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# Phthalide-containing poly(ether-imide)s based thermal rearrangement membranes for gas separation application

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The diamine monomer 3,3-bis[4-(3-hydroxy-4-amino-phenoxy)phenyl]phthalide (BHAPPP) was firstly synthesized by the nucleophilic substitution of 5-fluoro-2-nitrophenol and phenolphthalein, followed by a reduction reaction. A series of phthalide-containing poly(ether imide)s (PEI) were then prepared through the polycondensation of BHAPPP with six kinds of dianhydrides, including 4,4'-(hexafluoroisopropylidene)diphthalic anhydride (6FDA), 3,3',4,4'-benzophenone tetracarboxylic dianhydride (BTDA), 3,3',4,4'-biphenyl tetracarboxylic dianhydride (BPDA), 4,4'-oxydiphthalic dianhydride (ODPA), 1,2,3,4-cyclobutane tetracarboxylic dianhydride (CBDA) and pyromellitic dianhydride (PMDA), as well as thermal imidization. After further thermal treatment, the corresponding thermal rearrangement (TR) membranes were obtained. Due to the existence of the phthalide lactone ring, the PEIs probably underwent TR and crosslinking simultaneously. With the increase of thermal treatment temperature, the mechanical properties of the TR membranes dramatically decreased, but the gas separation properties obviously increased. When the PEIs were treated at 450 °C for 1 h, the CO<sub>2</sub>, H<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub> and CH<sub>4</sub> permeability of TR(BHAPPP-6FDA) reached 258.5, 190.5, 38.35, 4.25 and 2.15 Barrers, respectively. Meanwhile, the CO<sub>2</sub>/CH<sub>4</sub> selectivity of 120.2 sharply exceeded the 2008 Robeson limit, and O<sub>2</sub>/N<sub>2</sub> selectivity was 9.02, close to the 2015 upper limit. Therefore, the TR membranes derived from phthalide-containing PEIs exhibit superior gas separation performance, and are expected to be applied in the field of gas separation.

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## 1. Introduction

Gas membrane separation technology is a kind of new and efficient separation technology, which has attracted wide attention because of the advantages of being environment friendly, and having a low energy consumption and easy operation.<sup>1,2</sup> The separation membrane is the key material of this technology, mainly involving polymeric membrane and carbon membrane. Up to now, polymeric membrane has been mainly applied as a commercial separation membrane material, like silicon rubber, polyimide (PI) and polysulfone.<sup>3–7</sup> Moreover, polymer membrane exhibits a “trade-off” relationship between gas permeability and selectivity, which greatly limits its practical application.<sup>8–11</sup> Among polymer materials, PI is favored by engineers and researchers due to its excellent thermal stability, mechanical properties and chemical solvent resistance.<sup>12–14</sup> However, the low gas permeability of dense PI membrane commonly leads to a decrease of separation efficiency.

It is well known that gas permeability of polymer membranes is closely related to the free volume, which provides narrow tunnels for the transport of gas molecules. In order to increase the free volume of PI, some feasible methods have been proposed, including the introduction of bulky Cardo structure, triptycene group, large volume substituent and contorted linkage.<sup>15–20</sup> For instance, the introduction of bulky Cardo group can increase the interchain distance, reduce the interaction between molecular chains, and form more free volume, which is conducive to the transportation of gas molecules. Meanwhile, rigid macromolecular chains are always preferred for gas separation membranes to maintain high gas selectivity. As a result, the gas separation properties of PI membrane materials have been dramatically improved by these efforts.<sup>21–28</sup>

In recent years, thermal rearrangement (TR) polymers have been developed and investigated by researchers in the field of membrane separation.<sup>29–34</sup> Due to the transition from imide ring to benzoxazole structure, hydroxyl-containing polyimide (HPI) is transformed into polybenzoxazole (PBO), and a large amount of small molecule gas CO<sub>2</sub> is released.<sup>35–41</sup> TR polymers exhibit excellent gas permeability and moderate selectivity because of unique “hourglass” micropore structure, which have become a new generation of gas separation membrane

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materials.<sup>42</sup> The gas separation process of TR polymer is mainly followed by the solution-diffusion mechanism, accompanied by the sieving mechanism due to the existence of pore structures. According to the literatures,<sup>29–44</sup> the rearrangement reaction and gas separation performance of TR polymers are mostly affected by many factors, such as chemical structure, glass transition temperature ( $T_g$ ), thermal treatment atmosphere, time and temperature. For example, the HPI containing flexible linkage is easy to rearrange at a relatively low temperature because of better motion ability of chain segment, but the increase of gas permeability is not very significant. On the contrary, the HPI with rigid backbone needs higher rearrangement temperature to conduct the structural transformation, resulting in high gas permeability.

It is well known that the crosslinking could limit the movement of macromolecular chains and even release small molecule gas  $\text{CO}_2$ , which is helpful to improve the gas permeability, selectivity and plasticizing resistance of membrane materials.<sup>45–51</sup> For polyimide, 3,5-diaminobenzoic acid is a common crosslinking monomer to form crosslinking structure after decarboxylation reaction.<sup>52</sup> Besides, it is recently reported that the gas separation performance of polymer membranes has been improved by the crosslinking of phthalide ring.<sup>47–50</sup> For instance, our cooperative research group found that the poly aryl ether ketone (PEK-C) membrane with phthalide groups was thermally crosslinked by the decomposition of the lactone rings and further decarboxylation in  $\text{N}_2$  atmosphere.<sup>47</sup> The gas separation and anti-plasticization properties of PEK-C membrane were significantly enhanced due to the enlargement of the interchain distance and formation of free volume cavity. Especially, the permeability of  $\text{CO}_2$  was 110 times higher than that of the original PEK-C membrane. Moreover, Caili Zhang *et al.* reported that the thermal oxidation crosslinking in air for PI membranes containing phthalide groups took place at a relatively lower temperature than the carboxylic acid containing polyimides, which greatly enhanced the gas separation properties.<sup>48</sup> Thereby, phthalide group, as a kind of Cardo structure, has large steric hindrance and asymmetric structure, which is beneficial to decrease the packing density and enhance the free volume of polymers. In addition, after certain heat treatment, phthalide lactone ring could be broken, followed by the formation of crosslinked structures.<sup>47–50</sup> Therefore, the phthalide-containing PIs are attracting the attention of researchers in the field of membrane materials.

In this work, the diamine monomer containing phthalide group and ether linkage, 3,3-bis[4-(3-hydroxy-4-amino-phenoxy)phenyl]phthalide (BHAPPP) was firstly synthesized by the nucleophilic substitution of 5-fluoro-2-nitrophenol and phenolphthalein, followed by reduction reaction. Then, a series of phthalide-containing poly(ether imide)s (PEI) were prepared through the solution-polymerization of BHAPPP with six kinds of dianhydrides, followed by thermal imidization. After further thermal treatment, the corresponding TR membranes were obtained, accompanied with crosslinking reaction. The effects of chemical structure of dianhydrides and thermal treatment temperature on the structures and properties of the final membrane materials were studied. Due to the introduction of

phthalide group, these TR membranes exhibited excellent gas permeabilities, coupled with proper selectivities, which are expected to be used in the field of gas separation.

