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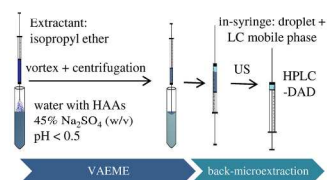
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Graphical Abstract  
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# Vortex-assisted emulsification microextraction followed by in-syringe ultrasound-assisted back-microextraction to determine haloacetic acids in waters

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## Abstract

We have evaluated a vortex-assisted emulsification microextraction (VAEME) procedure followed by in-syringe ultrasound-assisted back-microextraction for the determination of nine haloacetic acids in waters of different nature, using high-performance liquid chromatography with diode array detection. The optimized method requires 600  $\mu\text{L}$  of isopropyl ether as extractant solvent and 5 mL of the water sample containing:  $\text{Na}_2\text{SO}_4$  (45%, w/v) and a low pH value ( $< 0.5$ ). After emulsification assisted by vortex for 5 min, the droplet is separated from the water sample after centrifugation (5 min, 3500 rpm) using a syringe. This droplet is then back-microextracted in the syringe by mixing it with a low volume (50  $\mu\text{L}$ ) of an aqueous solution of  $(\text{NH}_4)_2\text{SO}_4$  (0.2M), to ensure compatibility with the HPLC mobile phase. After 5 min of sonication, the aqueous solution containing HAAs is directly injected in the chromatograph. The method is characterized by (a) average relative recoveries of 77.7-89.0%, depending on the spiked level, (b) average enrichment factors of  $\sim 10$  for the VAEME and of  $\sim 21$  for the overall method, (c) precisions of the overall method (expressed as relative standard deviations) between 5 and 23%, and (d) average extraction efficiencies of  $\sim 88\%$  for the VAEME method.

**Keywords:** Microextraction / Vortex-assisted emulsification / Haloacetic acids / Drinking Waters / Preconcentration / Back-microextraction

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## 1 Introduction

Chlorination is probably the most common worldwide treatment of waters intended for human consumption, because it efficiently removes pathogenic microorganisms like those responsible of malaria or typhus. However, the chlorine used in the process can react with the natural organic matter already present in waters, mainly humic and fulvic acids, originating disinfection byproducts (DBPs).<sup>1</sup> The extent of such formation is also dictated by the bromine content of waters as well as by the acidity.<sup>1-3</sup> Among disinfection byproducts, haloacetic acids (HAAs) and trihalomethanes (THMs) can be cited.

HAAs are highly polar compounds. Their structure is based in that of acetic acid molecule, but the alpha carbon adjacent to the carbonyl contains one, two or three halogens atoms (Br or Cl). There is a growing concern about the presence of HAAs in waters due to health issues.<sup>4,5</sup> Current *in vivo* studies with mice have proved toxic and carcinogen effect.<sup>6</sup> Indeed, the International Agency of Research on Cancer (IARC, <http://monographs.iarc.fr/ENG/Classification/ClassificationsAlphaOrder.pdf>) has classified four HAAs as possible human carcinogenic: dichloroacetic acid, trichloroacetic acid, dibromoacetic acid and bromochloroacetic acid; whereas the Environmental Protection Agency of United States (US-EPA, <http://water.epa.gov/drink/contaminants/#List>) classifies one HAA (trichloroacetic acid) as possible human carcinogen and another HAA (dichloroacetic acid) as probable human carcinogen.

In this sense, there is a need of analytical methods for the efficient determination of HAAs in waters. Current analytical methods take use of gas-chromatography (GC), high-performance liquid chromatography (HPLC), and ion-chromatography (IC), all in combination with a variety of detection systems. When GC is utilized, a derivatization step is needed to decrease the polarity and also to increase the volatility of HAAs, forming esters in the majority of cases.<sup>7,8</sup> Afterwards, the extraction is normally conducted using headspace (HS)<sup>9</sup> or headspace solid-phase microextraction (HS-SPME).<sup>10,11</sup> When HPLC is used, the most common strategy is to employ hydrophilic interaction liquid chromatography (HILIC),<sup>12,13</sup> generally in combination with a supported liquid membrane microextraction (SLMME) method.<sup>14,15</sup> When IC is used (with or without a suppressor column),<sup>16</sup> the extraction strategy normally involves solid-phase extraction (SPE).<sup>17,18</sup>

The utilization of microextraction procedures in sample preparation has been a hot topic in analytical chemistry during the past years,<sup>19,20</sup> because the elimination or minimization of the organic solvent consumption during the sample extraction step lies within the requirements of green analytical chemistry.<sup>21,22</sup> Among microextraction techniques, those based of liquid-phase microextraction (LPME) have been quite successful in its different performance modes.<sup>23-26</sup>

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67 Despite this, to the best of our knowledge SLMME is the only LPME mode that has been used  
68 for the HPLC determination of HAAs.<sup>14,15,27,28</sup>

69 Thus, the main purpose of this work is the utilization of LPME to determine a group of 9  
70 HAAs in different water samples. Specifically, it is intended the employment of the novel  
71 LPME mode vortex-assisted emulsification microextraction (VAEME),<sup>29</sup> which is based in the  
72 utilization of a low amount of extractant solvent, which is dispersed in the sample solution with  
73 the aid of vortex to assist the emulsification.<sup>30-33</sup> Furthermore, the method will be combined with  
74 an in-syringe ultrasound-assisted back-microextraction step to increase the sensitivity of the  
75 overall method and facilitate the compatibility with the HPLC mobile phase.

## 78 2 Materials and methods

### 80 2.1 Chemicals, reagents and materials

81 9 HAAs were used in the study (purity in %): chloroacetic acid (MCAA) (99%), bromoacetic  
82 acid (MBAA) (97%), bromochloroacetic acid (BCAA) (97%), dichloroacetic acid (DCAA)  
83 ( $\geq 99\%$ ), dibromoacetic acid (DBAA) (97%), trichloroacetic acid (TCAA) ( $\geq 99.5\%$ ),  
84 tribromoacetic acid (TBAA) (99%), chlorodibromoacetic acid (CDBAA) (94.6%), and  
85 bromodichloroacetic acid (BDCAA) (99.9%). DCAA, MCAA and TCAA were purchased from  
86 Sigma-Aldrich (Steinheim, Germany). BDCAA and CDBAA were supplied by Supelco  
87 (Bellefonte, PA, USA). The remaining HAAs were obtained from Aldrich (Steinheim,  
88 Germany). The EPA 552.3 acid calibration mix (with HAAs concentration of 200-2000  $\mu\text{g}\cdot\text{L}^{-1}$   
89 in methyl *tert*-butyl ether) was purchased from Supelco.

90 All experiments were carried out using deionized water (Milli-Q ultrapure grade) obtained  
91 by a water purification system A10 MilliPore (Watford, UK). Acetonitrile (ACN) and acetone  
92 were of HPLC grade (Chromasolv®), from Sigma-Aldrich. Octanol, pentane, trichloromethane  
93 and methyl *tert*-butyl ether (MTBE) were of pro-analysis purity grade, and obtained from  
94 Sigma-Aldrich. Decanol was purchased from Aldrich. Isopropyl ether was supplied from  
95 Panreac (Barcelona, Spain), with pro-analysis purity grade. Hexane was obtained from Merck  
96 (Darmstadt, Germany).

