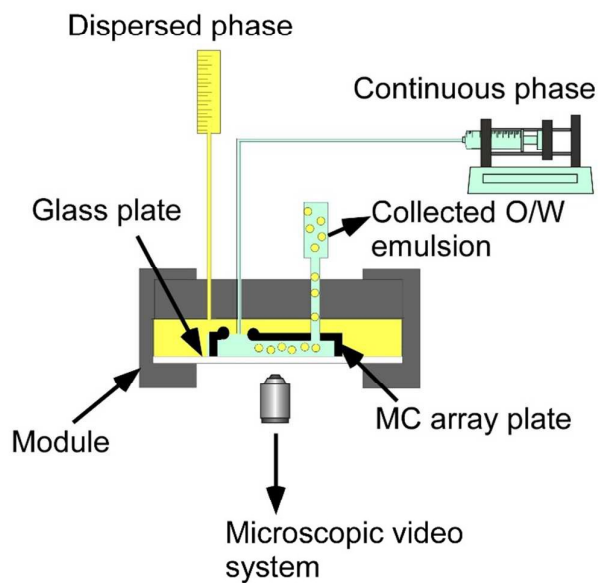
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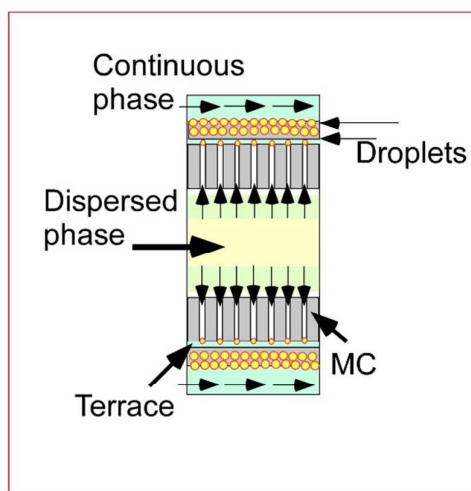
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26 (a)



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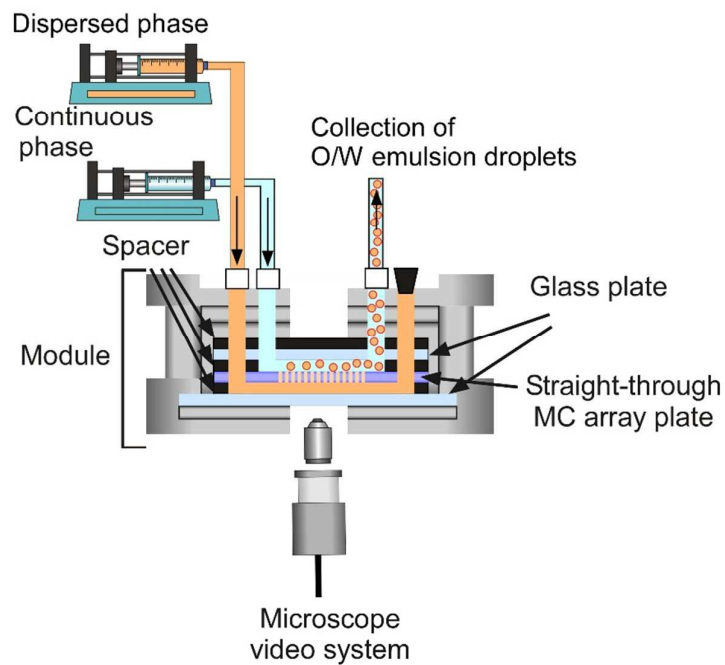
28 (b)



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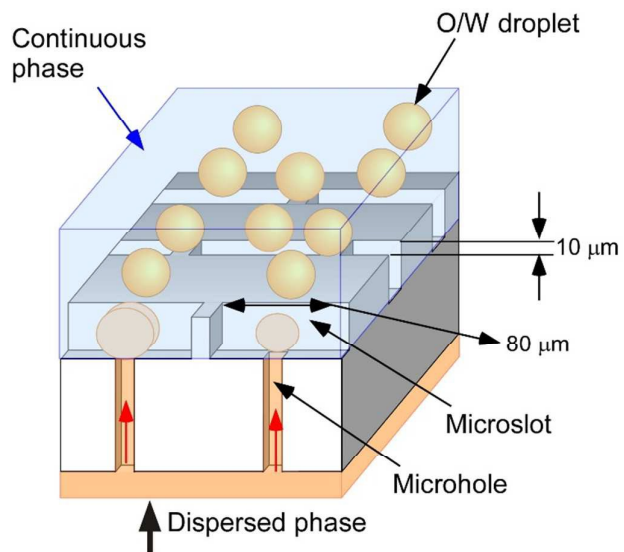
30 **Figure 3**