## 2. Experimental

### 2.1 Materials

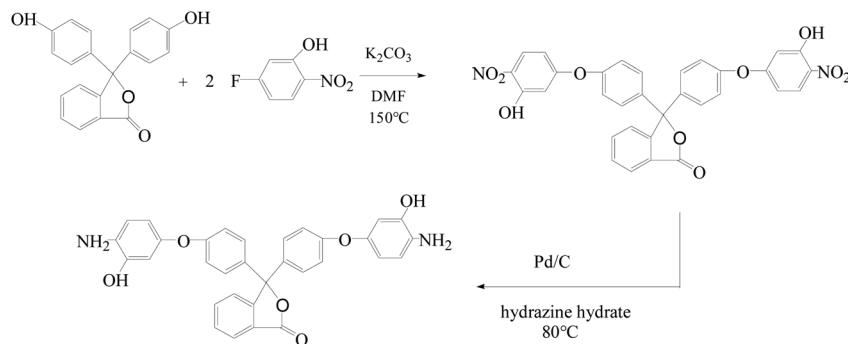
5-Fluoro-2-nitrophenol and phenolphthalein were purchased from Shanghai Haohong Biomedical Technology Co., Ltd. (China). Pyromellitic dianhydride (PMDA) was bought from Sinopharm Chemical Reagent Co., Ltd. (China). 1,2,3,4-Cyclobutane tetracarboxylic dianhydride (CBDA) was obtained from Liaoning Oxilan Huahui New Material Co., Ltd. (China). 4,4'-(Hexafluoroisopropylidene)diphthalic anhydride (6FDA), 3,3',4,4'-benzophenone tetracarboxylic dianhydride (BTDA), 3,3',4,4'-biphenyl tetracarboxylic dianhydride (BPDA) and 4,4'-oxydiphthalic dianhydride (ODPA) were purchased from Tianjin Chinattech Chemical Co., Ltd. (China). Pd/C (10% Pd), hydrazine hydrate, potassium carbonate ( $\text{K}_2\text{CO}_3$ ), ethanol, *N,N*-dimethylformamide (DMF) and *N,N*-dimethylacetamide (DMAc) were obtained from Sinopharm Chemical Reagent Co., Ltd. (China). The six anhydrides need to be fully dried at 180 °C for 24 h before use, and other chemicals were directly used.

### 2.2 Synthesis of diamine monomer

**(a) Synthesis of 3,3-bis[4-(3-hydroxy-4-nitrophenoxy)phenyl]phthalide (BHNPPP).** The preparation process is shown in Scheme 1. 5.000 g (15.7 mmol) of phenolphthalide, 4.936 g (31.4 mmol) of 5-fluoro-2-nitrophenol and 4.338 g (31.4 mmol) of  $\text{K}_2\text{CO}_3$  were added to a 100 mL two-neck round-bottom flask with 25 mL DMF. Under stirring, the mixture was heated to 150 °C for 12 h. After cooling to room temperature, some ice water was poured into the mixed solution to produce the yellow precipitates. The crude products were washed with deionized water for several times and dried in a vacuum oven at 80 °C for 24 h. The relative purity of dinitro compound BHNPPP was 98% (HPLC), and the yield was about 75%. Melting point: 320 °C (DSC).  $^1\text{H NMR}$  (500 MHz, DMSO)  $\delta$ : 11.14 (s, 2H), 7.99 (d, 1H), 7.98 (d,  $J = 2.9$  Hz, 1H), 7.92 (t,  $J = 7.2$  Hz, 1H), 7.73 (t,  $J = 7.5$  Hz, 1H), 7.46 (d,  $J = 8.8$  Hz, 4H), 7.24 (d,  $J = 8.8$  Hz, 4H), 6.61 (d,  $J = 2.6$  Hz, 2H), 6.58 (t,  $J = 1.9$  Hz, 4H). FTIR: 3280  $\text{cm}^{-1}$  (O–H stretching vibration), 1585–1324  $\text{cm}^{-1}$  (N–O symmetric stretching vibration) 1251–1218  $\text{cm}^{-1}$  (=C–O stretching vibration).<sup>32,35,48</sup>

**(b) Synthesis of 3,3-bis[4-(3-hydroxyl-4-aminophenoxy)phenyl]phthalide (BHAPPP).** 5.000 g (9.3 mmol) BHNPPP and 0.250 g (7.0 mmol) Pd/C were placed into a 100 mL two-neck round-bottom flask with 30 mL of ethanol as solvent. In the reflux state, 20 mL hydrazine hydrate was slowly added dropwise to the solution. After 12 h of continuous reaction, the Pd/C was removed by hot filtration, and the residual filtrate was poured into a large amount of deionized water. There were a lot of white products, which were filtrated, washed with deionized water and dried in a vacuum oven at 60 °C for 24 h. The relative purity of diamine BHAPPP was 98% (HPLC), and the productivity was about 75%. Melting point: 120 °C (DSC).  $^1\text{H NMR}$  (500





Scheme 1 Synthetic route of BHNPPP and BHAPPP.

MHz, DMSO)  $\delta$ : 9.25 (s, 2H), 7.93 (d,  $J = 7.6$  Hz, 1H), 7.87–7.82 (t, 2H), 7.67 (t,  $J = 5.5$  Hz, 1H), 7.23 (d,  $J = 8.9$  Hz, 4H), 6.87 (d,  $J = 8.9$  Hz, 4H), 6.58 (d,  $J = 8.4$  Hz, 2H), 6.38 (d,  $J = 2.6$  Hz, 2H), 6.30 (dd,  $J = 8.4, 2.6$  Hz, 2H), 4.45 (s, 4H). FTIR: 3378–3308  $cm^{-1}$  (N–H stretching vibration), 3171  $cm^{-1}$  (O–H stretching vibration), 1256–1219  $cm^{-1}$  (=C–O stretching vibration).<sup>32,35,48</sup>

### 2.3 Preparation of PEI and TR membranes

The PEI membranes were prepared according to the thermal imidization method (Scheme 2). First, the diamine BHAPPP (4.0 mmol, 2.218 g) and 22.63 mL DMAc were added to a 100 mL two-neck round-bottom flask equipped with a mechanical stirrer. After stirring for 30 min, the equimolar dianhydride 6FDA was introduced and stirred continuously for 12 h. Then, the polyamic acid (PAA) solution with a concentration of 15 wt% was synthesized, which was evenly coated on a clean glass substrate. After the step-by-step heating treatment, including  $50^\circ C$  for 2 h,  $80^\circ C$  for 1 h,  $150^\circ C$  for 1 h, and  $250^\circ C$  for 0.5 h, the PEI membrane was obtained and named as PEI(BHAPPP-6FDA). Next, the membrane was further thermally treated in a tube furnace at a heating rate of  $3^\circ C min^{-1}$  and a  $N_2$  flow rate of 200  $mL min^{-1}$ , and the final temperature was set at  $450^\circ C$  and kept for 1 h. The obtained membrane was called as TR(BHAPPP-6FDA). Finally, other PEI and TR membranes were also prepared according to this process.

### 2.4 Characterization

The chemical structures of the compounds and polymer membranes were identified by a Is10 Fourier transform infrared spectrometer (FT-IR) instrument (Nicolet, USA) in the range of 4000 to 500  $cm^{-1}$ . The chemical shifts of BHNPPP and BHAPPP were detected by an Agilent-500 Nuclear magnetic resonance (NMR) spectrometers with deuterated DMSO as the solvent (Agilent, USA). After platinum spraying treatment, the fracture surface morphology of TR membrane was observed by an Apreo 2S Field emission scanning electron microscope (FE-SEM) (Thermo Fisher Scientific, US). The specific surface area and pore size were determined by a nitrogen adsorption-desorption test on Quantachrome Autosorb IQ-XR analyzer (US) at 77 K. The microstructures of the polymers were confirmed by a D8 ADVANCE X-ray diffractometer (XRD) (Bruker, German) with

a scanning range  $2\theta = 10\text{--}70^\circ$ . According to Bragg equation ( $2d \sin \theta = n\lambda$ ,  $\lambda = 1.54 \text{ \AA}$ ), the  $d$ -spacing values of polymer membranes were calculated. The mechanical properties, including tensile strength, Young's modulus and broken elongation, were measured by a HY0350 Universal material tensile testing machine (Shanghai Hengyi Precision Instrument Co. Ltd., China) with 5 cm of tested gauge length and  $10 \text{ mm min}^{-1}$  of tensile rate. The melting point of compounds and glass transition temperature ( $T_g$ ) of polymers were measured by DSC 4000 Differential scanning calorimetry (DSC) analyzer (PerkinElmer, USA) and DMA 8000 Dynamic thermomechanical analyzer (DTMA) (PerkinElmer, USA) in nitrogen atmosphere from  $50$  to  $400^\circ C$  at a heating rate of  $20^\circ C min^{-1}$  and  $10^\circ C min^{-1}$ , respectively. The STA 449F3 Thermogravimetric mass spectrometry (TG-MS) (Netzsch, Germany) was employed to test the thermal properties of PEI samples from room temperature to  $900^\circ C$  at a heating rate of  $10^\circ C min^{-1}$  under  $50 \text{ mL min}^{-1}$  of  $N_2$  flow. The chemical elements on the surface of membrane sample were characterized by an ESCALAB250Xi X-ray photoelectron spectroscopy (XPS) instrument (Thermo Fisher Scientific, USA).

