

Cite this: *Catal. Sci. Technol.*, 2017,  
7, 5900

# Unravelling the mechanisms of CO<sub>2</sub> hydrogenation to methanol on Cu-based catalysts using first-principles multiscale modelling and experiments†

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A way to address the challenge of carbon dioxide emissions causing global warming and climate change is the heterogeneous catalytic hydrogenation of CO<sub>2</sub>. When surplus electrical energy is available, hydrogen may be produced and used for conversion of CO<sub>2</sub> into fuels and chemicals. Industrially, a multifunctional metallic copper and zinc oxide catalyst on alumina (CZA) is commonly used. Presently, first-principles multiscale modelling was accomplished for a commercial-like catalyst (Zn<sub>3</sub>O<sub>3</sub>/Cu) and three other Cu/metal oxide combinations (Cr<sub>3</sub>O<sub>3</sub>/Cu, Fe<sub>3</sub>O<sub>3</sub>/Cu, and Mg<sub>3</sub>O<sub>3</sub>/Cu), synthesised *via* co-precipitation, characterised and experimentally tested. *Ab initio* plane wave density functional theory calculations were performed using different structural models to elucidate the adsorption of intermediates and elementary reaction steps, considering thermodynamics and kinetics. The results were fed into mean-field micro-kinetic expressions to calculate the conversion and selectivity in a continuous flow stirred-tank reactor vessel for various temperatures and pressures. Kinetic Monte Carlo simulations were used to obtain the detailed surface coverage, turnover frequency and catalytic performance. Although no experimental input besides the structure was applied for physico-chemical mechanism description, measurements were in agreement with theoretical predictions. It was shown that the formate species pathway (HCOO → H<sub>2</sub>COO → H<sub>2</sub>COOH → H<sub>2</sub>CO → H<sub>3</sub>CO) predominates on the examined Cu-based catalysts, although there are variations in the rate determining steps and the most abundant surface intermediate fractions. Whereas Zn<sub>3</sub>O<sub>3</sub>/Cu exhibited the highest conversion and a moderate CH<sub>3</sub>OH product selectivity, the former was lower for Mg<sub>3</sub>O<sub>3</sub>/Cu. Interestingly, Cr<sub>3</sub>O<sub>3</sub>/Cu was optimal in terms of yield, but with extremely low CH<sub>3</sub>OH productivity, while Fe<sub>3</sub>O<sub>3</sub>/Cu performed poorly overall. Our results highlight the superiority of Zn<sub>3</sub>O<sub>3</sub>/Cu, combining the estimations on micro-, meso- and reactor operation scales. Insights beyond traditional activity experiments may be attained and employed in full-scale reactor engineering and optimisation.

Received 15th August 2017,  
Accepted 24th October 2017

DOI: 10.1039/c7cy01659j

rsc.li/catalysis

## 1. Introduction

Technological breakthroughs that have revolutionized our world have been made possible by abundant energy. Historically, humanity has used accumulated solar energy, which has been stored in various forms. Coal and oil have been the cheapest and most plentiful energy sources and thus heavily relied upon. This, however, represents a great environmental burden, necessitating scientific approaches to tackle it.

Burning oil and coal is not a carbon neutral process because the carbon that is released as carbon dioxide has not

been in the atmosphere for millions of years. Thus it irreversibly increases the concentration of atmospheric CO<sub>2</sub>, which has been linked to global warming and ocean acidification. This problem can be avoided if carbon neutral energy sources are used, such as biomass, hydro, wind or nuclear energy. In the near future, the full transition towards carbon neutral economy is unfortunately not foreseeable. Thus, the problem of increasing carbon dioxide concentrations must be addressed proactively.<sup>1</sup>

One of the most promising methods for fixation of captured carbon dioxide is its catalytic hydrogenation to methanol at concentrated sources, such as in thermal power plants. In doing so, methanol is obtained, which is often a more convenient way of storing energy than H<sub>2</sub> itself. Methanol is both a clean energy source with a neutral carbon footprint and a versatile chemical for a number of chemical processes.

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† Electronic supplementary information (ESI) available: Animation with kMC results. See DOI: 10.1039/c7cy01659j



Several industrial methods for methanol production with hydrogenation of CO and CO<sub>2</sub> already exist. Mostly, syngas mixtures at high pressures up to 100 bar and temperatures of 200–300 °C are used. Although several non-copper catalysts have been proposed in the literature,<sup>2–5</sup> industrial processes use mainly copper/zinc/alumina (CZA) catalysts due to their low price and durability. They are prepared by a co-precipitation method to yield active Cu clusters and ZnO nanoparticles.<sup>6</sup> Effective catalysts have a high Cu:Zn ratio and large exposed Cu surfaces. Catalyst activity scales linearly with the accessible Cu surface area.<sup>7,8</sup> However, pure Cu is only weakly effective, proving that there is strong synergy between Cu and ZnO.<sup>9–11</sup> In the quest for the most effective and inexpensive catalyst, the secondary metal (Zn), support and method of synthesis are varied.

Considerable research efforts have been devoted to establishing the exact mechanism of this reaction. Most of the intermediates involved cannot be followed experimentally, therefore one must speculate about their existence based on other available experimental data and *ab initio* studies. Historically, two mechanisms have been proposed. Carbon dioxide is either hydrogenated on the carbon atom, yielding HCOO and following the formate route (H<sub>2</sub>COO, H<sub>2</sub>COOH, CH<sub>2</sub>O, CH<sub>3</sub>O), or hydrogenated on the oxygen atom, yielding COOH and following the reverse water–gas shift route. Most theoretical work on copper-based catalysts gives credence to the former method. In our previous work on spinel-type CuZnAl<sub>2</sub>O<sub>4</sub>, density functional theory (DFT) screening of all conceivable intermediates and elementary steps showed the formate pathway to predominate.<sup>12</sup> Other authors have reached similar conclusions on related catalysts. Grabow and Mavrikakis performed DFT simulations and microkinetic modelling on Cu(111) and confirmed the formate pathway.<sup>13</sup> Studt *et al.* studied the reaction on stepped copper surfaces with HCOO, HCOOH and H<sub>2</sub>COO intermediates.<sup>14</sup> DFT calculations and kinetic Monte Carlo from Yang *et al.*'s study on metal-doped Cu corroborated the formate pathway on pure Cu(111) and Au/Cu(111), while other noble metal dopants favoured the RWGS pathway.<sup>15</sup> Behrens *et al.* studied the reaction on Cu(111), Cu(211) and Zn-doped Cu(211) and confirmed the formate pathway mechanism.<sup>10</sup> The combined experimental and theoretical study by Kattel *et al.* confirmed this,<sup>16</sup> although there is some discussion whether Zn becomes oxidised or attaches to formate.<sup>17</sup> Nakatsuji and Hu studied this reaction on Cu(100) and Zn/Cu(100) and also established the formate pathway as the main source of methanol.<sup>18</sup> Zhao *et al.*, however, argued that on Cu(111), direct hydrogenation of CO<sub>2</sub> to HCOO is a mechanistic dead-end due to the high activation energies for further conversion of HCOO, and instead proposed an alternative pathway catalysed by co-adsorbed water.<sup>19</sup> Several studies also focused on more subtle effects, such as interface effects of Cu/ZnO by Tang *et al.*<sup>20</sup>

This work is a significant extension of our previous endeavour, which focused on DFT calculations,<sup>12</sup> albeit using a different atomistic model. Four copper-based catalysts were

synthesised, characterised and computationally studied. The secondary metals were Zn, Mg, Cr and Fe, present in their oxide form. An atomistic model simple enough to be computationally tractable and complex enough to account for the synergy of the Cu and metal oxide was formulated. Using DFT, adsorption energies and the complete energetics (barriers, energy changes, and vibrational analysis) were calculated. These data were fed into a complex microkinetic (MK) model with two types of reaction sites to study selectivity, conversion and equilibrium coverages in a continuous stirred-tank reactor (CSTR). Results were then contrasted with kinetic Monte Carlo (kMC).

The paper is structured as follows. After the Introduction in section 1, the experimental, theoretical, and computational methods are outlined in section 2. Experimental work is sketched in section 2.1. The DFT (section 2.2), MK (section 2.3), and kMC (section 2.4) methodologies are thoroughly explained. Results are reported in section 3, separately for DFT-calculated adsorption modes (section 3.1), reaction pathways and rates (section 3.2), MK modelling (section 3.3) and kMC results (section 3.4). Then, the results from different methods are compared among themselves and contrasted with the experimental data. The reasons for agreement and discrepancies are discussed (section 4), followed by a short conclusion (section 5).

## 2. Methodology

### 2.1. Catalyst synthesis and characterisation

Cu/M/Al catalysts (Cu:M:Al = 50:30:20, M = Zn, Mg, Cr, and Fe) were prepared by a co-precipitation method.<sup>21</sup> Details can be found in ref. 12. The catalysts were then dried for 12 h at 90 °C and further calcined in a positive flow of air at 300 °C for 4 h.

To obtain the necessary parameters for microkinetic modelling, characterisation was performed with temperature programmed desorption (H<sub>2</sub>-TPD) and a Brunauer–Emmett–Teller (BET) surface area measurement, as described in ref. 12. The dispersion of copper was measured using dissociative N<sub>2</sub>O-chemisorption, as described in ref. 22.

For catalytic testing, a GHSV of 6000 h<sup>-1</sup> for a mixture of CO<sub>2</sub> and H<sub>2</sub> (CO<sub>2</sub>:H<sub>2</sub> = 1:3) was used. The reactor pressure (20, 30, 40, 50 bar for different runs) and temperature (200, 220, 240, 260, 280, 300 °C for different runs) were kept constant for each run.

