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1	Fast preparation of a hydrophobic monolith by redox initiation and
2	its application in the separation of small molecules
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6	Abstract: A novel skeleton hydrophobic polymeric monolith was prepared by redox
7	initiation in this paper. At ambient temperature, benzoyl peroxide (BPO) and N,
8	N-dimethyl aniline (DMA) were used as initiators; 1-Dodecene (C12) as the monomer
9	and ethyleneglycol dimethacrylate as the crosslinking agent. The polymerization
10	conditions were optimized in order to use for chromatographic separations. The
11	characters of the monolith were investigated by scanning electron microscopy (SEM),
12	fourier transform infrared spectroscopy, mercury porosimeter and nitrogen
13	adsorption-desorption mercury porosimetry. Moreover, the prepared monolith was
14	used as the stationary phase of high performance liquid chromatography to separate
15	the mixture of benzenes in hydrophobic chromatography mode. Baseline separations
16	and high column efficiencies in excess of 11,000 theoretical plates per meter were

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17 obtained.

18 Keywords: Hydrophobic monolith; Redox initiation (BPO/DMA); 1-Dodecene (C12);

19 Skeleton structure; High performance liquid chromatography

20 1. Introduction:

In recent years, monolithic stationary phase, has attracted increasing attention 21 22 because of its excellent mass transfer properties and versatile surface modification 23 compared to conventional columns packed with particles [1-2]. Basically, monolithic 24 column are divided into two groups: rigid organic polymer-based monoliths and 25 silica-based monoliths. The two kinds of monoliths have been used in high 26 performance liquid chromatography (HPLC) [3-4], solid phase extraction (SPE) [5-6], and capillary electrophoresis (CE) [7-8]. The drawback of the silica-based monolith is 27 that it is subject to an insufficient hydrolytic of the Si - O - C linkage, especially 28 29 under moderately acidic or slightly alkaline conditions. Moreover, preparation of 30 silica-based monolithic columns is not only time-consuming but also difficult to 31 control the entire process, which leads to the problems with reproducibility. As an 32 alternate, the organic polymeric monolith shows stability within the entire range of pH 33 and exhibited excellent biocompatibility. However, it suffers from shrinking or 34 swelling under the influence of temperature or organic solvents. Besides, it is difficult 35 to prepare polymeric monoliths possessing both large through pores and multiple small pores in one step [9-12]. An alternative approach is carried out in this paper. 36

37 Hydrophobic polymeric monolithic column is an important liquid chromatography38 solid phase for analyzing small molecules. There are many approaches to prepare

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39 hydrophobic columns such as single electron transfer-living radical polymerization 40 (SET-LRP) and atom transfer radical polymerization (ATRP) [13-14]. In situ radical 41 polymerization has the disadvantages of slow initiation, fast increase, easy chain 42 transfer and quick chain termination which lead a non-uniform structure [15-17], and 43 resulting in low column efficiency, low permeability and low resolution.

44 The redox initiator which can reduce the activation energy of organic peroxides 45 decomposition, is mostly used in the resin curing process. The reaction can fast occur 46 under contact pressure and ambient temperature condition [18]. The system generally 47 consists of peroxide in combination with reducing agent. The usually used reducing agents are N, N-dimethyl toluidine, N, N-dimethyl aniline (DMA) [19-21] and 48 N-phenyl diethanol amine (PDEA). The benzovl peroxide (BPO) can initiate the 49 50 polymerization of vinyl monomers at ambient temperature [22]. The complex decomposes and gives free radicals or cation radicals which can then initiate radical 51 polymerization. This curing process is mostly used in the preparation of unsaturated 52 polyester resin, in which the linear polyester molecules are crosslinked into 53 54 three-dimensional network structure. This approach has several advantages: 55 effective control of the reaction rate, complete curing reaction, and good mechanical 56 stability of the products. Besides, a proper accelerator can meet various process 57 requirements. Compared to the reported references, the advantages of this method are that not time-consumed preparation and process occurring at room temperature. 58

In this work, a hydrophobic monolith was prepared by one-step redox initiation
process. Moreover, the prepared monolith was used as HPLC hydrophobic stationary

61 phase to separate benzenes small molecules successfully.