The gas permeabilities of the membranes were measured by a lab self-made permeation cell with constant-volume and variable-pressure method using high-purity gases at  $30^\circ C$  and 0.01 MPa (0.1 atm). The thicknesses of these membranes were about  $55 \pm 10 \mu m$ . Under the same test conditions, each membrane material was cut into  $1.5 \text{ cm} \times 1.5 \text{ cm}$ . More than 3 samples were tested to obtain the average value, and the measurement accuracy was about  $\pm 10\%$ . During the test, the membrane was unsupported. The gas permeability and selectivity were calculated according to the following formula:

$$P_i = \frac{F/S}{\Delta P/L} \quad (1)$$

$$\alpha_{A/B} = \frac{P_A}{P_B} \quad (2)$$

where  $P_i$  represents the permeability to  $i$  gas (Barrer, 1 Barrer =  $1 \times 10^{-10} \text{ cm}^3(\text{STP}) \text{ cm cm}^{-2} \text{ s}^{-1} \text{ cm Hg}^{-1}$ ),  $F$  means the gas volume flow rate,  $L$  is the thickness of the membranes,  $S$  represents the effective area of gas passing through the membranes and  $\Delta P$  is the pressure differential between the gas





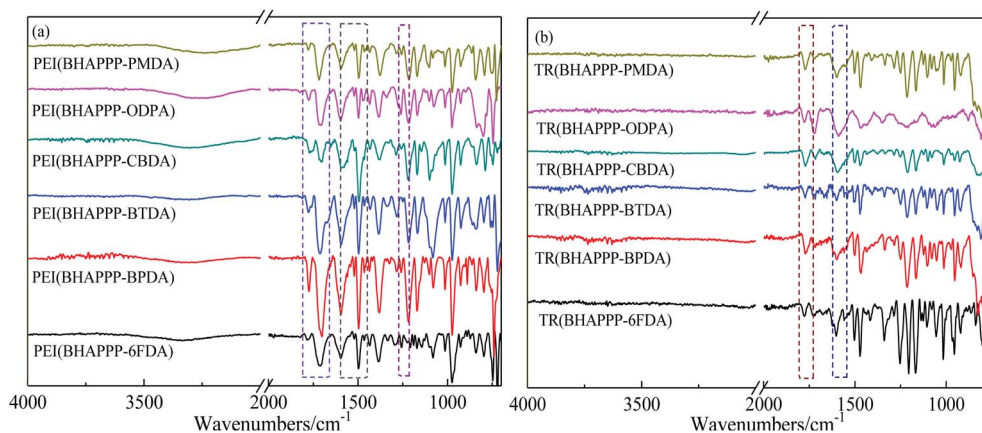


Fig. 1 FTIR spectra (a) PEI membranes, (b) TR membranes.

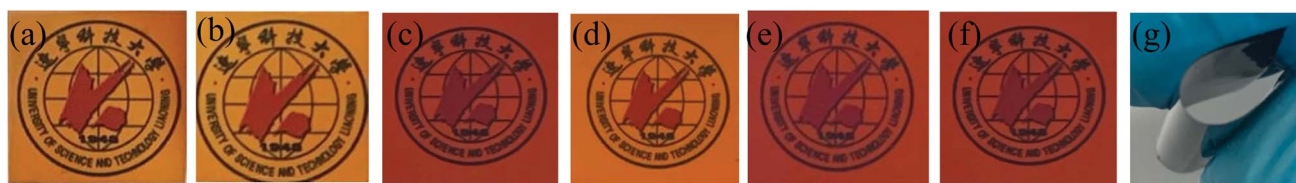


Fig. 2 Images of PEI and TR membranes (a) PEI(BHAPPP-6FDA), (b) PEI(BHAPPP-BPDA), (c) PEI(BHAPPP-PMDA), (d) PEI(BHAPPP-ODPA), (e) PEI(BHAPPP-BTDA), (f) PEI(BHAPPP-CBDA), (g) TR(BHAPPP-6FDA).

C=O and C-O, respectively. By calculating the peak area of  $-N\langle$  (400.2 eV) corresponding to imide ring and  $C=N-$  (399.1 eV) assigned to benzoxazole structure in Fig. 3(d), the conversion degree of thermal rearrangement could be roughly estimated to be 53.45%, indicating a partial conversion under the condition of 450 °C for 1 h.

### 3.2 Thermal properties of PEI and TR membranes

It was reported by Cailli Zhang *et al.* that the phthalide lactone ring of 6FDA-MPP synthesized by chemical imidization began to be decomposed and formed free radicals during the TGA test of 225–375 °C in  $N_2$ . However, Ruisong Xu *et al.* reported that the lactone rings in the phthalide Cardo moieties of PEK-C decomposed and released  $CO_2$  along with forming phenyl and methine free radicals during the thermal treatment of 400–500 °C in  $N_2$ . Finally, two adjacent phenyl radicals are most likely to combine to form a biphenyl crosslinking structure.<sup>47</sup> Furthermore, the thermal stability of aromatic polymers containing phthalide structures is generally excellent, with a high initial thermal decomposition temperature above 400 °C. We infer that the weight loss around 300 °C is more likely to be caused by incomplete imidization. Thus, the TGA-MS curves of PEI(BHAPPP-6FDA) tested in  $N_2$  and air were used to estimate the TR and crosslinking process, as shown in Fig. 4.

As can be seen from Fig. 4(a), there are three main weightlessness peaks under the condition of  $N_2$  and air. The first small weight loss around 300 °C is probably caused by the further imidization reaction. Because the PEI membranes were finally treated at 250 °C for 30 min, the residual PAA continued to be

closed ring during the test. The second peak around 400 °C is mainly attributed to the thermal rearrangement reaction, which may be accompanied by the decomposition of phthalide groups to form phenyl radical and methyl radical, leading to weight loss.<sup>48,51,55</sup> The HPI could undergo thermal rearrangement to form PBO, coupled with the release of  $CO_2$  gas. This result is consistent with some studies on thermally rearranged polymers.<sup>56–58</sup> Moreover, the phthalide lactone ring may be opened and remove  $CO_2$  to form a crosslinked structure.<sup>50,54</sup> The third peak of significant weightlessness about 520 °C is induced by the thermal decomposition of the main chain of polyimides.<sup>33,38</sup> In  $N_2$  and air atmospheres, the degree of thermal rearrangement and decomposition reactions is obviously different. It is clear that the thermal rearrangement reaction is easier to be carried out in nitrogen atmosphere. Besides, according to the  $MS = 44(CO_2)$  curves in Fig. 4(b), the  $CO_2$  is mainly released in the two temperature ranges, including around 400 °C assigned to the thermal rearrangement and possible decomposition of phthalide group as well as after 500 °C caused by the pyrolysis of polymer backbone. Considering the ability and type of TR and decomposition, the rearrangement reaction might be earlier than the thermal decomposition of phthalide structures. Hence, the thermal treatment temperature was set around the reaction temperature in  $N_2$ .