97 Sodium sulfate and ammonium sulfate were obtained from Scharlau (Barcelona, Spain).  
98 Sulfuric acid (97%) was purchased from Sigma-Aldrich.

99 The standard solutions of HAAs were prepared in different solvents:  $(\text{NH}_4)_2\text{SO}_4$  0.2 mol·L<sup>-1</sup>  
100 <sup>1</sup>, decanol, MTBE, octanol, or isopropyl ether, and stored at -18°C.

101 Treated water was collected from a desalination plant in Santa Cruz de Tenerife. Swimming  
102 pool water was sampled in a local pool (La Orotava). Two tap waters were also taken (La

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3 103 Orotava and La Laguna). Treated water and swimming pool water samples were kept at -18 °C  
4 104 until analysis. All water samples were filtered using Chromafil® Xtra PET-45/25, purchased  
5 105 from Panreac.  
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## 9 107 **2.2 Instruments**

10 108 The HPLC used was a L-2130 HITACHI model purchased from Merck, with an analytical  
11 109 column C18 (5 µm, 150x4.6 mm) obtained from Varian (Palo Alto, USA), and a Rheodyne  
12 110 7725i injection valve obtained from Supelco, with a loop of 20 µL. A diode array detector  
13 111 (DAD) Varian ProStart 330 was used, and the quantification wavelength was 210 nm. For the  
14 112 separation, the flow rate was linearly varied from 0.3 mL·min<sup>-1</sup> to 1 mL·min<sup>-1</sup> in 10 min,  
15 113 whereas the mobile phase, composed of ACN and (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> 0.2 mol·L<sup>-1</sup>, was also linearly  
16 114 varied from 0 to 10% (v/v) in ACN in 10 min, and then kept for 5 minutes.

17 115 A centrifuge model 5720 Eppendorf (Hamburg, Germany), a vortex from Reax-Control  
18 116 Heidolph GMBH (Schwabach, Germany), and an ultra sound bath KM (Shenzhen Codyson  
19 117 Electrical Co., Ltd. Shenzhen, China) were also utilized.  
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## 23 119 **2.3 Procedures**

24 120 The VAEME procedure was optimized using different organic solvents and volumes to find the  
25 121 maximum enrichment factor ( $E_F$ ) and droplet reproducibility. This procedure was carried out  
26 122 altogether with the back microextraction, necessary to ensure compatibility between the organic  
27 123 solvent containing HAAs (obtained in VAEME) and the chromatographic mobile phase used.  
28 124 Furthermore, the ultrasound-assisted back-microextraction was carried out *in situ* in the syringe  
29 125 used to sample the VAEME droplet, and optimized in order to incorporate an extra  
30 126 preconcentration step in the method. In this sense, organic solvents nature and volume, vortex  
31 127 time, centrifugation time, sample requirements, conditions for the *in situ* preconcentration, and  
32 128 so on were carefully optimized using a factor by factor procedure.

33 129 The optimum conditions for VAEME in combination with in-syringe ultrasound-assisted  
34 130 back-microextraction were: 5 mL of water sample were placed in a centrifuge tube of 15 mL  
35 131 volume, containing 2.25 g of ammonium sulfate and 130 µL of concentrated sulfuric acid (to  
36 132 ensure pH < 0.5). Then, 600 µL of isopropyl ether were added, followed by 5 min of vortex  
37 133 to ensure the efficient formation of droplets in the absence of a dispersive solvent. The tube was  
38 134 then centrifuged during 5 min at 3500 rpm. The obtained phase of isopropyl ether after VAEME  
39 135 (containing extracted HAAs) was collected with a Hamilton syringe (of 1 mL). Then, 50 µL of  
40 136 mobile phase (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> 0.2 mol·L<sup>-1</sup> (ratio 8:1 with the isopropyl ether, to increase the  
41 137 preconcentration factor) were also introduced in the same syringe (already containing HAAs in  
42 138 isopropyl ether) to perform the in-syringe ultrasound-assisted back-microextraction. The syringe  
43 139 was subjected to ultrasounds during 5 min, and the organic phase was discarded. Thus, the

aqueous phase ( $0.2 \text{ mol}\cdot\text{L}^{-1} (\text{NH}_4)_2\text{SO}_4$ ) containing HAAs was directly injected in the HPLC system avoiding this way compatibility problems.

## 2.4 Assessment of the method performance

The relative recovery was calculated as:

$$\text{RR}(\%) = 100 \cdot \frac{C_{\text{found}}}{C_{\text{initial}}} \quad (1)$$

being  $C_{\text{found}}$  the calculated concentration of the HAAs using the overall method (VAEME-back microextraction-HPLC-DAD) calibration, and  $C_{\text{initial}}$  the spiked concentration of HAAs in water.

In general, for microextraction methods it is expected the obtaining of relative recoveries around 100% if the precision of the method is acceptable.

The enrichment factor of the overall method is given by:

$$E_{\text{F}} = \frac{C_{\text{droplet}}}{C_{\text{initial}}} \quad (2)$$

being  $C_{\text{droplet}}$  the concentration of HAAs obtained in the final droplet that is injected in the HPLC, and so it can be calculated with the chromatographic calibration.

The overall extraction efficiency ( $E_{\text{R}}$ ) of the method can be calculated by:

$$E_{\text{R}} = 100 \cdot \frac{E_{\text{F}}}{E_{\text{Fmax}}} \quad (3)$$

being  $E_{\text{Fmax}}$  the maximum preconcentration that would be achieved if all HAAs (initially present in the water sample) were successfully transferred to the final droplet that is injected in the HPLC. This value can be estimated from the ratio  $V_{\text{initial}}/V_{\text{droplet}}$ , being  $V_{\text{initial}}$  the initial aqueous sample volume (5 mL).

The extraction efficiency only associated to VAEME was calculated indirectly, taking into account the overall extraction efficiency and the extraction efficiency solely associated to the in-syringe ultrasound-assisted back-microextraction step. The same comments are applied to the calculations of the  $E_{\text{F}}$  only associated to VAEME.

## 3 Results and discussion

### 3.1 Chromatographic determination

This work intended the determination of HAAs using HPLC with a conventional C18 column, and so the method is based on a modification of the work of Chen *et al.*,<sup>14</sup> but using lower content of ammonium sulfate, and with the help of ACN to decrease the analysis time. Under these conditions (see section 2.2.), adequate resolution of HAAs was achieved in 13 min (see Fig. S1 of the supplementary material). Table S1 of the supplementary material also includes several quality analytical parameters of the calibrations obtained.



