1. Introduction

Beyond the concept of conventional appliances, electronics is rapidly evolving toward a new paradigm of deformable electronics, where electronic devices can be deformed into various shapes. Stretchable electronics, in particular, is the most sophisticated form of deformable electronics in that it involves state-of-the-art technologies developed through the collaboration of various disciplines, ranging from materials science to electrical and mechanical engineering.\(^1\)\(^-\)\(^3\) Potential products employing stretchable electronics exhibit unprecedented attractive applications that strongly appeal to users. Typical examples include wearable healthcare devices, artificial skin and muscles, human–machine interfaces, stretchable displays, and stretchable batteries.\(^4\)-\(^10\)

As well described in some excellent previous reports,\(^1\)\(^,\)\(^11\)\(^,\)\(^12\) stretchable conductors, among various components, are one of the most important building blocks of stretchable electronics because electrodes and interconnects occupy a very large area portion of electronic devices, thereby absorbing most of the externally induced physical strains. Imparting optical transparency to stretchable electrodes is particularly important for the realization of stretchable optoelectronics, such as stretchable displays,\(^9\)\(^,\)\(^13\) photovoltaics,\(^14\) touch panels,\(^15\) and smart contact lenses.\(^16\) However, maintaining acceptable electrical and optical performances under mechanical elongation is not readily achieved even with flexible electrodes because a higher level of deformation is required for stretching or twisting than for bending. Therefore, extensive efforts have been recently dedicated to discovering alternative stretchable transparent electrodes beyond flexible transparent electrodes.

In most cases, the stretchability of transparent electrodes is rendered by certain structural configurations rather than by exploiting intrinsic properties of materials. Generally, these structural configurations include out-of-plane and in-plane structures of conducting materials. Three-dimensional wavy, crumpled, or coiled shapes are examples of the out-of-plane structure, whereas two-dimensional percolation networks and mesh-like geometries belong to the in-plane structure.

In this mini review, we focus specifically on stretchable transparent thin-film electrodes based on in-plane configurations. In section 2, we compare two distinctive strategies (i.e., out-of-plane and in-plane structure-based approaches) for the realization of stretchable transparent electrodes. Graphene- and conducting polymer-based electrodes are described to compare the two above-mentioned strategies. In sections 3–5, we elucidate the recent advances in stretchable transparent electrodes based on metal nanowires, metal nanomeshes, carbon nanotubes (CNTs), and some other unique approaches. Lastly, in section 6, we discuss present challenges and future directions for stretchable transparent electrodes.
2. Approaches based on out-of-plane or in-plane structures

Stretchability of transparent electrodes is usually achieved by structural configurations that accommodate most of the strain under mechanical deformation, thereby rendering little strain to the conducting material itself. These structural configurations can be classified into two approaches: out-of-plane and in-plane structures. The most common out-of-plane structure is the ‘wavy’ structure. The wavy structures can be generally obtained by depositing conductive materials on pre-strained elastomeric substrates, which are subsequently released to allow those conductive films to spontaneously form periodic wavy structures (Fig. 1a). In this wavy structure, most of the induced strain is absorbed by structural changes (i.e., increased buckling wavelengths and decreased buckling amplitudes), which is similar to accordion bellows. In addition to the simple wavy structures, some other out-of-plane structures have been explored as well, including coiled or spring-like structures.20,21

Graphene is a good example of a stretchable transparent electrode with out-of-plane configuration. Graphene has superior properties, such as high charge carrier mobility, mechanical robustness, chemical stability, and optical transparency and therefore has been investigated in numerous research areas.22–25 Because graphene can be synthesized on large-area templates26 and transferred onto specific substrates,27 many applications have been reported utilizing graphene as electrodes for transistors, supercapacitors, and displays.11 Various flexible devices exploiting the flexibility of graphene have also been demonstrated.28–30 However, despite the superb flexibility of graphene, a stretching-induced tensile strain over 6% causes mechanical failure of graphene due to the fractures within the unique honeycomb structure.27 Thus, the stretchability of graphene electrodes is usually achieved by imparting some structural configurations to graphene films. Recent studies revealed that wrinkled31 or crumpled7 graphene (i.e., graphene films with out-of-plane structures) can endure mechanical deformation, such as bending, distortion, and stretching. Chen et al.31 introduced wrinkled graphene synthesized on a wavy Cu template, showing that wrinkled graphene is able to maintain electrical performances under a strain of up to 40%. Zang et al.7 reported crumpled graphene prepared by transferring graphene onto a polydimethylsiloxane (PDMS) substrate with a pre-strain ($\varepsilon_{\text{pre}}$) of 400%, followed by the release of the pre-strained elastomer. This crumpled graphene sustained acceptable electrical properties during repeated stretching up to the level of the pre-strain. Such out-of-plane structured graphene films were applied to supercapacitors34 and artificial-muscle actuators.7 We observed the surface morphology change of a wrinkled graphene film, which was deposited on a pre-strained PDMS substrate ($\varepsilon_{\text{pre}}$ = 10%), upon stretching and releasing, as shown in Fig. 1b. As the film stretches from the released state to the fully stretched state ($\varepsilon$ = 10%), the film flattens out, becoming almost completely flat at 10% stretching. The graphene film recovers its wrinkled structure upon releasing. This structural change depending on the degree of stretching induces variations in optical transmittance due to light scattering on the surface (the bottom left plot of Fig. 1b), which is unfavourable for transparent electrode applications. Zang et al.7 also reported decreasing transmittance of the crumpled graphene electrode as the pre-strained substrate is released, as shown in Fig. 1c.

Similar to graphene, stretchable transparent electrodes using poly(3,4-ethylenedioxythiophene):poly(styrenesulfonate) (PEDOT:PSS), a representative conducting polymer, have been demonstrated by applying out-of-plane structures to PEDOT: PSS layers. Although PEDOT:PSS has been considered as a promising material for optoelectronics due to its low-cost processability via solution processes, a limited strain sustainability (<5%) restricts its use for stretchable electronics without the aid of structural configurations. Lipomi et al.14 successfully demonstrated a stretchable transparent PEDOT:PSS electrode for organic photovoltaics (OPVs) with a buckling structure. The resulting PEDOT:PSS electrode, made on a pre-strained elastomeric substrate, exhibited a stretchability of 20% (up to the pre-strain) with a sheet resistance of 750 Ω sq$^{-1}$ and transmittance of 96%. Vogueritchian et al.32 described the use of Zonyl fluorosurfactant to enhance the processability and electrical conductivity of PEDOT:PSS through controlled wettability and phase segregation. A stretchable transparent electrode was fabricated by spin-coating the mixed solution on a pre-strained PDMS substrate ($\varepsilon_{\text{pre}}$ = 15%) and subsequent releasing, providing buckles or waves (Fig. 1d). The resulting electrode showed a sheet resistance of 46 Ω sq$^{-1}$ with 82% transmittance (measured on a glass substrate) and reversible stretchability, with no change in resistance during 5000 cycles of 10% stretching. A similar approach was introduced by Seol et al.,34 where PEDOT:PSS was mixed with functionalized reduced graphene oxide. The electrode, fabricated by coating this mixture on a pre-strained PDMS substrate, exhibited a sheet resistance of ~68 Ω sq$^{-1}$ with 86% transmittance (measured on a glass substrate) and reversible stretchability to the level of pre-strain ($\varepsilon = 15\%$).