31 (a)



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33 (b)



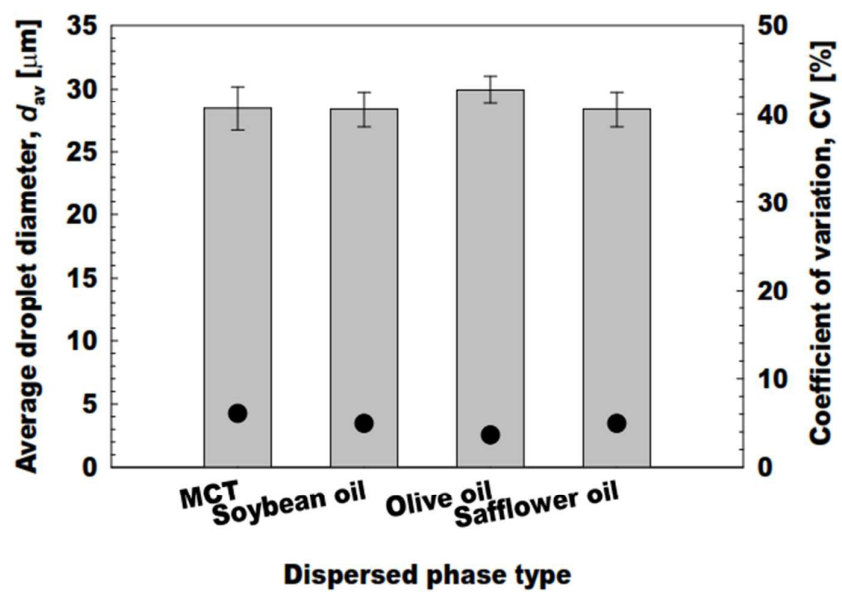
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35

36 **Figure 4**

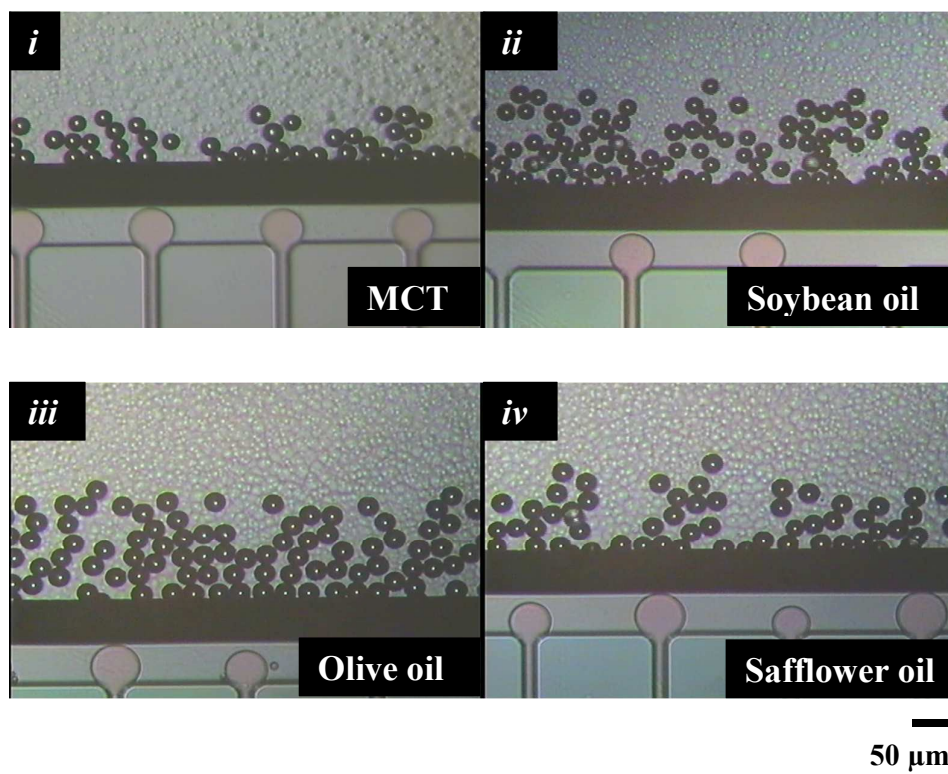
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38 (a)