62 2. Experimental:

63 **2.1Materials and instrumenttation**

1-Dodecene (C12) was purchased from Aladdin Co. Ltd. (Shanghai, China). 64 Ethyleneglycol dimethacrylate (EDMA) was produced by New Jersey (USA). Cetyl 65 alcohol, benzoyl peroxide (BPO), N, N-Dimethylaniline (DMA) and phenol, 66 67 1-naphthol, biphenyl, anthracene, triphenylamine, benzotriazole, 1-naphthylamine, 2,4-dinitrophénylhydrazine, for separated were obtained from Kermel Co. Ltd. 68 (Tianjin, China). Potassium bromide (KBr) was bought from Skylight Optical 69 70 Instrument Co. Ltd. (Tianjin, China). All of these chemicals and samples were 71 analytical reagent grade. Tripled distilled water was used for all experiments.

An Agilent Technologies (Agilent, USA) with a 1100 system which was consist of 72 a quaternary pump with an online vacuum degasser, an autosampler with variable 73 injection capacity ranged from 0.1 to 100 μ L, and a UV detector; Agilent liquid 74 chromatography system chemical software was used and operated under Windows XP 75 76 for data acquisition and integration. Microscopic analysis was carried out using a 77 Hitachi (Hitachi High Technologies, Tokyo, Japan) S-4300 SEM instrument. The 78 FT-IR spectra were recorded on an FTIR-8400S IR apparatus in the region of 400-4000 cm⁻¹ (SHIMADZU, Kyoto, Japan). Pore size distribution was achieved by 79 mercury intrusion porosimetry (AutoPore II 9220 V 3.04, Micromeritics Instrument 80 81 Co., Atlanta, GA). Nitrogen adsorption-desorption isotherms were measured using specific surface area analyzer (BUILDER, Beijing, China) SSA-4300 instrument. 82

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83 **2.2 Preparation of the monolith**

The monolithic column was prepared with the optimized condition by redox 84 initiator in stainless-steel tubes (50 mm \times 4.6 mm i.d.). Functional monomer C12 (0.60 85 mL) and cross linking agent EDMA (0.80 mL) and initiator DMA (0.03 mL) BPO 86 (3.0 mg) were dissolved in 0.2 g melted cetyl alcohol. The mixture was surged 87 88 ultrasonically and then poured into the stainless steel tube, which was sealed at both 89 ends with close column heads. The mixture was bubbled with nitrogen for 5 min to 90 remove gases. Then the polymerization was allowed to proceed at ambient 91 temperature for less than 10 min. The monolith with the steel-tube was connected to 92 the HPLC system and was washed by methanol online for 2h at a flow rate of 1.0 mL min⁻¹ to remove all of cetvl alcohol and other soluble compounds present from the 93 94 polymer rod. The polymerization scheme was given in Fig. 1.

95 **2.3 Characterization of the monolithic column**

96 The monoliths in the columns were pumped out and cut into small pieces followed by drying under vacuum at 60 $^{\circ}$ C overnight. Chemical groups of the monolith were 97 98 detected by infrared spectra method, 1-2 mg of the dried monolith and 200 mg of 99 dried KBr were mixed and grinded to less than 2 µm i.d., and then the powder was 100 pressed into transparent sheet by the hydraulic press. Microstructures of the dried 101 monolith samples were observed by scanning electron microscopy (SEM), the pieces 102 of monoliths were snapped apart and placed on sticky copper foils, which were 103 attached to a standard aluminum specimen stub. Then the attached monoliths were 104 coated with about 20 nm of gold by an Eiko IB-3 sputter coating instrument (Eiko,