Further stretchability can be achieved by fabricating devices on ultra-thin polymer substrates, such as 1.4 μm-thick polyethylene terephthalate (PET) films, and laminating them onto a pre-strained elastomer.4,8,17,35 The use of ultra-thin substrates leads to a decreased bending-induced strain within buckles, thereby giving rise to a finer wavy structure upon releasing of the pre-strain, which eventually renders improved stretchability. A PEDOT:PSS transparent electrode adopting this strategy showed excellent stretchability (resistance increased by 30% during 10 000 cycles of 50% stretching).17

Although the above-mentioned approaches render a high-level of stretchability to graphene and PEDOT:PSS electrodes, the out-of-plane morphology is also accompanied by several undesirable aspects. First, the corrugated or wrinkled out-of-plane structure causes significant light scattering on the surface, which in turn reduces the specular transmittance and raises the haziness of transparent electrodes, as described
above (Fig. 1b, c and e). In addition, the direction of stretchability is restricted by those of the pre-strain, while this pre-stretching scheme also presents a challenge for large-area fabrication. Lastly, the change of morphology of electrodes is likely to induce unreliable device operation for different levels of stretching.
Considering the above limitations of out-of-plane approaches, much effort has been dedicated to develop in-plane-structure-based stretchable transparent electrodes. Typical examples of in-plane structures include percolation networks of one-dimensional nanomaterials, such as metal nanowires and CNTs, as well as metal nanomeshes made of ultra-long metal nanofibers or nanotroughs. These entangled web-like structures maintain their conductive pathways even under mechanical deformation owing to the structural reconfiguration through sliding or rotating of nanomaterials against each other. In the following sections, various approaches toward the realization of in-plane-structure-based stretchable transparent electrodes are described. The overall performances of stretchable transparent electrodes based on in-plane structures are summarized in Table 1.

## 3. Metal nanowires

Stretchable transparent electrodes based on in-plane configurations employing one-dimensional (1D) nanomaterials have attracted much interest with an aim to overcome the above-mentioned drawbacks of out-of-plane structure-based stretchable electrodes. 1D nanomaterials with high aspect ratios, such as CNTs and metal nanowires, can organize entangled percolating networks using diverse techniques, including spin coating, spray coating, and drop coating. Among various 1D nanomaterials, metal nanowires have been studied extensively due to their high electrical conductivity and mechanical ductility.

### 3.1. Ag nanowires

Ag is the most widely explored metal in its nanowire form owing to its highest electrical conductivity among various metals. Therefore, much effort has been dedicated to deposit Ag nanowires (AgNWs) on various substrates. AgNWs can be synthesized using various methods, such as the hydrothermal method, polyol process, microwave-assisted process, electrochemical technique, UV irradiation technique, and template-assisted technique. Prior to the emerging interest in stretchable electronics, AgNW was investigated as a promising material for flexible and transparent electrodes. Early flexible transparent electrodes exploiting AgNWs were fabricated using several techniques, such as vacuum filtration or Meyer rod coating. These AgNW films were revealed to be thermally/chemically stable, as they maintained good conductivity even after the exposure to heat, water, and organic solvents (e.g., acetone and isopropyl alcohol). However, as-prepared AgNW networks on substrates are not favourable in terms of the surface roughness, and hence many studies have reported several methods to improve the roughness, such as the coating of PEDOT:PSS over the percolation network and the embedding of AgNWs into substrates. These AgNW electrodes with improved roughness were used to demonstrate flexible solar cells and light-emitting diodes (LEDs). Much effort has also been made to enhance the electrical performances of AgNW films by reducing junction resistance or increasing percolation paths. This has been achieved by employing various welding techniques or by introducing additional materials into the percolation networks.

During the improvement of properties and fabrication steps, stretchable transparent electrodes based on AgNWs have been studied at the same time to demonstrate stretchable devices. Akter et al. provided a stretchable AgNW electrode by improving adhesion between a polymer substrate and AgNW networks using poly-dopamine. Spray-deposited AgNW electrodes showed excellent properties with a low sheet resistance of 35 Ω sq⁻¹, high transmittance of about 80%, and an unchanged sheet resistance of up to 15% elongation. However, AgNW films that are directly coated on the substrate have undesirable high surface roughness. Alternatively, Pei's group contrived the embedding method where AgNWs are embedded in various polymer substrates, such as poly(tert-butylacrylate-co-acrylic acid), poly(urethane acrylate), and ethoxylated bisphenol A dimethacrylate with aromatic monomers. Adding acrylic acid (AA) into the polymer could improve the interactions between the polymer composite and AgNW networks. Fig. 2a and b show the effective transfer of the AgNWs into the polymer composite using AA. These fabricated transparent and stretchable electrodes were capable of being used for actuators and polymer light-emitting electrochemical cells (PLECs), as shown in Fig. 2c. More recently, Wang et al. reported a surfactant-assisted method using Zonyl fluorosurfactant to reduce the process temperature. They demonstrated that the AgNW/PDMS polymer composite with a sheet resistance of 4.5 Ω sq⁻¹ and a transmittance of 80% could stretch up to 100% with resistance increased by 32.8%.