### 2.2. DFT calculations

**2.2.1. Computational details.** Density functional theory (DFT) calculations were carried out with program suite Quantum Espresso 5.4,<sup>23</sup> which uses the PWscf code to calculate the electronic structure of periodic atomic structures. For visualization of the structures, an open-source tool XCrysDen was used.<sup>24</sup>

As the best compromise between accuracy and computational cost, the Perdew–Burke–Ernzerhof (PBE) functional was selected.<sup>25,26</sup> Ultrasoft pseudopotentials from scalar-



relativistic calculations were used. To account for the insufficient description of van der Waals interactions by DFT methods, a modified semi-empirical Grimme dispersion correction was included.<sup>27</sup> Convergence testing showed that a kinetic energy cut-off of 300 eV and a wavefunction cutoff of 2400 eV sufficed to obtain well converged results. The metallic nature of the catalyst was taken into account by using Gaussian spreading of width 0.1 Ry for Brillouin zone integration. It was sampled on a Monkhorst-Pack mesh with  $8 \times 8 \times 1$  points.<sup>28</sup> A convergence threshold of  $10^{-8}$  Ry for self-consistent cycles was selected. For geometric optimisation of adsorbates, residual forces were required to drop below  $10^{-3}$  Ry per au and energy change per step below  $10^{-4}$  Ry.

For gaseous species calculations, a large ( $25 \times 25 \times 25 \text{ \AA}$ ) cubic cell was used. As there is no periodicity to account for, the Brillouin zone was sampled at a single point ( $\Gamma$ ) and no dipole correction was used.

To seek transition states, the nudge elastic band (NEB) method was used.<sup>29</sup> After preliminary identification of the transition state structure, it was determined with the climbing image approach until forces orthogonal to the reaction pathway dropped below  $0.05 \text{ eV \AA}^{-1}$ .<sup>30</sup> Vibrational analysis was carried out to ensure that each transition state structure had exactly one imaginary frequency, corresponding to the movement along the reaction coordinate. For adsorbed species, zero-point energy (ZPE) correction was calculated from the vibrational component only, perturbing only adsorbate atoms

$$E_{\text{ZPE}} = \sum_i^{3N} \frac{h\nu_i}{2} \quad (1)$$

Adsorption energies of reactants, intermediates and products were calculated as

$$\Delta E_{\text{ads}} = E_{\text{adsorbed}} - E_{\text{catalyst}} - E_{\text{species}} + \Delta E_{\text{ZPE}} \quad (2)$$

The reaction barrier ( $E_A$ , activation energy) and reaction energy ( $\Delta E$ ) for each elementary step were calculated in a standard fashion as

$$E_A = E_{\text{TS}} - E_{\text{reactant}} \quad (3)$$

and

$$\Delta E = E_{\text{product}} - E_{\text{reactant}} \quad (4)$$

This allowed us to obtain the reaction rates as

$$k_{\text{fwd}} = \frac{k_B T}{h} \frac{q_{\text{vib,TS}}}{q_{\text{vib,reactant}}} \exp\left(-\frac{E_A}{k_B T}\right) \quad (5)$$

where  $k_B$  denotes the Boltzmann constant,  $T$  is the absolute temperature,  $h$  is the Planck constant and  $q_{\text{vib}}$  is the vibrational partition function, which is in turn estimated from the real vibrational contributions only (as the imaginary mode

along the reaction coordinate is factored out in transition state theory) as

$$q_{\text{vib}} = \prod_i^{3N} \left(1 - \exp\left(-\frac{h\nu_i}{k_B T}\right)\right)^{-1} \quad (6)$$

The equilibrium constants are obtained from

$$K = \exp\left(\frac{-\Delta E}{k_B T}\right) \quad (7)$$

and allow us to determine the rates for the reverse reactions

$$K = \frac{k_{\text{fwd}}}{k_{\text{rev}}} \quad (8)$$

For adsorbed hydrogen atoms, surface diffusion was explicitly taken into account as an elementary reaction, when hydrogen migrates from one fcc site on Cu to the adjacent one.

The kinetic constants for adsorption and desorption are obtained from collision theory. The rate of adsorption can be evaluated if we assume that the sticking probability equals unity as

$$k_{\text{ads}} = \frac{1}{N_0 \sqrt{2\pi m k_B T}} \quad (9)$$

where  $N_0$  denotes the number of reaction sites per catalyst to be  $1.9 \times 10^{17} \text{ m}^{-2}$  and  $m$  is the mass of a molecule. For the desorption rate, one calculates the equilibrium constant and by taking into account the vibrational, rotational and translational components of the partition function for gaseous species.

$$K = \frac{k_{\text{ads}}}{k_{\text{des}}} = \frac{q_{\text{vib,ads}}}{q_{\text{vib,g}} q_{\text{rot}} q_{\text{trans}}} \exp\left(-\frac{E_{\text{ads}}}{k_B T}\right) \quad (10)$$

**2.2.2. Catalyst model.** The catalyst was modelled as a slab of four atomic layers of pure Cu(111). Preliminary testing showed that the adsorption energies are in this case converged within 0.01 eV. Our converged crystal lattice constant for bulk copper was  $3.58 \text{ \AA}$ , which agrees with the experimental value  $3.61 \text{ \AA}$  within 1%.

To account for the bifunctional nature of the catalyst and the synergistic effects of Cu and the metal oxide, a small cluster of  $\text{M}_3\text{O}_3$  ( $\text{M} = \text{Zn}, \text{Mg}, \text{Fe}, \text{Cr}$ ) was deposited on top of the catalyst in a  $5 \times 5$  supercell (see Fig. 1). Several positions were tested to identify the one with the lowest energy. In this manner, we reproduce both the synergistic effect of metal/metal-oxide contact and the effect of a defect (step or terrace).

Admittedly, such an “inverse” model is particularly useful to describe the SMSI (strong metal-support interaction) state,<sup>31</sup> which is for instance well established in Cu/ZnO. The same model was chosen for other metals, despite them being



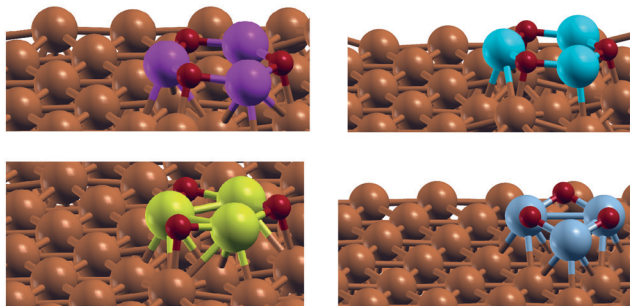


Fig. 1 Modelled active site of the  $M_3O_3/Cu$  catalyst (from top left, clockwise M: Zn, Mg, Cr, Fe) consists of  $M_3O_3$  deposited atop of the Cu(111) plane. Reactions proceed at the interphase boundary.

somewhat harder (Cu/MgO) or more easily reducible ( $FeO_x$ ), to allow for easier comparison. Structurally different models would probably quantitatively better describe each particular set of measurements, but would obscure fundamental properties we wish to explore across different metals. One should also keep in mind that this is one possible type of active site, as oxides can also be partially or totally reduced at high temperatures and hydrogen pressures.<sup>32</sup>

Work on pure Cu and Zn-doped Cu also showed that the active site might be located at a twin boundary, *i.e.* at a step size and not a terrace site. Our models, however, include oxides.<sup>10</sup>

The active site of the catalyst is the interface of Cu and  $M_3O_3$ . Throughout the calculations, the top two Cu layers,  $M_3O_3$  and adsorbed species were allowed to relax fully, while the bottom Cu layers were frozen in their bulk positions.

### 2.3. Microkinetic modelling

In order to investigate the effects of different catalyst compositions on  $CO_2$  hydrogenation, a micro-kinetic model, which is based on 33 reversible elementary steps (*vide infra* Table 2 for stable adsorbates and Table 3 for surface reactions), was developed. A thorough methanol synthesis reaction network with 26 distinct species and seven of them also in the bulk (gaseous phase) was considered, also taking into account possible formation of by-products such as formaldehyde and formic acid. The model includes all pathways as calculated using DFT without any assumptions regarding the rate determining step. The mean-field micro-kinetic model was used to predict the reaction kinetics. All surface reaction ( $k_{fwd}$ ,  $k_{rev}$ ) and adsorption rates ( $k_{ads}$ ,  $k_{des}$ ) were taken directly from DFT calculations and transition state theory or collision theory, respectively. To improve model stability and decrease computation times, all reaction rates were scaled. When scaled by a factor of  $10^{-3}$ , the results were the most in-line with the general observations reported in the methanol synthesis field and our experimental results.

Methanol synthesis is performed under dynamic conditions where reactant gases continuously flow through the reactor. To simulate this and to have similar conditions as those in kMC simulations, our model is based on the continuous stirred-tank reactor (CSTR). Simulation conditions were

chosen based on typical experimental set-ups. First, temperature dependence (480–680 K with increments of 20 K) was tested at 40 bar. Subsequently, pressure dependence (20–60 bar with increments of 10 bar) was checked at 540 K. During all simulations, the initial molar ratio between  $CO_2$  and  $H_2$  was 1:3 and the gas hourly space velocity (GHSV) was set to  $6000\text{ h}^{-1}$  with no other gases present in the influent. The reactor volume was 1 ml. The number of active sites was inferred from the  $H_2$ -TPD results. As shown later in Fig. 4 and Table 2, all intermediates except  $H^*$  and  $CO^*$  bind to the copper-metal interface active site, while the latter bind to copper. For this reason we de-convoluted the  $H_2$ -TPD profiles to three different peaks, with the  $\alpha$  peak attributed to copper sites ( $*$ ) and the  $\beta$  and  $\gamma$  peaks to interface sites ( $\#$ ).

The initial values of the gas composition are specified as written below and initially no species are bound to the catalyst's surface

$$\theta_{j(t=0s)} = 0 \rightarrow \theta_{(t=0s)}^* + \theta_{(t=0s)}^\# = 1, \quad (11)$$

where  $\theta_j$  is the fractional coverage of the adsorbate species, whereas  $\theta^*$  and  $\theta^\#$  are the fractional coverages of free active surface sites of Cu and Cu-M (their total ratio being 1:1), respectively.