In order to further study the thermal properties of the PEI samples, DSC and DMA measurements were conducted, and the corresponding results were given in Fig. 5 and Table 1. Generally, the  $T_g$  values of these PEIs are from 322 to 352 °C by DSC and from 325 to 378 °C by DTMA, which are higher than those of



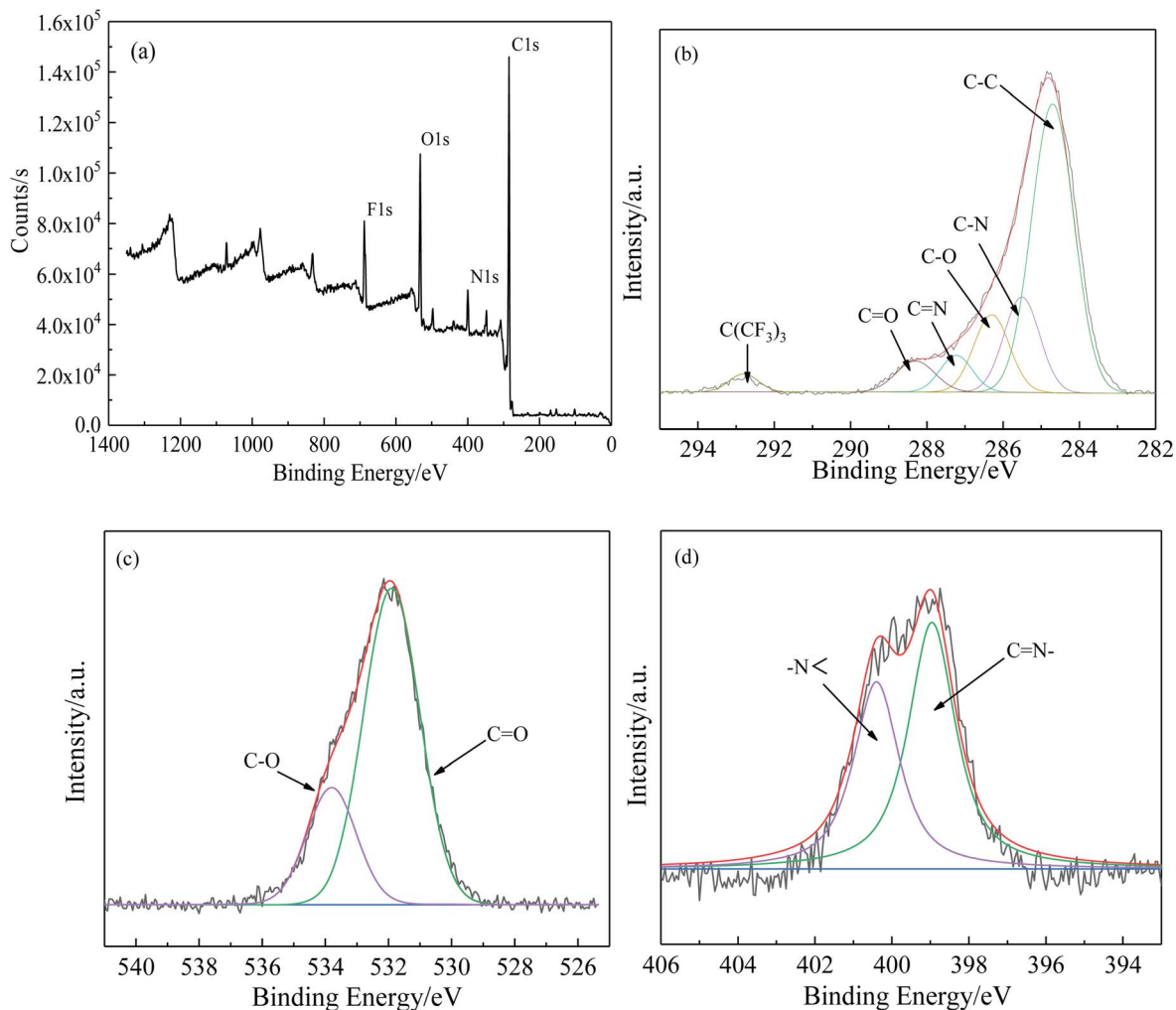


Fig. 3 XPS spectra of TR(BHAPPP-6FDA) (a) wide scan spectra, (b) fitting curves of C 1s, (c) fitting curves of O 1s, (d) fitting curves of N 1s.

the polyimide containing phthalide group without hydroxyl groups.<sup>48,50</sup> Due to the formation of hydrogen bond, the existence of hydroxyl groups could increase the interaction between the molecular chains and limit the movement of HPI segments, resulting in excellent thermal properties. As for the same

diamine BHAPPP, the chemical structure of dianhydride directly affects the properties of PEIs. Comparatively speaking, the PEI(BHAPPP-ODPA) shows a lower  $T_g$  because of the flexibility of ether linkage. Meanwhile, the PEIs derived from rigid dianhydrides, such as PEI(BHAPPP-PMDA) and PEI(BHAPPP-

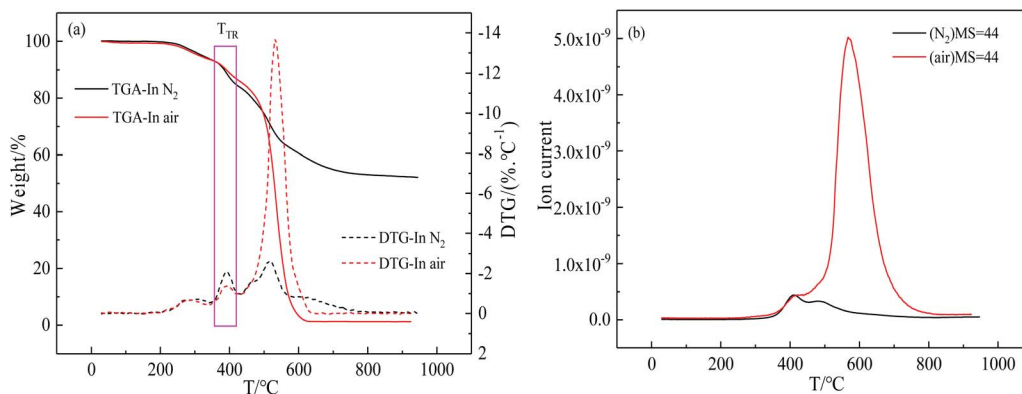


Fig. 4 TGA-MS curves of PEI(BHAPPP-6FDA) in N<sub>2</sub> and air (a) TGA curves, (b) MS = 44 curves.

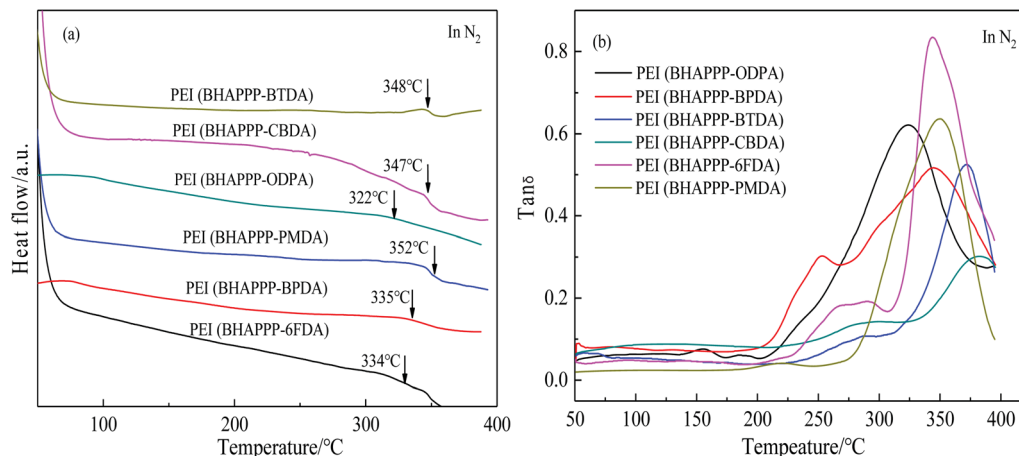


Fig. 5 (a) DSC curves of PEI membranes (b)  $\tan \delta$ - $T$  curves of PEI membranes.