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### 176 3.2 VAEME optimization

177 In order to adequately extract HAAs using a micro-volume of an organic solvent in VAEME (or  
178 in any liquid-phase microextraction technique), HAAs should be in nonionic form. HAAs  
179 present quite low  $pK_a$  values and so it is necessary to work at low pH values ( $pH < 0.5$ ), as it is  
180 also suggested by the EPA ([www.epa.gov/ogwdw/methods/pdfs/methods/met552\\_3.pdf](http://www.epa.gov/ogwdw/methods/pdfs/methods/met552_3.pdf)) This is  
181 achieved employing concentrated sulfuric acid (130  $\mu\text{L}$  to 5 mL of water sample). Water sample  
182 volume was fixed to 5 mL simply considering the volume capacity of our centrifuge.

183 Furthermore, it is also advisable to work with high ionic strengths to take advantage of the  
184 salting out effect. In this case,  $\text{Na}_2\text{SO}_4$  is used to adjust the ionic strength up to 45% (w/v) and  
185 not NaCl to avoid the artifact formation of HAAs containing chlorine. Other contents of  $\text{Na}_2\text{SO}_4$   
186 were tried and best performance was achieved at 45% (data not shown).

187 We conducted a simple optimization factor by factor with VAEME given the *a priori*  
188 relatively low number of variables to study: nature and volume of the extractant solvent and  
189 extraction time (vortex stirring).

190 The studied extractant solvents were: MTBE, isopropyl ether, decanol, octanol, hexane,  
191 trichloromethane and pentane, fixing their volumes to 100  $\mu\text{L}$  (with pH and ionic strength as  
192 abovementioned), and applying vortex for 1 minute and centrifugation at 3500 rpm. To ensure  
193 an adequate microdroplet formation, different centrifugation times were tested (from 1 to 8 min)  
194 and 5 min was selected. Thus, hexane, trichloromethane and pentane were discarded due to lack  
195 of reproducibility in the microdroplet obtained after centrifugation. To evaluate the extraction  
196 efficiency of the remaining solvents for HAAs in VAEME it is necessary to perform a solvent  
197 exchange step, to ensure the compatibility of the final solvent with HPLC. In this sense, we  
198 decided to carry out a back-microextraction rather than other possible solvent-exchange steps.

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#### 200 3.2.1 In-syringe ultrasound-assisted back-microextraction optimization

201 Once HAAs were extracted in the micro-droplet of organic solvent obtained by VAEME, it is  
202 sampled with a micro-syringe. Then, such micro-droplet is mixed within the syringe with an  
203 equivalent volume (1:1 ratio) of initial HPLC mobile phase ( $0.2 \text{ mol}\cdot\text{L}^{-1} (\text{NH}_4)_2\text{SO}_4$ ,  $pH = 5.18$ ).  
204 Thus, neutral HAAs present in the organic solvent pass to this aqueous phase in ionic form, and  
205 are ready to HPLC injection. Fig. 1 (A) schematically shows this step. Obviously, it is important  
206 to optimize this strategy that takes place *in situ* in the syringe, and to evaluate which organic  
207 solvent suits better for this back-microextraction.

208 The sonication time to which the syringe is subjected to ultrasounds in the back-  
209 microextraction step was studied from 2 to 10 min. For all solvents studied, there were not  
210 significant differences when sonication times were higher than 5 min, and so this time was  
211 selected. Fig. S2 of the supplementary material shows the results of such optimization when



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3 212 using isopropyl ether as organic solvent, and a concentration of  $5 \text{ mg}\cdot\text{L}^{-1}$  for the HAAs. In these  
4 213 studies, the volume of organic solvent in the syringe was  $100 \mu\text{L}$ .

5 214 The extraction efficiency of the back-microextraction itself was then evaluated, also using  
6 215  $100 \mu\text{L}$  of organic solvent in the syringe (and mixed in a 1:1 ratio with the aqueous salty phase),  
7 216 and a known concentration of HAAs. Table 1 shows the extraction efficiencies achieved in each  
8 217 case. Higher efficiencies were obtained with MTBE and isopropyl ether, with average values of  
9 218 77.8 and 67.2%, respectively. For decanol and octanol, lower efficiencies were obtained. In  
10 219 spite of low recoveries for decanol and octanol, they were not yet discarded, until the overall  
11 220 method was not tested. For all solvents, RSD values (in %) for the back-microextraction step  
12 221 were adequate, ranging between 2.7 and 17%. These values can be considered acceptable  
13 222 because it must be taken into account that this microextraction step takes place *in situ* in the  
14 223 micro-syringe, followed by HPLC injection, and so no further losses will be added to the  
15 224 method.  
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### 26 226 3.2.2 Overall VAEME and in-syringe ultrasound-assisted back-microextraction optimization

17 227 The overall VAEME and back-microextraction optimization was focused on the following  
18 228 parameters: VAEME vortex time, nature of the extractant solvent, and volume of extractant  
19 229 solvent.  
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21 231 Different vortex times were studied, between 1 to 10 min. In the majority of cases, the best  
22 232 option was a vortex time of 5 min. Fig. S3 of the supplementary material shows the effect of the  
23 233 vortex time for some HAAs (as examples) using  $200 \mu\text{L}$  of isopropyl ether as extractant solvent.

24 234 The selection of the extractant solvent was carried out once fixed the vortex time to 5 min.  
25 235 Thus, MTBE, isopropyl ether, decanol and octanol were evaluated using the same volume ( $200$   
26 236  $\mu\text{L}$ ). Decanol was discarded at this point due to low recoveries. Fig. 2 shows the results  
27 237 obtained. In the majority of cases, the best extractant solvent was isopropyl ether, generating  
28 238 higher extraction efficiencies, and therefore it was selected in further experiments.

29 239 The last study was the selection of the optimum volume of isopropyl ether. Volumes  
30 240 between  $300$  to  $700 \mu\text{L}$  were tested, as it is shown in Fig. 3. For the overall VAEME and back-  
31 241 microextraction procedure in combination with HPLC-DAD, higher extraction efficiencies  
32 242 ( $>75\%$  for the majority of HAAs) were obtained when using  $600 \mu\text{L}$  of isopropyl ether  
33 243 (generating a microdroplet in VAEME of  $\sim 500 \mu\text{L}$ ).

34 244 In summary, optimum conditions imply the use of  $5 \text{ mL}$  water containing  $2.25 \text{ g Na}_2\text{SO}_4$   
35 245 and  $130 \mu\text{L H}_2\text{SO}_4$  conc., which are mixed with  $600 \mu\text{L}$  of isopropyl ether (extractant solvent),  
36 246 subjected to  $5 \text{ min}$  vortex, and then centrifugation at  $3500 \text{ rpm}$  for  $5 \text{ min}$ . The in-syringe  
37 247 ultrasound-assisted back-microextraction step is then performed with a 1:1 ratio with the mobile  
38 248 phase and applying  $5 \text{ min}$  of ultrasounds.