Active sites must be either free or covered by an intermediate:

$$\begin{aligned} \theta^* + \theta^\# + \theta_H + \theta_{CO_2} + \theta_{CO} + \theta_{H_2O} + \theta_{CH_3OH} + \theta_{HCOOH} + \theta_{CH_2O} \\ + \theta_{HCOO} + \theta_{H_2COO} + \theta_{H_2COOH} + \theta_{H_2CO} + \theta_{CH_3OH} + \theta_{l-COOH} \\ + \theta_{c-COOH} + \theta_{COH} + \theta_{HCO} + \theta_{HCOH} + \theta_O + \theta_{OH} = 1 \end{aligned} \quad (12)$$

The corresponding rate equations for surface reactions (*cf.* Table 3 for numbering) can be written either as

$$r_i = k_f \theta_j \theta_j^* \text{ or } \# - k_r \theta_j \theta_j \quad (13)$$

for reactions when  $i = 3, 5, 9, 11, 13,$  and  $16$ ; or as

$$r_i = k_f \theta_j \theta_j - k_r \theta_j \theta_j^* \text{ or } \# \quad (14)$$

for reactions when  $i = 4, 6, 8, 10, 12, 14, 15, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27,$  and  $28$ .

In elementary reaction  $i = 7$ , where only the *cis-trans* configuration is changed, the rate equation is written as:

$$r_i = k_f \theta_j - k_r \theta_j \quad (15)$$

For the adsorption and desorption reactions, the rates are defined as:

$$r_i = k_f p_j \theta_j^n - k_r \theta_j^n, \quad (16)$$

where  $p_j$  is the bulk pressure of the species and  $n$  is the number of sites needed to adsorb one molecule.





Reactions are indexed to  $i$ , while adsorbate species and intermediates are indexed to  $j$ . The forward reaction constants  $k_i$  are calculated from the DFT results from eqn (5) and the reverse constants  $k_{-i}$  from eqn (7) and (8).

Mass balances of surface-bound species are defined as

$$\frac{d\theta_j}{dt} = \sum_{i=1}^n S_{ij} r_i, \quad (17)$$

where  $n$  is the number of reactions and  $S_{ij}$  is the “stoichiometric coefficient”, denoting how many times a particular species occurs in the reaction. It is positive for products, negative if consumed, and 0 if it the species does not participate in the reaction. Mass balances of bulk species are defined as:

$$\frac{dC_j}{dt} = \frac{M_{\text{sites}}}{\varepsilon} \sum_{i=1}^n S_{ij} r_i + \frac{F}{\varepsilon V_R} (C_{j,\text{inlet}} - C_j), \quad (18)$$

where  $C_j$  is the species concentration in the bulk phase,  $M_{\text{sites}}$  is the total concentration of catalyst sites in the reactor volume,  $\varepsilon$  is the void fraction of the catalyst bed (volume of the intraparticle space divided by the reactor volume),  $F$  is the total volumetric flow through the reactor,  $V_R$  is the reactor volume and  $C_{j,\text{inlet}}$  is the inlet bulk concentration of species.

Micro-kinetic simulations were carried out with MATLAB®, a script-based numerical computing environment by MathWorks Inc. Using the systematic approach described above, a system of 26 non-linear ordinary differential equations was obtained. The system is not solvable analytically; therefore numerical methods were used to obtain a solution. Although only steady state reactor operation was required, a transient solution was calculated as the stability of the system would prevent any noticeable computational savings with steady-state solvers. Because the system is numerically very stiff, the usual Runge–Kutta methods proved to be too unstable. Instead, we had to resort to more stiff-orientated solvers. MATLAB's built-in solver ode23s was used. This solver is based on backwards differential formulas, an implicit method widely used for solving stiff systems. Such solvers use variable orders of the said formulas. The system was solved successfully for a sufficient time to achieve a steady state.

After simulation  $\text{CO}_2$  conversion was calculated as:

$$\text{CO}_2 \text{ conversion} [\%] = \frac{n(\text{CO}_{2,\text{in}}) - n(\text{CO}_{2,\text{out}})}{n(\text{CO}_{2,\text{in}})} \times 100\%, \quad (19)$$

and methanol C-based selectivity as:

$$S_{\text{CH}_3\text{OH}} [\%] = \frac{n(\text{CH}_3\text{OH})}{n(\text{CH}_3\text{OH}) + n(\text{CO}) + n(\text{CH}_2\text{O}) + n(\text{HCOOH})} \times 100\%. \quad (20)$$

#### 2.4. kMC simulations

Kinetic Monte Carlo (kMC) simulations are nowadays widely used in theoretical chemistry applications, and are gaining

particular importance in the field of heterogeneous catalysis.<sup>33,34</sup> In combination with the atom-scale DFT computations, kMC provides a mesoscopic description of reactor performance, enabling the studies of catalyst kinetics in a stochastic manner.<sup>35</sup> Using kMC, we can statistically evaluate the surface chemistry kinetics, and ultimately estimate the activity, selectivity, conversion, *etc.* of a catalyst under operating conditions.

In this paper, we used the kMC software package Zacros.<sup>34</sup> Zacros employs the graph-theoretical kMC framework, which apart from simulating adsorption, desorption, diffusion, and reactions on lattices, allows for treatment of complex chemistries such as multidentate species or complex neighbouring lattice site coverage. The catalysts that we study in this paper are alloys of Cu and metal (Zn, Mg, Fe, Cr) oxides, which due to complex geometries require accurate handling of adsorbate lateral interactions and active site occupancies.

Following the methanol synthesis pathway presented in Fig. 5 and using the DFT obtained results, we set up our kMC simulations. Species formation energies were mapped with Zacros using DFT obtained absolute energies using the standard procedure.<sup>36,37</sup> We defined a custom periodic cell lattice (size of  $48 \times 48$  cells) with unit cell vectors  $\alpha = (4.78, 0.0) \text{ \AA}$  and  $\beta = (2.39, 4.14) \text{ \AA}$ , representing the geometry of our Cu alloys. These values correspond to the position of Cu atoms in pure Cu(111). We used two distinct active site types (their ratio being 1 : 1), because DFT simulations showed that hydrogen atoms and CO tend to adsorb on Cu, while other intermediates favour the interface between Cu and the dopant metal ( $\text{M}_3\text{O}_3$  cluster). In total, the lattice consists of 4608 active sites. In this model, this cluster acts as a surface defect where the reaction takes place. Intermediates with two oxygen atoms were considered bidentate, adsorbing on two neighbouring distinct-type sites. The pre-exponential factors for each reaction were obtained as in ref. 36 and 38, where the temperature and pressure dependence was taken into account through rotational, translational, and vibrational partition functions.

Overall, the methanol synthesis model consists of 19 lattice and 7 gaseous species and 32 reversible reaction steps (see Tables 2 and 3 and Fig. 5). To avoid unnecessary and physically unimportant repetition of some steps, which would render simulations intractably time-consuming, hydrogen surface diffusion and  $\text{CO}_2$  adsorption had to be slowed down by a factor of  $10^4$ . According to Prats *et al.*, such modifications speed up the simulations considerably without significantly affecting the results.<sup>39</sup>

Also, in Zacros the gas molar fraction is treated as constant throughout the reaction and we used a  $\text{H}_2:\text{CO}_2 = 3:1$  molar ratio throughout our simulations. Therefore desorption of HCOOH and  $\text{CH}_2\text{O}$  had to be turned off, since both are prone to desorption but due to the constant gaseous phase composition could never re-adsorb. Our experimental results show negligible amounts of formed HCOOH and  $\text{CH}_2\text{O}$ , warranting this approximation in the model.



## 3. Results

### 3.1. Experimental

**3.1.1. Catalyst characterisation.** In Table 1, the results from H<sub>2</sub>-TPD, BET and N<sub>2</sub>O chemisorption are shown for the four catalysts.

It is believed that the reducible nature of copper species and the copper surface area are important parameters for the catalytic performance of copper-based catalysts.<sup>40–42</sup> A linear relationship between CO<sub>2</sub> conversion on Cu-based catalysts and their exposed Cu surface area is often reported.<sup>43,44</sup> In the present study, trends of the catalytic activity are consistent with the exposed Cu surface area and Cu<sup>+</sup>/Cu<sup>0</sup> ratio.

The amount of chemisorbed hydrogen on the catalyst surface is influenced by the second metal (M), being the highest for Cu/Zn, followed by Cu/Mg, Cu/Fe, and Cu/Cr. It has been reported in the literature that higher amounts of chemisorbed hydrogen are also due to the formation of sub-surface hydrogen.<sup>45</sup>

Surface area is the largest for Cu/Mg, followed by Zn, Cr, and Fe. The relatively low surface area of Cu/Cr and Cu/Fe catalysts (in comparison to Cu/Zn and Cu/Mg) could be caused by blocking of the alumina pores with the crystallites of chromium and iron oxides.<sup>46,47</sup>

The metal dispersion of all tested catalysts ranges from 17 to 37%, while the Cu metallic surface area remains in the range 21–35 m<sup>2</sup> g<sup>-1</sup>. In particular, the Cu/Cr catalyst showed lower dispersion and surface area than other catalysts. In general, for catalysts prepared with co-precipitation, small catalyst crystallites are correlated with higher dispersion and BET surface area.<sup>48</sup> Our results confirm this. The Cu metallic surface area follows the order: Cu/Mg > Cu/Zn = Cu/Fe > Cu/Cr.

**3.1.2. Catalytic performance.** In Fig. 2, temperature dependence of the performance of the synthesised catalysts is shown at 20 bar and GHSV = 6000 h<sup>-1</sup>. Methanol, carbon monoxide and water are the only products under all operating conditions. Except for the lowest temperature where conversion is negligible for all catalysts, Zn<sub>3</sub>O<sub>3</sub>/Cu constantly has the best conversion, followed by Mg<sub>3</sub>O<sub>3</sub>/Cu, Fe<sub>3</sub>O<sub>3</sub>/Cu and Cr<sub>3</sub>O<sub>3</sub>/Cu. These results are nicely correlated with Cu metal dispersion and Cu metallic surface area. It has previously been postulated that the reducible nature of copper species and in particular copper surface area are important parameters for the catalytic performance of Cu-based catalysts.<sup>42</sup> A linear relationship between CO<sub>2</sub> conversion and the total amount of exposed copper has already been pro-

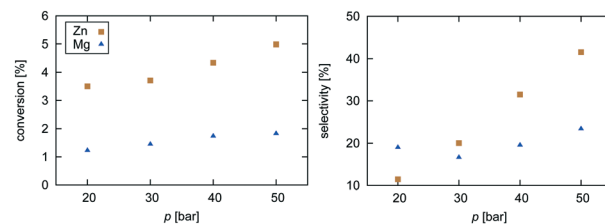


Fig. 2 Experimental data for pressure dependence of selectivity towards CH<sub>3</sub>OH and conversion of CO<sub>2</sub> for the investigated Zn<sub>3</sub>O<sub>3</sub>/Cu and Mg<sub>3</sub>O<sub>3</sub>/Cu catalysts at T = 533 K and GHSV = 6000 h<sup>-1</sup>.

posed.<sup>43,44</sup> From the metallic surface area and dispersion, it is evident that the interaction between copper and zinc is stronger than that between Mg, Cr, and Fe with copper (Fig. 3).