Table 1 Thermal and mechanical properties of PEI membranes

Samples	$T_g$ ( $^{\circ}\text{C}$ )		Tensile strength (MPa)	Young's modulus (GPa)	Elongation at break (%)
	DTMA	DSC			
PEI(BHAPPP-BPDA)	344	335	$108.2 \pm 3.0$	$4.1 \pm 0.1$	$3.0 \pm 0.2$
PEI(BHAPPP-BTDA)	372	348	$122.9 \pm 2.0$	$3.7 \pm 0.2$	$4.4 \pm 0.1$
PEI(BHAPPP-CBDA)	378	347	$92.8 \pm 3.0$	$5.1 \pm 0.2$	$1.8 \pm 0.2$
PEI(BHAPPP-ODPA)	325	322	$88.7 \pm 2.0$	$4.4 \pm 0.2$	$2.0 \pm 0.2$
PEI(BHAPPP-PMDA)	350	352	$94.3 \pm 2.0$	$4.5 \pm 0.2$	$2.5 \pm 0.2$
PEI(BHAPPP-6FDA)	343	334	$85.4 \pm 2.0$	$3.3 \pm 0.2$	$2.6 \pm 0.1$
PEI(BHAPPP-6FDA)-375	—	—	$47.1 \pm 2.0$	$2.5 \pm 0.2$	$1.8 \pm 0.1$
PEI(BHAPPP-6FDA)-400	—	—	$33.6 \pm 2.0$	$2.1 \pm 0.1$	$1.5 \pm 0.2$
PEI(BHAPPP-6FDA)-425	—	—	$18.8 \pm 1.0$	$2.6 \pm 0.2$	$0.7 \pm 0.1$
PEI(BHAPPP-6FDA)-450	—	—	$14.2 \pm 1.0$	$2.2 \pm 0.1$	$0.5 \pm 0.1$
PEI(BHAPPP-6FDA)-475	—	—	$9.8 \pm 1.0$	$1.3 \pm 0.1$	$0.5 \pm 0.1$

CBDA), exhibit higher  $T_g$  values. Furthermore, the bulky phthalide group could increase the steric hindrance and hinder the movement of segments. Therefore, these phthalide-containing PEIs display excellent thermal properties.

### 3.3 Microstructure of PEI and TR membranes

The surface morphology of broken TR(BHAPPP-6FDA) membrane was observed by SEM, as shown in Fig. 6. It is clear that the surface is uniform and dense, without obvious defects. Furthermore, the curve of pore size distribution obtained from  $\text{N}_2$  adsorption-desorption measurement is given in Fig. 7. The pore width is chiefly centered at 2–7 nm, and the specific surface area is  $94.162 \text{ m}^2 \text{ g}^{-1}$ . The introduction of micro/meso pores is desirable in the transport of gas molecules. Thus, the TR(BHAPPP-6FDA) polymer exhibits porous microstructure, which is expected to be applied as the gas separation membranes.

In order to further clarify the microstructural change of the polymer membranes, XRD measurement was carried out. As we know, the gas separation mechanism of polymer membranes is reasonably explained by solution-diffusion process, in which

the free volume plays a very important role for gas transport.<sup>14–16</sup> Based on XRD results, the obtained  $d$ -spacing value could be used to realize the microstructure of membrane materials. A larger  $d$ -spacing value is often more conducive to the transport of gas molecules, resulting in a higher gas permeation flux.<sup>15,16,28,59</sup> The XRD curves of PEI and TR membranes are shown in Fig. 8. It is found from Fig. 8(a) that the PEI(BHAPPP-6FDA) exhibits a larger  $d$ -spacing about 0.54 nm, while other PEIs show  $d$ -spacing values around 0.43 nm. The introduction of bulky and non-coplanar hexafluoroisopropyl group in 6FDA could increase the distance and destroy the close stacking of macromolecular chain, resulting in the formation of high free volume.<sup>14,15,38</sup> The physical properties of these PEIs are recorded in Table 2, and the fractional free volume (FFV) is calculated according to the Bondi method, which is basically consistent with the  $d$ -spacing values. Cardo structure is conducive to increase the distance between molecular chains, and flexible ether bond is helpful to close the arrangement of molecular chains. Under the two effects, the dianhydride plays a more important role in the layer spacings. In Fig. 8(b), after thermal rearrangement at 450  $^{\circ}\text{C}$  for 1 h, the layer spacings of these TR membranes enhance with varying degrees, among which



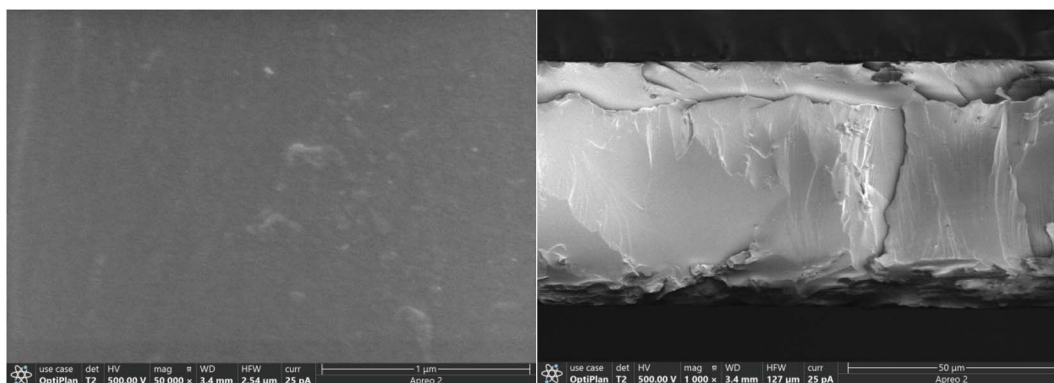


Fig. 6 FE-SEM images of fracture surface of TR(BHAPPP-6FDA).

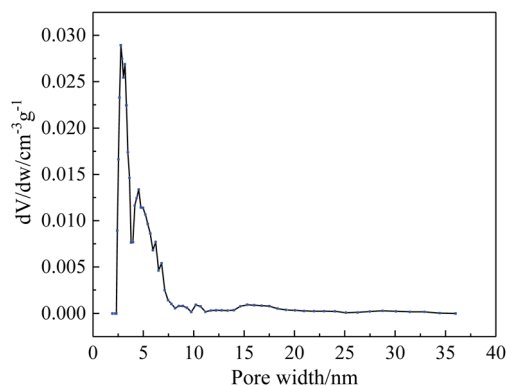


Fig. 7 Pore size distribution curve of TR(BHAPPP-6FDA) membrane.

TR(BHAPPP-6FDA) exhibits an obvious increase of  $d$ -spacing from 0.54 to 0.63 nm. The  $d$ -spacing is larger than that of other reported PI containing phthalide structure, such as TCM-450-1 h<sup>47</sup> and 6FDA-MPP-400,<sup>48</sup> which extremely contributes to the improvement of gas transmission. Hence, the TR membrane based on 6FDA is more suitable for gas separation membrane materials. The effect of thermal treatment temperature on the layer spacings of TR(BHAPPP-6FDA) membranes are investigated by the XRD curves in Fig. 8(c). With the increase of thermal treatment temperature, the interlayer spacing increases gradually, which is mainly due to the increasing conversion degree of rearrangement. Thus, the microstructure of TR membranes could be obviously affected by the thermally treated temperature.

#### 3.4 Mechanical properties of PEI and TR membranes

Because gas separation membranes are often used in high temperature and high pressure environment, the mechanical properties of membrane materials are very important for its practical application. The stress-strain curves of PEI and TR(BHAPPP-6FDA) membranes are shown in Fig. 9, and the corresponding mechanical properties are listed in Table 1. The tensile strength, Young's modulus and elongation at break of PEI membranes are 85.4–122.9 MPa, 3.3–5.1 GPa and 1.8–4.4% respectively, indicating that they have excellent mechanical

properties to undergo further thermal treatment. For these PEI membranes, the existence of flexible ether bond is helpful to improve the film-formation and mechanical properties. Among them, the PEI membranes derived from rigid dianhydrides PMDA, BPDA and CBDA exhibit higher tensile strength and modulus. The PEI derived from dianhydride BTDA exhibits the highest tensile strength, which may be ascribed to the oxidative crosslinking and hydrogen bonding due to the existence C=O. After thermal treatment, the mechanical properties of the TR membranes based on 6FDA drop sharply from 85.4 (250 °C) to 9.8 (475 °C) MPa. Too high thermal treatment temperature easily induces the slight pyrolysis of polymer main chain, resulting in the loss of mechanical properties. Furthermore, the porous structure caused by thermal rearrangement and crosslinking might make the polymer membrane heterogeneous, leading to the serious degradation of mechanical properties.<sup>39</sup>