The single material of AgNW has clear limitations, such as high inter-nanowire junction resistances, dependence of sheet resistance on pattern sizes, chemical oxidation, and failure due to electrical breakdown. Therefore, the formation of hybrid structures with graphene oxide (GO), CNT, and graphene has been investigated to complement the limitations. As shown in Fig. 2d, the GO–AgNW network fabricated by soaking the AgNW film into the GO dispersion was introduced by Pei's group to reduce the junction resistance without any heat treatment. Here, GO flakes provided a soldering effect between crossed AgNWs. This microstructure of the GO–AgNW was applied to a LED with 14 Ω sq⁻¹ sheet resistance and 88% transmittance at 550 nm. The LED still operated even after 100 stretching cycles of 40% strain. More recently, hierarchical multiscale hybrid AgNW/CNT nanocomposites were introduced to achieve a high level of mechanical compliance, conductivity, and transparency, simultaneously. In this hierarchical nanocomposite, CNTs wrap the AgNW junctions and prevent the separation of junctions even at harsh stretching conditions. Although this work used the pre-strain method (εpre = 150%), the composite electrode retained its functionality even under a strain of 400%. The schematic and scanning electron microscopy (SEM) images of nanocomposites based on longer (thicker) AgNWs (diameter: ~150 nm, length: ~50–100 μm) and shorter
Table 1  Summary of the performances of stretchable transparent electrodes based on in-plane structures

<table>
<thead>
<tr>
<th>Materials</th>
<th>Transmittance</th>
<th>Electrical property</th>
<th>Stretchability</th>
<th>Reliability (cyclic test)</th>
<th>Applications</th>
<th>Ref.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Graphene</td>
<td>∼80%</td>
<td>~280 Ω sq⁻¹</td>
<td>Mechanical failure above ~6% stretching (without pre-strain)</td>
<td>3 cycles (ε ~ 6%)</td>
<td>LEDs</td>
<td>27</td>
</tr>
<tr>
<td>AgNW (spray coating)</td>
<td>80%</td>
<td>35 Ω sq⁻¹</td>
<td>Rs almost unchanged (ε ~ 15%)</td>
<td></td>
<td>PLECs</td>
<td>5</td>
</tr>
<tr>
<td>AgNW (drop-casting/embedded)</td>
<td>80%</td>
<td>88.6 Ω sq⁻¹</td>
<td>Rs &lt; 10 kΩ sq⁻¹ (εmax = 160%)</td>
<td>5000 cycles (ε ~ 90%)</td>
<td>Actuators</td>
<td>54</td>
</tr>
<tr>
<td>AgNW (embedded)</td>
<td>80%</td>
<td>10 Ω sq⁻¹</td>
<td>Stable within εmax = 120%</td>
<td>1000 cycles (ε ~ 30%)</td>
<td></td>
<td>9</td>
</tr>
<tr>
<td>AgNW (drop-casting/embedded)</td>
<td>80%</td>
<td>10 Ω sq⁻¹</td>
<td>Rs (50.8 Ω sq⁻¹) increased by 11.7 times (ε = 33%)</td>
<td>600 cycles (ε ~ 50%)</td>
<td>LEDs</td>
<td>55</td>
</tr>
<tr>
<td>AgNW (spray coating/embedded)</td>
<td>80%</td>
<td>15 Ω sq⁻¹</td>
<td>Rs increased by 8.5 times, 600 cycles (ε ~ 50%)</td>
<td>100 cycles (ε ~ 40%)</td>
<td>Photodetectors</td>
<td>56</td>
</tr>
<tr>
<td>AgNW/GO (bar coating)</td>
<td>88%</td>
<td>25 Ω sq⁻¹</td>
<td>Rs increased slightly, 50 cycles (ε ~ 50%)</td>
<td>100 cycles (ε ~ 40%)</td>
<td>PLEDs</td>
<td>13</td>
</tr>
<tr>
<td>AgNW/CNT (solution filtration)</td>
<td>&gt;90%</td>
<td>24–27 Ω sq⁻¹</td>
<td>Stable within εmax &gt; 460% (pre-strain: 150%)</td>
<td></td>
<td>LEDs, TSPs</td>
<td>15</td>
</tr>
<tr>
<td>AgNW/graphene (spin coating)</td>
<td>94%</td>
<td>33 Ω sq⁻¹</td>
<td>Negligible resistance change within ε = 100%</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>AgNW/graphene (spin coating)</td>
<td>94%</td>
<td>33 Ω sq⁻¹</td>
<td>Negligible resistance change within ε = 100%</td>
<td>Negligible resistance change, 10 000 cycles (ε = 100%)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>AgNW/graphene (spin coating)</td>
<td>90%</td>
<td>25 Ω sq⁻¹</td>
<td>FET arrays: stable within εmax = 20%</td>
<td></td>
<td>Biosensors</td>
<td>6</td>
</tr>
<tr>
<td>AgNW/graphene</td>
<td>80–92%</td>
<td>98.8 Ω sq⁻¹</td>
<td></td>
<td></td>
<td>Interactive human–machine interfaces</td>
<td>57</td>
</tr>
<tr>
<td>Cu@Cu-Ni NW (embedded)</td>
<td>80%</td>
<td>62.4 Ω sq⁻¹</td>
<td>Resistance increased by 3 times (ε ~ 20%)</td>
<td>600 cycles (ε ~ 20%)</td>
<td>OLED circuits</td>
<td>66</td>
</tr>
<tr>
<td>CuNW (embedded)</td>
<td>91%</td>
<td>220 Ω sq⁻¹</td>
<td>Resistance increased twice (ε ~ 15%)</td>
<td>Resistance increased linearly, 20 cycles (ε ~ 10%)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>CuNW (embedded)</td>
<td>84.5%</td>
<td>56.2 Ω sq⁻¹</td>
<td>Rs &lt; 10² Ω sq⁻¹ (ε = 60%)</td>
<td>Stable up to 200 cycles (ε ~ 60%)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>CuNW (plasmonic welding)</td>
<td>79.5%</td>
<td>56.2 Ω sq⁻¹</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Au nanomesh</td>
<td>82.5%</td>
<td>25 Ω sq⁻¹</td>
<td>Stable within ε &gt; 250%</td>
<td>Rs increased by 10–20%, 800 cycles (ε = 250%)</td>
<td>TSPs</td>
<td>69</td>
</tr>
<tr>
<td>Pt nanomesh</td>
<td>75.2%</td>
<td>1 kΩ sq⁻¹</td>
<td>Rs increased by 3.2 times (ε = 160%)</td>
<td>Stable for 1000 cycles (ε ~ 50%)</td>
<td>TSPs</td>
<td>86</td>
</tr>
<tr>
<td>CuNF</td>
<td>90%</td>
<td>1 Ω sq⁻¹</td>
<td>Resistance unchanged (ε = 16.8%)</td>
<td>Resistance unchanged, 1000 cycles (ε = 10%)</td>
<td>Solar cells</td>
<td>63</td>
</tr>
<tr>
<td>AuNF</td>
<td>81%</td>
<td>25 Ω sq⁻¹</td>
<td>Rs increased by 56% (ε ~ 100%)</td>
<td>Resistance unchanged, 1000 cycles (ε = 10%)</td>
<td>Solar cells</td>
<td>97</td>
</tr>
<tr>
<td>PtNF</td>
<td>90%</td>
<td>80 Ω sq⁻¹</td>
<td>Rs increased by 10% (ε = 25%)</td>
<td>Rs increased by 10% (ε = 25%)</td>
<td>TSPs</td>
<td>98</td>
</tr>
<tr>
<td>Cu nanotrough</td>
<td>90%</td>
<td>131 Ω sq⁻¹</td>
<td>Rs increased by 40% (ε = 50%)</td>
<td>Rs increased by 60% (ε = 80%)</td>
<td>TSPs</td>
<td>102</td>
</tr>
<tr>
<td>AuNT/graphene</td>
<td>91%</td>
<td>2 Ω sq⁻¹</td>
<td>Rs increased by 10% (ε = 23%)</td>
<td>Rs increased by 40% (ε = 50%)</td>
<td>TFPs</td>
<td>103</td>
</tr>
<tr>
<td>CNT sheets</td>
<td>&gt;85%</td>
<td>&gt;85%</td>
<td>Resistance increased by ~6% (ε = 100% with pre-strain of 105%)</td>
<td>Resistance increased by ~6% (ε = 100% with pre-strain of 105%)</td>
<td>First cycle: ΔR/R0 = 6%</td>
<td>OLEDS</td>
</tr>
<tr>
<td>CNT thin films</td>
<td>&gt;80%</td>
<td>75 Ω sq⁻¹</td>
<td>Resistance increased by ~6% (ε = 100% with pre-strain of 105%)</td>
<td>Resistance increased by ~6% (ε = 100% with pre-strain of 105%)</td>
<td>First cycle: ΔR/R0 = 6%</td>
<td>Loudspeakers</td>
</tr>
<tr>
<td>SACNT films</td>
<td>83%</td>
<td>24 Ω sq⁻¹</td>
<td>εmax &gt; 200% (perpendicular to drawing direction)</td>
<td>εmax &gt; 120% (perpendicular to drawing direction)</td>
<td>TSPs</td>
<td>117</td>
</tr>
<tr>
<td></td>
<td>90%</td>
<td>208 Ω sq⁻¹</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
### Table 1 (Cont.)