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40 (b)



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44 Figure 5

45 (c)

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55 **Figure 5 (cont.)**

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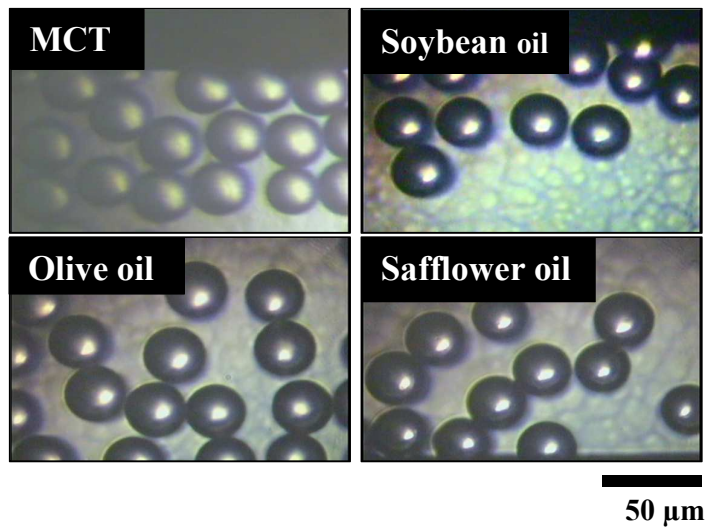
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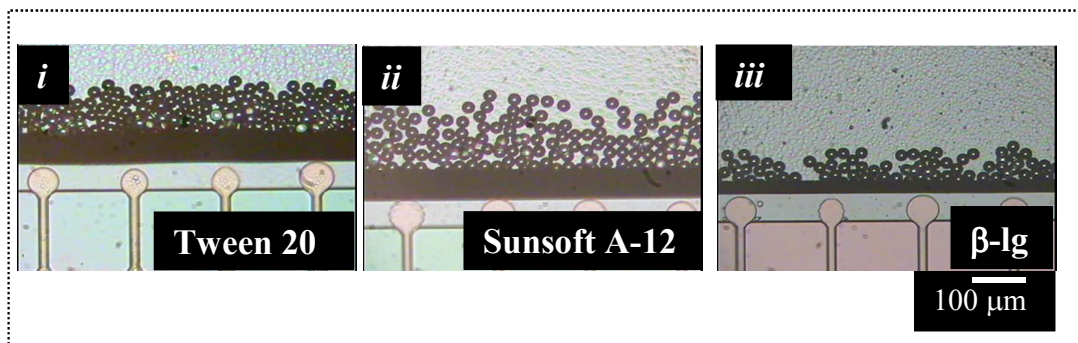
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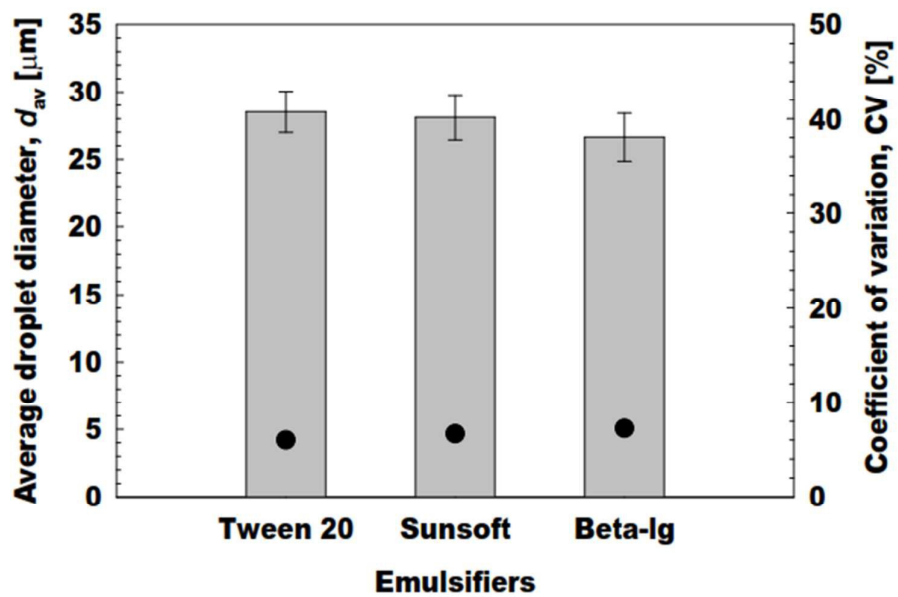