Selectivity is shown only for Zn<sub>3</sub>O<sub>3</sub>/Cu and Mg<sub>3</sub>O<sub>3</sub>/Cu catalysts as they have the best conversion. As expected, the selectivity sharply drops with increasing temperature as RWGS becomes more favourable and more CO is formed. The slightly higher selectivity of Mg<sub>3</sub>O<sub>3</sub>/Cu is in agreement with microkinetic modelling (see Fig. 7 later on), but the overall lower conversion makes this catalyst less suitable anyway. Note that this trend reverses under high pressure.

Pressure dependence was investigated only for Zn<sub>3</sub>O<sub>3</sub>/Cu and Mg<sub>3</sub>O<sub>3</sub>/Cu catalysts at 533 K and GHSV = 6000 h<sup>-1</sup>. Upon increasing the pressure, the chemical potential of CO<sub>2</sub> and H<sub>2</sub> is higher, resulting in higher catalyst surface coverage. As expected, conversion increases as pressure is increased. From simple thermodynamic analysis it follows that selectivity must increase with pressure, also shown by our data. A slight decrease in selectivity over Mg<sub>3</sub>O<sub>3</sub>/Cu when going from 20 to 30 bar is attributed to experimental uncertainty. It is experimentally known that at low pressures, methanol is formed *via* the formate route, but at higher pressure the RWGS route also becomes accessible.<sup>45</sup> We see that except at 20 bar, the selectivity of the Zn<sub>3</sub>O<sub>3</sub>/Cu catalyst is better than that of Mg<sub>3</sub>O<sub>3</sub>/Cu.

### 3.2. Adsorption modes

In Table 2, we show the calculated ZPE-corrected adsorption energies for all the species considered. We list the adsorption

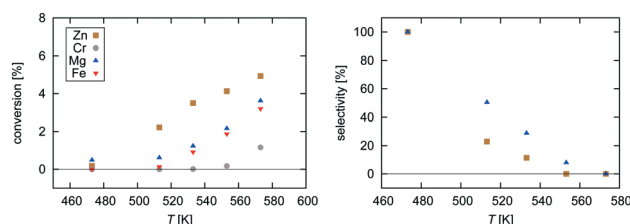
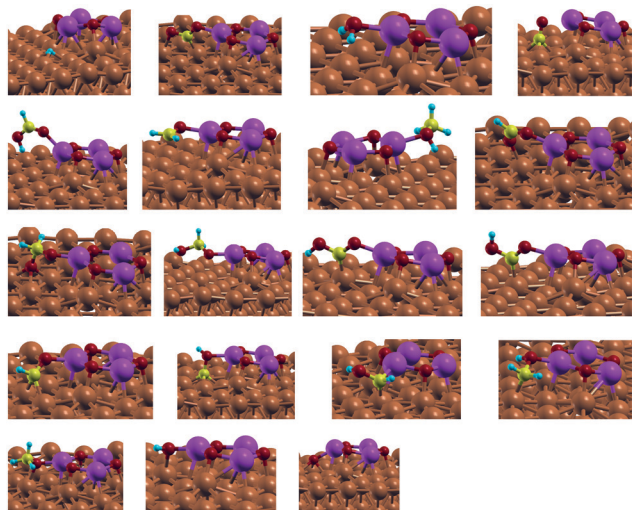


Fig. 3 Experimental data for temperature dependence of selectivity towards CH<sub>3</sub>OH and conversion of CO<sub>2</sub> for all four investigated catalysts at p = 20 bar and GHSV = 6000 h<sup>-1</sup>. Selectivity is shown only for the most active catalysts.

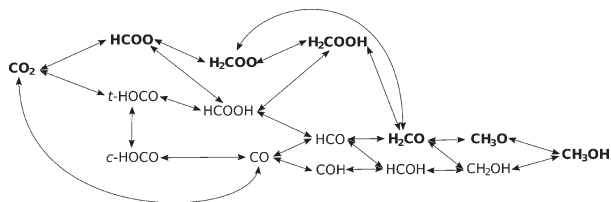
Table 1 Particulate properties of Cu/M catalysts prepared by a co-precipitation method

	Cu/Zn	Cu/Mg	Cu/Cr	Cu/Fe
Cu metallic surface area (m <sup>2</sup> g <sup>-1</sup> )	48	35	21	29
Cu metal dispersion (%)	28	27	17	23
Surface area (m <sup>2</sup> g <sup>-1</sup> )	96	85	29	24
H <sub>2</sub> -TPD (μmol g <sup>-1</sup> )	9.5	7.3	5.8	6.1





**Fig. 4** The most stable adsorption modes of stable intermediates on the active site of the  $\text{Zn}_3\text{O}_3/\text{Cu}$  catalyst. Geometries of the other catalysts are conceptually similar and thus not shown here (except  $\text{CO}_2$  does not adsorb to the Cu/Fe catalyst). From top left: H,  $\text{CO}_2$ ,  $\text{H}_2\text{O}$ , CO, HCOOH,  $\text{CH}_2\text{O}$ ,  $\text{CH}_3\text{OH}$ , HCO,  $\text{H}_2\text{COO}$ ,  $\text{H}_2\text{COOH}$ , *t*-COOH, *c*-COOH, HCO, COH, HCOH,  $\text{CH}_2\text{OH}$ ,  $\text{CH}_3\text{O}$ , OH and O.



**Fig. 5** A schematic overview of all the elementary reaction steps considered. Intermediates along the most probable route are printed in bold. Note that only principal species are written out; hydrogen and oxygen atoms, and hydroxyl groups are implied. For clarity, the dissociation of HCOO into HCO and O is omitted from the figure due to very high activation energy.

energies for each catalyst and the adsorption site. Hydrogen and carbon monoxide bond exclusively to the pure copper surface, while other species can bond to both the  $\text{M}_3\text{O}_3/\text{Cu}$  interface and pure Cu. To keep the model reasonably manageable, we consider only adsorption modes to the interface for these species. Preliminary computations showed that this interaction is in all cases more favourable than binding to pure Cu, which is both an understandable and desirable property of the model.

As follows from basic thermodynamics, adsorption energies are negative. For adsorption to be spontaneous, it has to be exothermic. Molecules lose degrees of freedom upon adsorption, thus decreasing the entropy of the system, which must be offset by a greater release of energy for the Gibbs free energy to be negative.

Hydrogen binds dissociatively to the pure copper surface with very similar adsorption energies (around  $-2.20$  eV). This

**Table 2** ZPE-corrected adsorption energies of all considered species in their most stable adsorption modes for all four studied catalysts

Adsorbate	Site	$E_{\text{ads}}^{\text{ZPE}}$ (eV)			
		$\text{Zn}_3\text{O}_3/\text{Cu}$	$\text{Mg}_3\text{O}_3/\text{Cu}$	$\text{Cr}_3\text{O}_3/\text{Cu}$	$\text{Fe}_3\text{O}_3/\text{Cu}$
<b>Stable molecules</b>					
H	Cu	-2.18	-2.21	-2.28	-2.18
$\text{CO}_2$	Interface	-0.23	-0.80	-0.69	0.00
$\text{H}_2\text{O}$	Interface	-0.79	-1.25	-0.72	-0.67
CO	Cu	-0.65	-1.37	-1.42	-0.81
HCOOH	Interface	-0.59	-1.28	-0.83	-0.70
$\text{CH}_2\text{O}$	Interface	-0.90	-1.46	-1.60	-0.85
$\text{CH}_3\text{OH}$	Interface	-1.09	-1.51	-0.91	-0.94
<b>Intermediates</b>					
HCOO	Interface	-3.13	-3.75	-3.44	-2.99
$\text{H}_2\text{COO}$	Interface	-4.83	-5.22	-5.56	-4.76
$\text{H}_2\text{COOH}$	Interface	-2.92	-3.10	-2.78	-2.84
<i>t</i> -COOH	Interface	-2.16	-2.96	-2.60	-2.22
<i>c</i> -COOH	Interface	-2.30	-2.93	-2.63	-2.26
HCO	Interface	-1.92	-2.38	-2.59	-1.79
COH	Interface	-3.08	-3.65	-3.80	-2.96
HCOH	Interface	-2.64	-2.90	-2.92	-2.25
$\text{CH}_2\text{OH}$	Interface	-1.77	-2.24	-1.81	-1.68
$\text{CH}_3\text{O}$	Interface	-2.84	-3.16	-3.48	-2.60
OH	Interface	-3.49	-3.99	-4.04	-3.24
O	Interface	-5.59	-6.08	-6.36	-5.28

is the only activated adsorption (*cf.* Table 3), as its activation energies range from 0.39 eV on  $\text{Cr}_3\text{O}_3/\text{Cu}$  to 0.55 eV on the  $\text{Mg}_3\text{O}_3/\text{Cu}$  catalyst. Carbon dioxide shows great variations in its affinity to bind to the catalyst.  $\text{CO}_2$  does not bind to Cu/Fe and only weakly physisorbs to  $\text{Zn}_3\text{O}_3/\text{Cu}$  ( $-0.23$  eV), indicative of an Eley–Rideal mechanism.  $\text{Mg}_3\text{O}_3/\text{Cu}$  and  $\text{Cr}_3\text{O}_3/\text{Cu}$ , however, bind  $\text{CO}_2$  quite strongly ( $-0.80$  and  $-0.69$  eV, respectively), following the Langmuir–Hinshelwood mechanism. In all three instances,  $\text{CO}_2$  binds in a bent configuration, with one oxygen atom interacting with the secondary metal and the carbon atom binding to copper.  $\text{Mg}_3\text{O}_3/\text{Cu}$  and  $\text{Cr}_3\text{O}_3/\text{Cu}$  strongly bind CO, as well ( $-1.37$  and  $-1.42$  eV, respectively), as opposed to the moderate interaction of CO with  $\text{Zn}_3\text{O}_3/\text{Cu}$  and  $\text{Fe}_3\text{O}_3/\text{Cu}$  ( $-0.65$  and  $-0.81$  eV, respectively). CO binds in the vicinity of the interface but not at the interface, perpendicularly to the copper surface with the carbon atom interacting with copper. Water binds with its oxygen atom to the secondary metal, while its hydrogen atoms point towards the copper surface. In a similar fashion, HCOOH,  $\text{CH}_2\text{O}$  and  $\text{CH}_3\text{OH}$  also bind to the secondary metal through their oxygen atoms.  $\text{CH}_2\text{O}$  adopts a planar orientation, while HCOOH and  $\text{CH}_3\text{OH}$  orient their hydroxyl hydrogen atoms towards the Cu surface.