#### 3.5 Gas separation of PEI and TR membranes

It is well known that the gas separation properties of polymer membranes are controlled by gas solution-diffusion process. Due to the difference in the solution and diffusion coefficients of various gases in the membrane, the relative permeation rate of the gases is apparently different. Hence, the gas permeabilities of polymer membranes strongly depend on the free volume, which provides a path for the transmission of gas molecules. In view of XRD results, the as-prepared PEI and TR membranes are expected to exhibit excellent gas separation properties, so the gas permeabilities for H<sub>2</sub>, CO<sub>2</sub>, O<sub>2</sub> and N<sub>2</sub> are determined at 30 °C and the results are listed in Table 3. It can be seen from Table 3 that the gas permeabilities of PEI membranes are relatively low and follow the orders:  $P(\text{H}_2) > P(\text{CO}_2) > P(\text{O}_2) > P(\text{N}_2)$ , which is in reverse order of molecular dynamics diameter of four gases. Meanwhile, the gas permeabilities of PEI(BHAPPP-6FDA) are higher than those of other PEI membranes, which is consistent with the result of the  $d$ -spacing values measured by XRD and calculated FFV. Based on the same diamine, the dianhydrides take an important influence on the gas separation performance. The gas permeabilities of PEI(BHAPPP-ODPA) is comparatively low, because the flexible –O– linkage causes a dense packing of molecular segments. The





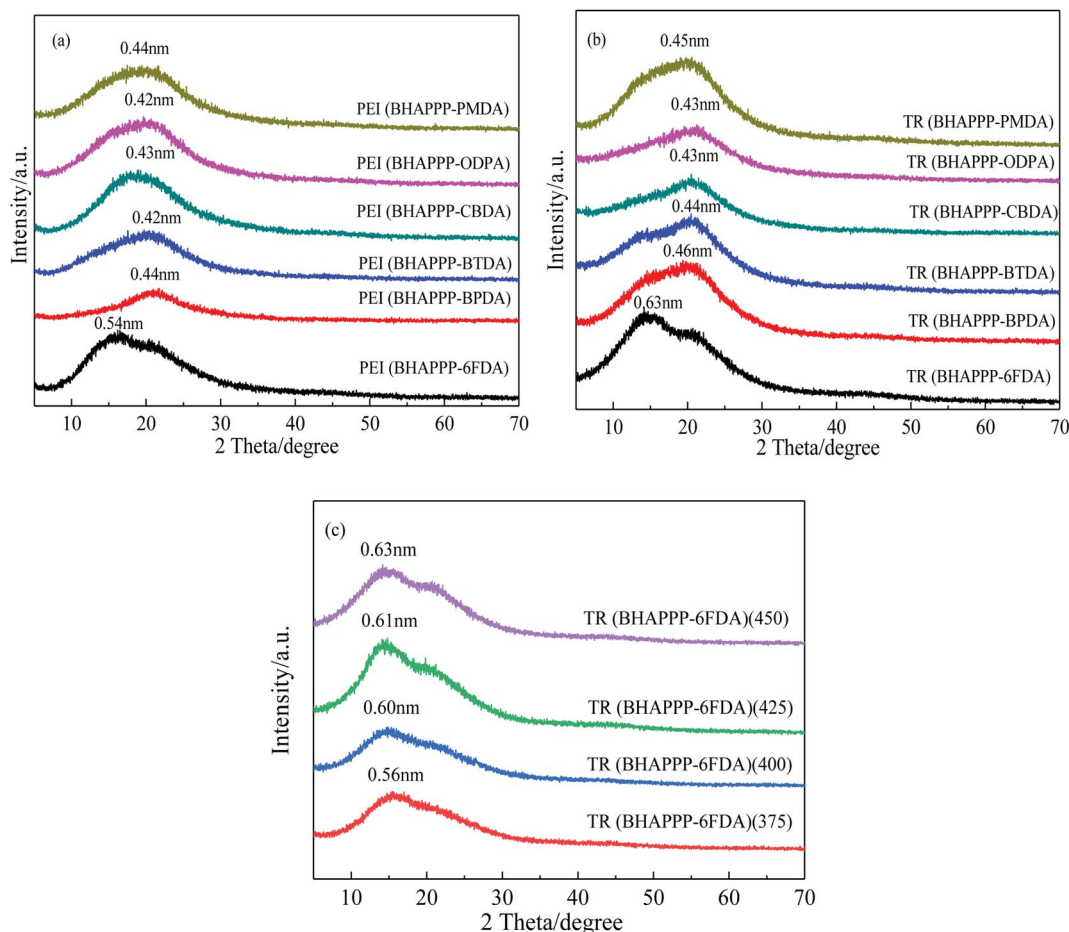


Fig. 8 XRD curves (a) PEI membranes, (b) TR membranes and (c) TR(BHAPPP-6FDA) treated at different treatment temperature.

Table 2 Physical properties of PEIs

Polymers <sup>a</sup>	Density (g cm <sup>-3</sup> )	Molar mass, $M_0^b$ (g mol <sup>-1</sup> )	Molar volume, $V_0$ (cm <sup>3</sup> mol <sup>-1</sup> )	van der Waals volume, $V_w$ (cm <sup>3</sup> mol <sup>-1</sup> )	Fractional free volume, FFV <sup>c</sup>	$d$ -spacing (nm)
PEI(BHAPPP-CBDA)	1.3317	764	573.7	390.1	0.116	0.43
PEI(BHAPPP-PMDA)	1.3636	688	504.5	342.3	0.118	0.44
PEI(BHAPPP-BPDA)	1.3377	764	571.1	386.6	0.120	0.44
PEI(BHAPPP-ODPA)	1.3573	780	574.7	392.1	0.114	0.42
PEI(BHAPPP-BTDA)	1.3536	792	585.1	398.3	0.115	0.42
PEI(BHAPPP-6FDA)	1.2502	914	731.1	475.1	0.156	0.54

<sup>a</sup> Thermally treated at 250 °C for 30 min. <sup>b</sup> Estimated by assuming 100% imidization conversion. <sup>c</sup> Fractional free volume of PEI membranes calculated by Bondi method.

PEI(BHAPPP-6FDA) shows higher gas permeabilities, which are attributed to the introduction of the large volume  $-C(CF_3)_2-$  structure. The reason for it is that the increase of interchain spacing promotes the transport of gas molecules. The gas permeabilities of PEI(BHAPPP-6FDA) reach 7.35 Barrer for CO<sub>2</sub>, 9.25 Barrer for H<sub>2</sub>, 1.184 Barrer for O<sub>2</sub>, 0.249 Barrer for N<sub>2</sub>, coupled with CO<sub>2</sub>/N<sub>2</sub> of 29.51 and H<sub>2</sub>/N<sub>2</sub> of 37.15. The PEI membranes containing phthalide groups exhibit no better gas permeabilities compared with some reported polymer

membranes, such as PIMs and Matrimid, which is probably attributed to the dense packing of macromolecular chains caused by large amounts of hydrogen bonds because of the existence of hydroxyl groups.<sup>60</sup>

After thermal treatment at 450 °C for 1 h, the gas permeabilities of these TR membranes were enhanced because of the thermal rearrangement from hydroxyl-containing PEI to PBO.<sup>34,44,59</sup> The improvement of gas permeabilities is roughly in alignment to the XRD results. The obvious increase of  $d$ -spacing



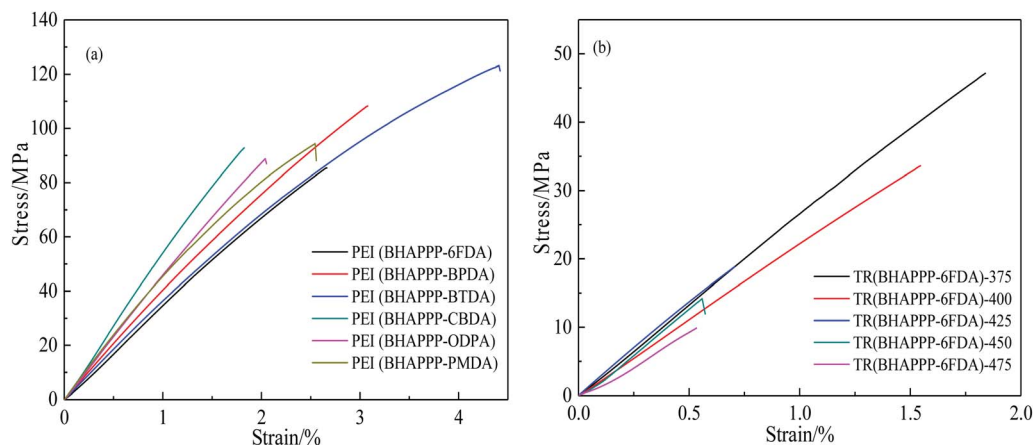


Fig. 9 Stress-strain curves (a) PEI membranes and (b) TR(BHAPPP-6FDA) membranes.