65 (a)



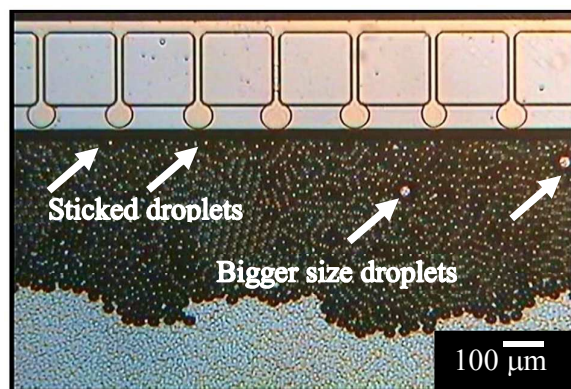
66

67 (b)



68

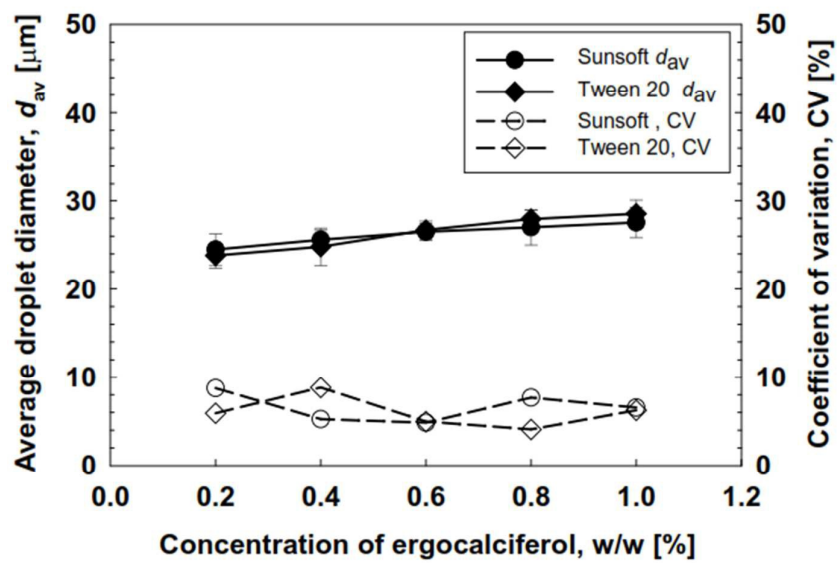
69 (c)



70

71 Figure 6

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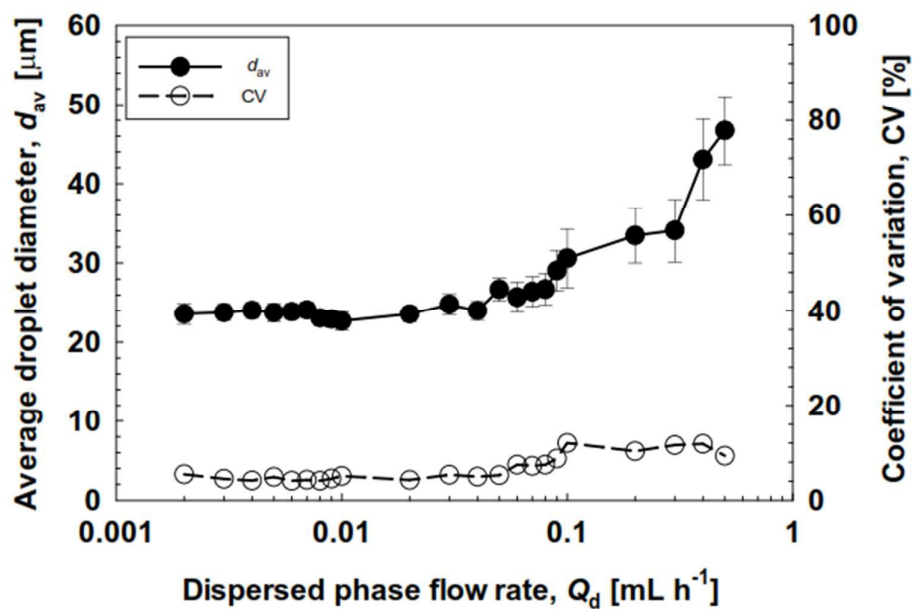