While the formate species (HCOO) binds in a monodentate and bidentate configuration on the pure copper surface,<sup>19</sup> it binds solely as bidentate on stepped surfaces.<sup>12</sup> This is also the case in our model, with HCOO binding in a tilted orientation with one oxygen to the metal atom and the other oxygen to copper. Hydroxycarbonyl (COOH) exists in two orientations, either *cis* or *trans* with respect to the C–O bond. Their adsorption energies are similar, although *c*-COOH binds marginally more strongly (except for Cu/Mg).





**Table 3** ZPE-corrected activation energies ( $E_A$ ) and reaction energies ( $\Delta E$ ) for all elementary steps considered at all studied catalysts. Hydrogen surface diffusion is also included

<i>i</i>	Elementary reaction	In eV	Catalyst			
			Zn <sub>3</sub> O <sub>3</sub> /Cu	Mg <sub>3</sub> O <sub>3</sub> /Cu	Cr <sub>3</sub> O <sub>3</sub> /Cu	Fe <sub>3</sub> O <sub>3</sub> /Cu
1	H <sub>2</sub> + 2* → 2 H* (dis. ads.)	$E_A$	0.47	0.55	0.39	0.53
		$\Delta E$	-0.13	-0.20	-0.33	-0.13
2	H* → H* (diffusion)	$E_A$	0.16	0.20	0.24	0.16
3	CO <sub>2</sub> ** → CO* + O*	$E_A$	0.60	0.57	0.78	1.03
		$\Delta E$	+0.06	-0.57	-1.02	-0.06
4	H* + CO <sub>2</sub> ** → HCOO** + *	$E_A$	0.59	0.47	0.71	0.12
		$\Delta E$	-0.65	-0.68	-0.41	-0.80
5	HCOO** → HCO* + O*	$E_A$	1.70	1.93	1.78	1.89
		$\Delta E$	+0.74	+0.41	-0.40	+1.05
6	H* + CO <sub>2</sub> ** → <i>t</i> -COOH**	$E_A$	0.71	0.76	0.88	0.64
		$\Delta E$	+0.10	-0.10	+0.21	-0.24
7	<i>t</i> -COOH** → <i>c</i> -COOH**	$E_A$	0.44	0.55	0.54	0.56
		$\Delta E$	-0.07	+0.10	+0.06	+0.03
8	H* + <i>t</i> -COOH** → HCOOH** + *	$E_A$	0.60	0.60	0.56	0.49
		$\Delta E$	-0.15	-0.01	+0.15	-0.20
9	<i>c</i> -COOH** → OH* + CO*	$E_A$	0.69	1.03	0.84	0.96
		$\Delta E$	-0.18	-0.77	-1.18	-0.13
10	H* + HCOO** → H <sub>2</sub> COO** + *	$E_A$	0.90	1.23	0.74	1.10
		$\Delta E$	+0.32	+0.58	-0.01	+0.24
11	H <sub>2</sub> COO** → CH <sub>2</sub> O* + O*	$E_A$	0.55	0.81	0.49	1.09
		$\Delta E$	+0.14	-0.52	-0.60	+0.44
12	H* + HCOO** → HCOOH** + *	$E_A$	0.92	0.81	1.14	0.77
		$\Delta E$	+0.60	+0.57	+0.77	+0.36
13	HCOOH** → HCO* + OH*	$E_A$	0.80	0.95	0.82	1.21
		$\Delta E$	-0.06	-0.35	-1.05	+0.41
14	H* + HCOOH** → H <sub>2</sub> COOH** + *	$E_A$	0.46	0.78	0.74	0.74
		$\Delta E$	-0.51	+0.03	-0.04	-0.32
15	H* + H <sub>2</sub> COO** → H <sub>2</sub> COOH** + *	$E_A$	0.32	0.89	0.93	0.42
		$\Delta E$	-0.23	+0.02	+0.74	-0.21
16	H <sub>2</sub> COOH** → CH <sub>2</sub> O* + OH*	$E_A$	0.81	0.68	0.03	0.68
		$\Delta E$	+0.16	-0.73	-1.23	+0.37
17	H* + CO* → HCO* + *	$E_A$	0.60	0.59	0.64	0.70
		$\Delta E$	+0.03	+0.31	+0.22	+0.31
18	H* + CO* → COH* + *	$E_A$	1.24	1.92	1.80	1.48
		$\Delta E$	+0.63	+0.81	+0.78	+0.91
19	H* + COH* → HCOH* + *	$E_A$	0.65	0.57	0.50	0.51
		$\Delta E$	-0.45	-0.11	+0.09	-0.18
20	H* + HCO* → CH <sub>2</sub> O* + *	$E_A$	0.41	0.29	0.55	0.33
		$\Delta E$	-0.29	-0.35	-0.22	-0.37
21	H* + HCO* → HCOH* + *	$E_A$	0.93	0.91	1.06	0.98
		$\Delta E$	+0.15	+0.39	+0.65	+0.41
22	H* + HCOH* → CH <sub>2</sub> OH* + *	$E_A$	0.55	0.39	0.83	0.22
		$\Delta E$	-0.52	-0.69	-0.18	-0.83
23	H* + CH <sub>2</sub> O* → CH <sub>2</sub> OH* + *	$E_A$	0.46	0.36	1.07	0.67
		$\Delta E$	-0.08	+0.05	+0.68	-0.04
24	H* + CH <sub>2</sub> O* → CH <sub>3</sub> O* + *	$E_A$	0.38	0.37	0.62	0.20
		$\Delta E$	-0.79	-0.52	-0.64	-0.61
25	H* + CH <sub>2</sub> OH* → CH <sub>3</sub> OH	$E_A$	0.72	0.63	0.79	0.57
		$\Delta E$	-0.92	-0.84	-0.61	-0.86
26	H* + CH <sub>3</sub> O* → CH <sub>3</sub> OH* + *	$E_A$	0.46	0.42	0.80	0.31
		$\Delta E$	-0.20	-0.27	+0.71	-0.29
27	H* + O* → OH* + *	$E_A$	0.74	0.88	0.57	0.85
		$\Delta E$	-0.20	-0.19	+0.12	-0.28
28	H* + OH* → H <sub>2</sub> O + *	$E_A$	0.50	0.47	0.82	0.38
		$\Delta E$	-0.18	-0.10	+0.53	-0.31

Another crucial intermediate is H<sub>2</sub>COO,<sup>49</sup> which plays a vital role in methanol synthesis. It binds to the metal atom with one oxygen and to copper with another oxygen atom. H<sub>2</sub>-COOH is another important intermediate. It binds to the

metal atom with the oxygen atom and to copper through its hydroxyl group, similarly to HCOOH. The methoxy fragment (CH<sub>3</sub>O) assumes a similar configuration to methanol, *i.e.* it binds to the interface through its oxygen atom.

HCO and COH behave noticeably differently. Although both bind to the interface through the oxygen atom and to copper with carbon, HCO assumes a planar orientation, while COH sits upright, similar to CO. HCOH is the only species that binds to the metal atom through carbon and not oxygen. CH<sub>2</sub>OH is oriented similarly to HCO.

Hydroxyl (OH) binds to the interface in a planar orientation through the oxygen atom. Atomic oxygen preferentially binds to the copper plane.

It should be noted that oxygen-containing species bind more strongly to the Mg<sub>3</sub>O<sub>3</sub>/Cu and Cr<sub>3</sub>O<sub>3</sub>/Cu catalysts than to Zn<sub>3</sub>O<sub>3</sub>/Cu and Fe<sub>3</sub>O<sub>3</sub>/Cu. This can be easily explained; Mg is considerably more electropositive than Zn and Fe. Cr on the other hand normally preferentially assumes the oxidation state +3, meaning that it is coordinatively unsaturated with oxygen atoms in the model Cr<sub>3</sub>O<sub>3</sub> moiety. Nevertheless, stronger adsorption to Mg<sub>3</sub>O<sub>3</sub>/Cu and Cr<sub>3</sub>O<sub>3</sub>/Cu reflects better catalytic performance, as shown by microkinetic modelling.

### 3.3. Reaction pathways

A complex network of possible elementary reactions yielding methanol from CO<sub>2</sub> can be constructed. In addition to formate and reverse water-gas shift (RWGS) pathways, various side pathways with somewhat exotic intermediates (such as HOCO, HOCHO or COH) can be proposed. Since our previous work<sup>12</sup> and literature review showed the formate and RWGS pathways to predominate,<sup>13,15</sup> we limit our investigations to these two pathways, resulting in the scheme shown in Fig. 5.

In Table 3, we list all the elementary reaction steps considered with their respective activation barriers and reaction energies on the four investigated catalysts. We also include the dissociative hydrogen adsorption and hydrogen surface diffusion since both processes are activated. From the activation barriers and activation energies, the reaction rates (not shown) in the transition state theory (TST) approximation were calculated as explained in the Methodology section and used in the microkinetic modelling.