Table 3 Gas separation performance of PEI and TR membranes

Samples	Permeability <sup>a</sup> /Barrer <sup>b</sup>				Ideal selectivity <sup>c</sup>		
	CO <sub>2</sub>	H <sub>2</sub>	O <sub>2</sub>	N <sub>2</sub>	CO <sub>2</sub> /N <sub>2</sub>	O <sub>2</sub> /N <sub>2</sub>	H <sub>2</sub> /N <sub>2</sub>
PEI(BHAPPP-BPDA)	5.83	6.24	1.167	0.269	21.67	4.34	23.20
PEI(BHAPPP-BTDA)	4.67	5.43	1.224	0.241	19.45	5.10	22.53
PEI(BHAPPP-PMDA)	5.02	5.87	0.963	0.235	21.36	5.21	24.98
PEI(BHAPPP-CBDA)	2.49	3.12	0.481	0.111	22.43	4.33	28.11
PEI(BHAPPP-ODPA)	1.37	2.07	0.257	0.057	24.03	4.51	36.31
PEI(BHAPPP-6FDA)	7.35	9.25	1.184	0.249	29.51	4.75	37.15
TR(BHAPPP-BPDA)	178.96	154.97	37.86	7.39	24.21	5.12	20.97
TR(BHAPPP-BTDA)	119.23	97.05	24.00	4.56	26.14	5.26	21.28
TR(BHAPPP-PMDA)	162.11	150.60	35.41	7.24	22.39	4.89	20.80
TR(BHAPPP-CBDA)	67.98	53.13	13.98	2.72	24.99	5.13	19.53
TR(BHAPPP-ODPA)	57.77	53.86	12.06	1.87	30.89	6.45	28.80
TR(BHAPPP-6FDA)	258.5	190.5	38.35	4.25	60.82	9.02	44.82
6FDA-MPP-400 <sup>48</sup>	194	—	42.2	10.6	18.30	3.98	—
PEBO-6FDA <sup>32</sup>	245.04	272.34	60.73	10.58	23.16	5.74	25.7
6FDA-Durene/MPP <sup>50</sup>	219.9	689.4	66.5	24.9	8.83	2.7	25.7
6FDA-CADA1-450 <sup>51</sup>	1858	—	369	108	17.2	3.42	—
R-TR-PBOIa-1 h <sup>56</sup>	75	143	17	3.3	23	5	44

<sup>a</sup> All gas permeation results were obtained at 30 °C and 0.01 MPa (0.1 atm). <sup>b</sup> 1 Barrer = 10<sup>-10</sup> cm<sup>3</sup> (STP) cm cm<sup>-2</sup> s<sup>-1</sup> cm Hg<sup>-1</sup> = 3.35 × 10<sup>-16</sup> mol m<sup>-2</sup> s<sup>-1</sup> Pa<sup>-1</sup>. <sup>c</sup> Ideal selectivities were obtained by the ratio of two gas permeabilities.

of TR(BHAPPP-6FDA) indicates that the conversion rate of thermal rearrangement is relatively high, forming more free volume to readily transport the gas molecules. Among them, the TR(BHAPPP-6FDA) shows higher gas permeabilities and excellent selectivities, including CO<sub>2</sub> of 258.5 Barrer, H<sub>2</sub> of 190.5 Barrer, O<sub>2</sub> of 38.35 Barrer, N<sub>2</sub> of 4.25 Barrer and CH<sub>4</sub> of 2.15 Barrer, coupled with CO<sub>2</sub>/CH<sub>4</sub> of 120.2 and O<sub>2</sub>/N<sub>2</sub> of 9.02. Compared with the PEBO-6FDA membrane containing fluorene groups reported by our group, the as-prepared TR(BHAPPP-6FDA) exhibit extremely higher gas selectivities, which is mostly assigned to the thermal crosslinking of phthalide groups.<sup>32</sup>

In addition, compared with 6FDA-MPP-400<sup>48</sup> and 6FDA-Durene/MPP<sup>50</sup> containing phthalide structure, the TR(BHAPPP-6FDA) displays higher gas permeabilities. However, compared with 6FDA-CADA1-450 with a carboxyl group from the ring-

opening of phthalide structure,<sup>51</sup> the gas permeabilities are obviously lower. This may be due to the fact that the phthalide groups of TR(BHAPPP-6FDA) don't completely open ring and decarboxylate, and the cross-linking process is relatively limited in the TR process. For polymer membranes, the gas separation mainly follows to the solution-diffusion mechanism.<sup>12</sup> With the occurrence of TR and crosslinking reaction, a large number of porous and network structures are formed, resulting in sieving separation.<sup>47</sup> Meanwhile, the formation of crosslinking structure enhances the interaction between macromolecular chains and forms rigid networks, which greatly contributes to the increase of gas selectivities. The possible crosslinking model is shown in Fig. 10, in which the biphenyl crosslinking structure is formed between adjacent phenyl radicals according to the literature.<sup>47</sup> Furthermore, it is observed from Table 3 that the permeability of CO<sub>2</sub> for TR membranes exceeds that of H<sub>2</sub>,



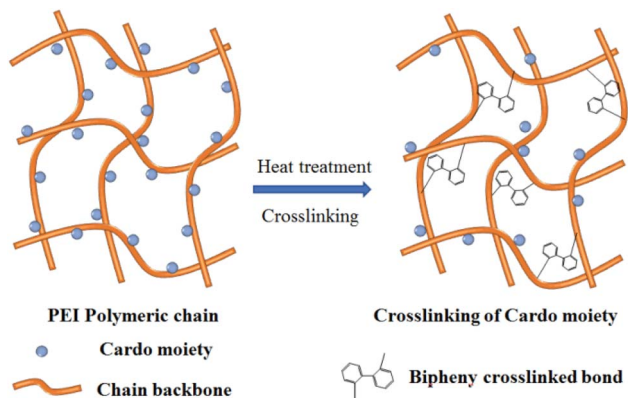


Fig. 10 Crosslinking model of phthalide Cardo moiety during TR process.

indicating the better solubility of CO<sub>2</sub> in the TR matrix. As a result, the gas permeabilities of these TR membrane materials are significantly increased after thermal rearrangement, while the selectivities are also increased in varying degrees or declined slightly, which overcome the trade-off relationship in some sense.

Selected the TR(BHAPPP-6FDA) sample as target, the effects of thermally treated temperature and time on the gas permeabilities are also investigated, and the obtained data are illustrated in Fig. 11 and 12, respectively. With the increase of thermally treated temperature and time, the degree of thermally rearranged reaction gradually increase, resulting in the more release of CO<sub>2</sub>. It can be found that the four gas permeabilities of TR membranes extremely increase with the increase of temperature, but too high temperature will lead to the pyrolysis reaction instead of the rearrangement reaction. Thus, within the temperature range of TR, the structure conversion is partially completed and the gas permeabilities are improved significantly. Besides, CH<sub>4</sub> gas was also used to test the gas permeabilities of TR(BHAPPP-6FDA)-450 membrane with

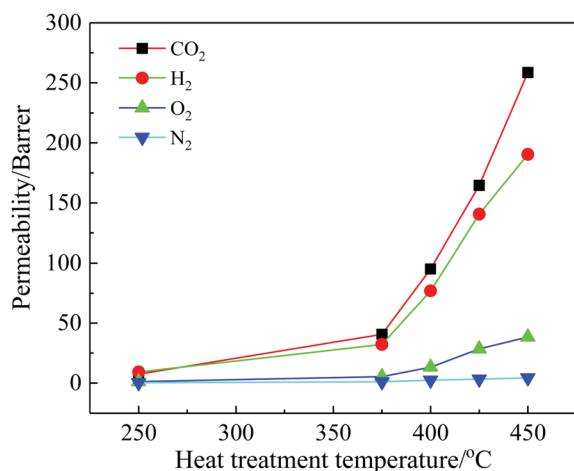


Fig. 11 Gas permeabilities of TR(BHAPPP-6FDA) membranes treated at different temperatures.