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74 **Figure 7**

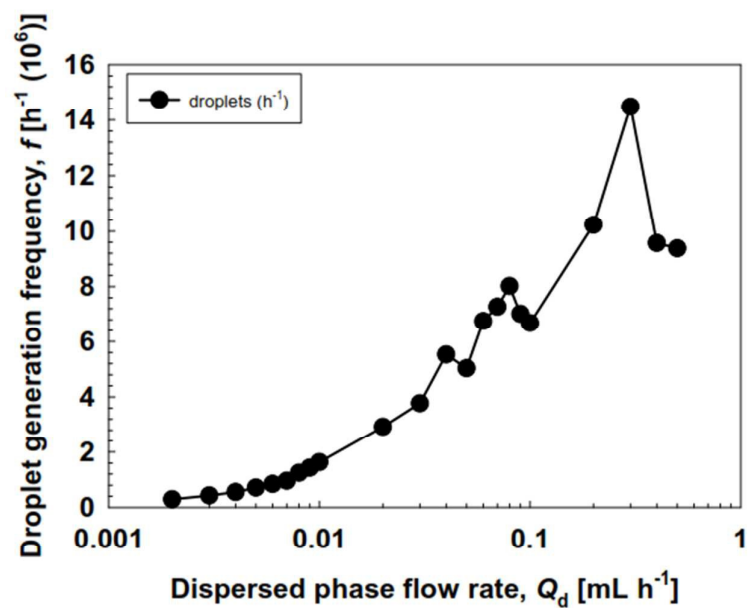
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76 (a)



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78 (b)

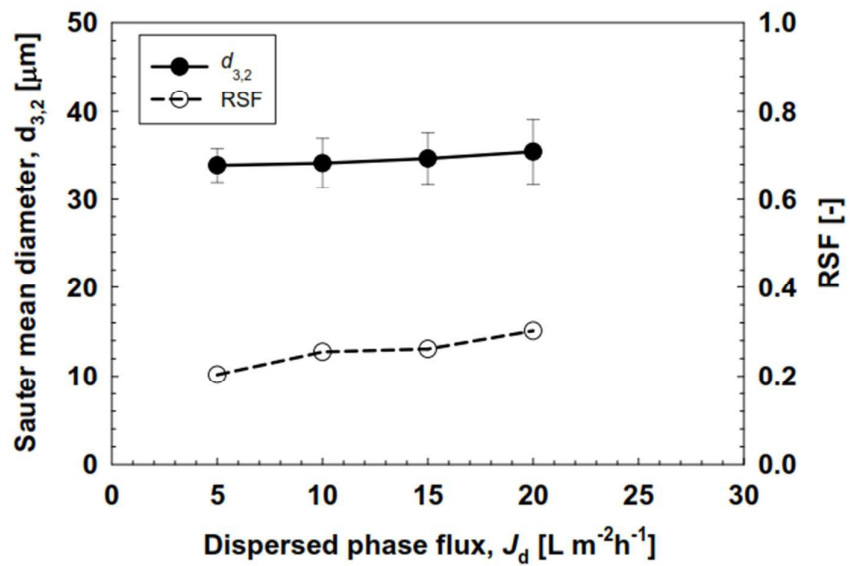


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81 Figure 8

82 (a)