105	Tokyo, Japan). The pore size distribution was determined by mercury intrusion					
106	porosimetry and nitrogen adsorption-desorption isotherm.					
107	The permeability of monoliths was assessed by the pressure drop of the monolithic					
108	column at different flow rates by using water and methanol as mobile phase,					
109	respectively. The values of the system pressure were measured at each flow rate					
110	without or with the monolith being connected, and the difference between the two					
111	values was calculated as the pressure drop across the monolith. According to the					
112	Darcy's law permeability of the monolith was calculated [23].					
113	2.4 HPLC measurements					
114	2.4.1 Selection of the mobile phase					
115	In order to select a suitable mobile phase for the separation of the analytes, isocratic					
116	elution with methanol and water being used as mobile phase was tested.					
117	2.4.2 Chromatographic separation of small molecules					
118	Chromatographic separation of small molecules was obtained by a monolithic					
119	column (50 mm \times 4.6 mm i.d.). The flow rate was 1.0 mL min ⁻¹ , UV wavelength was					
120	set at 254 nm and the temperature was 25 $^{\circ}$ C. The injection volume of the sample was					
121	1.0 μ L. All sample solutions injected in the chromatographic system were filtered					
122	through a millipore membrane (0.22 $\mu m)$ to remove particles and large aggregates.					
123	Methanol/water (75/25, v/v) was used as mobile phase.					
124	3. Results and discussions					
125	3.1 Optimization of polymeric conditions					
126	In order to obtain materials with porous and uniform structure, the conditions of the					

6

polymerization were optimized. Different compositions of polymerization mixtures
were tested. The resulting polymers were qualitatively evaluated for consistency,
rigidity and optical aspects. The results were summarized in Table 1.

130 Monomer and cross linking agent both play important roles in the preparation of the 131 monolith. They have significant effects on not only the rigidity and porosity, but also the selectivity and column efficiency of the monolith. Three monolithic columns 132 133 (column A - C in Table.1) were prepared with different volume of C12 to investigate 134 the influence of C12 amount. Column B, D and E in Table.1 were prepared to 135 investigate the effects of EDMA on the monolith. According to the preliminary 136 experiments listed in Table.1, when the rate of monomer and cross linking agent was 0.6/0.8 (v/v), material with good mechanical property was obtained. SEM was used to 137 138 investigate the morphology of the monoliths.

139 **3.2 Effect of the porogen on the structure**

140 The choice of pore-forming solvent or porogen is a tool that may be used for the control of porous properties without changing the chemical composition of the final 141 142 polymer. Fig. 2 showed the effects of the content of cetyl alcohol in the 143 polymerization mixture on pore size distribution. In general, larger pores would be 144 obtained by using more macroporogen because of the earlier onset of phase separation. 145 According to the visualized results, the monolithic column using 0.2 g cetyl alcohol as 146 porogen had well-distributed pore size and submicron skeleton structure which led to 147 high permeability and high efficiency. Based on these results the composition of the 148 polymerization mixture chosen for further experiments was 0.60 mL of C12, 0.80 mL

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149 of EDMA, and 0.2 g of cetyl alcohol.

The choice of porogens for the preparation of porous polymer monoliths remains an 150 151 art rather than science. For example, Santora et al. carried out experiments with single 152 solvent porogens including tetrahydrofuran, acetonitrile, toluene, chlorobenzene, hexane, methanol, dimethylformamide, and methyl-t-butyl ether, and prepared series 153 154 poly(divinylbenzene), poly(styrene-co-divinylbenzene), of poly(ethylene 155 dimethacrylate), and poly(methyl methacrylate-co-ethylene dimethacrylate) monoliths 156 [24]. Although some of these solvents afforded polymers with a surface area as 820 $m^2 g^{-1}$, it is unlikely that they would be permeable to flow since the pores were rather 157 158 small [25]. This is why not many porogens have been used and most often proven 159 porogen mixtures are applied. It is generally accepted that good solvents serve as 160 microporogens to provide high surface areas, while poor solvents act like 161 macroporogens to provide good bulk flow properties. For C12-based monoliths, cetyl 162 alcohol is a common solvent, which offered good solubility for C12 and EDTA.