**3.3.1. Hydrogen adsorption and diffusion.** Hydrogen adsorbs dissociatively on metallic catalysts. In all our cases, hydrogen adsorbs on the Cu(111) surface on the fcc sites and not on M<sub>3</sub>O<sub>3</sub>. Consequently, the adsorption energy is very similar in all examples. The reaction barrier, however, differs markedly on the account of involvement of M<sub>3</sub>O<sub>3</sub> in the transition state. It is the lowest for Cr<sub>3</sub>O<sub>3</sub>/Cu (0.39 eV) and similar for Zn<sub>3</sub>O<sub>3</sub>/Cu, Mg<sub>3</sub>O<sub>3</sub>/Cu and Fe<sub>3</sub>O<sub>3</sub>/Cu (0.47, 0.55, 0.53 eV, respectively).

It is already well established that the hydrogen spill-over is an important bottleneck in the CO<sub>2</sub> hydrogenation reaction. This fact is nicely reflected in the model used, as hydrogen binds to Cu(111) but the reaction then proceeds at the





interface. Therefore, hydrogen surface diffusion on Cu(111) is also important. This is a fast reaction with activation energies ranging from 0.16 eV on Zn<sub>3</sub>O<sub>3</sub>/Cu to 0.24 eV on Cr<sub>3</sub>O<sub>3</sub>/Cu (*cf.* kMC methodology for necessary artificial downscaling of this reaction rate). The spill-over effect is cumulatively accounted for as hydrogen surface diffusion over Cu(111) and its transfer from Cu(111) to the interface during the elementary reaction steps.

**3.3.2. Carbon dioxide adsorption.** Interestingly, carbon dioxide interacts with the investigated catalysts in three different manners. On Zn<sub>3</sub>O<sub>3</sub>/Cu, CO<sub>2</sub> adsorbs weakly. Although its interaction with the catalyst is only -0.23 eV, its geometry is changed considerably as it assumes a bent orientation. On Mg<sub>3</sub>O<sub>3</sub>/Cu and Cr<sub>3</sub>O<sub>3</sub>/Cu, CO<sub>2</sub> binds much more strongly with -0.80 eV and -0.69 eV, respectively. Interestingly, on Fe<sub>3</sub>O<sub>3</sub>/Cu, CO<sub>2</sub> does not adsorb noticeably.

**3.3.3. Formate pathway.** Making the formate pathway kinetically accessible is paramount for the production of methanol. It has been shown previously and confirmed by our kMC studies (*vide infra*) that the formate pathway is responsible for the production of methanol and that the RWGS pathway is responsible for CO production. The formate pathway consists of the following intermediates: HCOO, H<sub>2</sub>COO, H<sub>2</sub>COOH, CH<sub>2</sub>O, and CH<sub>3</sub>O.

First, adsorbed or gaseous CO<sub>2</sub> is hydrogenated to HCOO. On pure Cu(111), this reaction has a moderate activation energy of 0.62 eV,<sup>19</sup> which is slightly lowered on Zn<sub>3</sub>O<sub>3</sub>/Cu and Mg<sub>3</sub>O<sub>3</sub>/Cu catalysts (0.59 and 0.47 eV, respectively) and higher on Cr<sub>3</sub>O<sub>3</sub>/Cu (0.71 eV). It is less straight-forward to compare this value with the activation energy on Fe<sub>3</sub>O<sub>3</sub>/Cu (0.12 eV) because of a different reaction mechanism.

HCOO could in principle dissociate to HCO and O, but on account of the extremely large activation energies (1.7 eV or larger), it does not. Instead, it forms either H<sub>2</sub>COO on Zn<sub>3</sub>O<sub>3</sub>/Cu (0.90 eV) and Cr<sub>3</sub>O<sub>3</sub>/Cu (0.74 eV) or HCOOH on Mg<sub>3</sub>O<sub>3</sub>/Cu (0.81 eV) and Fe<sub>3</sub>O<sub>3</sub>/Cu (0.77 eV). On pure Cu(111), the activa-

tion barrier for the formation of H<sub>2</sub>COO is 1.20 eV and for HCOOH it is 0.70 eV.<sup>19</sup> This demonstrates the effect of Zn in particular in lowering the overall activation energy and guiding the reaction towards the desirable route. On Zn<sub>3</sub>O<sub>3</sub>/Cu, H<sub>2</sub>COO is hydrogenated to H<sub>2</sub>COOH, while on Cr<sub>3</sub>O<sub>3</sub>/Cu it directly dissociates to H<sub>2</sub>CO and O. On Mg<sub>3</sub>O<sub>3</sub>/Cu and Fe<sub>3</sub>O<sub>3</sub>/Cu, HCOOH is hydrogenated to H<sub>2</sub>COOH. When H<sub>2</sub>COOH is formed, it is then cleaved into CH<sub>2</sub>O and OH.

On all catalysts, CH<sub>2</sub>O is preferentially hydrogenated to CH<sub>3</sub>O, although on Cr<sub>3</sub>O<sub>3</sub>/Cu non-negligible amounts of CH<sub>2</sub>-OH can also form. Either intermediate is then hydrogenated to the final product methanol. All these activation energies are lower than on Cu(111).

**3.3.4. RWGS pathway.** When CO<sub>2</sub> is first hydrogenated on the oxygen atom, yielding *t*-COOH, the reaction follows the RWGS pathway. On all investigated catalysts, this reaction has a higher activation energy than the formation of HCOO, although it is still lower than on pure Cu(111). In a fast subsequent step, *t*-COOH isomerizes into *c*-COOH on Zn<sub>3</sub>O<sub>3</sub>/Cu, Mg<sub>3</sub>O<sub>3</sub>/Cu and Cr<sub>3</sub>O<sub>3</sub>/Cu. On Fe<sub>3</sub>O<sub>3</sub>/Cu, *t*-COOH can also be hydrogenated into HCOOH, which is further converted in the formate pathway. Once *c*-COOH is formed, it decomposes into OH and CO in a very exothermic step.

On Zn<sub>3</sub>O<sub>3</sub>/Cu and Fe<sub>3</sub>O<sub>3</sub>/Cu, CO can either desorb or react further to HCO. On Mg<sub>3</sub>O<sub>3</sub>/Cu and Cr<sub>3</sub>O<sub>3</sub>/Cu, CO is bound more strongly and will preferentially react to HCO. In neither case is COH formed upon hydrogenation of CO. HCO is then further hydrogenated in the consecutive steps to H<sub>2</sub>CO, CH<sub>3</sub>O and CH<sub>3</sub>OH, the last two steps being the same as in the formate pathway.

In any case, CO cannot form through the formate pathway but *via* RWGS.

**3.3.5. CO<sub>2</sub> dissociation.** There is also an alternative route for the production of CO in addition to the aforementioned stepwise reduction *via* the RWGS. It is possible for carbon dioxide to dissociate directly as CO<sub>2</sub> → CO + O. This reaction is less favourable than hydrogenation to HCOO, which is a desirable property for catalysts designed for methanol synthesis. However, the activation energy for direct dissociation is lower than for CO formation through RWGS on Zn<sub>3</sub>O<sub>3</sub>/Cu, Mg<sub>3</sub>O<sub>3</sub>/Cu and Cr<sub>3</sub>O<sub>3</sub>/Cu. This reaction is usually not included in models on simple metallic surfaces.

**3.3.6. Water formation.** Regardless of the reaction route followed, water will inevitably form. Adsorbed O readily reacts with hydrogen to hydroxyl radicals in a slightly exothermic (except on Cr<sub>3</sub>O<sub>3</sub>/Cu) reaction. This reaction is not excessively exothermic and could thus in theory be reversible. However, under high hydrogen pressure, catalyst active sites are saturated with adsorbed hydrogen, making OH decomposition to O and H unlikely. Additionally, the activation barrier for OH hydrogenation to H<sub>2</sub>O is lower than for its decomposition and is moderately exothermic.

In Fig. 6, a potential energy surface for the most probable route on all catalysts is shown.

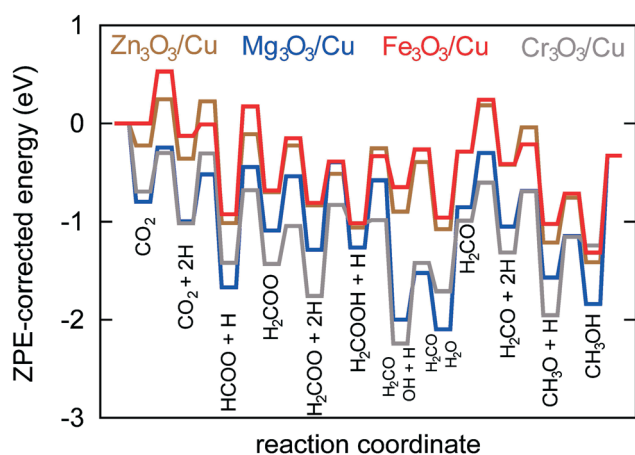


Fig. 6 Potential energy surface for the most probable reaction route on all four studied catalysts. Note that CO<sub>2</sub> does not bind to the Fe<sub>3</sub>O<sub>3</sub>/Cu catalyst, effectively making the reaction follow the Eley-Rideal mechanism.



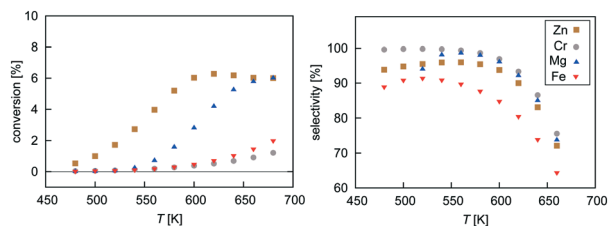


Fig. 7 Temperature dependence of selectivity towards CH<sub>3</sub>OH and conversion of CO<sub>2</sub> for all four investigated catalysts from microkinetic modelling at  $p = 40$  bar and GHSV = 6000 h<sup>-1</sup>.

### 3.4. Microkinetic modelling

Mean-field microkinetics modelling was used to predict the reaction kinetics from first principles, *i.e.* reaction rates obtained taken directly from DFT calculations. The calculated selectivities towards methanol and total CO<sub>2</sub> conversion for all four catalysts are shown as a function of temperature and pressure in Fig. 7 and 8, respectively.