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3 249 3.2.3 Inclusion of a preconcentration step within the back-microextraction  
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5 250 All experiments abovementioned have been carried out using a 1:1 ratio in the back-  
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7 251 microextraction step. In order to increase the overall sensitivity of the extraction method, we  
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9 252 decided to use other ratios. Given the fact that 500  $\mu\text{L}$  of isopropyl droplet are obtained in the  
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11 253 optimum method after VAEME, 400  $\mu\text{L}$  are sampled in the syringe. This implies mixing 400  
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13 254  $\mu\text{L}$  of isopropyl ether with 400  $\mu\text{L}$  of the aqueous salty solution for the 1:1 ratio, 400  $\mu\text{L}$  of  
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15 255 isopropyl ether with 200  $\mu\text{L}$  of aqueous salty solution for the 2:1 ratio, and so on. All  
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17 256 experiments were carried out using a concentration of  $5 \text{ mg}\cdot\text{L}^{-1}$  for HAAs. Table S2 of the  
18  
19 257 supplementary material shows the extraction efficiency of the overall method when using  
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21 258 different ratios in the back-microextraction (1:1, 2:1, 4:1 and 8:1). Higher extraction efficiencies  
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23 259 (almost quantitative) were obtained with the 1:1 ratio. On the other hand, worse extraction  
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25 260 efficiencies were obtained when using the 8:1 ratio. Despite the obtaining of worse extraction  
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27 261 efficiencies with the 8:1 ratio, we selected it because it is accompanied by an important  
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29 262 preconcentration step, as it is clearly shown in Fig. 4 and it is pursued the achieving of low  
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31 263 limits of detection. It is important to highlight the difficulty in achieving extraction efficiency  
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33 264 values close to 100% in microextraction procedures. Indeed, these values are valid as long as  
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35 265 the performance of the method fulfills the requirements of a given application.<sup>34</sup>  
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### 267 **3.3 Quality analytical parameters of the optimum VAEME, in-syringe ultrasound-** 268 **assisted back-microextraction and HPLC-DAD method.**

269 The optimum conditions of overall method are depicted in Fig. 1 (B). Calibrations were  
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271 undertaken using standards of HAAs dissolved in deionized water, which were subjected to the  
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273 overall method (VAEME, back-microextraction, and HPLC). Table 2 includes several quality  
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275 analytical parameters of the overall method: microextraction procedures and chromatographic  
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277 separation. Correlation coefficients for the overall calibration method were higher than 0.990 for  
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279 all HAAs, except for MCAA (with R being 0.986). LODs and LOQs were calculated on a signal  
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281 to noise ratio of three and ten, respectively; and verified by preparation of standards spiked at  
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283 such levels and subjected to the overall method. Thus, LODs ranged from  $1.02 \text{ }\mu\text{g}\cdot\text{L}^{-1}$  for  
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285 TBAA and  $9.95 \text{ }\mu\text{g}\cdot\text{L}^{-1}$  for DCAA, whereas higher values were obtained for MCAA and MBAA  
(being  $44.1$  and  $60.1 \text{ }\mu\text{g}\cdot\text{L}^{-1}$ , respectively).

279 Given the fact that there are no other published works of VAEME for HAAs and HPLC,  
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281 the comparison of the present mode with other literature data will be mainly carried out with  
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283 other LPME modes, such as SLLME, in combination with HPLC. Thus, LODs for the 9 HAAs  
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285 using SLLME and HPLC-UV have been reported to vary between  $0.10$  and  $6.84 \text{ }\mu\text{g}\cdot\text{L}^{-1}$  (without  
calibration performance),<sup>14</sup>  $0.02$  and  $2.69 \text{ }\mu\text{g}\cdot\text{L}^{-1}$  (being the calibration range  $0.4$ - $20 \text{ }\mu\text{g}\cdot\text{L}^{-1}$ ),<sup>27</sup>  
 $2.23$  and  $107 \text{ }\mu\text{g}\cdot\text{L}^{-1}$  (being the calibration range  $20$ - $20000 \text{ }\mu\text{g}\cdot\text{L}^{-1}$ ),<sup>28</sup> and down to  $0.072$ - $40.3$   
 $\text{ng}\cdot\text{L}^{-1}$  when utilizing electromembrane extraction with a SLM containing toluene (being the

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3 286 calibration range 5-200  $\mu\text{g}\cdot\text{L}^{-1}$ ).<sup>15</sup> These literature methods require extraction times ranging  
4 287 from 15 to 60 min (~17 min in the present work), samples volumes between 23 and 100 mL  
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6 288 (only 5 mL in the present work), and solvents such as dihexyl ether and toluene (being isopropyl  
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8 289 ether in the present work).<sup>14,15,27,28</sup>

9  
10 290 Other works in the recent literature also included different microextraction steps and other  
11 291 determination techniques, such as single-drop microextraction with derivatization in  
12 292 combination with GC-mass spectrometry (MS)<sup>35</sup>, getting LODs between 0.33 to 1.5  $\mu\text{g}\cdot\text{L}^{-1}$ ,  
13 293 liquid-liquid microextraction with derivatization in combination with HS-GC-MS<sup>36</sup>, with LODs  
14 294 between from 0.02 to 0.4  $\mu\text{g}\cdot\text{L}^{-1}$ ; IC coupled with SPE<sup>37</sup> being the LODs between 1.89 and 11.8  
15 295  $\mu\text{g}\cdot\text{L}^{-1}$ , or not coupled with a SPE step<sup>38</sup>, being the LODs between 0.37 and 31.64  $\mu\text{g}\cdot\text{L}^{-1}$ ; and  
16 296 also HPLC in HILIC mode in combination with MS<sup>13</sup>, with LODs between 0.18 and 71.5  $\mu\text{g}\cdot\text{L}^{-1}$   
17 297 <sup>1</sup>.

18 298 The performance was assessed by the extraction efficiency of the overall method ( $E_R$  in %),  
19 299 the efficiency only associated to the VAEME step ( $E_R'$  in %), the enrichment factor of the  
20 300 overall method ( $E_F$ ), the enrichment factor only associated to the VAEME step ( $E_F'$ ), the  
21 301 precision of the overall method (as RSD in %), and the relative recovery of the overall method  
22 302 (RR in %).

23 303 In this work,  $E_{F\text{max}}$  (theoretical value) has a value of 11.4 only considering VAEME, and of  
24 304 91.2 if considering the overall method.

25 305 Table 3 includes the results obtained for the extraction performance of the method  
26 306 according to these parameters. This study was accomplished using deionized waters spiked at  
27 307 two different levels (100 and 700  $\mu\text{g}\cdot\text{L}^{-1}$ ), and subjected to the overall method ( $n = 4$ ).  $E_R'$  is  
28 308 calculated considering  $E_R$  as well as the losses obtained in the in-syringe ultrasound-assisted  
29 309 back-microextraction using the 8:1 ratio (Table S2).

30 310 In all cases, it can be observed adequate relative recoveries, with average values of 89.0 and  
31 311 77.7% for the higher and the lower spiked level, respectively. RSD values ranged from 7.5% for  
32 312 DCAA and 22% for MCAA for the higher spiked level, and from 5.2% for DCAA and 23% for  
33 313 MCAA for the low spiked level.

34 314 Average enrichment factors only associated to VAEME ( $E_F'$ ) were 10.1 for the lower  
35 315 spiked level and 10.0 for the higher spiked level. Both values are quite close to the  $E_{F\text{max}}$  (11.4),  
36 316 which already indicates that the extraction efficiency only associated to VAEME ( $E_R'$ ) is almost  
37 317 quantitative. Indeed, average  $E_R'$  values ranged from 88.5% for the lower spiked level to 87.7%  
38 318 for the higher spiked level.