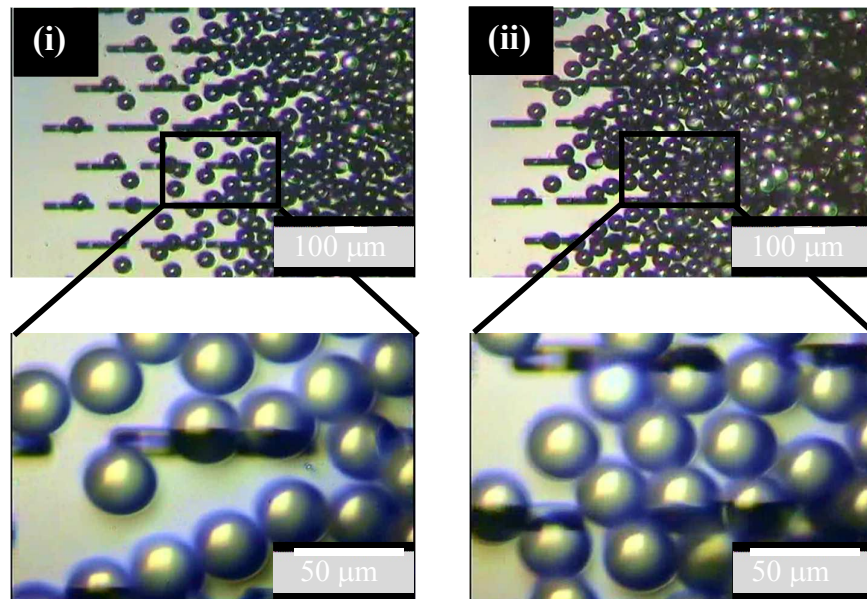


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84

85 (b)

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87

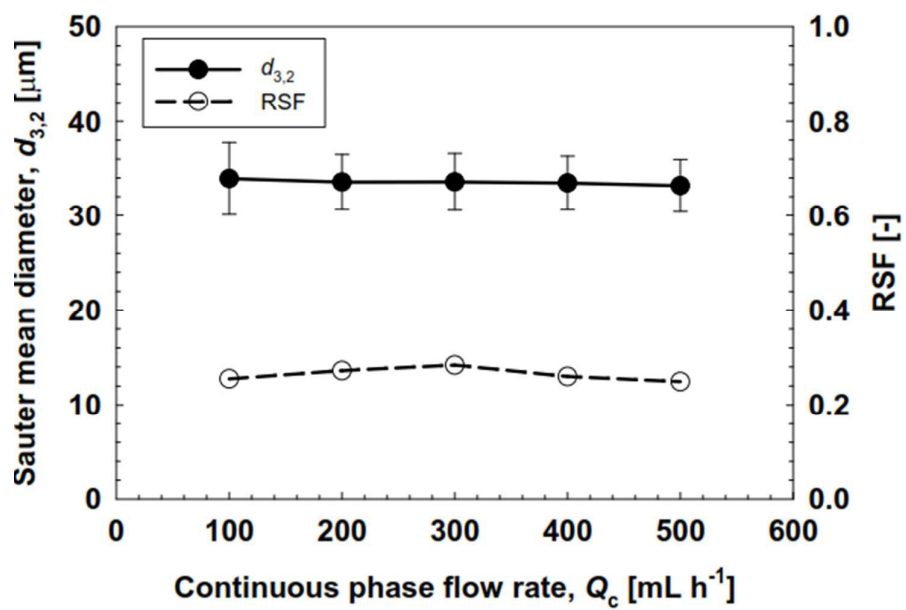
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91 (c)

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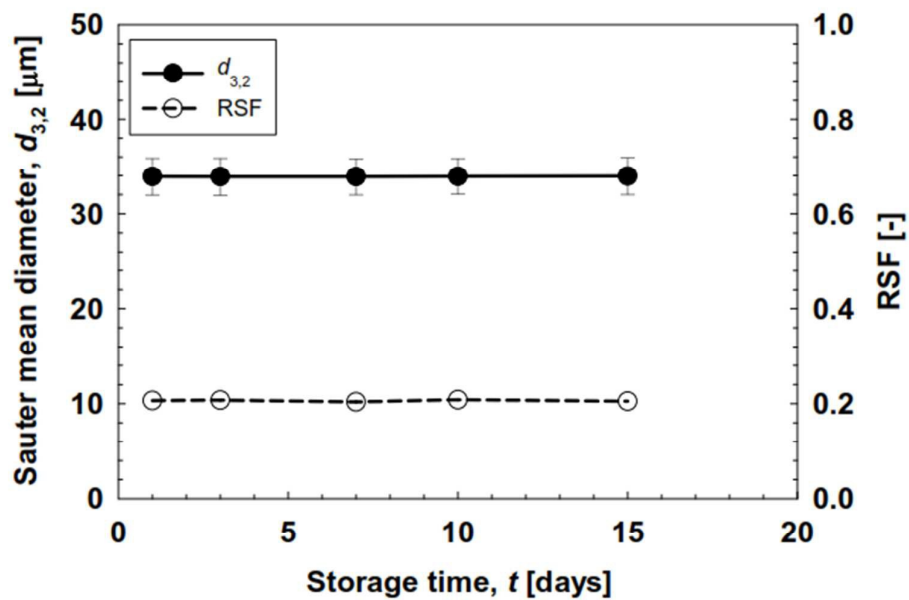
95 **Figure 9**