At low temperatures, high selectivities towards methanol are obtained for all catalysts. For the Mg<sub>3</sub>O<sub>3</sub>/Cu catalyst, conversion below 520 K was too low for a meaningful determination of the selectivity. Methanol synthesis from carbon dioxide is an exothermic process, favoured at low temperatures and high pressures. However, high temperatures are needed for a reasonable conversion. Accordingly, selectivities decreased with increasing temperature for all catalysts while conversions increased. Among the catalysts, the highest selectivity was exhibited by Cr<sub>3</sub>O<sub>3</sub>/Cu, but its conversion was the lowest. On the other hand, the Zn<sub>3</sub>O<sub>3</sub>/Cu catalyst had the highest conversion and a reasonable selectivity, making it the most suitable for methanol production. This is in agreement with the fact that Zn<sub>3</sub>O<sub>3</sub>/Cu is predominantly used in industry.

As expected from thermodynamic considerations, an increase in selectivity and conversion with increasing pressure was observed, as shown in Fig. 8. The effect is most pronounced on Zn<sub>3</sub>O<sub>3</sub>/Cu. The only exception was observed for the Mg<sub>3</sub>O<sub>3</sub>/Cu catalyst, where conversion showed a peculiar decrease with increasing pressure. This is due to catalyst surface saturation.

To sum it up, Zn<sub>3</sub>O<sub>3</sub>/Cu showed the best activity among all catalysts considered, especially at lower temperatures, which are more suitable for industrial processes. This is both expected and understandable, since industrially Zn<sub>3</sub>O<sub>3</sub>/Cu is used almost exclusively.

### 3.5. Insights from kinetic Monte Carlo

kMC simulations for each of the four catalysts were performed at various temperatures (ranging from 480 K to 600 K) and pressures (ranging from 20 bar to 60 bar). For each simulation, we randomly chose an initial random seed. We studied how the overall selectivity towards methanol, relative frequencies of the reaction steps, and lattice coverage change over time as a function of temperature and pressure.

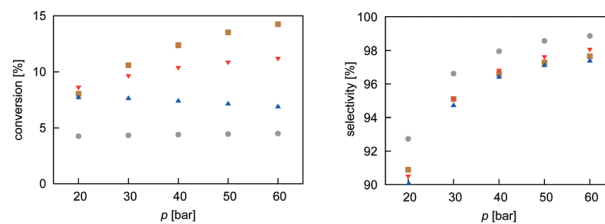


Fig. 8 Pressure dependence of selectivity towards CH<sub>3</sub>OH and conversion of CO<sub>2</sub> for all four investigated catalysts from microkinetic modelling at  $T = 540$  K and GHSV = 6000 h<sup>-1</sup>. Colour code as in Fig. 7.

The simulations ran for five days (elapsed wall time 432 000 s), each on a single core, reaching the typical simulation times between 10<sup>-4</sup> s and 10<sup>-2</sup> s, depending on the pressure, temperature, and catalyst. On average, 3 × 10<sup>7</sup> kMC steps (events) occurred during a simulation.

Fig. 9 shows selectivity towards methanol at various temperatures and pressures for each catalyst. The selectivity peaks at 97% for high pressure and low temperature for each catalyst type but drops with decreasing pressure and increasing temperature (*i.e.* at 600 K selectivity for Mg<sub>3</sub>O<sub>3</sub>/Cu catalyst drops below 80%). The best catalysts in terms of selectivity are Cr<sub>3</sub>O<sub>3</sub>/Cu and Zn<sub>3</sub>O<sub>3</sub>/Cu, which also show the most stable behaviour across the whole temperature and pressure range. Fig. 9 also shows the production of CH<sub>3</sub>OH and CO in terms of the total number of molecules produced in the simulations, again as a function of temperature or pressure. We see that the temperature dependence is much stronger than the pressure dependence. This is expected as higher temperatures accelerate the rate of all reactions. Trends in selectivity and CH<sub>3</sub>OH and CO production are in good agreement with experimental data (*cf.* sections 3.1 and 4).

As seen in Fig. 7, HCOO is the most abundant species on the surface until very late. This is in line with recent studies which show that formation of methanol is mainly controlled by the surface coverage of formate and hydrogen at the steady state.<sup>50</sup>

To show the behaviour of the active catalyst in more detail, we plot in Fig. 10 (see also the ESI† for the animated video) a

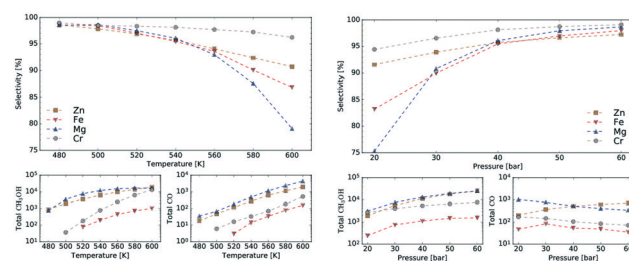


Fig. 9 Temperature (left) and pressure (right) dependence of selectivity towards CH<sub>3</sub>OH for all four investigated catalysts, as obtained from kMC simulations at  $P = 20$  bar (left) and  $T = 540$  K (right). Smaller plots show the total number of CH<sub>3</sub>OH and CO molecules produced during the runtime of the simulation. Increase of selectivity with decreasing temperature and increasing pressure is observed.



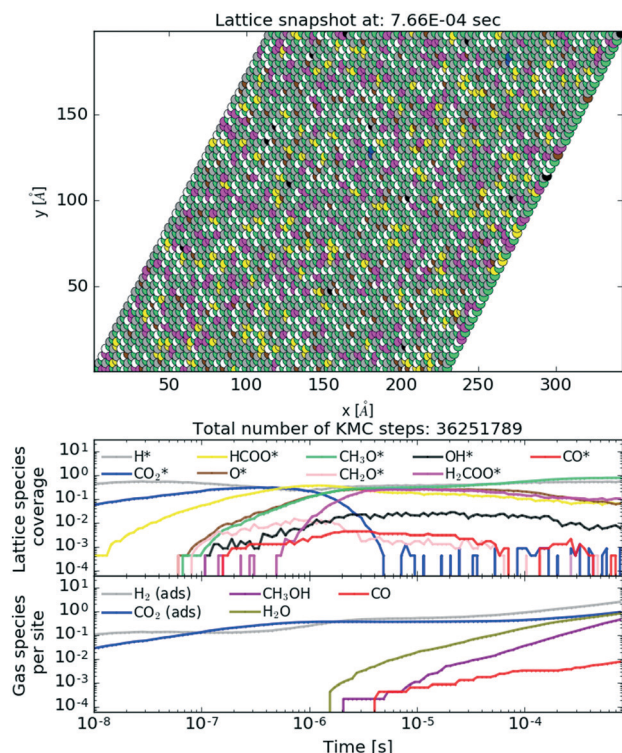


Fig. 10 Lattice snapshot plot at  $8 \times 10^{-4}$  s (top) with temporal evolution of lattice coverage (middle) and gas fraction composition (bottom) for the  $\text{Cr}_3\text{O}_3/\text{Cu}$  catalyst. See the ESI† for the animated video.

snapshot of the lattice coverage for the  $\text{Cr}_3\text{O}_3/\text{Cu}$  catalyst at  $T = 500$  K and  $P = 40$  bar upon reaching a steady state and temporal evolution of lattice coverage and gaseous fraction composition. In the top plot, the most abundant intermediates on the lattice are  $\text{CH}_3\text{O}$  and  $\text{H}$ , which recombine into  $\text{CH}_3\text{OH}$ . This particular reaction is among the most frequent reactions for the  $\text{Cr}_3\text{O}_3/\text{Cu}$  catalyst, as depicted in Fig. 11.

From the lattice coverage evolution in Fig. 10, we see that the stationary conditions on the lattice are reached after  $\sim 5 \times 10^{-6}$  s; thereafter production of gaseous species follows at a constant rate. Similar timescales are also apparent for other studied catalysts. Our simulations reached typical times of  $10^{-3}$  s, which is sufficient to reach steady state conditions. To make sure of that, one simulation for the  $\text{Zn}_3\text{O}_3/\text{Cu}$  catalyst at  $T = 500$  K and  $P = 40$  bar was run for twice as long (wall time of 10 days). The obtained results were consistent.

Fig. 11 shows the frequency of the reaction steps for all four catalysts for  $T = 500$  K and  $P = 40$  bar. The frequency is defined as the number of instances a particular reaction step occurred per active site divided by the total simulation time. The event frequency distribution shows that the reaction pathway towards methanol production differs among the catalysts (*cf.* section 4). There are greater differences observed between  $\text{Mg}_3\text{O}_3/\text{Cu}$  and  $\text{Fe}_3\text{O}_3/\text{Cu}$  catalysts, which have much poorer selectivities. In contrast,  $\text{Zn}_3\text{O}_3/\text{Cu}$  and  $\text{Cr}_3\text{O}_3/\text{Cu}$  have better selectivity and are also more comparable.

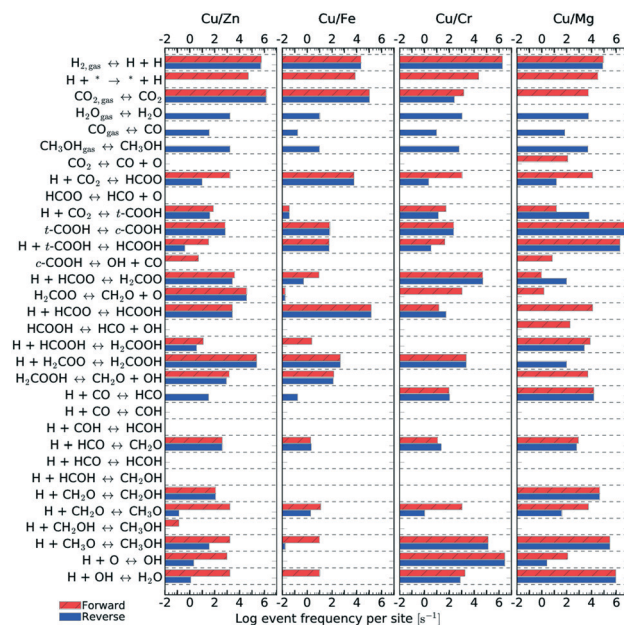


Fig. 11 Elementary step frequency for the case of  $T = 500$  K and  $P = 40$  bar, for all four types of catalysts. Red steps indicate forward reactions, while blue ones indicate reverse reactions.