39 319 Regarding the overall method, the overall extraction efficiency is lower, mainly to the  
40 320 losses associated to the back-microextraction step when using the 8:1 ratio, with average values  
41 321 of 22.6% for the lower spiked level and 22.9% for the higher spiked level. It must be  
42 322 highlighted that it is difficult to achieve  $E_R$  values close to 100% in any microextraction

323 procedure, and so  $E_R$  values are valid as long as the LODs,  $E_F$  values, and reproducibility of the  
324 method are sufficient for a given application.

325 The overall method is characterized for average  $E_F$  values of 20.6 for the lower spiked level  
326 and of 20.8 for the higher spiked level. Thus, despite the losses in the back-microextraction,  
327 adequate reproducibility, low detection limits, and overall preconcentration factors of ~21 are  
328 obtained using HPLC with a conventional C18 column. Comparing with other SLLME-HPLC-  
329 UV works,  $E_F$  values of 500,<sup>14</sup> 300-3000,<sup>27</sup> and 10-65;<sup>28</sup> and  $E_R$  values of 54%,<sup>15</sup> and 16-50%,<sup>28</sup>  
330 have been reported.

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### 332 **3.4 Analysis of different water samples using the optimized method**

333 Several waters have been analyzed with this methodology as a preliminary study to test its  
334 validity with more complex samples. Tap waters from La Laguna University and from La  
335 Orotava, pool water from a local pool in La Orotava, and re-mineralized water from a  
336 desalination plant (Santa Cruz de Tenerife) were analyzed in order to assess the applicability of  
337 the method with real samples. Samples were filtered, and their pH was adequately adjusted  
338 before carrying out the overall optimum procedure. Each sample was analyzed by triplicate.  
339 Results from this study are shown in Table 4. Furthermore, accuracy and precision studies were  
340 performed with tap waters from La Laguna, spiked at 400  $\mu\text{g}\cdot\text{L}^{-1}$  level, getting RSD values  
341 lower than 18.4% (as intra-day precision) and average relative recovery of 79.3%.

342 Tap waters were shown to be free of HAAs, as well as the pool water. However six HAAs  
343 were detected in waters coming from the desalination plant (MCAA, MBAA, BCAA, DBAA,  
344 CDBAA and TBAA), and four of them were quantified, being for example the content of  
345 MCAA up to  $244 \pm 22 \mu\text{g}\cdot\text{L}^{-1}$ . Ongoing work is carried out to utilize this methodology as a  
346 monitoring technique with real samples.

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## 349 **4 Conclusions**

350 A VAEME method followed by in-syringe ultrasound-assisted back-microextraction has been  
351 developed for first time and applied for the determination of a group of nine haloacetic acids in  
352 real water samples. The VAEME method is quick, simply based on the extraction of HAAs  
353 using a low volume of isopropyl ether, being the emulsification assisted by vortex. Afterwards,  
354 an in-syringe back-microextraction is carried out to ensure the further compatibility with HPLC.  
355 Moreover, this in-syringe step is carried out incorporating a preconcentration strategy (by  
356 mixing the organic droplet containing HAAs with a much lower volume of an aqueous solution  
357 of  $\text{Na}_2\text{SO}_4$ ), to increase the overall sensitivity of the method. Furthermore, the HPLC method  
358 with diode array detector is carried out with a conventional C18 column. Under optimized

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3 359 conditions, average relative recoveries of 77.7 to 89.0%, depending on the concentration level  
4 360 considered, and precision values lower than 23% (as RSD) were obtained.

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6 361 The overall method is therefore fast (~17 min for the overall microextraction procedure,  
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8 362 and ~15 min for the chromatographic run), it does not use toxic organic solvents, and it results  
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10 363 quite simple. The applicability of the procedure was verified by considering sample matrices of  
11 364 different complexities, and the performance of the method was still successful.

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3 430 **Figure Captions**  
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6 431 **Fig. 1** A) Scheme of the in-syringe ultrasound-assisted back-microextraction procedure using a  
7 432 1:1 ratio. B) Scheme of the overall procedure under optimum conditions: VAEME followed by  
8 433 in-syringe ultrasound-assisted back-microextraction using a 8:1 ratio, and HPLC injection.  
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12 435 **Fig. 2** Effect of the solvent nature on the extraction efficiency (as peak area) of HAAs when  
13 436 applying the overall method by triplicate (VAEME, back-microextraction and HPLC-DAD),  
14 437 and using 200  $\mu\text{L}$  of extractant solvent. Rest of conditions as described in the text.  
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18 439 **Fig. 3** Effect of the isopropyl ether volume on the extraction efficiency of HAAs (spiked  
19 440 concentration of  $5 \text{ mg}\cdot\text{L}^{-1}$ ) using the overall method by triplicate (VAEME, back-  
20 441 microextraction and HPLC-DAD), and 5 min of vortex. Rest of conditions as described in the  
21 442 text.  
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25 444 **Fig. 4** Effect of different ratios of the back-microextraction step (HAA concentration of  $5 \text{ mg}\cdot\text{L}^{-1}$ )  
26 445 on the sensitivity of the overall method.  
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447 **Table 1** Extraction efficiencies when using different organic solvents solely associated to the back-microextraction step.

HAAs	MTBE <sup>a</sup>		Decanol <sup>b</sup>		Octanol <sup>b</sup>		Isopropyl ether <sup>b</sup>	
	Obtained concentration (mg·L <sup>-1</sup> ) ± SD <sup>c</sup>	Extraction efficiency (%)	Obtained concentration (mg·L <sup>-1</sup> ) ± SD <sup>c</sup>	Extraction efficiency (%)	Obtained concentration (mg·L <sup>-1</sup> ) ± SD <sup>c</sup>	Extraction efficiency (%)	Obtained concentration (mg·L <sup>-1</sup> ) ± SD <sup>c</sup>	Extraction efficiency (%)
MCAA	3.59 ± 0.58	62.7	2.07 ± 0.34	41.4	2.94 ± 0.36	58.8	3.37 ± 0.37	67.3
MBAA	2.67 ± 0.19	68.8	2.09 ± 0.32	41.7	2.95 ± 0.24	59.0	3.13 ± 0.45	67.0
DCAA	6.85 ± 0.60	116	3.19 ± 0.38	63.7	4.03 ± 0.34	80.5	3.38 ± 0.13	67.6
BCAA	4.06 ± 0.41	99.9	2.83 ± 0.46	56.7	3.62 ± 0.34	72.4	3.54 ± 0.19	70.7
DBAA	1.97 ± 0.11	92.9	2.73 ± 0.42	54.6	2.80 ± 0.25	56.0	3.34 ± 0.09	66.8
TCAA	1.57 ± 0.22	76.9	2.23 ± 0.24	44.6	1.05 ± 0.18	21.1	2.31 ± 0.25	46.1
BDCAA	2.33 ± 0.24	53.4	2.51 ± 0.16	50.3	1.36 ± 0.11	27.1	3.52 ± 0.28	70.4
CDBAA	7.24 ± 0.95	72.2	3.11 ± 0.23	62.2	3.28 ± 0.50	65.6	2.48 ± 0.29	49.5
TBAA	12.7 ± 0.75	57.6	2.81 ± 0.21	56.2	3.31 ± 0.29	66.1	5.96 ± 0.81	99.3
Average		77.8		53.4		56.3		67.2