<table>
<thead>
<tr>
<th>Materials</th>
<th>Transmittance $^a$</th>
<th>Electrical property $^b$</th>
<th>Stretchesability</th>
<th>Reliability (cyclic test)</th>
<th>Applications</th>
</tr>
</thead>
<tbody>
<tr>
<td>SACNT ribbons/ PDMS</td>
<td>60% (400–800 nm)</td>
<td>18.5 $\Omega$</td>
<td>Stable for 30 cycles ($\epsilon = 120%$)</td>
<td>Resistance increased by 1.5 times after 109 cycles ($\epsilon = 100%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>PDMS/SACNT ribbons</td>
<td>79%</td>
<td>328 $\Omega$ (sq$^{-1}$)</td>
<td>Resistance increased by $-5%$after 12,500 cycles ($\epsilon = 100%$)</td>
<td>Stable for 12,500 cycles ($\epsilon = 100%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>Polyacrylate/SACNT/Pt/Pd</td>
<td>68%</td>
<td>53 $\Omega$ (sq$^{-1}$)</td>
<td>Resistance increased by $-13%$after 50 cycles ($\epsilon = 100%$)</td>
<td>Stable for 50 cycles ($\epsilon = 100%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>Porous SWCNT/Pt/Pd</td>
<td>77%</td>
<td>200 $\Omega$ (sq$^{-1}$)</td>
<td>Resistance increased by $-8%$after 100 cycles ($\epsilon = 100%$)</td>
<td>Stable for 100 cycles ($\epsilon = 100%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>POMAS/SACNT/Pd/Pt/Ag(NPs)</td>
<td>93% (300–1,800 nm)</td>
<td>42.1 $\Omega$ (sq$^{-1}$)</td>
<td>Conductivity: $83 \ S \ m^{-1}$</td>
<td>Resistance increased linearly with stretch ($\epsilon = 82.0%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>Polyacrylate/PDMS</td>
<td>63%</td>
<td>5 $\lambda_{d}$ (at $T = 82.0%$)</td>
<td>Conductivity: $2.1 \times 10^{-2} \ S \ m^{-1}$</td>
<td>Electrical failure at $\epsilon = 55%$</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>Porous CNT/Pt</td>
<td>77%</td>
<td>5 $\lambda_{d}$ (sq$^{-1}$)</td>
<td>Conductivity: $0.22 \ S \ m^{-1}$</td>
<td>Resistance increased linearly with stretch ($\epsilon = 20%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>Hydrogel based SWNT/Pt/Pd</td>
<td>95.9%</td>
<td>73% (400–800 nm)</td>
<td>Conductivity: $4.1 \times 10^{-2} \ S \ m^{-1}$</td>
<td>Stable for 300 cycles ($\epsilon = 20%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
<tr>
<td>Hydrogel based SWNT/Pt/Pd</td>
<td>95.9%</td>
<td>73% (400–800 nm)</td>
<td>Conductivity: $4.1 \times 10^{-2} \ S \ m^{-1}$</td>
<td>Stable for 300 cycles ($\epsilon = 20%$)</td>
<td>Actuators, loudspeakers</td>
</tr>
</tbody>
</table>

$^a$ Transmittance indicates the value at the wavelength of 550 nm, unless otherwise specified.
$^b$ Electrical property indicates sheet resistance ($R_s$), unless otherwise specified.

(Thinner) CNTs (diameter: $\sim 1.2 \ nm$, length: $\sim 2–10 \ \mu m$) are presented in Fig. 2e.

The combination of two-dimensional (2D) nanomaterials, such as graphene with AgNWs has been intensively explored as well. Park’s group fabricated stretchable transparent electrodes based on graphene and AgNWs, as shown in Fig. 2f.6,16,58 These hybrid structures achieved high transmittance (94%) and low resistance (33 $\Omega$ sq$^{-1}$), which can be attributed to the increased conducting pathways compared to the electrode consisting solely of AgNWs. Fig. 2g shows that the AgNW/graphene hybrid electrode can be stretched up to 100% with a negligible change in resistance. This hybrid electrode has been applied to various stretchable and transparent electronics, including LEDs (Fig. 2h), biosensors, and human–machine interfaces.6,16,57

### 3.2. Cu nanowires

Although AgNW-based stretchable transparent electrodes show promising optoelectronic and mechanical characteristics, low availability of natural Ag gives rise to the cost issue, which is critical for mass production. Thus, Cu nanowires (CuNWs) have been rising as an alternative due to their comparable conductivity and flexibility with AgNWs as well as low cost originating from relatively high natural abundance of Cu.11,28 CuNWs can be synthesized using a number of methods, including aqueous reduction of copper salts,60,61 non-aqueous self-catalytic growth62 and electrospinning.63,64 One of the main drawbacks of CuNW-based stretchable transparent electrodes is that they are easily oxidized throughout the growth and device fabrication processes. The oxidation of CuNWs eventually degrades the performance and reliability of devices that adopt CuNW-based electrodes. Therefore, improving the chemical stability is the most urgent subject for successful applications of CuNW-based stretchable transparent electrodes.