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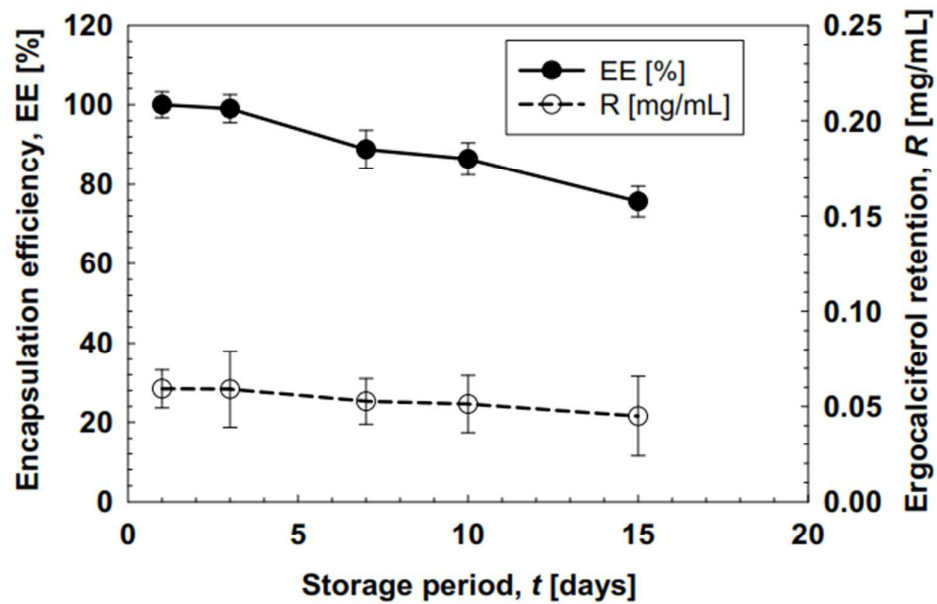
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101 **Figure 10**

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106 **Figure 11**

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Table 1: Fluid properties of the systems containing ergocalciferol together with different oils used for preparing O/W emulsions

	Dispersed phase				Emulsifiers in Milli-Q water	Continuous phase		
	$\eta_d$ (mPa s)	$\rho_d$ (kg m <sup>-3</sup> )	$\gamma_d$ (mN m <sup>-1</sup> )	** $\zeta$ (-)		$\eta_c$ (mPa s)	$\rho_c$ (kg m <sup>-3</sup> )	$\gamma_c$ (mN m <sup>-1</sup> )
*MCT	22.5±0.3	946.9±0.2	5.3±0.4	24.7	0.5% Tween 20	0.89±0.1	997.3±0.6	5.1±0.2
*Soybean oil	53.0±0.1	921.9±0.4	5.6±0.1	58.2	1.0% Tween 20	0.91±0.1	998.4±0.6	5.2±0.1
*Olive oil	68.2±0.1	911.9±0.2	6.2±0.2	75.0	1.5% Tween 20	0.96±0.1	999.1±0.8	5.2±0.2
*Safflower oil	53.2±0.1	918.9±0.1	5.3±0.2	58.5	2.0% Tween 20	0.99±0.1	1000.1±0.1	5.4±0.3
					1.0% $\beta$ -lg	0.95±0.1	999.9±0.2	12.6±0.9
					1.0% Sunsoft A-12	0.97±0.1	998.5±0.6	4.8±0.2

\* Dispersed phase contains 0.5% (w/w) ergocalciferol and interfacial tension was measured in the presence of 1% (w/w) Tween 20 in Milli-Q water, \*\* Viscosity ratio ( $\zeta$ ) was defined as the ratio of dispersed phase viscosity over continuous phase viscosity