163 Nitrogen adsorption is extensively used for determination of porous properties of 164 monoliths in their dry state. It allows a useful estimate of expected total surface areas 165 of porous polymeric materials and the existence of a permanent mesoporous pore 166 space at least qualitatively [26]. We had been ascertained that monolithic column with no porogen having a surface area of 1.8 m² g⁻¹ were not suitable for the efficient 167 168 separation of small molecules .When 0.2 g cetyl alcohol was used as porogen the surface area increased to 279 m² g⁻¹. Additionally, the nitrogen adsorption-desorption 169 170 isotherm exhibited typical type-IV hysteresis, indicative of the presence of mesopores

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Fig. 3.

In order to characterize the mechanical performance and permeability of the

174 monoliths, the back pressures of the monolith at different flow rates were studied. Fig. 175 4 showed an excellent linear and the regression factors were 0.9997 and 0.9998, that 176 used methanol and water as mobile phase respectively, which indicated that the 177 internal structures of the monoliths were not damaged in the range of back pressure 178 from 13 to 90 bar. This superior flow-through property could be attributed to high cross-linking homogeneity and large pore size. Moreover, the efficiency of 179 180 chromatographic separation was not affected after subjecting the high flow rates. 181 Besides, in order to evaluate its mass transfer property, the permeability behavior, 182 which is one of the most practical factors in designing a novel type of monolithic 183 column, was investigated. Column permeability (k) reflects through-pore size and 184 external porosity, or a domain size at a constant through-pore size/skeleton size ratio. 185 According to Darcy's law, the equation is as follow:

186
$$Q = \frac{-kA}{\mu} \cdot \frac{P_b - P_a}{L}$$

3.3 Mechanical strength and permeability

Wherein, the total discharge, Q (units of volume per time, e.g., $m^3 s^{-1}$) is equal to the 187 product of the permeability of the medium, $k (m^2)$, the cross-sectional area to flow, A 188 (units of area, e.g., m^2), and the pressure drop, all divided by the viscosity, μ (Pa·s) 189 190 and the length over which the pressure drop is taking place [27]. The negative sign is 191 needed because fluid flows from high pressure to low pressure. The good permeability value of 8.97×10^{-14} m² was calculated based on the Darcy's law at ambient 192

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temperature which supported the internal morphology information of Fig. 2(c). So the skeleton structure not only had good permeability and fast mass transfer, but also had higher surface which could benefit the chromatographic separation. And skeleton structure had higher column efficiency and resolution than accumulated structure. These results indicated that skeleton structure provided larger surface area and excellent permeability.

199 **3.4 FT-IR spectra of the monolith**

The FT-IR spectra of the monolith were shown in Fig. 5, in which, typical and expected bands were found. The peak at 3000 cm⁻¹ was due to the stretching in C-H of aliphatic or alkenes. The clear absorption peaks at 1510 cm⁻¹ and 1100 cm⁻¹ were caused by the C-O-C group; The spectrum at 1725 cm⁻¹ showed the presence of the -C=O of esters.

3.5 Pore size distribution of the monolith

The measurement of pore size distribution for the monoliths was carried out by mercury intrusion porosimetry. Pore size distribution determines the fraction of the total pore volume accessible to molecules of a given size and shape, which is a very important property of the monolith. The obtained result is depicted in Fig.6. Based on Fig.6, the total intrusion volume, median pore diameter and the porosity were 2.37 mL g^{-1} , 3.5µm and 70.5%, respectively.

212 **3.6 Chromatographic separation of small molecules**

The poly (C12-co-EDMA) monolith was used as the stationary phase of HPLC to separate small molecules. Fig.7(a, b) showed the chromatograms, and in which two

215 groups of small molecular compounds distinct peaks could be observed. The retention 216 factors (k) of each sample of the first group small molecules on the poly 217 (C12-co-EDMA) monoliths were determined at various concentration of methanol in 218 the mobile phase and the results were shown in Fig.8. The elution capacity is 219 gradually increased with the increase of the amount of methanol, but the column 220 efficiency is not changed significantly which obtained from the calculation of 221 theoretical plate number. This indicates that the hydrophobic interaction between the 222 solutes and the stationary phase plays a dominating role in retaining the solutes on the 223 monoliths. The separations of basic compounds were always suffered from peak 224 tailing in previous reports due to non-specific adsorption on the stationary phases. 225 However, this phenomenon was not observed on the hydrophobic organic monolithic 226 column.