One method that is known to hamper the oxidation of CuNWs is Ni coating on the surface of CuNWs.65,66 Song et al. reported a stretchable transparent electrode using CuNWs with Cu$_x$Ni alloying shells (Cu@Cu–Ni NWs) embedded in an elastomer substrate, as shown in Fig. 3a.66 This Cu@Cu–Ni NW-based electrode (sheet resistance of 62.4 $\Omega$ sq$^{-1}$ and transmittance of 80%) showed remarkable chemical stability against oxidation in a natural environment for over 30 days while the bare CuNW-based electrode showed resistance increase of 100% after 10 days. The electrode based on Cu@Cu–Ni NWs retained its electrical performance even after cyclic stretching (20%), bending, or twisting.

However, the Ni coating onto the surface of CuNWs degrades the overall transparency of the resulting electrodes. Thus, several research groups have demonstrated stretchable transparent electrodes using pristine CuNWs where the oxidation was prevented by embedding CuNWs into the polymeric substrates (Fig. 3b).57,67 The polymer matrix not only prevents the oxidation of CuNWs, but also provides intimate contact within the nanowires, which eventually leads to an enhanced durability under stretching. The electrode based on CuNWs partly embedded in the poly(acrylate) substrate exhibited a transmittance of 91% and a sheet resistance of 220 $\Omega$ sq$^{-1}$.67
The resistance increased by about 100% at the rupture strain of ∼15% (Fig. 3c) and showed a linearly increasing tendency for 20 stretching cycles of 15% elongation (Fig. 3d). Pei’s group added an additional chemical (6-aminohexanoic acid) to the polymer matrix to prevent the delamination of CuNWs from the polymeric substrate during the stretching. The electrode using 6-aminohexanoic acid showed less change in the electrical performance compared to the electrode without 6-aminohexanoic acid at 40% stretching, as shown in Fig. 3e and f.

The conventional thermal annealing process for the welding of the junctions between nanowires also induces the oxidation of CuNWs. To solve this problem, Han et al. reported plasmonic nanowelding of CuNWs (Fig. 3g), which not only improves the sheet resistance of resulting transparent conductors but also reduces the oxidation of CuNWs during the welding process. The resulting electrode using plasmonic-nanowelded CuNWs exhibited a transmittance of ∼80% at 550 nm and a sheet resistance of 37 Ω sq⁻¹. The electrode transferred onto an Eco-flex film endured a very large strain (>250%) with negligible resistance changes, and it was successfully utilized for a touch screen panel, as shown in Fig. 3h.

According to some previous reports, welded metal nanowire (AgNW or CuNW) networks also show more stable
electrical performance under mechanical deformations than non-welded networks. This can be ascribed to the difference in deformation between non-welded and welded networks. While a non-welded network accommodates strains by rotating and/or sliding of each nanowire against others at the junctions, a welded network accommodates strains by reconfiguring the network structure in the same manner that a fishnet changes its shape when it is stretched. Thus, the junctions in a non-welded network can be easily detached or broken by bending or stretching, whereas the junctions in a welded network firmly connect distinct nanowires even under harsh stretching.

4. Metal nanomeshes

To achieve high quality stretchable transparent electrodes using metal nanowires, defect-free nanowires should be synthesized with conductivities close to those of bulk metals.\(^{38,41,52,63,74-76}\) These refined metal nanowires should then be carefully deposited on a substrate with a density above the percolation threshold to provide sufficient current paths within the percolation networks.\(^{77,78}\) This percolation threshold could be fulfilled more easily if metal nanowires had higher aspect ratios.\(^{77}\) Additionally, ultra-long metal nanowires reduce the dependence of total resistance of transparent

---

**Fig. 3** CuNW-based stretchable transparent electrodes. (a) Schematic illustration of Cu@Cu–Ni NWs embedded in an elastomer substrate. Reproduced with permission from ref. 66. Copyright 2014, American Chemical Society. (b) Schematic illustration of the fabrication process of a CuNW–PU composite electrode. Reproduced with permission from ref. 68. Copyright 2013, Royal Society of Chemistry. (c) Resistance change of a CuNW/poly(acrylate) electrode (R0 = 5.8 Ω) during the first stretching and releasing. (d) Resistance change for a 5 Ω CuNW/poly(acrylate) electrode being cycled between 0% and 10% strain for 20 times. (c and d) Reproduced with permission from ref. 67. Copyright 2014, Royal Society of Chemistry. (e and f) Normalized transient resistance of (e) pristine CuNW/PU composite electrodes and (f) 6-aminohexanoic acid pretreated CuNW/PU composite electrodes during the cyclic stretching–releasing process with the peak strain of 40% at the stretching speed of 0.01 mm s\(^{-1}\). (e and f) Reproduced with permission from ref. 68. Copyright 2013, Royal Society of Chemistry. (g) Schematic illustration of the plasmonic laser nanowelding process of CuNWs. (h) Demonstration of the touch-screen panel fabricated with a laser-nanowelded CuNW transparent conductor. (g and h) Reproduced with permission from ref. 69. Copyright 2014, John Wiley and Sons.
electrodes on the junction resistances between nanowires. Based on this idea, alternative nanostructures, such as nanomeshes, nanofibers, and nanotroughs, have been extensively explored to realize stretchable transparent electrodes.