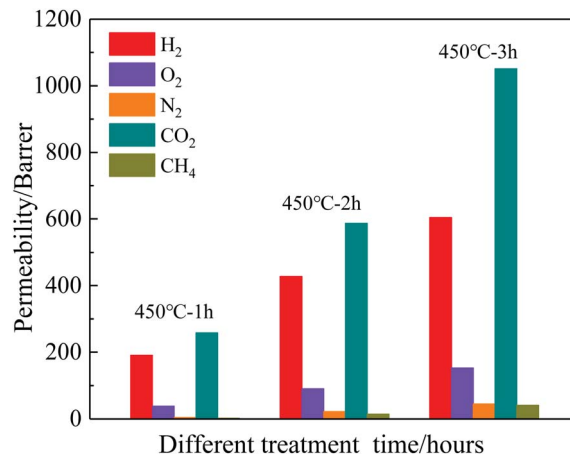


Fig. 12 Gas permeabilities of TR(BHAPPP-6FDA) membranes treated at 450 °C with different time.

different treatment time. With the extension of thermal processing time, the permeabilities of five gases are greatly increased. When the thermal rearrangement time is 3 h, the permeabilities of H<sub>2</sub>, CO<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub> and CH<sub>4</sub> separately reach 604, 1051, 152, 45 and 41 Barrers, but the selectivity of O<sub>2</sub>/N<sub>2</sub> drops from 8.97 to 3.38 and CO<sub>2</sub>/CH<sub>4</sub> decreases from 120.97 to 25.63. Hence, the thermal treatment temperature and time play a key role on the gas separation performance.

In order to investigate the effect of test pressure, the gas permeability test of TR(BHAPPP-6FDA) membrane was carried out at 0.1, 0.5 and 1.0 atm, respectively. Because the tested membrane sample was unsupported, too high pressure wasn't adopted to avoid rupture of the membranes. Fig. 13 gives the gas permeabilities at different pressures, and it can be seen that the permeabilities of four gases exhibit a slight downward trend as the pressure gradually increases. Among them, the permeability of CO<sub>2</sub> is obviously affected by test pressure due to the decrease of gas adsorption or dissolution in membrane materials. This behavior is typical for glassy polymers.<sup>61</sup>

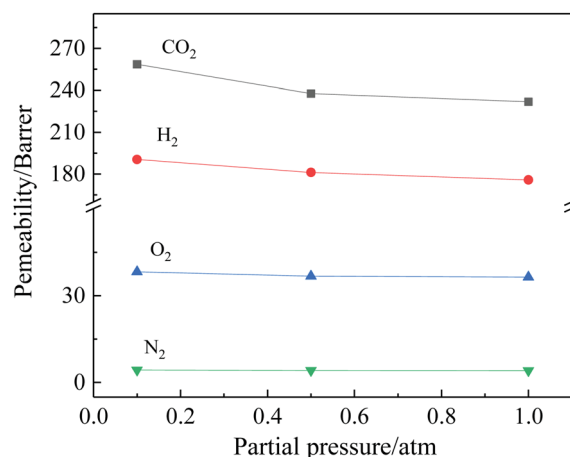


Fig. 13 Gas permeabilities of TR(BHAPPP-6FDA) membrane at different test pressure.



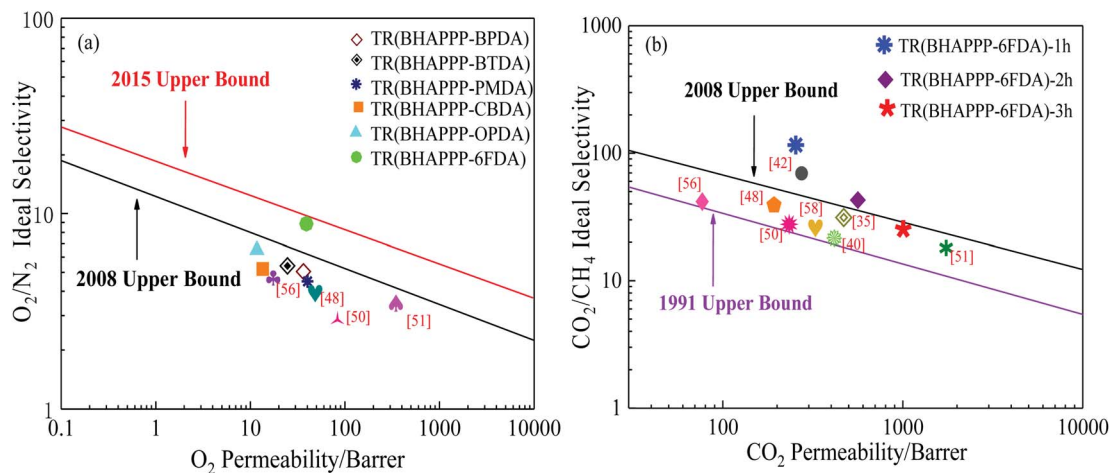


Fig. 14 Evaluation of separation performance of TR membranes (a) O<sub>2</sub> vs. O<sub>2</sub>/N<sub>2</sub>; (b) CO<sub>2</sub> vs. CO<sub>2</sub>/CH<sub>4</sub>.

In gas separation application, the “trade-off” relationship between permeability and selectivity constantly exists, resulting in any improvement in gas permeability accompanied with a decrease of selectivity. The O<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/CH<sub>4</sub> separation properties of TR membranes in this work and many reported TR membranes are depicted in Fig. 14. Compared with aPBO,<sup>58</sup> R-TR-PBOIa-1 h,<sup>56</sup> PEBO-6FDA,<sup>32</sup> 6FDA-MPP-400,<sup>48</sup> 6FDA-CADA1-450,<sup>51</sup> and 6FDA-Durene/MPP,<sup>50</sup> the TR(BHAPPP-6FDA) membrane exhibits the best O<sub>2</sub>/N<sub>2</sub> separation properties, close to the 2015 upper limit. Moreover, the CO<sub>2</sub>/CH<sub>4</sub> separation properties of TR(BHAPPP-6FDA) show a decline trend with the lapse of thermal treatment time, but the TR(BHAPPP-6FDA)-1 h still greatly exceeds the 2008 upper limit. Thus, among the six TR membranes, the TR(BHAPPP-6FDA) membrane displays superior gas separation performance due to the larger *d*-spacing caused by  $-\text{C}(\text{CF}_3)_2-$  structures, which is expected to be applied as separation materials in the future.

## 4. Conclusions

The diamines 3,3-bis[4-(3-hydroxy-4-aminophenoxy)phenyl]phthalide (BHAPPP) were successfully synthesized and polymerized with six kinds of dianhydrides to prepare PEI membranes. Then, the corresponding TR membranes were obtained by thermal treatment at 450 °C for 1 h. The PEI membranes showed excellent mechanical properties, such as tensile strength of 85.4–122.9 MPa and Young’s modulus of 3.3–5.1 GPa. However, as the thermal treatment temperature increased, the mechanical properties of the membranes sharply decreased. Meanwhile, the gas permeabilities were greatly increased because of the thermal rearrangement from hydroxyl-containing PEI to TR membranes. Particularly, during the thermal rearrangement, the thermal crosslinking reaction derived from phthalide groups took place simultaneously, resulting in the obvious improvement in gas selectivities than similar structure TR membranes containing fluorenyl structures. Importantly, the treatment temperature and time played a major role in gas separation performance of TR membranes.

Comparatively, the gas permeabilities of TR(BHAPPP-6FDA) for CO<sub>2</sub>, H<sub>2</sub>, O<sub>2</sub>, N<sub>2</sub> and CH<sub>4</sub> reached 258.5, 190.5, 38.35, 4.25 and 2.15 Barrers, respectively. The selectivity for O<sub>2</sub>/N<sub>2</sub> was 9.02, close to the 2015 Robeson upper limit, and CO<sub>2</sub>/CH<sub>4</sub> reached 120.2, which significantly exceeded the 2008 Robeson upper limit. Therefore, this work provides a kind of TR membranes based on phthalide groups with excellent gas separation properties, which are expected to be used as gas separation materials in the practical application.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

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