<sup>a</sup>MTBE containing the following concentration of HAAs (mg·L<sup>-1</sup>): 5.73 for MCAA, 3.88 for MBAA, 5.90 for DCAA, 4.70 for BCAA, 2.12 for DBAA, 2.04 for TCAA, 4.36 for BDCAA, 10.03 for CDBAA and 22.0 for TBAA (obtained by dilution of the EPA 552.3 acid calibration mix)

<sup>b</sup>HAAs concentration: 5 mg·L<sup>-1</sup>

<sup>c</sup>standard deviation (n = 6)

448 **Table 2** Quality analytical parameters of the calibration for the overall method (VAEME, back-microextraction with 8:1 ratio and HPLC-DAD  
 449 determination).

HAAs	Linearity range ( $\mu\text{g}\cdot\text{L}^{-1}$ )	Slope $\pm t_{n-2}\times\text{SD}^{\text{a}}$	Intercept $\pm t_{n-2}\times\text{SD}^{\text{a}}$	R	LOD <sup>b</sup> ( $\mu\text{g}\cdot\text{L}^{-1}$ )	LOQ <sup>b</sup> ( $\mu\text{g}\cdot\text{L}^{-1}$ )
MCAA	150 - 300	158 $\pm$ 49	-14015 $\pm$ 9047	0.986	44.1	147
MBAA	200 - 1000	729 $\pm$ 43	-18671 $\pm$ 20904	0.997	60.1	200
DCAA	100 - 1000	608 $\pm$ 157	-18252 $\pm$ 31882	0.992	9.95	33.2
BCAA	25 - 1000	962 $\pm$ 99	6405 $\pm$ 43399	0.993	4.95	16.5
DBAA	28 - 1000	1610 $\pm$ 123	9090 $\pm$ 61961	0.997	8.36	27.9
TCAA	100 - 1000	641 $\pm$ 90	19228 $\pm$ 38463	0.990	9.06	30.2
BDCAA	25 - 1000	1233 $\pm$ 142	3420 $\pm$ 69413	0.991	1.46	4.89
CDBAA	10 - 1000	1515 $\pm$ 120	-15700 $\pm$ 52896	0.991	2.95	9.84
TBAA	10 - 1000	1579 $\pm$ 125	38407 $\pm$ 55209	0.991	1.02	3.39

<sup>a</sup>confidence level ( $\alpha = 0.05$ ) for  $n = 14$ , except MCAA and MBAA with  $n = 6$

<sup>b</sup>calculated as described in the text

450 **Table 3** Extraction efficiency and precision study for the overall method (VAEME, back-microextraction with 8:1 ratio and HPLC-DAD determination) and  
 451 performance solely associated to VAEME.

HAA	Spiked level: 100 $\mu\text{g}\cdot\text{L}^{-1}$ (n = 4)						Spiked level: 700 $\mu\text{g}\cdot\text{L}^{-1}$ (n = 4)					
	RR <sup>a</sup> (%)	RSD <sup>b</sup> (%)	E <sub>R</sub> <sup>c</sup> (%)	E <sub>R</sub> <sup>d</sup> (%)	E <sub>F</sub> <sup>e</sup>	E <sub>F</sub> <sup>f</sup>	RR <sup>a</sup> (%)	RSD <sup>b</sup> (%)	E <sub>R</sub> <sup>c</sup> (%)	E <sub>R</sub> <sup>d</sup> (%)	E <sub>F</sub> <sup>e</sup>	E <sub>F</sub> <sup>f</sup>
MCAA	62.8	23	80.2	11.3	9.19	10.3	78.1	22	71.8	12.9	8.23	11.8
MBAA	63.4	21	80.9	17.4	9.27	15.9	83.8	12	82.0	18.5	9.39	16.9
DCAA	125	5.2	98.0	29.5	11.2	26.9	96.3	7.5	94.5	26.0	10.8	23.1
BCAA	77.0	6.7	83.6	20.1	9.58	18.3	89.8	8.8	84.8	21.3	9.72	19.4
DBAA	83.7	10	93.5	23.7	10.7	21.6	91.1	7.8	91.8	22.0	10.5	20.1
TCAA	63.4	11	105	22.7	12.0	20.7	102	8.7	106	24.1	12.2	22.0
BDCAA	80.7	9.2	86.7	22.6	9.94	20.6	80.3	9.2	86.9	22.8	9.96	20.8
CDBAA	76.0	11	91.1	28.1	10.4	25.6	99.9	8.6	95.0	32.0	10.9	29.2
TBAA	67.3	8.8	77.8	28.3	8.91	25.8	80.1	8.9	76.1	26.6	8.72	24.3
Average	77.7		88.5	22.6	10.1	20.6	89.0		87.7	22.9	10.1	20.8

<sup>a</sup>relative recovery of the overall method

<sup>d</sup>extraction efficiency of the overall method

<sup>b</sup>relative standard deviation of the overall method

<sup>e</sup>enrichment factor only associated to VAEME

<sup>c</sup>extraction efficiency only associated to VAEME

<sup>f</sup>enrichment factor of the overall method

**Table 4** Analysis of real water samples using the overall optimized procedure.

HAA	Tap water 1 (La Laguna)			Tap water 2 (La Orotava)		Swimming pool water (La Orotava)	Desalination plant water (Santa Cruz)
	non spiked Conc <sup>a</sup> ± SD <sup>b</sup>	spiked (400 µg·L <sup>-1</sup> ) RSD <sup>c</sup> (%)	RR <sup>d</sup> (%)	non spiked Conc <sup>a</sup> ± SD <sup>b</sup>	non spiked Conc <sup>a</sup> ± SD <sup>b</sup>	non spiked Conc <sup>a</sup> ± SD <sup>b</sup>	non spiked Conc <sup>a</sup> ± SD <sup>b</sup>
MCAA	nd	16.4	67.4	nd	nd	224 ± 22	
MBAA	nd	12.6	116	nd	nd	nq	
DCAA	nd	15.5	64.9	nd	nd	nd	
BCAA	nd	18.4	64.0	nd	nd	31.3 ± 5.6	
DBAA	nd	12.2	88.5	nd	nd	nq	
TCAA	nd	10.2	63.9	nd	nd	nd	
BDCAA	nd	7.43	110	nd	nd	nd	
CDBAA	nd	17.0	79.3	nd	nd	21.3 ± 3.8	
TBAA	nd	5.06	60.0	nd	nd	6.27 ± 4.02	