4.1. Metal grids

A metal grid with a grating structure is the most basic form of a metal nanomesh for flexible or stretchable transparent electrodes. The transmittance and sheet resistance of metal grids can be controlled using key parameters such as film thickness, grid line width and grid pattern pitch.\(^{79,80}\) To obtain high transmittance (above 90% at 550 nm) and maintain low sheet resistance, the grid line width should be reduced and the grid pattern pitch should be optimized considering the trade-off between sheet resistance and transmittance. In addition to the conventional photolithography,\(^{80-82}\) which requires multiple fabrication steps, including a vacuum process, various fabrication methods have been utilized to demonstrate metal grid electrodes, including inkjet printing,\(^{83}\) electrohydrodynamic inkjet,\(^{79,84}\) direct writing,\(^{85}\) and imprinting.\(^{74}\)

Although the optoelectronic characteristics of metal grid electrodes can be readily tuned, they only present the stretchability along a diagonal direction to the grating pattern. The elongation of the grating pattern along the orthogonal directions is likely to induce undesired cracks or failure of the electrode. Therefore, metal grids with random or meandering networks have recently been investigated to obtain the stretchability without any directivity. Guo et al. reported a stretchable transparent Au nanomesh electrode using grain boundary lithography.\(^{86}\) This electrode showed a sheet resistance of 21 \(\Omega\) sq\(^{-1}\) and a transmittance of 82.5%. Also, it can be stretched up to 160% with the sheet resistance increased by 3.2 times. They also reported the recovery effect of Au nanomesh electrodes under cyclic stretching or compression by taking advantage of the cold-welding phenomenon, where welding of damaged parts occurs due to the pressures induced by mechanical deformation,\(^{87}\) thereby providing a durable and generally applicable stretchable transparent electrode.\(^{88}\) Jang et al. reported a hexagonal Pt nanomesh electrode using anodized aluminium oxide (AAO) template as a substrate. Pt was sputtered on an AAO template and then the AAO template was removed, providing a transferable Pt nanomesh with a honeycomb structure.\(^{89}\) This Pt nanomesh electrode showed a sheet resistance of 71 \(\Omega\) sq\(^{-1}\) with a transmittance of 75.2%, and it could be stretched up to 16.8% without any significant changes in resistance.

4.2. Metal nanofibers and nanotroughs

As mentioned previously, the meandering design\(^{90}\) and smaller line width\(^{79,80}\) are prerequisites for preferable stretchable transparent electrodes. Therefore, conducting random networks with high aspect ratio nanomaterials beyond nanowires are required.\(^{91}\) Based on this idea, metallic nanofibers have been attracting substantial interest as an alternative material for stretchable transparent electrodes. Most metallic nanofibers have been fabricated by electrospinning, which is a facile method to make continuous and long nanofibers from polymeric solutions using electrohydrodynamics.\(^{92,93}\)

The first attempt to fabricate metallic nanofibers via electrospinning adopted the precursor-based method\(^{63,94-96}\) where the metal salts (precursors) were dissolved in appropriate solvents, followed by electrospinning of this solution. The polymeric components were then selectively removed by calcination at high temperature. To convert the resulting metal oxide nanofibers to metallic nanofibers, a further reduction process was required. As shown in Fig. 4a, Cui’s group fabricated Cu nanofibers (CuNFs) by electrospinning copper acetate dissolved in poly(vinyl acetate).\(^{63}\) The resulting CuNFs had ultrahigh aspect ratios of up to 100 000 and fused crossing points with ultralow junction resistances (Fig. 4b), which were utilized for stretchable electrodes with a high transmittance (90%) and a low sheet resistance (50 \(\Omega\) sq\(^{-1}\)). As shown in Fig. 4c, this CuNF-based transparent electrode exhibited negligible conductance degradation after stretching by 10% strain, while the resistance of thin Cu films increased 100 times under the same stretching conditions.

The electrode prepared by the precursor-based method showed limited flexibility or stretchability due to the coalescence of nanofibers at the intersections and required high-temperature heat treatment for the reduction process. To simplify the fabrication steps of metallic nanofibers, the vacuum deposition method was proposed.\(^{97,98}\) Servati’s group demonstrated Au nanofiber (AuNF) networks by sputtering Au onto the electrospun polyacrylonitrile (PAN) nanofiber networks (Fig. 4d), which mimicked the natural fibrous structure.\(^{97}\) The resulting web consisted of a conductive Au shell and a flexible PAN core, exhibiting a transmittance of 81% and a sheet resistance of 25 \(\Omega\) sq\(^{-1}\). In addition, the PAN/Au nanofiber networks transferred to a PDMS substrate presented 56% increase in resistance and 6% increase in optical transmittance upon 100% stretching. Even at 100% strain, AuNFs were deformed with partial cracks, but without electrical disconnection (Fig. 4e and f). The increased optical transmittance at the stretched state was attributed to the sparse nanofiber networks and wider empty spaces generated by the stretching. Also, the resistance of the electrode remained almost unchanged even after 1000 stretching cycles (\(\epsilon = 10\%\)).

More recently, for cost reduction and mass production, non-vacuum processes, such as the electroless deposition and the mask template method, have been reported.\(^{99-101}\) Zhu’s group reported CuNFs using PAN nanofibers as an etching mask (Fig. 4g).\(^{99}\) Electrospun PAN nanofibers were flattened by solvent vapour annealing to provide intimate contact with the underlying thin Cu film. After the Cu etching and removal of the PAN NFs, a CuNF-based transparent electrode was obtained with a sheet resistance of 24 \(\Omega\) sq\(^{-1}\) at 92% transmittance. Cui’s group reported the fabrication of Ag nanofiber (AgNF) or CuNF networks via the combination of electrospinning and electroless deposition, which is a well-known technique to form metal films at a low cost and a large scale.\(^{100}\) Polyvinyl butyral (PVB)/tin(II) chloride
(SnCl₂) NFs were first formed by electrospinning, and then immersed in the silver nitrate (AgNO₃) aqueous solution to form the Ag seed layer only on the surface of nanofibers. Subsequent metallization via electroless deposition provided AgNF or CuNF networks, achieving a sheet resistance of around 10 Ω sq⁻¹ and a transmittance of 90% (Fig. 4h). These electrodes, however, still exhibited limited flexibility and stretchability due to the coalescence of nanofiber junctions.

In addition to the nanofibers, metal nanotroughs with a concave shape were also reported using a low step coverage metal deposition process, as shown in Fig. 5a. Cui’s group reported a Cu nanotrough-based transparent electrode (Fig. 5b) and demonstrated a flexible touch-screen device (Fig. 5c). The electrode had outstanding opto-electronic performance (sheet resistance: ~2 Ω sq⁻¹, transmittance: 90%) and showed reasonable stretchability (~40% increase in resistance upon 50% uniaxial tensile strain).