Meanwhile, some chromatographic parameters such as retention time and resolution, symmetry factor and theoretical plate number of each sample were calculated and the results were shown in Table 2, in which the theoretical plate number of biphenyl could be up to 10⁴. It could be seen that the poly (C12-co-EDMA) monoliths are excellent stationary phase for separation of these analytes. Furthermore these results strongly suggested further potential of this novel monolith for an efficient downstream processing of benzenes small molecules.

234 **3.7 Advantages compared with other hydrophobic monoliths**

Organic polymeric monoliths, generally, are widely used as stationary phases for
bio-molecule separation because efficient separation of small molecules is not easily

realized in the normal columns (4.6 mm i.d.). However, achieving good column efficiency for small molecules has been easy to obtain for capillary liquid chromatography (cLC) and capillary electrochromatography (CEC). But compared with the normal column in HPLC, both cLC and CEC methods can't achieve high throughput separation.

242 A series of hydrophobic interaction monolithic columns have also been prepared in 243 a similar manner such as single electron transfer-living radical polymerization 244 (SET-LRP) and atom transfer radical polymerization (ATRP). Nevertheless, the 245 preparation processes of these monoliths are rather tedious and time-consuming. We 246 have used a simple one-set approach for preparing the organic polymeric monolith, 247 which represented a new way to prepare the organic polymeric monoliths with variety 248 of organic monomers. In this article the polymerization was allowed to proceed at 249 ambient temperature for less than 10 min. With the excellent hydrophobic of C12, column efficiencies in excess of 11,000 theoretical plates per meter were obtained. 250 251 However, much less work has been performed with C12 as monomer in the field of 252 monolith.

3.8 The effects of eluent linear flow velocity on the separation

The plate height (H) of the first group small molecular on the poly (C12-co-EDMA) monoliths were determined at various linear flow rate [28]. Fig. 9 shows that the van Deemter plot demonstrating effect of velocity on efficiency of monolithic column for small molecular. Fig.8 and Fig.9 were the average of seven cycle measurement results derived from succedent section 3.8 where the experimental results demonstrate a good

repeatability process. Separately, benzene was employed as the mobile phase velocity
marker in this experiment according to the cited reference [29].

261 **3.9 Repeatability and stability**

262 A good column-to-column repeatability and monolith stability are important 263 measure of the process. An excellent repeatability characterized by relative standard 264 deviations (RSDs) for the retention times in the range of 1.3-2.6% was achieved on 265 poly (C12-co-EDMA) monoliths using the same process and conditions (n=7). 266 Furthermore, the chromatograms on the poly (C12-co-EDMA) monoliths were 267 obtained after numerous equilibrations and separation runs involving the small 268 molecular mixture. The results demonstrated that the preparation process had a good 269 repeatability and the monoliths were stable.

4. Conclusion

271 In order to obtain a hydrophobic monolithic column with uniform structure by a 272 simple approach, one-step redox initiation is used in the preparation of monolith in 273 this study. A monolithic structure with hydrophobic surface properties was obtained in 274 this study without post surface modification. The monolith had high performance in 275 the hydrophobic separation of benzenes small molecules which was high to 11,000 276 plates per meter (diphenyl). The results suggested that it's a simple, cheap and 277 effective method to prepare hydrophobic monolith. Hence the novel method presents a promising alternative to commercially available monolithic supports. 278

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Caption for figures and tables

Fig. 1. Synthesis scheme of the poly (C12-co-EDMA) monolithic column.

Fig. 2. Effects of varying porogen on the morphology of poly (C12-co-EDMA)

monolithic columns: (a) no porogen, (b) 0.1 g cetyl alcohol, (c) 0.2 g cetyl alcohol, (d)

0.3 g cetyl alcohol.

Fig.3. Nitrogen adsorption-desorption isotherm.