## 4. Discussion

We have synthesised a commercial-like  $\text{Zn}_x\text{O}_y/\text{Cu}$  catalyst for carbon dioxide hydrogenation to methanol and three variants where Zn has been substituted with Mg, Fe and Cr. These three metals have been chosen as the most active ones among a larger battery of synthesised catalysts (including Ca, Sr, Ba, Ni, Mn, Co). Although a commercial catalyst could have been purchased, we opted for in-house synthesis. This allowed us to avoid potential effects of unwanted components (binders, stabilisers *etc.*) and impurities that might be present in the commercial catalyst.

The activity of all four synthesised catalysts has been tested experimentally. Extensive multiscale modelling has been performed to account for the observed trends in catalytic activity, conversion and selectivity. Our aim was to describe their performance solely from catalyst characterisation (Table 1) and first-principles calculations without any input of catalytic performance and then compare these results with experimental data.

In catalyst modelling, a compromise had to be struck between the veracity of the catalyst description, computational tractability and comparability of the four tested catalysts. In reality, every catalyst has many different active sites. In addition to different surface planes, kinks, steps, defects and lattice strain also play important roles.<sup>51,52</sup> Experimentally observed catalytic activity is thus an amalgam of activities of all present active sites, while in DFT calculations we can only manageably follow the reaction on one active surface. Thus, a  $\text{M}_3\text{O}_3$  active cluster deposited on Cu(111) has been selected as the most suitable depiction of the active site.





It should be noted that  $M_3O_3$  is a model cluster and by no means the only or even predominant structure in the real catalyst. To thoroughly analyse the exact oxide stoichiometry on the catalyst, a comprehensive thermodynamic analysis would have to be performed. This would further complicate an already complex model, which focuses on the kinetic considerations and not phase stability.

A comprehensive reaction pathway with all possible interconversions has been proposed (Fig. 5) and calculated (Tables 2 and 3). Although often used to predict the most probable reaction route and rate-determining steps, solely DFT results cannot provide this information in the case of a complex and intertwined reaction scheme. In our case, we see that the hydrogenation of  $CO_2$  first leads to HCOO and not *t*-COOH. In further reactions, however, their reversibility means that the actual pathway will be more complex than a simple potential energy surface (Fig. 4) would lead us to assume. Thus, a micro-kinetic analysis is essential.

In our micro-kinetic model, no assumptions about the reaction pathway have been made. Instead, all possible reactions have been included. This means that the included reactions spanned a large range of rates, making the model numerically challenging. Due to the stiffness of the system, the ode23s solver was used with very tight convergence criteria and short time steps. All reaction steps were scaled down but our preliminary testing showed that this did not impact the results noticeably. The calculation times (wall time) also varied from a few seconds to a few hours, depending on the conditions imposed (temperature, pressure, GHSV, influx composition). To test the reliability of the results, we made sure that the output did not vary upon changing the convergence criteria and that trends across temperatures and pressures did not show any outliers.

From micro-kinetic modelling, selectivity towards methanol and conversion were obtained for each catalyst under various operating conditions. Selectivities show expected trends. In general, they decrease with temperature and are above 90% in the operating range. This is consistent with our choosing the four most active catalysts among many synthesised. It might seem odd that the  $Cr_3O_3/Cu$  catalyst exhibits the highest selectivity but it is only marginally higher than those of  $Mg_3O_3/Cu$  and  $Zn_3O_3/Cu$ . However, the conversion of  $Cr_3O_3/Cu$  and  $Fe_3O_3/Cu$  catalysts is very poor, making their overall activity low. We see that conversion on  $Zn_3O_3/Cu$  and  $Mg_3O_3/Cu$  catalysts plateaus above 650 K, reaching thermodynamic equilibrium. For pressure dependence, the anticipated and experimentally measured effects are smaller, again evidenced by micro-kinetic modelling. In general, selectivity and conversion should increase with pressure, which is also the case except for conversion on Mg, where a slight decrease with pressure is observed.

Micro-kinetics employs a mean-field approximation. Thus, it only deals with average values for surface coverage with each species. In reality, surface diffusion plays an important role and two reactants can only react if they are adsorbed on adjacent sites. In our case, this limitation is not particularly

severe because catalysts can be considered covered with atomic hydrogen (evidenced also by kinetic Monte Carlo simulations), which is one reactant in all elementary reactions with two reactants. For decomposition reactions (e.g.  $H_2COOH^* \rightarrow H_2CO^* + OH^*$ ), an empty site is needed in the vicinity of the adsorbed species. This is implicitly accounted for with treating all species with two oxygen atoms as bidentate. Such an assumption is well founded on DFT-obtained geometries (Fig. 4).

From kMC simulations, we see that selectivity towards methanol is favoured at low temperatures and high pressures, as expected from thermodynamics and experiments. kMC results compare favourably with those of micro-kinetic modelling, although they differ in some details. This is expected and cannot be avoided since the methods use different assumptions. kMC is not a mean-field approach but instead explicitly treats every active site on the catalytic surface. It is thus crucial to accurately describe adsorption and surface diffusion. Although we performed micro-kinetic modelling for a CSTR, which is the closest to the conditions in kMC, they are not the same. In current kMC implementation in Zacros, the gas composition above the catalyst is considered constant. Any side products that would possibly desorb (such as HCOOH or  $CH_2O$ ) can never re-adsorb due to their gaseous phase concentration being zero. To avoid this, desorption of stable side products (except for CO) has been switched off. Micro-kinetic modelling and experiments showed that this is a reasonable assumption.

kMC can also provide information on the relative frequency of particular elementary steps, which helps determine the dominant reaction pathway, which cannot be surmised from micro-kinetic modelling. As shown in Fig. 11, the relative frequencies span many orders of magnitude. Adsorption of  $CO_2$  and hydrogen surface diffusion were artificially slowed down as described in section 2.4. Therefore, only the selectivities are meaningful and we do not report the conversions. A productivity measure is the total number of  $CH_3OH$  and CO molecules produced during the runtime of the simulation, which is reported for the same time for all catalysts.

From the relative frequencies, we see that the reaction pathway is slightly different on different catalysts. On  $Zn_3O_3/Cu$ , the following intermediates are formed: HCOO,  $H_2COO$ ,  $H_2COOH$ ,  $CH_2O$ ,  $CH_2OH$  and  $CH_3O$ . On  $Fe_3O_3/Cu$  and  $Cr_3O_3/Cu$ ,  $CH_2OH$  does not form. On  $Mg_3O_3/Cu$ , HCOOH is an important intermediate, as well. This is also the only catalyst where direct  $CO_2$  dissociation into CO and O occurs. In line with the generally low activity and selectivity of  $Fe_3O_3/Cu$ , we see that all reactions are less frequent on this catalyst. When comparing the catalysts with the best selectivity ( $Zn_3O_3/Cu$  and  $Cr_3O_3/Cu$ ), we notice additional differences, such as  $CH_2O$  (which is then further hydrogenated to methanol) being produced mainly from  $H_2COOH$  on  $Zn_3O_3/Cu$  and from  $H_2COO$  on  $Cr_3O_3/Cu$ .

The overall agreement between experimental results, micro-kinetic modelling and kinetic Monte Carlo simulations is remarkable. Exact reproduction of experimental data is





currently out of scope even for state-of-the-art theoretical methods, but very good approximations can be achieved. It should be noted that this model is an approximation of the real conditions and cannot be expected to quantitatively recapture every experimental nuance. There is admittedly room for improvement. For instance, for CO and several other species multiple adsorption modes could be considered. As CO binds less strongly on Cu(111) far from the interface, this would increase its production and bring theoretical predictions even more in line with experimental measurements. However, such extensions are beyond the scope of this work.

Experimentally, conversion is the highest for  $\text{Zn}_3\text{O}_3/\text{Cu}$ , followed by  $\text{Mg}_3\text{O}_3/\text{Cu}$ ,  $\text{Fe}_3\text{O}_3/\text{Cu}$  and  $\text{Cr}_3\text{O}_3/\text{Cu}$  (Fig. 2). This is exactly the same order as that obtained from microkinetics (Fig. 7). Selectivity is better for  $\text{Mg}_3\text{O}_3/\text{Cu}$  than for  $\text{Zn}_3\text{O}_3/\text{Cu}$  at moderate pressures. Again, microkinetics provides the same information. The same trend is also discovered by kMC simulations at moderate temperatures (up to 540 K). At higher temperatures, however, the trend is different as the selectivity on  $\text{Mg}_3\text{O}_3/\text{Cu}$  plummets. Similarly, pressure dependence trends show very good agreement.

## 5. Conclusions

Among several synthesised copper-based catalysts for  $\text{CO}_2$  hydrogenation to methanol, the four best performing ones were selected. Experimental testing across a wide range of temperatures and pressures was performed to determine and quantify their activity. A comprehensive reaction framework of all possible elementary steps was established. An atomistic model for each catalyst was constructed based on the characterisation data. All reactions were calculated from first-principles using each model. Results were used for microkinetic modelling and kinetic Monte Carlo simulations.

Very good agreement between experimental measurements of catalytic activity and modelling data is a strong indication that the proposed model is correct. Remarkably, although absolutely no input from experimental data on catalytic activity was used for modelling, first-principles modelling very well described the temperature and pressure trends in selectivity and conversion. This agreement allows us to trust additional data that only theoretical methods could provide, such as coverage and relative reaction step frequency.

Several conclusions can be drawn from the presented data. First and foremost, the formate pathway has been irrefutably proved to account for the bulk of methanol production, both by DFT analysis alone and statistics from kMC simulations. It predominates on all copper-based catalysts regardless of the second metal. Secondly, the superiority of the  $\text{Zn}_3\text{O}_3/\text{Cu}$  catalyst has been proved experimentally and computationally. No other copper-based catalyst has been found to have better of similar performance. Thirdly, we have shown that microkinetic modelling and kMC simulations present an important complement to DFT results, as naïve interpretation and back-of-the-envelope estimations of the latter do not offer adequate insight into the reaction mechanism.

## Conflicts of interest

The authors declare no conflicts of interest.

## Acknowledgements

This work was made possible by funding from the EU Framework Programme for Research and Innovation Horizon 2020 under grant agreement No. 637016 (Project MefCO2) and the Slovenian Research Agency (ARRS) through Core Grant P2-0152.

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