Hybrid structures of metal nanotroughs and other nanomaterials (e.g., graphene) were also investigated to resolve several problems of nanotroughs, such as (i) high contact resistance with other layers, (ii) percolation problem associated with the pattern size, and (iii) instability in harsh environments. Park’s group reported Au nanotrough (AuNT)/graphene hybrid structures, where graphene served as an auxiliary conducting layer and an anti-oxidation layer as well, as shown in Fig. 5d. With the combination of AuNTs and graphene, the resulting transparent electrode exhibited outstanding electrical characteristics with remarkable uniformity (sheet resistance: 1 ± 0.1 Ω sq⁻¹) at 91% transmittance. Also, this electrode showed less than 60% increase in resistance upon 80% stretching, while the AuNT-only film showed 60% increase in resistance for 50% stretching. A skin-attachable, flexible, and highly transparent thin film transistor backplane was demonstrated using this AuNT/graphene hybrid electrode (Fig. 5e–g).
5. Other candidates

Apart from the above-mentioned methods, several distinct approaches have been developed for stretchable transparent electrodes, including CNTs, metal nanoparticle-incorporated composites, and hydrogel-based ionic conductors. These unique approaches have diversified the application of stretchable transparent electrodes.

5.1. Carbon nanotubes

CNT is one of the most famous allotropes of carbon with a high aspect ratio cylindrical tube shape composed of one or more layers of graphitic carbon (single-walled CNT (SWCNT) or multi-walled CNT). These cylindrical structures of carbon have remarkable properties, such as high mechanical strength, thermal conductivity, and electrical conductivity. CNTs can be synthesized using various simple methods, while chemical vapour deposition (CVD), arc discharge, and laser ablation are the most commonly used methods. Since the initial discovery of the CNT in 1991, numerous studies have been conducted on CNTs, owing to its unique properties and relatively simple preparation methods.

The early studies on stretchable conductors or electrodes based on CNTs focused on the CNT/polymer composite. CNTs with outstanding mechanical and electrical properties were attractive filler materials blended with a polymer matrix. Although CNT/polymer composites were suitable for stretchable conductors, most of them were not optically transparent due to the high concentration of CNT fillers. To expand the usage of stretchable CNT electrodes, many interesting studies have been carried out to improve the optical transparency of CNT-based electrodes.

5.1.1. Aligned CNTs. The initial strategy to render CNT-based stretchable transparent electrodes was to use directly drawn aligned CNTs from a CNT forest, as shown in Fig. 6a. These unidirectional, transparent and stretchable CNT sheets...
with a meter-long scale (up to several centimetres wide) were utilized as electrodes for organic light-emitting diodes (OLEDs) (Fig. 6b), loudspeakers, supercapacitors, and touch panels (Fig. 6c). However, these CNT sheets were anisotropic with regard to optical, electrical, and mechanical properties due to the fixed drawing direction (e.g., transmittance of a CNT sheet was >85% for perpendicular polarization and >65% for parallel polarization). These anisotropic characteristics of highly aligned CNT sheets were the main obstacles to be utilized as stretchable transparent electrodes. In this regard, several studies have been conducted to improve their limited characteristics.

Based on a previous report, where CNT sheets drawn from a short height of the CNT forest had no large bundles and achieved high transmittance, Feng et al. reported highly transparent and roll-to-roll processable superaligned...
CNT (SACNT) films by reducing the height of the CNT forest and removing residual large bundles in SACNT films with plasma and laser trimming, respectively. Oxygen plasma effectively reduced the height of a SACNT array, and laser trimming removed the outermost CNTs of large bundles from as-drawn SACNT films. In addition, to achieve better electrical conductivity, metals (Au or Ag) were deposited onto the SACNT film, which then exhibited excellent opto-electronic performances with sheet resistances and transmittance of 208 Ω sq⁻¹ at 90% or 24 Ω sq⁻¹ at 83.4%, respectively. The same research group then reported a cross-stacked structure of SACNT films to solve the anisotropy, as shown in Fig. 6d. The resulting SACNT film could be stretched up to 35% along a diagonal direction relative to the stacking angle.118

Despite the above-mentioned interesting progress in the aligned CNT approach, the transparent electrodes made of aligned CNTs showed incomplete stretchability in that they undergo irreversible plastic deformation upon a tensile strain.118 Several strategies to solve this problem were demonstrated by embedding aligned CNTs into the elastomeric matrix.118,119 The resulting electrode exhibited nearly unchanged resistance (35.5 ± 0.3 kΩ) after 6 cycles of 100% stretching.119

5.1.2. Random network CNTs. In addition to the aligned CNTs, random networks of CNTs have also been introduced for stretchable transparent electrodes via direct deposition onto or embedding into elastomers. Lipomi et al.120 obtained spring-like buckled 2D SWCNT films (Fig. 6e) by stretching and releasing the as-sprayed random network CNTs on a PDMS substrate. This electrode had a sheet resistance of 328 Ω sq⁻¹ with a transmittance of 79% and survived even at 150% tensile strain. Free-standing SWCNT films with hierarchical reticulate structures were directly synthesized by a floating-catalyst CVD, which provided stretchable transparent electrodes.121 To impart further stretchability, Cai et al.122 embedded the SWCNT film with a hierarchical reticulate structure into a PDMS substrate (Fig. 6f), providing a stretchable transparent electrode with a transmittance of 62% at 550 nm and a sheet resistance of 53 Ω sq⁻¹, which exhibited 125% increase upon a tensile strain of 60%.

Another approach was also demonstrated with a composite of a porous SWCNT three-dimensional (3D) network and elastomer. Yu et al.123 reported the fabrication of nanoporous SWCNT network–polymer composites by Meyer rod coating124 and in situ UV curing of tert-butyl acrylate. This electrode showed a transmittance of >77% and a sheet resistance of 200 Ω sq⁻¹, which increased by 78% under a 50% tensile strain. It was utilized as both the anode and cathode for PELCs. Another interesting method to fabricate porous SWCNT 3D networks was also reported, where ultratight and electrically conducting SWCNT aerogels were prepared by the freeze-drying method.125,126 SWCNT aerogel-based PDMS composites were obtained through the penetration of PDMS into the porous SWCNT aerogel.127 This highly stretchable and transparent (maximum ε = 250% and T = 90%) electrodes showed no significant changes in resistance after 20 cycles of 100% stretching.

Electrospun nanofiber-assisted SWCNT–polymer nanoweb has been emerging as another strategy to obtain random SWCNT network-based electrodes. CNTs can effectively form well-connected conducting networks without agglomeration by simple drop-casting on a well-distributed polymer nanofiber scaffold.128,129 Kim et al.130 also created an acid-treated SWCNT network on web-shaped polyurethane nanofibers through simple electrospinning and dip-coating methods, as shown in Fig. 6g. Utilizing the stretching-releasing method, stretchable electrodes with noodle-like structures were achieved, which exhibited a sheet resistance of 424 Ω sq⁻¹ at 63% transmittance and sustained stable conductivity after 6 cycles of 100% stretching.