Fig. 4. Back pressures of the poly (C12-co-EDMA) monoliths at different linear flow rates. Mobile phase: 1 water, 2 methanol.

Fig. 5. The FT-IR spectrum of the poly (C12-co-EDMA) monolith.

Fig.6. The measurement of pore size distribution for the poly (C12-co-EDMA)

monolith. Pore size distribution profile measured by mercury intrusion porosimetry.

Fig. 7. Elution profiles of small molecules on the poly (C12-co-EDMA) monoliths.

HPLC conditions: the prepared hydrophobic monolith, 50 mm× 4.6 mm i.d.; flow rate

1.0 mL min⁻¹, UV detection at 254 nm .Samples a: the analytes are 1: phenol, 2:

1-naphthol, 3: biphenyl, 4: anthracene, 5: triphenylamine; Samples b: the analytes are

1: benzotriazole, 2:1-naphthylamine, 3: 2,4-dinitrophénylhydrazine, 4: biphenyl;

Mobile phase: methanol/water (75/25, v/v), b methanol/water (65/35, v/v).

Fig.8. Relationship between *k* and methanol concentration on the poly (C12-co-EDMA) monolith. The retention factors (*k*) was defined as $(t_r-t_0)/t_0$, where t_r and t_0 represent the retention times of an analytes and an unretained compound, respectively.

Fig.9. Plate height curves obtained from separations on a monolithic poly

(C12-co-EDMA) column (1 phenol, 2 1-naphthol, 3 biphenyl, 4 anthracene, 5 triphenylamine). Mobile phase: 75% (v/v) methanol in water. In general the plate heights were fitted to the van Deemter equation $H = A + B/\mu + C\mu$.

Table 1. Qualitative comparison of polymer compositions.

Table 2. Chromatographic parameters of separation of the small molecules.

C12	EDMA	Cetyl	Permeability	Plate	Resolution	Symmetry	Optical	Mechanical/
(mL)	(mL)	alcohol	$(\times 10^{-14} \mathrm{m}^2)$	numbers		factor	properties	physical
		(g)		(plates m ⁻¹)				properties
A 0.3	0.8	0.2					White	Soft,
								granulous
B 0.6	0.8	0.2	≤8.97	≤11884	≪4.61	≤0.90	White	Quite, hard
C 1.0	0.8	0.2	≤0.81	≤1385	≤1.07	≤0.52	White	Hard, brittle
D 0.6	0.5	0.2					White	Soft, fluffy
E 0.6	1.0	0.2	≤1.78	≤1874	≤1.43	≤0.61	White	Hard
F 0.3	0.5	0.2					Translucid	Gel like

	Retention time	Resolution	Symmetry	Plate numbers
	(min)		factor	(plates m^{-1})
Phenol	1.170	2.84	0.62	9540
1-Naphthol	2.032	3.37	0.70	8626
Biphenyl	3.735	2.69	0.78	11686
Anthracene	6.058	1.54	0.73	9632
Triphenylamine	8.442		0.62	5830

	Retention time (min)	Resolution	Symmetry factor	Plate number (plates m ⁻¹)
Benzotriazole	1.394	4.61	0.67	8943
1-Naphthylamine	3.676	3.19	0.79	8222
2,4-Dinitrophényl hydrazine	6.921	1.92	0.82	8707
Biphenyl	9.742		0.90	11884

One equation has been used to calculate the plate number:

$$N = \frac{5.55(T_r / W_{0.5})^2}{L}$$

N is the theoretical plate number per m and Tr is the retention time of the analyte in

min and $W_{0.5}$ is the peak width at half height in min and L is the length of the column.



80x45mm (300 x 300 DPI)



80x65mm (300 x 300 DPI)



80x63mm (300 x 300 DPI)



80x63mm (300 x 300 DPI)



80x51mm (300 x 300 DPI)



80x60mm (300 x 300 DPI)



80x60mm (300 x 300 DPI)



80x60mm (300 x 300 DPI)



80x62mm (300 x 300 DPI)



80x63mm (300 x 300 DPI)