<sup>a</sup>concentration in µg·L<sup>-1</sup><sup>b</sup>standard deviation (n = 3)<sup>c</sup>relative standard deviation (n = 3)<sup>d</sup>relative recovery (n = 3)

nd: non-detected

nq: non-quantified

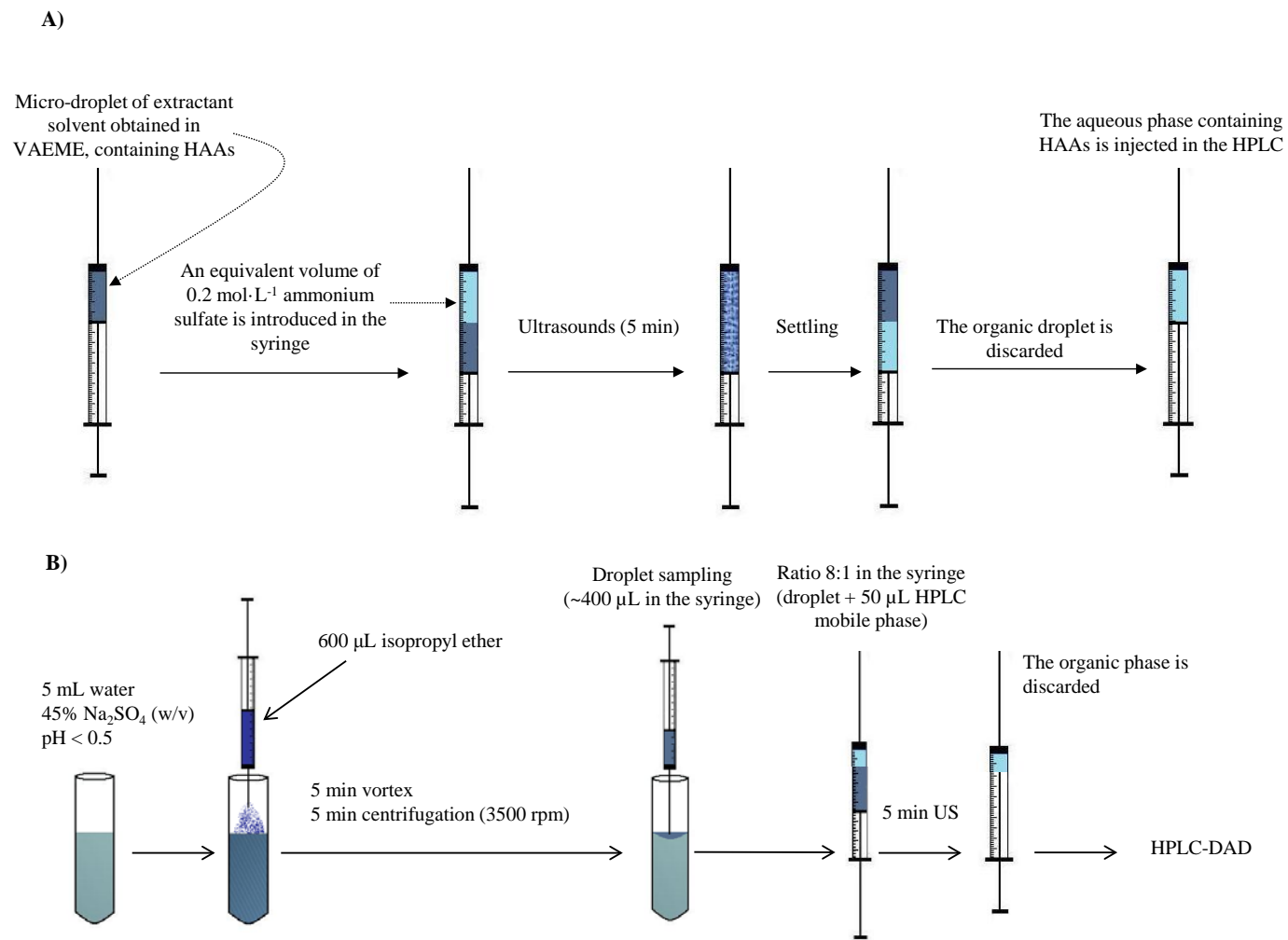


Figure 1

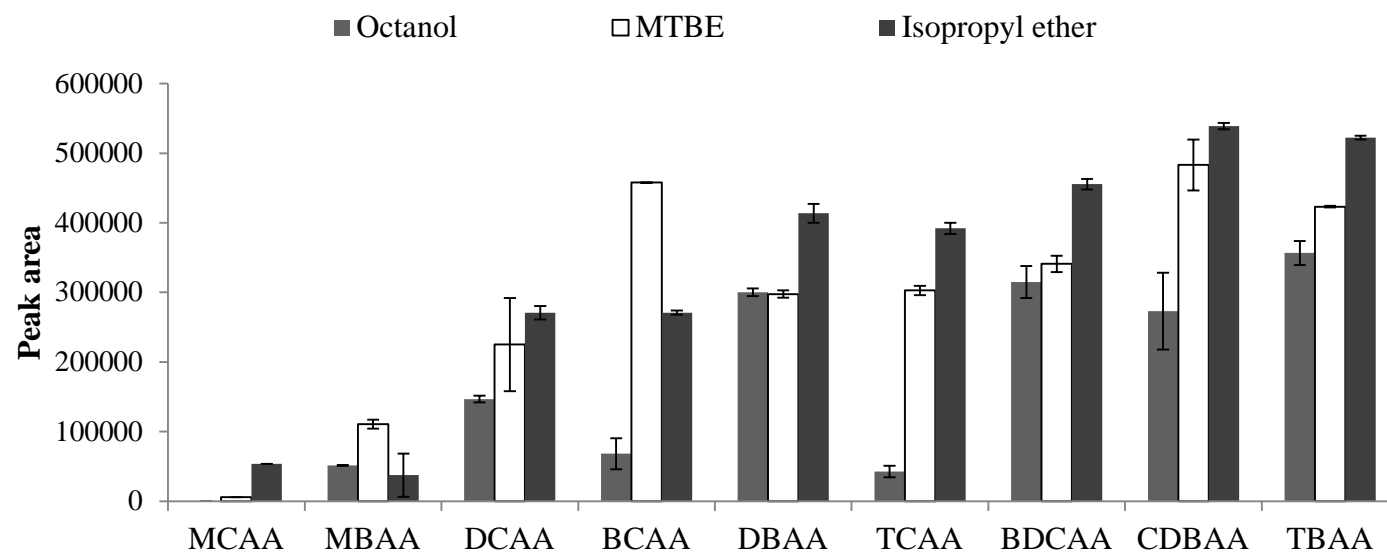


Figure 2



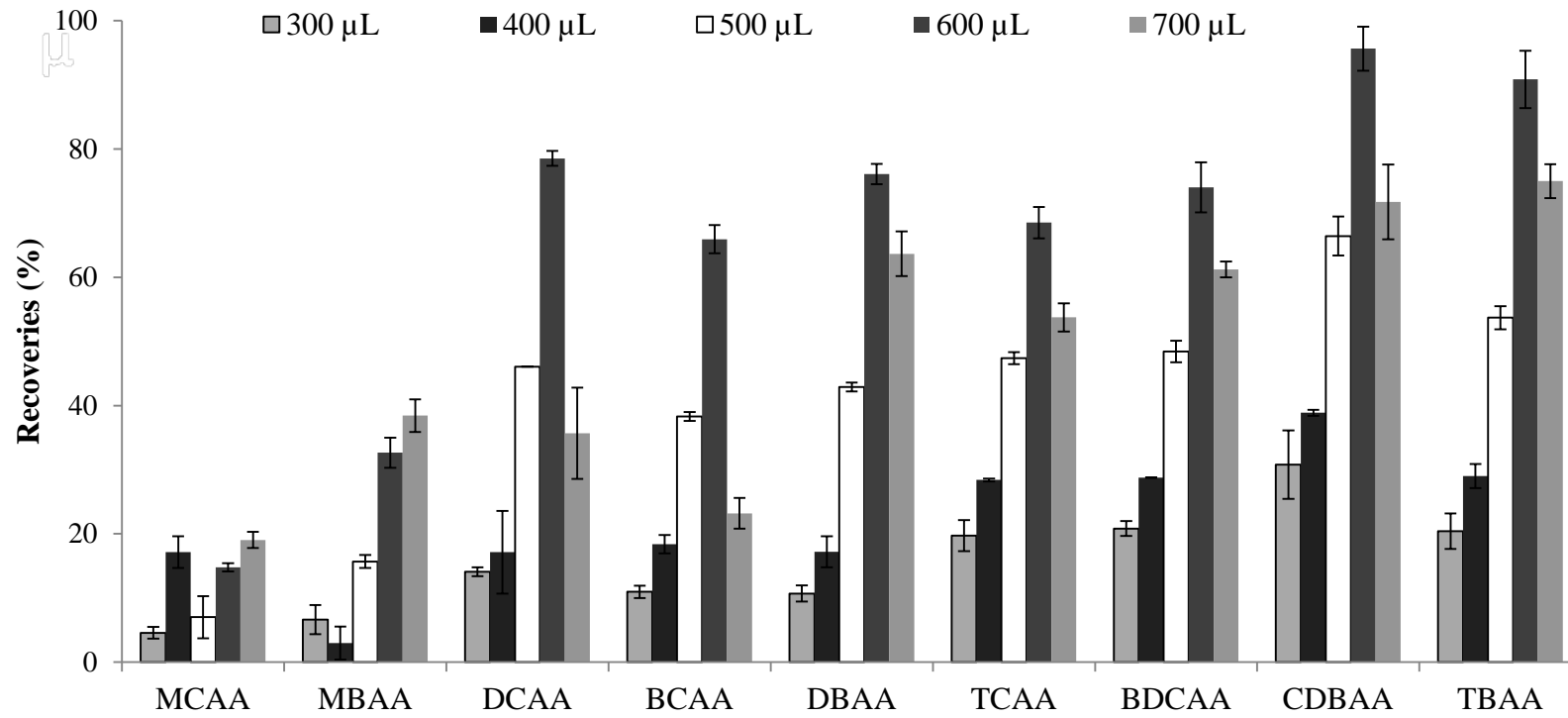


Figure 3

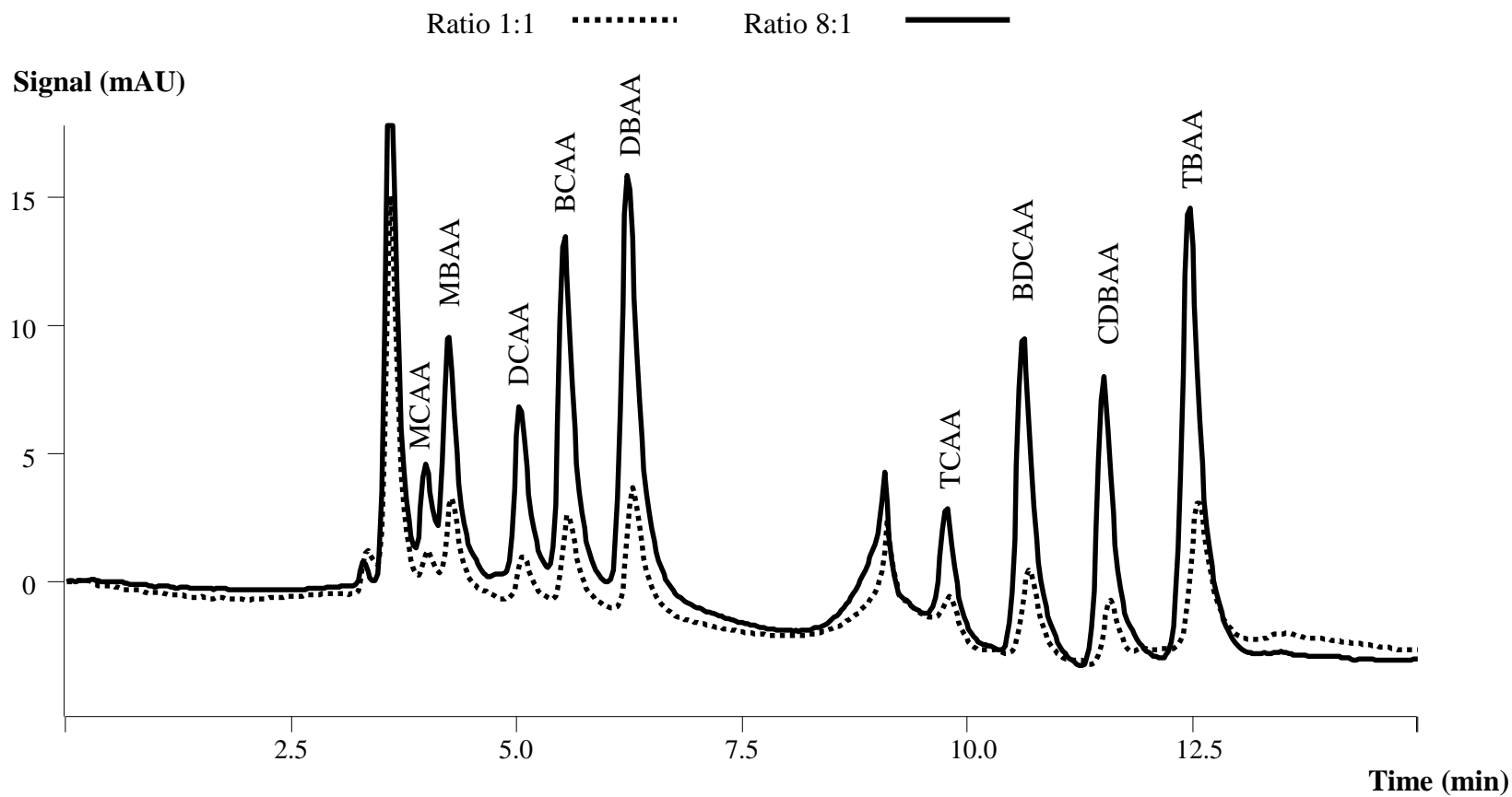


Figure 4