5.2. Other approaches for stretchable transparent electrodes

Besides metal nanomaterials and CNTs, several unconventional strategies have been developed to realize stretchable transparent electrodes, such as bio-inspired fabrication of stretchable carbon films,131 polymer gel/metal nanoparticle composites,132 and hydrogel-based ionic conductors.133,134

5.2.1. Pyrolyzed polydopamine. A carbon-based stretchable transparent electrode was demonstrated on a PDMS substrate using pyrolyzed polydopamine (PDA) films.131 The pyrolyzed PDA film was prepared by immersion of a substrate in a self-polymerizable dopamine solution and subsequent pyrolysis at high temperature (800–1000 °C), as shown in Fig. 7a. The pyrolyzed PDA film prepared in this low-cost and scalable process may be regarded as a multi-layered graphene film. As shown in Fig. 7b, the pyrolyzed PDA film on a Cu foil was dry-transferred to a PDMS substrate, resulting in a stretchable transparent electrode (T = 62.6%). The resistance increased linearly (R/RO ≅ 50) upon stretching from 0% to 20%. A cyclic stretching test (ε = 20%) showed reliability of the electrode without significant changes in electrical properties. A photodetector with rapid and repeatable sensing was demonstrated as well using this pyrolyzed PDA electrode.

5.2.2. Polymer gel/metal nanoparticle composites. A metal nanoparticle-based composite was reported by Hyun et al.132 as a promising candidate for stretchable transparent electrodes. A mixture of a UV-crosslinkable polymer (poly(ethylene oxide)-diacrylate (PEG-DA)) and a metal precursor (silver trifluoroacetate (STA)) was spin-coated on the polystyrene (PS)-coated PDMS substrate with a wavy structure, as shown in Fig. 7c. Subsequent UV exposure and chemical reduction yielded PEG gel/Ag nanoparticle composite patterns, which were then transferred to a new elastomer substrate with a flattening of the wavy PDMS template by applying a tensile strain. The stretchability was achieved by 2D zigzag patterns of the composite generated by releasing of the wavy template (Fig. 7d). This composite pattern exhibited conductivity of ~10⁶ S m⁻¹ at 50% strain without electrical degradation; however, it showed dramatic decrease in conductivity at 55% strain due to mechanical failure. Repeated stretching (900 cycles for 20% strain) of this electrode caused no substantial
changes in electrical properties. Fig. 7e displays a composite film with transmittance of ∼70%, which can be improved by enlarging empty regions in the composite pattern.

5.2.3. Ionic conductors. As a new candidate for stretchable transparent electrodes, Keplinger et al.\textsuperscript{133} suggested a hydrogel-based ionic conductor. The electrical conduction in this approach was enabled by mobile ions from NaCl, and the hydrogel based on a polymer network and water took a solid form, exhibiting a transmittance of 98.9% (this was reported as the highest value amongst all transparent conductors). The stretchability of this hydrogel-based ionic conductor is depicted in Fig. 7f, where the resistance increases proportionally to the square of \(\lambda\) \((\text{i.e., } R/R_0 \propto \lambda^2, \text{where the ‘stretch (} \lambda \text{)’ indicates } \lambda \text{-times stretching from its initial length). A transparent loud speaker and an actuator were introduced as applications that utilize this ionic conductor (Fig. 7g).

Although the hydrogel-based ionic conductor described above can be obtained in a low-cost manner, it is not suitable for applications in open air because hydrogels dry out as water evaporates. To avoid this issue, Chen et al.\textsuperscript{134} developed an ionogel in which an elastic polymer network hosted a conducting ionic liquid. The volatility of the ionogel was assessed and compared to that of a hydrogel by measuring the weight loss in a thermostatic chamber held at 100 °C. The ionogel showed a weight loss of 12.43% within 12 h while the hydrogel showed a weight loss of 93.69% within 1 h. The conductivity of the ionogel was 0.22 ± 0.01 S m\(^{-1}\) with a transmittance of 96.95%, and the resistance increased proportionally to the square of ‘stretch (} \lambda \text{),’ just like the hydrogel-based one.
6. Concluding remarks

We have witnessed surprising advances in stretchable electronics over the past decade. As an essential component for stretchable electronics, stretchable transparent electrodes have progressed remarkably, as summarized in this mini review. Metal nanomaterials, such as nanowires, nanofibers, and nanoroughs, exhibit promising characteristics even under high-level mechanical deformation. Also, CNTs and other unique approaches increase the number of feasible options for stretchable transparent electrodes.

Stretchable transparent electrodes based on in-plane configurations, however, still require further improvement in several aspects. First, the preparation of high-quality and defect-free nanomaterials should be further refined for acceptable functionalities of electrodes thereof. The chemical stability (e.g., stability against oxidation) of these nanomaterials also needs to be enhanced to guarantee the reliable long-term operation of resulting devices in practical uses. The hybridization of nanomaterials (e.g., AgNWs + graphene) has proven feasible by combining the strengths of these materials and compensating the weaknesses of each material, and should be further investigated by exploiting various materials and hierarchical structures. In addition to the material itself, adhesion and interfacial interactions of stretchable transparent electrodes with elastomeric substrates and other constituent active components should be considered as well for the durable operation of final products. Lastly, scalable and low-temperature fabrication processes depending on the materials should be developed in a low-cost manner to facilitate the advent of practical stretchable electronics.

We are now about to see a great leap of electronics towards stretchable form where conventional constraints from rigid form-factors no longer matter. Tremendous research efforts over the past decade have revealed a cornucopia of stretchable electronics with regard to research opportunities and potential applications. Unprecedented applications employing stretchable electronics, including biomedical, healthcare, and wearable devices, are expected to emerge and change our ways of life in the near future.

Acknowledgements

This work was supported by the Ministry of Science, ICT & Future Planning and the Ministry of Trade, Industry and Energy of Korea through Basic Science Research Program of National Research Foundation (2013R1A2A2A01068542), Materials Original Technology Program (10041222), Technology Innovation Program (Grant 10044410), Convergence Technology Development Program for Bionic Arm (NRF-2014M3C1B2048198), and Pioneer Research Center Program (NRF-2014M3C1A3001208). Also, the authors thank Samsung Display and financial support by the Development Programs of Manufacturing Technology for Flexible Electronics with High Performance (SC0970) funded by Korea Institute of Machinery and Materials and by Development of Interconnect System and Process for Flexible Three Dimensional Heterogeneous Devices funded by MOTIE in Korea.

Notes and references


Nanoscale Minireview

A. Greiner and J. H. Wendorff


